

# Total water levels along the South Atlantic Bight during three along-shelf propagating tropical cyclones: relative contributions of storm surge and wave runup

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**Abstract.** Total water levels (*TWLs*), including the contribution of wind waves, associated with tropical cyclones (TC) are among the most damaging hazards faced by coastal communities. TC-induced economic losses are expected to increase because of stronger TC intensity, sea level rise, and increased populations along the coasts. TC intensity, translation speed, and distance to the coast affect the magnitude and duration of increased *TWLs* and wind waves. Under climate change, the proportion of high-intensity TCs are projected to increase globally, whereas the variation pattern of TC translation speed also depends on ocean basin and latitude. There is an urgent need to improve our understanding of the linkages among TC characteristics and *TWL* components. In the past years, hurricanes Matthew (2016), Dorian (2019), and Isaias (2020) propagated over the South Atlantic Bight (SAB) with similar paths but resulted in different coastal impacts. We combined *in situ* observations and numerical simulations with the Coupled Ocean–Atmosphere–Wave–Sediment Transport (COAWST) modeling system to analyze the extreme *TWLs* under the three TCs. Model verification showed that the *TWL* components were well reproduced by the present model setup. Our results showed that peak *TWLs* depend mainly on the TC intensity, the distance to the TC eye, and the TC heading direction. A decrease of TC translation speed primarily led to longer exceedance durations of *TWLs*, which may result in more severe economic losses. Wave-dependent water level components (i.e., wave setup and wave swash) were found to dominate the peak *TWL* within the near-TC field. Our results also showed that in specific conditions, the pre-storm wave runup associated with the TC-induced swell may lead to *TWLs* higher than at the peak of the storm. This was the case along the SAB during Hurricane Isaias. Isaias’s fast TC translation speed and the fact that its swell was not blocked by any islands were the main factors contributing to these peak *TWLs* ahead of the storm peak.

## 1 Introduction

Total water levels (*TWLs*), defined as the combination of astronomic tides, mean sea level, storm surge, and wave runup (combination of wave setup and wave swash), associated with tropical cyclones (TC) are among the leading hazards faced by coastal communities (e.g., Kalourazi et al., 2020; Sallenger, 2000). The Saffir–Simpson Hurricane Wind Scale (SSHWS) has been used to estimate the potential impacts and economic losses caused by TCs based on the maximum sustained wind speed.

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However, the maximum sustained wind speed, the TC translation speed (Liu et al., 2007; Xu et al., 2007), the size of the storm (Irish et al., 2008), and the storm track (Suh and Lee, 2018; Wang et al., 2020) affect wave heights, wave periods, and storm surge levels along the coast differently. Alipour et al. (2022) pointed out that using SSHWS as a proxy of the expected impacts alone may lead to severe miscalculation, and they proposed a new scaling system associated with rainfall, storm surge, and wind speed. Irish and Resio (2010) proposed a hydrodynamics-based surge scale for hurricane surge hazard and an approach for predicting expected flood inundation and economic losses. Sallenger (2000) proposed a more complex approach in which the *TWL* relative to the dune crest ( $D_{crest}$ ) and dune base ( $D_{base}$ ) elevations was used to classify four expected morphological impact regimes: swash ( $TWL < D_{base}$ ), collision ( $D_{base} \leq TWL < D_{crest}$ ), overwash and inundation ( $D_{crest} \leq TWL$ ). In the overwash regime *TWL* exceeds  $D_{crest}$  when the wave swash effects are accounted for. In the inundation regime *TWL* exceeds  $D_{crest}$  even without the effect of the wave swash. Among these regimes, coastal dunes experience the direct impacts of surf-zone processes in the inundation regime, when *TWL* exceeds  $D_{crest}$ . Thus, the inundation regime is expected to induce the highest economic losses among the four impact regimes while the swash regime represents the least severe condition with less anticipated economic losses. *TWL* thus represents the combination of storm independent (the mean sea level and astronomic tides) and storm dependent (wave runup and storm surge) water level components, being a better indicator of the increased water levels than the storm surge alone (Stockdon et al., 2007). We assume that astronomic tides and storms are at first order independent, although extreme winds and storm surges can interact with the tidal wave and cause tidal distortions (e.g., Paniagua-Arroyave et al., 2019). The wave runup is a wind wave dependent parameter composed by a wave-averaged sea level variation known as ‘wave setup’ and a wave-varying fluctuating component known as ‘wave swash’ (Stockdon et al., 2006). Previous efforts have shown the complexity and uncertainty of TC-induced surges and compound floods. However, the response of *TWL* to storm characteristics is more complicated than that corresponding to the storm surge, and the relative role of the wave runup and storm surge, and the dependency with storm characteristics are still poorly understood. There are primarily two approaches for computing *TWLs* during extreme storms: with numerical models (e.g., Hegermiller et al., 2019) and with observed water levels and waves (e.g., Serafin and Ruggiero, 2014). For example,  $\eta_0$  (i.e., the sum of astronomic tides, mean sea level, and storm surge) observations were available at National Oceanic and Atmospheric Administration (NOAA: <https://tidesandcurrents.noaa.gov/>) tide gauges. Coupled ocean-wave modeling systems such as Coupled Ocean-Atmosphere-Wave-Sediment Transport model (COAWST; Warner et al., 2010) can also be applied to predict  $\eta_0$  deterministically and probabilistically. However, the wave runup component needed to compute the *TWL* is not captured by tide gauges, and regional ocean models usually do not have sufficient spatial resolution to reproduce the wave setup accurately. Moreover, due to the use of phase-averaged models, coupled modeling systems such as ROMS-SWAN are not able to reproduce the wave swash component. While models such as InWave (Infragravity Wave model, installed within COAWST; Olabarrieta et al., 2023) can solve infragravity waves, phase resolving models like FUNWAVE (Shi et al., 2012) can be applied to simulate the wave swash. However, InWave and FUNWAVE require higher resolution in space and time, which makes them relatively not efficient for large spatial areas.

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To overcome this modeling challenge, the wave runup can be computed using empirical formulas and linearly added to  $\eta_0$ . For example, Serafin and Ruggiero (2014) applied the empirical formula proposed by Stockdon et al. (2006) to compute the wave runup at NOAA tide gauges using the wave parameters observed at nearby National Data Buoy Center (NDBC; <https://www.ndbc.noaa.gov/>) wave buoys along the U.S. West Coast. While the wave runup of Stockdon et al. (2006) formulation is represented by a linear increase with increasing deep-water zero-order moment wave height ( $H_0$ ), Senechal et al. (2011) suggested an upper limit of wave runup at highly dissipative beaches under energetic conditions (e.g., tropical cyclone). Senechal et al. (2011) proposed another empirical formula for wave runup based on wave height alone, to avoid the over-prediction under such scenarios, and stated that the saturation of wave runup required further studies and measurements under diverse beach scenarios before generalization. Despite the importance of the wave runup on TWL estimation, the sensitivity of wave runup to the choice of these formulas had not been thoroughly examined. In the meantime, the sensitivity and the applicability of these formulas under different storm conditions is poorly understood.

Parker et al. (2023) recently characterized the relative contributions of astronomic tides, storm surge and wave setup to extreme water levels along the U.S. Southeast Coast, discovering regional patterns in the average contributions of waves and storm surge to extreme water levels over the 38-year hindcast. Here, we analyzed how TC characteristics affect the relative contributions of storm surge and wave runup to TWLs and their impacts by applying the COAWST modeling system to simulate TWLs along the South Atlantic Bight (SAB; extending from North Carolina to Florida) during three historical TCs with similar tracks. In the recent past, three hurricanes (Matthew 2016, Dorian 2019, and Isaias 2020) propagated through the shelf of the SAB with similar tracks (Fig 1). The average TC characteristics and the associated economic losses of these three TCs according to the International Best Track Archive for Climate Stewardship (IBTrACS; Knapp et al., 2018; <https://www.ncei.noaa.gov/products/international-best-track-archive>) are indicated in Table 1. While the economic loss from Matthew (\$10.0 billion; Stewart, 2017) was the highest from all storms, it was one order of magnitude higher than that of Dorian (\$1.6 billion by Dorian; Avila et al., 2020), even with similar maximum sustained wind speeds ( $V_{max}$ ). Surprisingly, while Dorian had a stronger intensity than Isaias according to the SSHWS, Isaias caused higher economic loss. (\$4.8 billion; Latto et al., 2021). Isaias had the fastest translation speed ( $V_t$ ) across all three hurricanes within the SAB, whereas Dorian had the slowest  $V_t$  and the smallest radius of maximum wind ( $R_{max}$ ) on average. How the differences in  $V_{max}$ ,  $V_t$ , and distance to the coast influenced the TWL components during these three TCs is still not well understood. With similar tracks over the SAB, these three historical TCs provided the opportunity to determine the effects of each TC property on waves and TWL along the coast. Because the proportion of high-intensity TCs (i.e., SSHWS category 4 to 5) and the corresponding maximum sustained wind are projected to increase at the global scale (Masson-Delmotte et al., 2021) due to climate change, understanding how TC characteristics influence the makeup of the TWL is essential for preparing for future coastal impacts.

Table 1. Averaged values of TC parameters of the three historical hurricanes within the SAB. The values were calculated from the International Best Track Archive for Climate Stewardship (IBTrACS) and National Hurricane Center datasets.  $V_t$  is the translation speed of storms;  $V_{max}$  is the maximum sustained wind;  $P_{min}$  is the minimum atmosphere pressure;  $R_{max}$  is the radius of maximum wind; economic loss is estimated in billion USD.

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$$R_2 = 1.1 \left( 0.35\beta_f (H_0 L_0)^{\frac{1}{2}} + \frac{[H_0 L_0 (0.563\beta_f^2 + 0.004)]^{\frac{1}{2}}}{2} \right), \quad 0.3 \leq \xi_0 <$$

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$$R_2 = 0.043 (H_0 L_0)^{\frac{1}{2}}, \quad \xi_0 < 0.3, \quad (2) ¶$$

in which foreshore beach slope ( $\beta_f$ ) and deep-water wave parameters ( $H_0$ =deep water zero moment order wave height and deep water peak wavelength) and the Iribarren number ( $\xi_0$ ) (Eq. were required.  $\xi_0$  was used to categorize wave breaker types

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<u>Hurricane</u>	<u><math>V_t</math> (m s<sup>-1</sup>)</u>	<u><math>V_{max}</math> (m s<sup>-1</sup>)</u>	<u><math>P_{min}</math> (mb)</u>	<u><math>R_{max}</math> (km)</u>	<u>Economic loss (billion USD)</u>
<u>Matthew</u>	<u>6.17</u>	<u>45.25</u>	<u>959.44</u>	<u>52.67</u>	<u>10.0</u>
<u>Dorian</u>	<u>3.27</u>	<u>58.80</u>	<u>945.36</u>	<u>35.52</u>	<u>1.6</u>
<u>Isaias</u>	<u>6.26</u>	<u>32.11</u>	<u>993.06</u>	<u>53.38</u>	<u>4.8</u>

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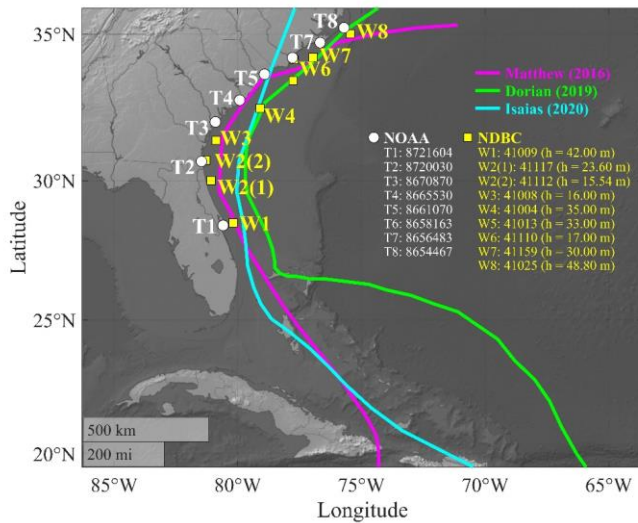


Figure 1. Best tracks of hurricanes Matthew 2016 (magenta), Dorian 2019 (green), and Isaias 2020 (cyan) and NOAA tide gauges (white circles), NDBC wave buoys (yellow squares) selected for the model verification.  $h$  represents the water depth.

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This paper is organized as follows: a brief review of the modeling system and model setup is presented following the introduction. Model verification based on the comparison with historical observations at eight NOAA tide gauges can be found next.  $JWL$  components along the SAB during Matthew 2016, Dorian 2019, and Isaias 2020 are analyzed and compared in the result and discussion section. The applicability of the two empirical wave runup formulas and the effect of TC characteristics

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## 2 Methods

245 Following the modeling framework of Hegermiller et al. (2019), we configured COAWST as a coupled ocean–wave model and set it up to simulate the ocean and wave dynamics during hurricanes Matthew (2016), Dorian (2019) and Isaias (2020). Ocean dynamics were resolved with the Regional Ocean Modeling System (ROMS; Shchepetkin and McWilliams, 2005), while wind wave generation and propagation were simulated with Simulating WAVes Nearshore (SWAN; Booij et al., 1999). The computational flowchart of the ocean circulation–wave coupling applied here is shown in the appendix (Fig. A1). The  
250 ocean and wave models used the same horizontal grids, with a 5 km resolution parent grid covering the entire U.S. East Coast and a 1 km resolution child grid covering the southern SAB.

### 2.1 Ocean model (ROMS)

ROMS solves the Reynolds Averaged Navier–Stokes equations (RANS) utilizing a three–dimensional terrain–following framework with a curvilinear coordinate transformation and finite–difference approximations (Shchepetkin and McWilliams, 255 2005). Additional information on the wave–current closures models included in ROMS is provided in Kumar et al. (2012), Warner et al. (2008), and Warner et al. (2010).

### 2.2 Wave model (SWAN)

The third–generation spectral wave model SWAN (Booij et al., 1999) solves the wave action evolution while considering refraction, shoaling, wave–current interactions, wind–wave generation, and varied wave energy dissipation (bottom friction, 260 breaking, and white–capping). The semi–empirical formula derived from the JOint North Sea Wave Project (JONSWAP) was used to calculate bottom friction (Hasselmann et al., 1973). We calculated wind wave growth and white–capping using the formulas presented by Komen et al. (1984). We used discrete interaction approximation (DIA; Hasselmann et al., 1985) for the non–linear quadruplet wave–wave interactions.

### 2.3 Model setup

265 In the current work, winds, atmospheric pressure, relative humidity, and surface air temperature from the RAPid refresh (RAP) re–analyzed data (Benjamin et al., 2016; <https://www.nco.ncep.noaa.gov/pmb/products/rap/>) were employed to force ROMS. This dataset comprised atmospheric pressure at mean sea level (MSL) and wind speeds 10 meters above MSL. Although RAP only covers a portion of the computational domain, it has a spatial resolution of 13 km at hourly time intervals. The Global Forecast System (GFS; 50 km resolution with a 3–hour time interval; <https://www.ncdc.noaa.gov/data-access/model-data/model-datasets/global-forecast-system-gfs>) provided wind and atmospheric pressure forces for offshore regions that RAP did not cover.

The U.S. East Coast domain had a horizontal grid resolution of 5 km with 896 ( $\xi$ –direction)  $\times$  336 ( $\eta$ –direction) grid cells. The SAB domain had a horizontal grid resolution of 1 km with 272 ( $\xi$ –direction)  $\times$  376 ( $\eta$ –direction) grid cells. The numerical

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Using the Model Coupling Toolkit, water levels, current velocities and wave fields are two–way coupled in COAWST (Warner et al. 2008a). A data exchange interval of 30 minutes between ROMS and SWAN, including water surface elevation, current velocities, statistical wave bulk parameters (e.g. zero–order moment wave heights, peak and mean wavelengths, peak and mean wave period and peak and mean wave directions and wave dissipation). This exchange interval has been tested and used by Hegermiller et al. (2019) and Hsu et al. (2023). This exchange interval was found to replicate, in which the nearshore hydrodynamics was replicated adequately and was. Thereby, we applied the same data exchange interval in the present work. Specifics regarding the coupling method and an example case study are provided (Warner et al., 2008b; 2010). The wind shear stresses and sea surface roughness (Taylor and Yelland (2001) at the sea surface were computed and used to force the ocean model. The vortex–force formulation (Kumar et al., 2012; Uchiyama et al., 2010) was employed in the current study to account for wave–current interaction. Furthermore, the wave and current boundary layer properties were estimated with the SSW\_BBL option, which used the Madsen model (1994).¶

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grids of ROMS had 16 vertical layers. For the SAB grid and the U.S. East Coast grid, the baroclinic time steps in ROMS were 30 seconds and 15 seconds, respectively. To determine the initial conditions for the surface water levels, velocities, salinity, and temperature, we used the re-analyzed data from the HYbrid Coordinate Ocean Model (HYCOM; Metzger et al., 2014; [https://www.ncei.noaa.gov/thredds-coastal/catalog/hycom\\_region1/catalog.html](https://www.ncei.noaa.gov/thredds-coastal/catalog/hycom_region1/catalog.html)). 13 tidal elements (M2, S2, N2, K1, K2, O1, P1, Q1, MF, MM, M4, MS4, and MN4) from the TPXO Tide Model database at Oregon State University (Egbert and Erofeeva, 2002) were applied to the parent grid to simulate astronomic tides. The Flather boundary condition (Flather, 1976) was applied at the boundaries of the ROMS model (the northeast and southeast boundaries of the black-dashed box in panel a of Fig. A2 in the appendix) for the momentum balance to radiate out deviations from exterior values at the speed of the external ocean waves. A two-day spin-up was done, followed by an 11-day simulation (i.e., 13 days in total). The initial conditions, such as currents, water levels, temperature, and salinity, were examined to show that the two-day spin-up is adequate for them to achieve the equilibrium state in the model. It was determined that an 11-day simulation period, including at least five days prior to the storm's peak, was sufficient to track the development and spread of swells near the SAB.

For the boundary conditions of the SWAN model for Hurricane Matthew, hourly statistical wave bulk parameters (e.g., zero-order moment wave height, mean wave direction, and peak wave period) from NOAA's WAVEWATCH III re-analyzed global dataset (The WAVEWATCH III Development Group, 2016; <https://polar.ncep.noaa.gov/waves/ensemble/download.shtml>) were imposed at 47 boundary segments along the southeast and northeast boundaries of the U.S. East Coast grid (the black-dashed box in Fig. A2 in the appendix) assuming the JONSWAP wave spectra. NOAA's WAVEWATCH III re-analyzed global dataset did not have available data during Dorian and Isaias. Thus, we employed a larger grid to cover the North Atlantic Ocean and the Gulf of Mexico with our modeling system to generate the wave boundary conditions for these two TCs for input as boundary conditions to the SWAN model. Wave spectrum was solved with 60 and 25 directional and frequency bins. The parent and child grids were solved with 30 and 15 seconds as their computational time steps, respectively. As for the atmospheric forcing, SWAN used the same GFS-RAP input as ROMS.

Using the Model Coupling Toolkit, water levels, current velocities, and wave fields are two-way coupled in COAWST (Warner et al., 2008). In our simulations, the data exchange interval between ROMS and SWAN was set to 30 minutes, including water surface elevation, current velocities, statistical wave bulk parameters (e.g., zero-order moment wave heights, peak and mean wavelengths, peak and mean wave periods, peak and mean wave directions and wave dissipation). This exchange interval has been tested and used by Hegermiller et al. (2019) and Hsu et al. (2023), in which the nearshore hydrodynamics was replicated adequately. Thereby, we applied the same data exchange interval in the present work. Specifics regarding the coupling method and an example case study were provided (Warner et al., 2008; 2010). The wind shear stresses and sea surface roughness by Taylor and Yelland (2001) at the sea surface were computed and used to force the ocean model. The vortex-force formulation (Kumar et al., 2012; Uchiyama et al., 2010) was employed in the current study to account for wave-current interaction. Furthermore, the wave and current boundary layer properties were estimated with the SSW\_BBL option, which used the model of Madsen (1994).

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## 2.4 Empirical formulas for wave runup

We followed the work of Serafin and Ruggiero (2014) and applied the empirical formulas proposed by Stockdon et al. (2006) and Senechal et al. (2011) to compute the wave runup at NOAA tide gauges using the wave parameters at nearby NDBC wave buoys along the SAB. The locations of the tide gauges and wave buoys are indicated in Fig 1. The empirical formula proposed by Stockdon et al. (2006) (Eqs. 1 and 2) provides the 2% exceedance percentile of extreme wave runup ( $R_2$ ):

$$R_2 = 1.1 \left( 0.35\beta_f(H_0L_0)^{\frac{1}{2}} + \frac{[H_0L_0(0.563\beta_f^2+0.004)]^{\frac{1}{2}}}{2} \right), 0.3 \leq \xi_0 < 4.0, \quad (1)$$

$$R_2 = 0.043(H_0L_0)^{\frac{1}{2}}, \xi_0 < 0.3, \quad (2)$$

in which foreshore beach slope ( $\beta_f$ ) and deep-water wave parameters ( $H_0$  is the deep water zero-order moment wave height and  $L_0$  is the deep-water peak wavelength) and the Iribarren number ( $\xi_0$ ) (Eq. 3) were required.  $\xi_0$  was used to categorize wave breaker types (Battjes, 1974). In Eq. 1, the first part ( $1.1 \cdot 0.35\beta_f(H_0L_0)^{\frac{1}{2}}$ ) represents wave setup, and the second part ( $1.1 \cdot \frac{[H_0L_0(0.563\beta_f^2+0.004)]^{\frac{1}{2}}}{2}$ ) represents the combination of infragravity swash and incident swash. The foreshore beach slope is used in the calculation of wave runup and Iribarren number.

$$\xi_0 = \frac{\beta_f}{(H_0/L_0)^{1/2}}, \quad (3)$$

While beach slopes depend on local coastal morphology, wave heights and wavelengths also depend on storm characteristics. Stockdon et al. (2007) pointed out that the swash zone can be moved onshore along the beach profile due to the large waves and storm surges during extreme weathers. Consequently, the mean beach slope ( $\beta_m$ ), measuring the slope of the beach from the shoreline to the dune base, was suggested and defined as the relevant slope in Eqs. 1 and 3 during hurricanes. The deep-water wave parameters can be calculated by de-shoaling the waves from a given point along the coast or shelf to deep water using the linear wave theory. The empirical formula developed by Stockdon et al. (2006) separated intermediate to wave-reflective beach scenarios ( $0.3 < \xi_0 < 4.0$ , Eq. 1) from extremely dissipative conditions ( $\xi_0 < 0.3$ , Eq. 2). According to their dataset,  $R_2$  under  $\xi_0 < 0.3$  did not necessarily linearly depend on the beach slope and was generally dominated by infragravity waves. Thus, Stockdon et al. (2006) suggested to use a parameterization with a similar form for infragravity swash to model the  $R_2$  under  $\xi_0 < 0.3$  (Eq. 2). While the field data employed by Stockdon et al. (2006) did not specifically include highly energetic conditions during storms, Stockdon et al. (2014) compared the numerical simulated wave runup of XBeach (Roelvink et al., 2009) with the parameterized wave runup of Stockdon et al. (2006) under storm conditions. Stockdon et al. (2014) showed that the parameterized wave runups were consistent with XBeach model results for SSHWS category 1 scenario, while the wave runups associated with more energetic conditions still require further discussions.

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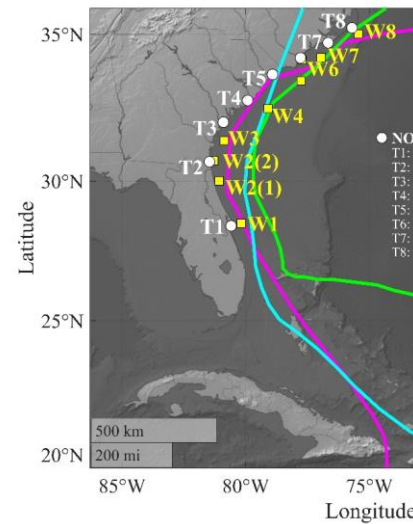


Figure 1. the paths of hurricanes Matthew 2016 (magenta), Dorian 2019 (green), and Isaias 2020 (cyan).  $h$  represents the water depth. NOAA tide gauges (white circles), NDBC wave buoys (yellow squares) selected for the model verification, and

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While  $R_2$  in the Stockdon et al. (2006) formulation is represented by a linear increase with increasing  $H_0$ , Senechal et al. (2011) suggested an upper limit of  $R_2$  at highly dissipative beaches under energetic conditions (e.g., tropical cyclone). Senechal et al. (2011) proposed another empirical formula for  $R_2$  based on  $H_0$  alone (Eq. 4), to avoid the over-prediction under such scenarios.

$$R_2 = 2.14 \tanh(0.4H_0), \quad (4)$$

While the observed data used in Stockdon et al. (2006) included part of the study area of the present work (i.e., North Carolina), most of the scenarios (>93%) at the peaks of hurricanes Matthew, Dorian, and Isaias along the SAB belonged to intermediate beach conditions, on which Stockdon et al. (2006) primarily focused ( $0.3 < \xi_0 < 4.0$ ). On the contrary, Senechal et al. (2011) specifically considered dissipative beach conditions.

### 3 Model verification

We used the observed data from eight NOAA tide gauges and nine NDBC buoys along the SAB to verify the model performance (Fig 1). These NOAA tide gauges and NDBC buoys were selected based on the observed data availability during the three hurricanes. Tide gauges T1, T7, and T8 are installed behind a barrier island, while tide gauge T2 is installed within an estuary. The other four tide gauges are installed at piers in local beaches. Thus, the measured TWLs at T1, T2, T7, and T8 may not reflect the exact water levels at the beach. The model performance on statistical wave bulk parameters (zero-order moment wave height, mean wave direction, and peak wave period) and the wave energy spectra resulting from the current model setup have been verified and discussed by Hsu et al. (2023). In the present study, we followed the approach of Serafin and Ruggiero (2014) to compute TWLs, including wave runup ( $R_2$ ), and used the measurements at NOAA tide gauges (T1–T8) and the nearby NDBC wave buoys (W1–W8) as the ‘observational data’. While seven of these NOAA tide gauges had corresponding NDBC buoys used for wave runup estimation, two NDBC buoys (W2(1) and W2(2)) were assigned to the tide gauge T2 (NOAA 8720030) for different storm events due to the lack of data. Wave parameters (zero-order moment wave height,  $H_{m0}$ , and peak wave period,  $T_p$ ) at W1–W8 were used to estimate the corresponding  $R_2$  at T1–T8 using the formula of Stockdon et al. (2006). We used the linear wave dispersion relation to compute the representative deep-water peak wave parameters ( $H_0$  and  $L_0$ ). For model results, we used the predicted  $H_{m0}$  and  $T_p$  extracted at the COAWST computational grid with the shortest distance to the U.S. Geological Survey (USGS; <https://coastal.er.usgs.gov/data-release/doi-F7GF0S0Z/>) data points along the SAB. The mean beach slopes measured by USGS before Hurricane Matthew along the SAB (Doran et al., 2015; Doran et al., 2017) were used to compute  $R_2$  (Eq. 1). While USGS had some post-Matthew field surveys, these later measurements only covered a relatively small range or did not overlap with the SAB. To simplify the problem and to focus on the comparison of TC-induced water level components under the three historical TCs, the coastal morphology was assumed not to change between storms.

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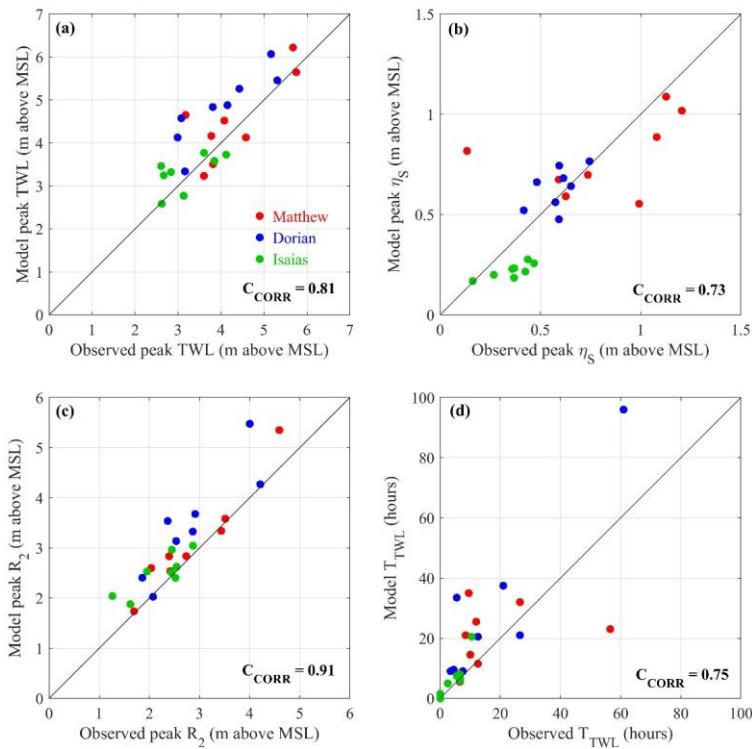
**Moved (insertion) [6]:** While seven of these NOAA tide gauges had corresponding NDBC buoys used for wave runup estimation, two NDBC buoys (W2(1) and W2(2)) were assigned to the tide gauge T2 (NOAA 8720030) for different storm events due to the lack of data.

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465 To quantify the model performance, we used the correlation coefficient between the “measured” and modeled peak storm surge, peak wave runup, and maximum continuous duration of  $TWL \geq D_{base}$  at these eight NOAA tide gauges (Fig. 2). Overall, model results showed good agreement with NOAA observations: from the 24 data points at eight NOAA tide gauges during three storms with the correlation coefficient higher than 0.7 for the peak  $TWL$ , the peak storm surge ( $\eta_S$ ), the peak wave runup ( $R_2$ ), and the maximum continuous duration of  $TWL \geq D_{base}$  ( $T_{TWL}$ ). We utilized the Lanczos low-pass filter (Duchon, 1979) to remove the astronomic tides from  $\eta_0$  and obtained the storm surge ( $\eta_S$ ). It is noted that there were larger discrepancies of the peak  $\eta_S$  and  $T_{TWL}$ . There may be several reasons causing the discrepancy between observed and model results. For example, the observed data at NOAA tide gauges may not reflect the actual extreme water levels and the corresponding durations at beach because of their locations, especially at tide gauges T1, T2, T7, and T8 which are located within estuaries or behind barrier islands. The current spatial resolution of the computational grid may not completely reflect the details of the bathymetry around these estuaries and narrow barrier islands. Secondly, the potential influence of rainfall and river discharge nearby these observed locations may also contribute to the  $TWL$ . As we used a low-pass filter to remove the contribution from astronomic tides, rainfall and river discharge may contribute to the resulting water level as well. Accordingly, we used the model results from the ROMS-SWAN model to focus on the storm-forced water level components induced by wind and atmospheric pressure at beaches along the SAB in the present work, which also allows for a higher spatial and temporal resolution of  $TWL$  at beach.

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**Figure 2.** Model verification of (a) the peak TWLs, (b) the peak storm surge, (c) the peak wave runup, and (d) the maximum continuous duration of  $TWL \geq D_{base}$  ( $T_{TWL}$ ) at eight NOAA tide gauges during the three historical hurricanes. The red, blue, and green points denote the data of hurricanes Matthew, Dorian, and Isaias, respectively. The corresponding correlation coefficients ( $C_{CORR}$ ) are shown on the bottom-right corner in each panel.

#### 4 Results and discussion

This section compares the temporal and spatial changes of  $\eta_S$  and  $R_2$  along the SAB caused by hurricanes Matthew in 2016, Dorian in 2019, and Isaias in 2020. Additionally, the relationship between TC characteristics and the TC-induced water level components is examined.

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$$\text{Deleted: } skill = 1 - \frac{\sum_1^N |X_{model} - X_{obs}|^2}{\sum_1^N (|X_{model} - \bar{X}_{obs}| + |X_{obs} - \bar{X}_{obs}|)^2} \quad (5) \quad \text{¶}$$

where  $N$  was the total number of data elements;  $X_{model}$  was the model result;  $X_{obs}$  was the observed data; the bar denotes time average. ¶

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Deleted: Figure 3. TWLs time series at six NOAA tide gauges during the three historical hurricanes. The  $skill$  was calculated with the formula of Willmott (1981), and the  $RMSE$  denoted root-mean-square errors between model results (blue curves) and observations (red points). ¶

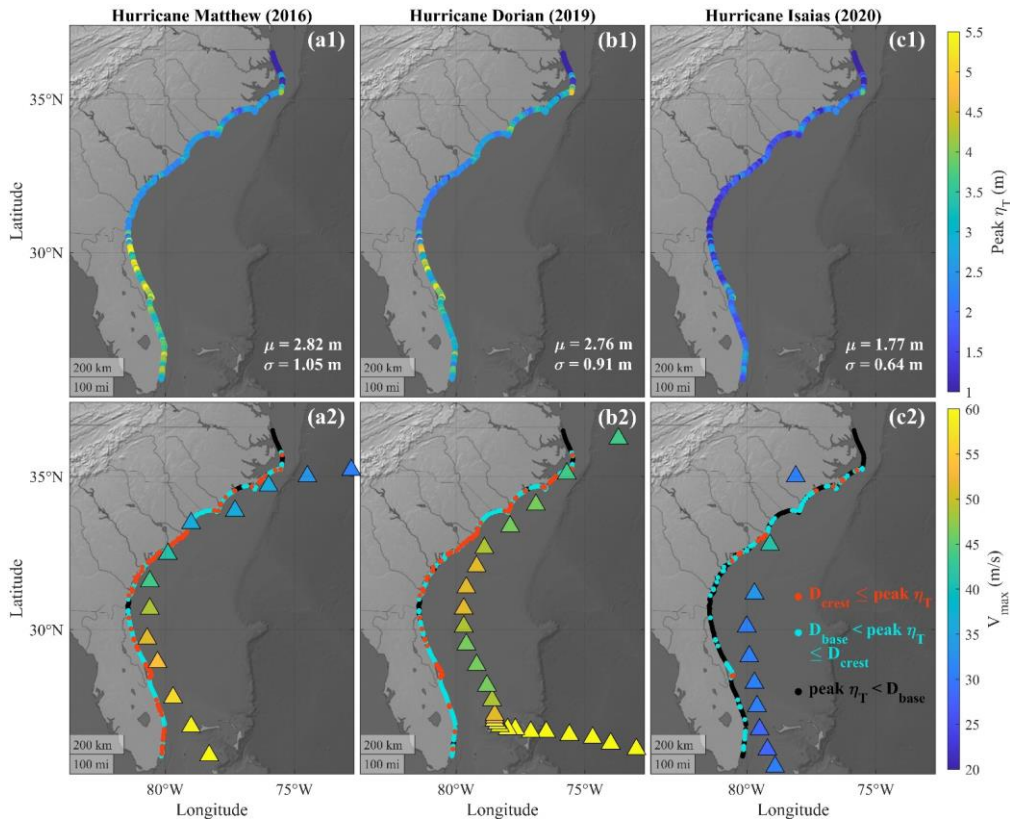
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605 **4.1 Storm forced water level components**

TWL depends on the astronomic tides, which is at first order independent of TC characteristics, in such a way that the peak of the TC-induced water level can occur at any tidal level. Here, we focused on the influences of  $V_{max}$ ,  $V_t$  and TC path on two TC-induced water level components:  $\eta_S$  and  $R_2$ . We combined  $\eta_S$  with the  $R_2$  estimated by the Stockdon et al. (2006) formulation to obtain the peak TC-induced water level,  $\eta_T$  (panels a1, b1, and c1 in Fig. 3).



610 **Figure 3. a1, b1, and c1** Peak  $\eta_T$  (i.e., the sum of  $\eta_S$  and  $R_2$ ) along the SAB during the three hurricanes;  $\mu$  represented the average and  $\sigma$  was the standard deviation along the SAB. **a2, b2, and c2** IBTrACS data of the TC every six hours with the colormap presenting instantaneous maximum sustained wind ( $V_{max}$ ); the red, blue, and black points indicated the most severe levels achieved during the TC. We followed Sallenger (2000) and used local  $D_{crest}$  and  $D_{base}$  elevations to categorize the peak  $\eta_T$ . These categorizations were  $D_{crest} \leq \text{peak } \eta_T$ ;  $D_{base} \leq \text{peak } \eta_T < D_{crest}$ ; and  $\text{peak } \eta_T < D_{base}$ .

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#### 4.2 Peak values and durations of $\eta_T$ and TWL over specified thresholds along the SAB

Matthew and Dorian had stronger  $V_{max}$  on average (45.25 m s<sup>-1</sup> and 58.80 m s<sup>-1</sup> respectively) within the SAB compared to Isaias (32.11 m s<sup>-1</sup>; Table 1), which led to lower surge levels during Isaias (15 cm to 90 cm lower than Matthew and Dorian). Meanwhile, Matthew's distance to the coastline (47.38 km) was shorter compared to Dorian (96.73 km) and Isaias (97.24 km) along the SAB on average. The peak  $\eta_T$  along the SAB had similar values and distribution patterns during Matthew and Dorian, while during Isaias was 60% to 65% smaller on average (panels a1, b1, and c1 in Fig. 3). Along Florida's southeast coast the peak  $\eta_T$  was higher during Matthew compared to Dorian and Isaias, but decreased significantly along Georgia and South Carolina as Matthew propagated northward and weakened. This led to a higher deviation of peak  $\eta_T$  along the SAB during Matthew compared to Dorian and Isaias.

We used  $D_{crest}$  and  $D_{base}$  as thresholds to categorize the peak  $\eta_T$  and TWL into the morphological impact regimes of Sallenger (2000) along the SAB. The peak  $\eta_T$  can occur coincidentally with either the high tide or the low tide. Without the astronomic tides, the present work isolated and determined the contribution of TC-induced water level components and its dependency on TC characteristics. While Sallenger (2000) used the thresholds to categorize the morphological impacts caused by the TWLs, we utilized the thresholds to categorize the levels of TC-induced water levels ( $\eta_T$ ) specifically. 23.0% and 19.9% of the coastal sites experienced peak  $\eta_T \geq D_{crest}$  (red points in panels a2, b2, and c2 of Fig. 3) during Matthew and Dorian, respectively. These percentages were higher during Matthew and Dorian compared to those during Isaias (3.5%) (Table 2).

**Table 2. Percentage of coastal sites of each categorization of peak  $\eta_T$  and peak TWL during the three historical TCs along the SAB.**

	Categorizations of the peak $\eta_T$			Categorizations of the peak TWL		
	$D_{crest} \leq$ peak $\eta_T$	$D_{base} \leq$ peak $\eta_T < D_{crest}$	peak $\eta_T$ < $D_{base}$	$D_{crest} \leq$ peak TWL	$D_{base} \leq$ peak TWL < $D_{crest}$	peak TWL < $D_{base}$
Matthew	23.0%	55.6%	21.4%	41.6%	46.4%	12.0%
Dorian	19.9%	54.8%	25.3%	42.0%	49.2%	8.8%
Isaias	3.5%	22.1%	74.4%	18.7%	46.0%	35.3%

The proportion of coastal sites experiencing peak TWL  $\geq D_{crest}$  was at least 1.8 times more than peak  $\eta_T \geq D_{crest}$  (Table 2), which showed the importance of astronomic tides in coastal inundation levels. Matthew had a shorter distance to the coast along the SAB compared to Dorian, while Dorian had stronger intensity north to Georgia (Fig. 3 and Table 1). Consequently, Matthew and Dorian induced comparable peak  $\eta_T$  along the SAB.

In addition to the peak  $\eta_T$ , we used  $D_{base}$  as the threshold to compute the maximum continuous durations of  $\eta_T \geq D_{base}$  ( $T_{ETA}$ ; panels a1, b1, and c1 in Fig. 4) and TWL  $\geq D_{base}$  ( $T_{TWL}$ ; panels a2, b2, and c2 in Fig. 4) along the SAB throughout each of the entire storm events. These were determined by calculating the maximum continuous duration that  $\eta_T$  or TWL was higher

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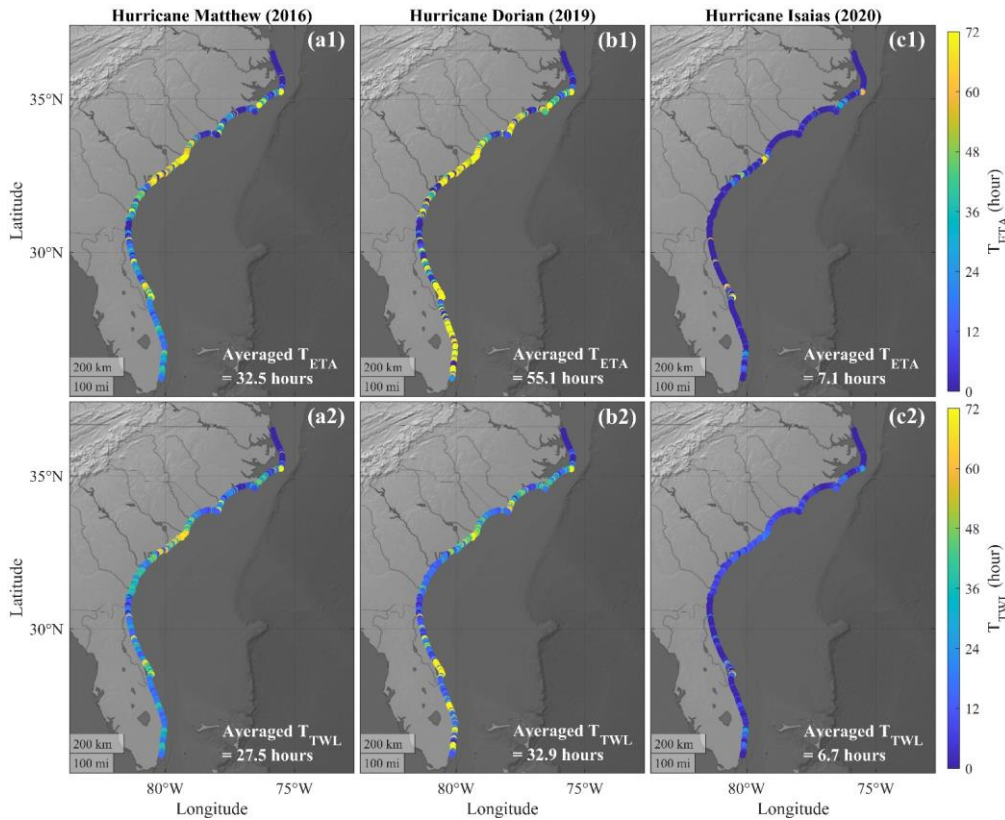
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than the thresholds without interruption. The  $D_{base}$  was applied here because ~~less than 23%~~ of all coastal sites experienced peak  $\eta_T \geq D_{crest}$  during the three TCs (Table 2). The averaged  $T_{ETA}$  along the SAB during Dorian (55.1 hours) was longer than those during Matthew (32.5 hours) and Isaias (7.1 hours) (Fig. 4). Considering the contributions from astronomic tides, the averaged  $T_{TWL}$  along the SAB were 27.5, 32.9, and 6.7 hours during Matthew, Dorian, and Isaias, respectively (Fig. 4).

685 Note that the difference of averaged  $T_{TWL}$  during Matthew and Dorian (i.e., ~~32.9-27.5=5.4 hours~~) was 76% smaller than the corresponding difference of averaged  $T_{ETA}$  (i.e., ~~55.1-32.5=22.6 hours~~). This was mainly related to the smaller tidal range during Hurricane Matthew compared to Dorian. Although  $TWL$  was larger than  $\eta_T$  at high tides (crests of astronomic tidal signal), it was smaller than  $\eta_T$  at low tides (troughs of astronomic tidal signal). This pointed out the importance of the instantaneous tidal range in the inundation duration under extreme weather conditions.



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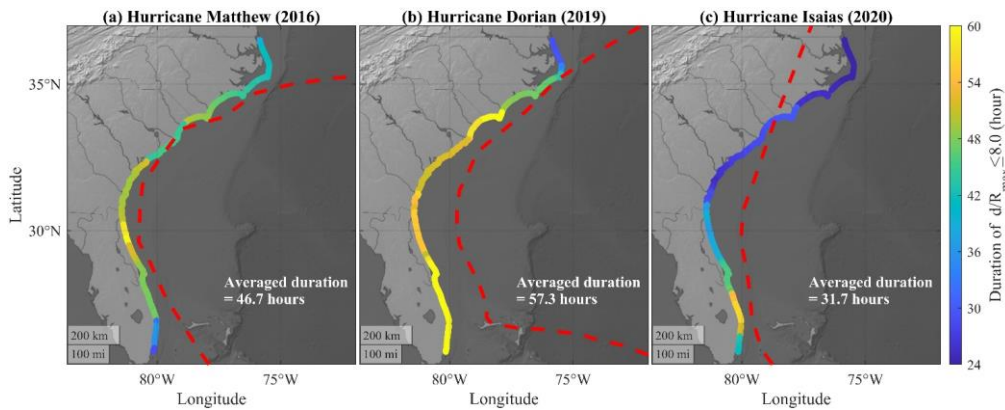
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**Figure 4.** The maximum continuous duration of  $\eta_T$  ( $T_{ETA}$ ; panels a1, b1, and c1) and  $TWL$  ( $T_{TWL}$ ; panels a2, b2, and c2) over  $D_{base}$  at each USGS coastal site along the SAB throughout each of the three historical hurricanes.

We calculated the maximum continuous duration of  $d/R_{max} \leq 8.0$  at each coastal site throughout each of the three storm events, where  $d$  was the distance between TC eye and each coastal site along the SAB and  $R_{max}$  was the instantaneous radius of maximum wind (Fig. 5). This threshold followed the distance threshold of near-TC field (Collins et al., 2018; Young, 2006). While Young (2006) also considered  $V_{max}$  in the definition of near-TC field, we did not consider the threshold for  $V_{max}$  here, because  $V_{max}$  was relatively small along the SAB during Isaias. We found the duration of  $d/R_{max} \leq 8.0$  had a correlation coefficient ( $C_{CORR}$ ) = 0.47 with  $T_{ETA}$  considering the coastal sites along the SAB during hurricanes Matthew, Dorian, and Isaias. In particular, the durations of  $d/R_{max} \leq 8.0$  during Matthew and Dorian (Fig. 5) showed similar patterns as  $T_{ETA}$  (panels a1, b1, and c1 in Fig. 4). Meanwhile, the path of Hurricane Isaias had short distances to Florida's southeast coast and resulted in the duration of  $d/R_{max} \leq 8.0$  longer than 48 hours. However, it did not lead to longer  $T_{ETA}$ , primarily because of the weaker  $V_{max}$  of Isaias along the SAB.



**Figure 5.** The durations of  $d/R_{max} \leq 8.0$  along the SAB during three historical hurricanes. The red curves represented the historical track of each hurricane respectively.

#### 4.3 Relative contributions of $\eta_S$ and $R_2$ to $\eta_T$

In addition to the peak  $\eta_T$  along the SAB during the three historical hurricanes, we compared the proportions of  $\eta_S$ , wave setup, and wave swash at three specified locations: Edisto Island, South Carolina (32.51°N, 80.26°W); Sea Island, Georgia (31.20°N, 81.33°W); and the barrier island south of Matanzas Inlet, Florida (29.68°N, 81.22°W) (Fig. 6). Edisto Island, South Carolina ( $D_{crest}=2.10$  m and  $D_{base}=1.26$  m) and Sea Island, Georgia ( $D_{crest}=3.49$  m and  $D_{base}=2.41$  m) had relatively low dune elevations, in which dune overwash was more likely to occur during extreme weather events, according to the USGS (<https://www.usgs.gov/news/national-news-release/fl-ga-sc-beaches-face-80-95-percent-chance-erosion-hurricane-matthew>).

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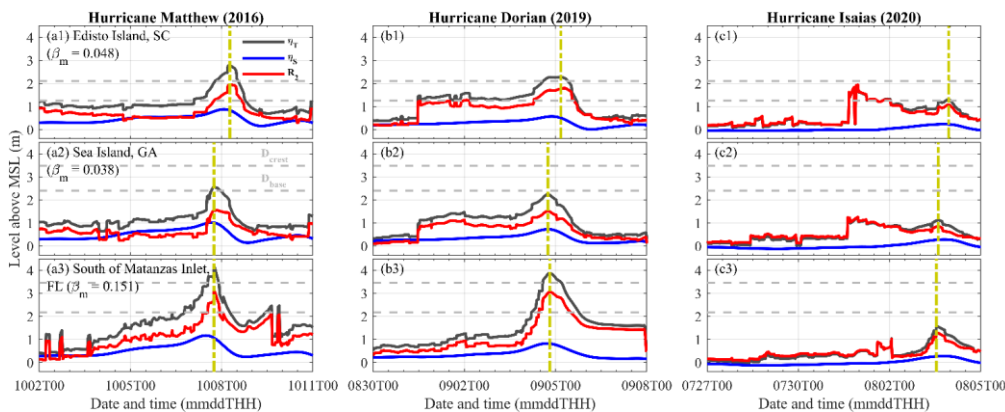
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The peak  $\eta_T$  south of Matanzas Inlet, Florida during the storms were 1.41 m to 1.62 m (51% to 64%) greater than the two barrier islands mentioned above in the near-TC field during Matthew and Dorian (time instants shown by the vertical yellow dash lines in Fig. 6). One of the factors causing higher estimated  $R_2$  was the larger mean beach slope at the barrier island south of Matanzas Inlet (0.151) compared to Sea Island (0.038) and Edisto Island (0.048) (Fig. A3 in the appendix).  $R_2$  consisted of wave setup and wave swash. The percentage of wave swash in the peak  $\eta_T$  outnumbered that of wave setup by 25% to 34% at Sea Island and Edisto Island during all three TCs, while the swash only outnumbered wave setup by less than 9% at the barrier island south of Matanzas Inlet (Fig. A4 in the appendix). Meanwhile, we found that  $\eta_S$  contributed to less than 40% in the peak  $\eta_T$  at the three locations as these three historical TCs approached. Surge levels at the peak  $\eta_T$  generally decreased from south to north during the three hurricanes, whereas wave setup and wave swash did not experience such a pattern.



**Figure 6.** The time series of  $\eta_T$  (black curves),  $\eta_S$  (blue curves), and  $R_2$  (red curves) at three selected locations during the three historical hurricanes. The horizontal gray dash lines were the local  $D_{crest}$  and  $D_{base}$  measured by USGS before Matthew (2016), and the vertical yellow dash lines were the peak  $\eta_T$  in the near-TC field.

Within the near-TC field, waves in most frequency bands kept receiving energy from the local wind, and  $\eta_T$  was directly impacted by the instantaneous TC characteristics. The peak  $\eta_T$  occurred within the near-TC field between 15:00 UTC 07 October 2016 and 07:00 UTC 08 October 2016 during Matthew, while it took place between 14:00 UTC 04 September 2019 and 04:00 UTC 05 September 2019 during Dorian (panels a1, a2, a3, b1, b2, and b3 in Fig. 6). The peak  $\eta_T$  at the three locations occurred in the near-TC field during Matthew and Dorian, without a second comparable peak  $\eta_T$  throughout the time series. The conditions during Isaias were unique and different from Matthew and Dorian. First, the instantaneous  $V_{max}$  did not reach  $33 \text{ m s}^{-1}$  during Isaias when  $d/R_{max} \leq 8.0$  at most coastal sites along the SAB. Second,  $\eta_T$  generally experienced an abrupt increase before Isaias reached the coastal sites along the SAB. This earlier increase of  $\eta_T$  at Edisto Island (South Carolina) even exceeded the peak value within the near-TC field (panel c1 in Fig. 6). This increased  $\eta_T$  before the peak of the

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storm occurred between 21:00 and 23:00 UTC 31 July 2020 at Sea Island and Edisto Island, when Isaias was still far away from these three selected locations (i.e., distances larger than 1300 km).

$\eta_S$  and  $R_2$  at the coast depended on the instantaneous TC characteristics within the near-TC field. The differences between the peak  $\eta_T$  within the near-TC field during hurricanes Matthew and Dorian were less than 1.0 m at the three selected locations.

785 The peak  $\eta_T$  at the same locations during Hurricane Isaias within the near-TC field (03 August 2022 UTC) was 1.0 m to 2.7 m less than that of Matthew and Dorian.  $\eta_S$  during Isaias was 50% to 80% lower than that of Matthew and Dorian within the near-TC field at the three locations (numbers listed in Fig. A4 in the appendix). The peak  $R_2$  (i.e., the sum of setup and swash) during Isaias was 40% to 60% smaller compared to that of Matthew and Dorian in the near-TC field. This was related to Isaias's smaller  $V_{max}$  within the SAB (28% to 36% smaller than Matthew and Dorian; Table 1).

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**Table 3. Maximum continuous durations of  $\eta_T$  and  $TWL$  over the local  $D_{base}$  at the three barrier islands during the three historical TCs in hours.  $T_{ETA}$  was the maximum continuous duration of the scenario  $\eta_T \geq D_{base}$ ;  $T_{TWL}$  was the maximum continuous duration of the scenario  $TWL \geq D_{base}$ .**

	$T_{ETA}$ (hour)			$T_{TWL}$ (hour)		
	Edisto Island	Sea Island	South of	Edisto Island	Sea Island	South of
			Inlet			Inlet
Matthew	40.5	7.5	35.5	31.0	10.5	23.0
Dorian	125.0	0.0	37.0	24.5	6.0	24.0
Isaias	16.5	0.0	0.0	6.0	0.5	1.5

795 The duration of the same  $\eta_T$  category ( $\eta_T \geq D_{crest}$ ;  $D_{base} \leq \eta_T < D_{crest}$ ; and  $\eta_T < D_{base}$ ) varied with TC characteristics.  $T_{ETA}$  at Edisto Island lasted up to more than five days during Dorian, which was much longer compared to the  $T_{ETA}$  during Matthew and Isaias (40.5 hours and 16.5 hours, respectively; Table 3).  $T_{ETA}$  at the barrier island south of Matanzas Inlet during Dorian (37.0 hours) was longer compared to Matthew (35.5 hours), but the difference was smaller than that at Edisto Island. While  $T_{ETA}$  primarily depends on TC characteristics,  $T_{TWL}$  also depends on the instantaneous local tidal range. The  $TWLs$  at tidal troughs were lower with a larger tidal range. This led to a shorter  $T_{TWL}$  when compared to  $T_{ETA}$  in the three hurricanes, as  $TWLs$  dropped lower than  $D_{base}$  at tidal troughs. Although Dorian had a stronger  $V_{max}$  and slower  $V_t$  along the SAB on average, Matthew and Isaias had shorter distances to the coast. Moreover, the tidal range during Matthew was approximately 40 cm smaller compared to Dorian and Isaias on average at the eight NOAA tide gauges (shown in Fig. 1). With similar  $V_{max}$ , shorter distances to the coast and a smaller tidal range, Matthew had longer  $T_{TWL}$  at Edisto Island and Sea Island compared to Dorian (Table 3).

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5 Discussion¶



#### 4.4 Storm forced water level variation

Suh and Lee (2018) utilized two historical TCs to analyze and compare the propagation processes of forerunner surges and primary surges in the Yellow Sea, and these processes were linked to the heading direction, path, and translation speed of the storm. Similarly, we observed distinct patterns of storm-dependent water-level component variations during three different storm events and at various locations along the SAB.

During Matthew and Dorian, the peak  $\eta_T$  occurred when the coastal sites started to be covered by the near-TC field, which was induced by the wind waves and  $\eta_S$  associated with higher TC intensities (i.e., larger pressure deficits and higher wind speeds). However, the  $\eta_T$  at the three coastal sites had another local maximum at 15:30 UTC 31 July 2020 during Isaias, when the storm was still located around 21.5°N and 73.5°W, i.e., south of the SAB (Fig. 7b and Fig. 7d). This was primarily the result of two factors. First, before entering the SAB (i.e., south of 26.0°N and east of 79.0°W), the translation speeds of Matthew (maximum of 7.52 m s<sup>-1</sup> and average of 4.17 m s<sup>-1</sup>) and Dorian (maximum of 7.35 m s<sup>-1</sup> and average of 5.35 m s<sup>-1</sup>) were slower compared to Isaias (maximum of 9.81 m s<sup>-1</sup> and average of 6.74 m s<sup>-1</sup>). Xu et al. (2007) found that the swell energy and wavelength increased when  $V_t$  was comparable to the group wave celerity and under 13 m s<sup>-1</sup>. This allowed wind waves to experience an extended wind fetch and resulted in the growth of wavelength and wave height. According to Eq. 1 (Stockdon et al., 2006),  $R_2$  increases with the deep-water peak wavelength and the deep-water zero-order moment wave height. Second, before arriving at the Island of Hispaniola (19.0°N), the swell generated by Matthew on its right-hand side was blocked by the Island of Hispaniola and was unable to propagate towards the SAB on its path. By contrast, the swell generated by Isaias on its front-right quadrant was not blocked by any island (see Fig. 1). Thus, the condition during Isaias was better for swell's wavelength to be lengthened and to propagate ahead of the storm.

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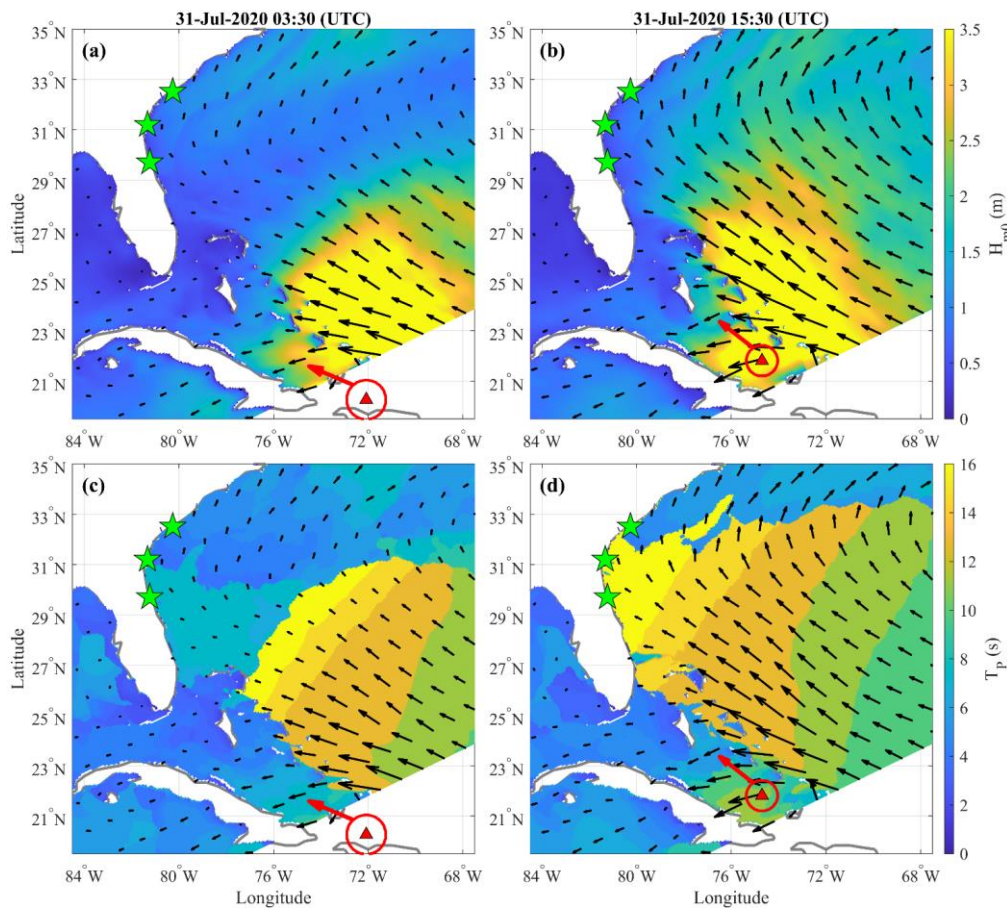
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865 **Figure 7.** The propagation of the swells generated by Hurricane Isaias on its right-hand side. The green stars indicated the three  
 870 selected barrier islands, i.e., Edisto Island, Sea Island, and the barrier island south of Matanzas Inlet (from North to South). The  
 red triangles represented the eye of Isaias with the red circle denoting the instantaneous radius of maximum wind and the red arrow  
 denoting the heading direction. The black arrows were the mean wave directions from COAWST simulation. The colormaps in  
 panels (a) and (b) showed the distribution of  $H_{m0}$  at 03:30 UTC 31 July 2020 and 15:30 UTC 31 July 2020, respectively. The  
 colormaps in panels (c) and (d) showed the distribution of  $T_p$  at 03:30 UTC 31 July 2020 and 15:30 UTC 31 July 2020, respectively.

According to the model results and linear wave dispersion relation, the peak wave period was 19.1 s and the corresponding  
 deep-water phase celerity was larger than  $25 \text{ m s}^{-1}$  at Sea Island, Georgia at 15:30 UTC 31 July 2020 during Isaias (when the  
 abrupt elevated  $R_2$  occurred). This swell with a relatively long wave period generated by Isaias on its right-hand side arrived

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at the SAB coast much earlier (one to two days) than the storm, which led to an abrupt increase in  $R_2$ . Around 16:00 UTC 01 August 2020, the instantaneous  $V_t$  of Isaias decreased from  $7.0 \text{ m s}^{-1}$  to ~~less than~~  $4.5 \text{ m s}^{-1}$ . Additionally, waves with different periods travel with different phase celerities according to linear wave dispersion relation. This is also consistent with the distribution pattern of peak wave periods shown in Fig. 7c and Fig. 7d (i.e., waves with higher  $T_p$  moved forward faster and approached the SAB earlier). Consequently, the wavelength of the swell arriving later at the SAB decreased, which led to a decrease of  $R_2$ .

#### 4.5 Coastal impact regimes of Sallenger (2000) and the temporal variation of $\beta_m$

The dune elevations measured by the USGS before Matthew did not reflect the realistic conditions during Dorian and Isaias, since the beach morphology (e.g., dune heights and beach slopes) changed in time. However, the time-invariant dune elevations allowed the present work to focus on determining the relative contributions of TC-induced water level components ( $\eta_S$  and  $R_2$ ) during various TCs. The coastal impact regimes (Sallenger, 2000) were determined with the relative  $TWLs$  depending on storm forced parameters ( $\eta_S$  and  $R_2$ ), astronomic tides, and coastal morphology (dune elevations and beach slopes). However, the real coastal impact regimes during specific events require an update of the beach slopes and dune elevations. The problem was that this information was not always available at the spatial scale of this study.

To determine the sensitivity of the wave runup to the beach slopes, we used the post-Matthew  $\beta_m$  from Georgia to North Carolina measured by USGS (Doran et al., 2017) to compare  $TWLs$  and  $T_{TWL}$  associated with the model results of Hurricane Dorian with the pre-Matthew surveyed  $\beta_m$  (Fig. 8). We used the post-Matthew beach morphological information to determine the difference in the estimated storm-induced water levels. The post-Matthew dataset showed that  $\beta_m$  experienced an averaged decrease of  $-0.026$  after Hurricane Matthew. According to Eqs. 1 and 2,  $TWLs$  and  $T_{TWL}$  during Hurricane Dorian would decrease, considering the change of  $\beta_m$ . Results showed that 50% of the coastal sites between Georgia and North Carolina experienced an absolute difference of simulated peak  $TWL$  less than  $0.5 \text{ m}$  as  $\beta_m$  changed. The averaged decrease of peak  $TWL$  was  $0.56 \text{ m}$  with a standard deviation of  $0.87 \text{ m}$ . Meanwhile, an averaged decrease of  $T_{TWL}$  of  $11.23 \text{ hours}$  was observed (Fig. 8).

Based on Sallenger's (2000) categorization, our model results showed that the  $TWL$  (i.e., the sum of  $\eta_T$  and astronomic tides) scenarios belonged to the overwash and collision regimes during Matthew and Dorian, respectively, under the assumption of constant dune elevations and  $\beta_m$ . However, dune heights and  $\beta_m$  are expected to decrease after storm events, which is consistent with the post-Matthew conditions from the observed data. While a decreased dune elevation led to more severe and longer impact regimes, a milder  $\beta_m$  resulted in a lower wave runup.

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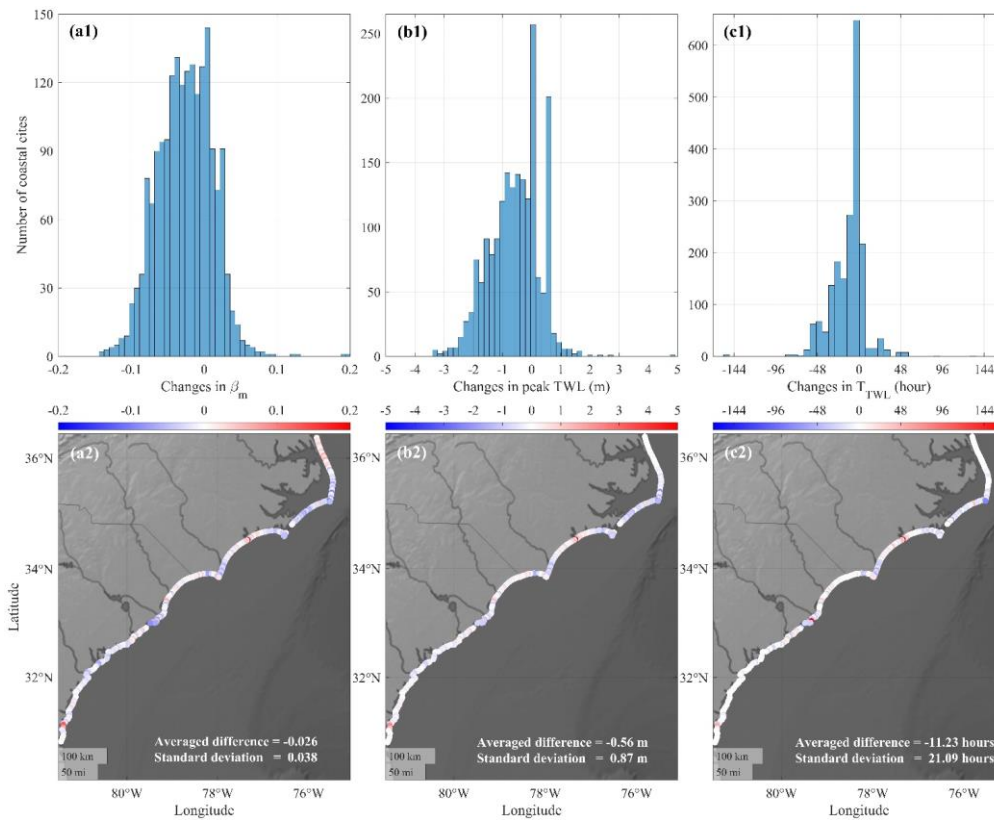


Figure 8. Histograms (top panels) and spatial distributions (bottom panels) of the differences of  $\beta_m$ , peak  $TWL$ , and  $T_{TWL}$  under pre- and post-Matthew conditions from Georgia to North Carolina coasts: [a1, a2](#))  $\beta_m$ ; [b1, b2](#)) peak  $TWL$ ; [c1, c2](#))  $T_{TWL}$ .

#### 4.6 Arrival timing of the peak storm-dependent components

Beside beach morphology and TC-dependent parameters ( $\eta_T = \eta_S + R_2$ ), TC-independent parameters like astronomic tides also influenced the coastal impact regimes. Take the barrier island south of Matanzas Inlet, Florida for example, we found that the peak  $TWL$  exceeded  $D_{crest}$ , while the  $\eta_T$  did not exceed  $D_{crest}$ . This was related to the coincidence of the timing of the high tide and the peak  $\eta_T$ . In the case that the peak  $\eta_T$  occurred at low tide, the peak  $TWL$  would be lower than the peak  $\eta_T$ . With the time-invariant dune elevation, both the peak  $TWL$  and the peak  $\eta_T$  did not reach  $D_{crest}$  at this location during Dorian. However, both peak  $TWL$  and peak  $\eta_T$  would exceed  $D_{crest}$  in case that the dune elevation became lower.

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#### 4.7 Effects of TC properties on the durations of $\eta_T$

Hurricane Dorian traveled with a slower  $V_t$  ( $3.27 \text{ m s}^{-1}$ ) on average, which was not only slower than the other two historical storms but also slower than the global average of TCs in all categories ( $4.20 \text{ m s}^{-1}$  to  $6.00 \text{ m s}^{-1}$ ). While the instantaneous  $V_{max}$  had significant impacts on the  $\eta_T$ , the slow movement of the TC resulted in a longer duration of  $T_{ETA}$  at which a specific location was under its impact. The peak  $\eta_T$  did not reach  $D_{base}$  ( $T_{ETA}=0.0 \text{ hour}$ ) at Sea Island during Dorian while the peak  $\eta_T$  at the same location exceeded  $D_{base}$  for 6.0 hours during Matthew.  $V_t$  was the primary factor determining  $T_{ETA}$  at the other two coastal sites. However, as  $V_{max}$  increased and/or the distance to the TC eye decreased,  $T_{ETA}$  may also increase. The variations of  $T_{ETA}$  at the three coastal sites during the three historical TCs implied that the peak water level alone may not be sufficient to predict the coastal impacts in practical scenarios. For instance,  $T_{ETA}$  experienced a 67.7% difference (84.5–hour difference) at Edisto Island between Matthew and Dorian, while the peak  $\eta_T$  at this location belonged to the same categories during these two TCs.

#### 4.8 Estimations of $R_2$ using different empirical formulas for $R_2$

Stockdon et al. (2006) used different formulas of  $R_2$  for the scenarios  $0.3 \leq \xi_0 < 4.0$  and  $\xi_0 < 0.3$ . The range  $0.3 \leq \xi_0 < 4.0$  represents intermediate to more reflective beach scenarios. The formula of Senechal et al. (2011) was proposed based on the regression of their observed runup data to improve the estimation under highly dissipative and saturated beach conditions ( $\xi_0 < 0.3$ ), specifically.

We compared the  $R_2$  estimated by the formulas of Stockdon et al. (2006) and Senechal et al. (2011) at the same locations previously considered (Edisto Island, South Carolina; Sea Island, Georgia; and the barrier island south of Matanzas Inlet, Florida) during the three historical hurricanes (Fig. 9). The difference between the peak  $R_2$  estimated by the two formulas reached up to 1.34 m at the barrier island south of Matanzas Inlet (panels a3 and b3 in Fig. 9; Stockdon's prediction was 76% higher than Senechal's prediction during Matthew and Dorian).

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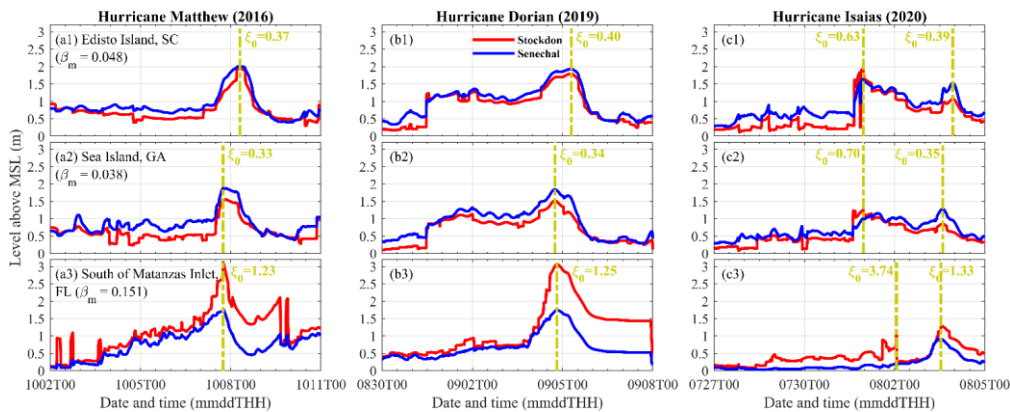
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**Figure 9.** The  $R_2$  estimated by the formulas of Stockdon et al. (2006; red curves) and Senechal et al. (2011; blue curves) at three coastal sites during three hurricanes. The Iribarren numbers ( $\xi_0$ ) corresponding to the peak  $R_2$  (vertical yellow dash lines) were listed.

The  $R_2$  estimated by Stockdon's formula showed a distinctive pattern during Isaias: another peak occurred before the storm approached the observed location. This was related to Isaias's unique path and faster  $V_t$ . The  $R_2$  by Senechal's formula did not show this pattern, since Senechal et al. (2011) did not include the effect of  $L_0$ . The results showed that Stockdon's approach returned a larger  $R_2$  compared to Senechal et al. (2011) especially under  $\xi_0 > 0.6$  (with a difference up to 1.34 m). On the contrary, Senechal et al. (2011) gave larger values of  $R_2$  under  $\xi_0 < 0.5$  compared to the results by Stockdon et al. (2006) but with a smaller difference (i.e., less than 0.50 m).

We computed the differences between the time series of  $R_2$  derived from the formulas of Stockdon et al. (2006) and Senechal et al. (2011) (i.e.,  $\delta_R = R_{2-Stockdon} - R_{2-Senechal}$ ) along the SAB. Next, we calculated the  $C_{CORR}$  between this difference and five parameters:  $\xi_0$ ,  $H_0$ ,  $L_0$ ,  $T_p$ , and  $\beta_m$ . The results showed the difference between the two formulas had higher correlation coefficients with  $\beta_m$  ( $C_{CORR}=0.64$ ),  $\xi_0$  ( $C_{CORR}=0.47$ ), and  $L_0$  ( $C_{CORR}=0.42$ ).  $\delta_R$  increased as the mean beach slope, the Iribarren number, and the deep-water peak wavelength increased, which resulted in more reflective beach conditions. Stockdon's approach predicted that  $R_2$  increased as wavelength increased under certain conditions (faster  $V_t$  and TC path allowing the swell to propagate toward the coasts).

## 5 Conclusions

We used the coupled ROMS-SWAN modeling system to simulate  $\eta_5$  and the wave fields (wave energy spectrum and bulk wave parameters) within the SAB during Matthew 2016, Dorian 2019, and Isaias 2020. Following Serafin and Ruggiero (2014), we used the measured  $\eta_0$  and waves to estimate the TWLs from observations. We used the linear wave theory to

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calculate the deep-water wave parameters and estimate the 2% exceedance wave runup using Stockdon (2006)'s empirical formula. We followed the same procedure with the results from COAWST and compared the TWLs estimated with both methods. COAWST model results showed good agreement with the peak TWLs, peak storm surges, peak wave runups, and exceedance durations.

060 We used our model results to compare the peak  $\eta_T$  along the SAB and at three coastal sites specifically. The instantaneous  $V_{max}$  and the distance to the hurricane eye were the key factors determining the peak  $\eta_T$  within the near-TC field, whereas the maximum continuous duration of  $\eta_T$  and TWLs over given thresholds were primarily determined by  $V_t$  and the distance to the hurricane eye. The contributions of wave runup (i.e., the sum of wave setup (16% to 38%) and wave swash (41% to 57%)) to the peak  $\eta_T$  was usually higher than  $\eta_S$  (17% to 40%) at the three selected coastal sites during the three historical TCs. The variability of  $\eta_S$  (up to 75%) at the peak  $\eta_T$  under different TC properties was larger than that of the wave runup (i.e., the sum of wave setup and wave swash; less than 59%). These wave-dependent parameters were not only functions of the TC characteristics but strongly depended on the local coastal morphology (e.g., beach slope). The time series of  $\eta_T$  revealed that with specific TC characteristics (e.g., path, heading direction, and  $V_t$ ) the peak  $\eta_T$  may occur before the storm's peak (i.e., outside the near-TC field). This was observed in the case of Hurricane Isaias as the hurricane traveled with a fast instantaneous  $V_t$  (maximum of 9.81 m s<sup>-1</sup> and average of 6.74 m s<sup>-1</sup>, which was 1.1 to 2.3 times of the global average in all categories) two to three days before approaching the location.

Two empirical formulas of wave runup estimation were compared. Stockdon's formula predicted the extreme pre-storm swells associated with TC's faster translation speeds, whereas this peak was not observed when using Senechal's empirical formula. Since runup observations during these storms were unavailable, it was not possible to determine which empirical formula was giving the best predictions. Given the relevance of accurately estimating TWLs, more observations of the wave runup during TCs are needed for the verification and calibration of wave runup parameterizations. With the present analysis of historical storms, it was difficult to determine the individual effect of each TC characteristic on TWLs. Further numerical experiments and analysis employing synthetic and idealized TCs are needed to quantify the individual impacts of  $V_t$ ,  $V_{max}$ , distance to the coast, and beach slope on TWLs and, thus, the coastal morphological impacts.

#### 080 Data availability

085 The raw data of hurricane tracks is publicly available from the International Best Track Archive for Climate Stewardship (IBTrACS; <https://www.ncei.noaa.gov/products/international-best-track-archive>; accessed on 28 August 2023). The raw historical wave records used in the analysis are publicly available from the National Data Buoy Center Historical Data & Climatic Summaries (<https://www.ndbc.noaa.gov/>; accessed on 28 August 2023). The Rapid refresh re-analyzed atmospheric data used in this work is publicly available from the National Centers for Environmental Prediction (<https://www.nco.ncep.noaa.gov/pmb/products/rap/>; accessed on 18 August 2020). The Global Forecast System re-analyzed atmospheric data is publicly available from <https://www.ncdc.noaa.gov/data-access/model-data/model-datasets/global->

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1100 [forecast-system-gfs](#) (accessed on 18 August 2020). The Hybrid Coordinate Ocean Model (HYCOM) re-analyzed data used in this work is publicly available from <https://www.hycom.org/dataserver/gofs-3pt1/analysis> (accessed on 31 March 2023). The information of tidal constituents is publicly available from Oregon State University TPXO Tide Model database (<https://www.tpxo.net/home>; accessed on 31 March 2023). The re-analyzed wave data used for the boundary conditions is publicly available from NOAA's WAVEWATCH III re-analyzed global dataset (<https://polar.ncep.noaa.gov/waves/ensemble/download.shtml>; accessed on 31 March 2023). Access to model results is available by contacting the authors.

#### CRediT authorship contribution statement

1110 Chu-En Hsu: Conceptualization, Formal analysis, Investigation, Writing – original draft, Validation, Visualization. Katherine A. Serafin: Methodology, Supervision, Writing – review and editing. Xiao Yu: Supervision, Writing – review and editing. Christie A. Hegemiller: Methodology, Software, Writing – review and editing. John C. Warner: Methodology, Software, Writing – review and editing. Maitane Olabarrieta: Conceptualization, Funding acquisition, Methodology, Supervision, Writing – review and editing, Visualization.

#### Competing interests

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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## Appendices

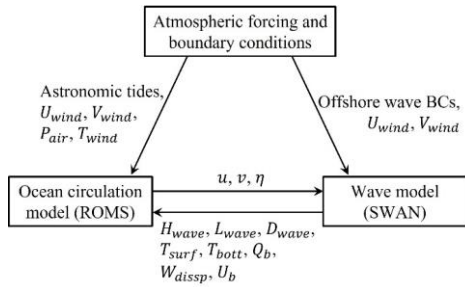


Figure A1. Computational flowchart of ocean circulation-wave coupling using COAWST modeling system.

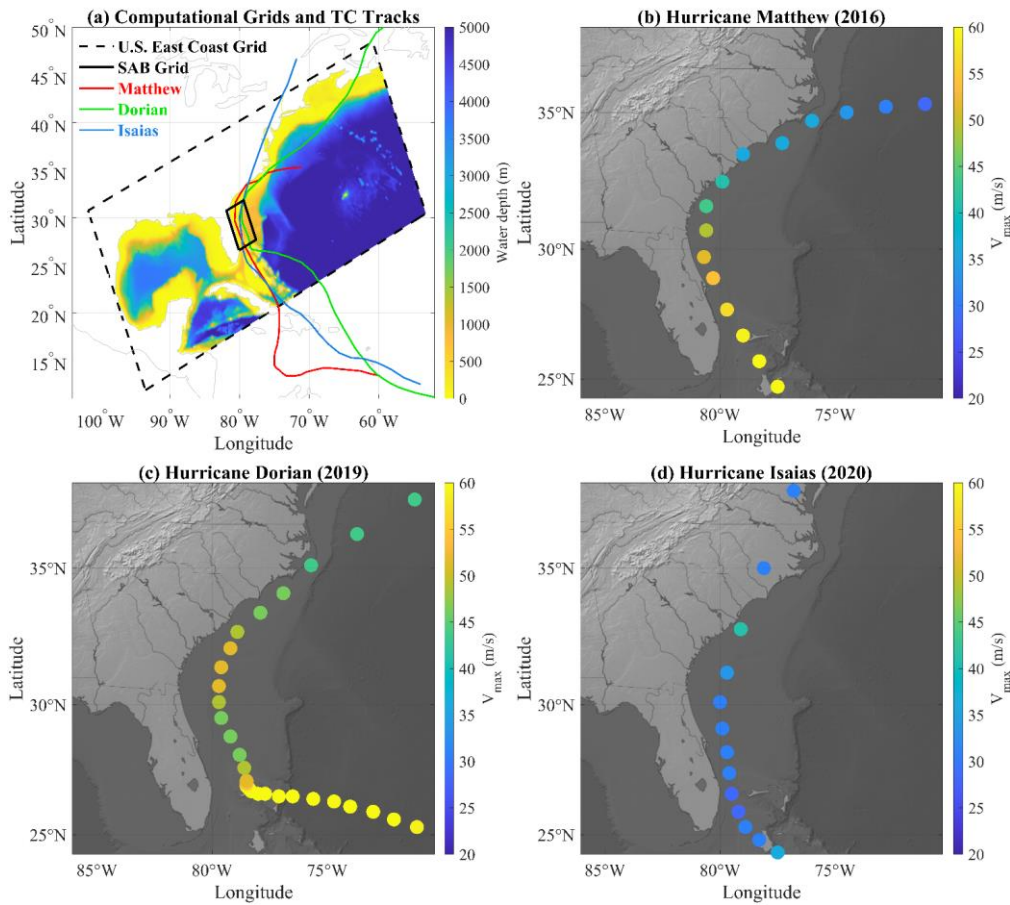


Figure A2. **a)** JBTACS (International Best Track Archive for Climate Stewardship) data of the three TCs and computational domain and bathymetry (red: Matthew; green: Dorian; blue: Isaias; black: the boundaries of computational grids; hypsometric map: water depth). Panels **b)**, **c)**, and **d)** illustrated the tracks of the TCs (dots position), with the colormap of circles representing the maximum sustained wind during Hurricanes Matthew, Dorian, and Isaias, respectively. The time interval between adjacent dots was 6 hours.

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Figure A4. Storm surge ( $\eta$ ) time series at six NOAA tide gauge during the three historical hurricanes. *Skill* was calculated with the formula of Willmott (1981), and *RMSE* denoted the root-mean-square error between model results (blue curves) and observations (red points).¶

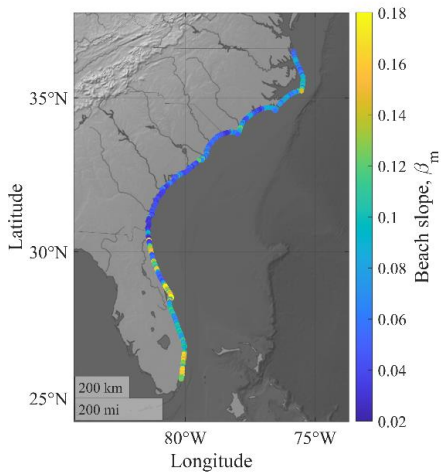


Figure A3. Pre-Matthew mean beach slopes along the SAB measured by USGS.

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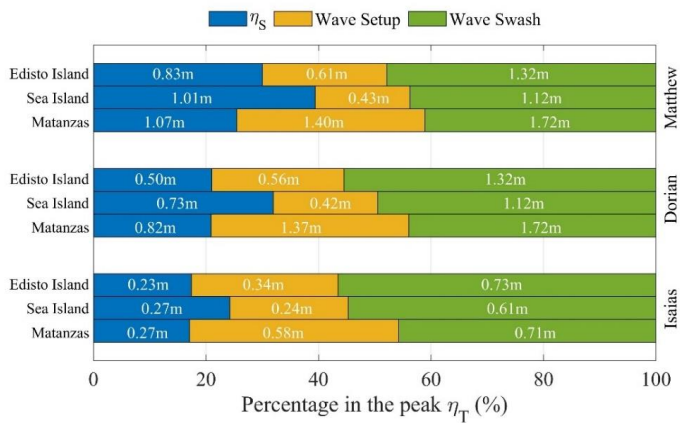


Figure A4. The contributions of  $\eta_S$ , wave setup, and wave swash in the peak  $\eta_T$  during the three historical hurricanes at the three coastal sites: South of Matanzas Inlet, Florida; Sea Island, Georgia; and Edisto Island, South Carolina with the corresponding contribution of each component (%) in the peak  $\eta_T$  and the level listed by the number written in white font.