1 An Assessment of Short-medium Term Intervention EffectsInterven-

2 <u>tions</u> Using CAESAR-Lisflood in <u>a</u> Post-earthquake Mountainous

3 Area

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9 Abstract. The 2008 Wenchuan earthquake <u>rapidly</u> triggered local geomorphic changes-<u>rapidly</u>, <u>producing</u>, <u>shifting</u> abundant 10 material through exogenic processes <u>and creating vast amounts of loose material</u>. The substantial material dynamics increased 11 the risks of geo-hazards (flash floods, landslides, and debris flows) induced by extreme precipitation in the area. Intervention 12 measures such as dams, levees, and vegetation revetments have been constructed in specified sites to reduce sediment transport, 13 thus mitigating the risk of ensuing geo-hazards.

This study <u>focused on assessing interventionassessed the</u> effects <u>of various interventions</u>, incorporated with <u>variousmultiple</u> facilities, on post-earthquake fragile mountains in the short-medium term. Taking the Xingping valley as an example, we used <u>the CAESAR-Lisflood software</u>, a two-dimensional landscape evolution model, to simulate three scenarios: unprotected landscapes, present protected landscapes, and enhanced protected landscapes between 2011 and 2013. We defined two indicators

- 18 to assess the intervention effects of the three scenarios by comparing the geomorphic changes and sediment <u>yield. yields.</u>
- The results <u>showedshow</u> that the mitigation facilities <u>wereare</u> effective, especially engineering efforts cooperating with vegetation revetments in the upstream area. The spatial patterns of erosion and deposition <u>changedchange</u> considerably <u>caused</u> of<u>due to</u> the intervention measures. Additionally, the effectiveness of each intervention scenario <u>showedshows</u> a gradual decline <u>over time</u> caused directly by the reduction <u>ofin</u> the reservoir<u>'s</u> capacity. The enhanced scenario <u>functionedperforms</u> better than the present one, with a smaller downward trend. The simulation results <u>assessedassess</u> the ability and effectiveness of cooperated control measures and <u>couldwill</u> support optimum mitigation strategies.

25 1 Introduction

26 Strong earthquakes can trigger co-seismic landslides-and crack the mountains, discontinuously, increasing crack mountains, 27 and thus increase weak structural planes (Huang, 2009) by weathering and erosion. Consequently, the source-material pro-28 ducedshifted from co-seismiccoseismal landslides and attendant mass failure failures caused by the weak slope increase in 29 mountainous regions and weakened slopes modify mountain landscapes by various surface processes for days, years, and mil-30 lennia (Fan et al., 2020). The 2008 Wenchuan Ms 8.0 (the surface-wave magnitude, which is the logarithm of the maximum 31 amplitude of the ground motion forof the surface waves with a wave period of 20 seconds) earthquake has been influencing 32 towns and other infrastructure in the affected area. Many studies have mapped the landslides triggered by thethis devastating 33 earthquake. One study, Gorum et al. (2011), performed an extensive landslide interpretation using a large set of high-resolution 34 optical images and mapped nearly 6000060,000 individual landslides, which are no less thanall impacting an area of 600 m²-35 or more. Another study, Xu et al. (2014), delineated 197481197,481 landslides formed by polygons, centroids, and top points 36 compiled from visual image interpretation. To estimate the threat of loose material in subsequent sediment disasters caused by 37 landslides, some research attempthas attempted to measure the volume of deposited material based on field surveys and

- assumptions. For example, Huang and Fan (2013) estimated that 400 million m³ of material was deposited in the heavy-heavily affected areas by assuming that the material was deposited on steep slopes with angles larger than 30° and a catchment area of more than 0.1 km². An approximate 27932.793 million m³ of sediment was calculated by Chen et al. (2009) using different deposited depth settings in different buffer zones of the Longmenshan central fault. In summary, a tremendous numberamount of loose material accumulated onin the gullies and hillslopes, ready to be eroded which became available for erosion and transported away over a long time.other exogenic processes for years to come. As a result, the mitigation in the Wenchuan
- 44 quake<u>earthquake</u>-stricken area is still in the long run<u>ongoing</u>.
- 45 Structural mitigation measures have been developed in the affected areas regardingdepending on the different site conditions 46 and other technical and economic feasibilities. For example, ecological mitigation, such as vegetation revetments, was con-47 ducted to stabilise the source area in hillslopes (Cui and Lin, 2013; Forbes and Broadhead, 2013; Stokes et al., 2014), and 48 check dams were used widely to intercept upriver sediment (Yang et al., 2021; Marchi et al., 2019). LateralAnd lateral walls 49 and levees were the longitude which are longitudinal structures (Marchi et al., 2019), can be built to protect the infrastructure-50 sinfrastructure in mountain watersheds with relatively higher sediment supply to therunoff into main streams.
- 51 Although comprehensive mitigation measures were performed inat potentially dangerous sites, disasters still occurred owing-52 due to rough terrain, vague source material, intensive precipitation, and relatively low-cost mitigating mitigation measures (Yu 53 et al., 2010; Cui et al., 2013). Therefore, understanding the effectiveness of intervention measures is crucial for mitigation 54 strategies. Some studies mainly focus on establishing post-evaluation effectiveness index systems that are not supported by 55 sufficient practices (Zhang and Liang, 2005; Wang et al., 2015). Some researchers compare the changes before and after the 56 intervention measures recorded by the recording long-term on-site measurement measurements, which face the challenges to 57 the investment of much needing a great deal of time, energy and financing (Zhou et al., 2012; Chen et al., 2013). Recent research 58 compares the has compared disaster characteristics before and after the mitigation actions, which are quickly obtained from the 59 numerical simulations (Cong et al., 2019; He et al., 2022). Nevertheless, these disaster characteristics express the process ignoringignore the long-timeterm effects of earthquakes on the geomorphic changes (longer than the duration of a 60 61 single event). Therefore, the short-medium term (from the duration of a single event to decades after) and spatial geomorphic 62 changes quickly obtained from the simulation willsimulations provide more details to interpret engineering measures in notable 63 locations, even in thoselocations inaccessible to humans.
- 64 CAESAR-Lisflood (C-L), which is based on the Cellular Automata cellular automata (CA) framework (Coulthard et al., 2013), 65 has powerful spatial modelling and computing capabilities to simulate complex dynamic systems (Batty and Xie, 1997; Cou-66 clelis, 1997; Coulthard et al., 2002). The model enables the study of many earth system interactions under different geoenvironmental. Representation of deposition and erosion within C-L is used widely in rehabilitation planning and soil erosion 67 68 predictions from ain post-mining landformlandforms (Saynor et al., 2019; Hancock et al., 2017; J.B.C. Lowry et al., 2019; 69 Thomson and Chandler, 2019; Slingerland et al., 2019) and as well as channel evolution and sedimentary budget withplanning 70 for dam settings (Poeppl et al., 2019; Gioia and Schiattarella, 2020; Ramirez et al., 2020, 2022). In addition, there werehave 71 been a series of studies in-the mountainous area involving secondary geo-hazard driving factors (Li et al., 2018; Wang et al., 72 2014b) and vegetation recovery (Zhang et al., 2018). One study, Li et al. (2020) and Xie et al. (2018) have-used C-L with 73 different rainfall scenarios or and future climate change scenarios to interpret the landscape evolution after the Wenchuan earth-74 quake. The methods and parameter values used in the above research helped to-promote thethis model's application in other 75 study areas.
- In this study, <u>the-hourly rainfall data of over</u> three years <u>waswere</u> generated by <u>daily</u> downscaling from <u>daily</u> to capture the extreme <u>eventevents</u>. Based on the input data, we simulated and compared the geomorphic changes and sediment yield in three scenarios that varied in <u>their mitigation compositions and intensities in <u>athe</u> catchment. The objectives <u>arewere 1</u>) to 1) assess</u>

the effectiveness of a set of mitigation facilities to reduce sediment transport, 2) to analyse the role of each facility on geomorphic changes, and 3) to determine the influence of vegetation-influence on catchment erosion.

81 2 Study area

82 2.1 Regional characteristics

83 The study area was the Xingping valley in the northeasternnorth-eastern Sichuan province, a Province, the left branch of the 84 Shikan riverRiver (a tributary of the Fu River) (Fig. 1). (Fig. 1). There are nearly two hundred households scattered among 85 more than five villages in the catchment. The topography of the catchment is rugged, with an elevation between 800 and 3036 86 m and an area of approximately 14 km². The catchment is characterised by a high longitudinal gradient (\sim 120‰) and more 87 than ten small V-shaped branch gullies. The length from the northeast to the southwest is 57705,770 m, and the other direc-88 tionwidth is 4,150 m in the perpendicular to which is 4150 m. Adirection. The region has a humid temperate climate with a 89 mean annual temperature of 14.7 °C-characterises the region. The mean annual precipitation is 807.6 mm, mainly concentrated 90 between May and September. The steep terrain and short-term heavy rainfall make andominate ephemeral streamstreams in 91 this area.

The local basement rocks are mainly metamorphic sandstones, sandy slate, crystalline limestone, and phyllite of <u>the</u> Triassic Xikang Group (T_{3xk}) and Silurian Maoxian Group (S_{mx}), which are easily worn away by <u>quicklyquick</u> weathering in a-static processprocesses after <u>disturbed in adisturbs caused from</u> strong <u>earthquakeearthquakes</u>. Consequently, the Wenchuan earthquake, with a Modified Mercalli Intensity scale of X, made this area one of the most severely affected locations (Wang et al., 2014a) and produced 10⁶ m³ loose material by triggering landslides and subsequent weathering in Mayuanzi, Zhengjiashan, and Wujiaping (<u>Fig. 1)(Guo et al., 2018)</u>(Fig. 1)(Guo et al., 2018).

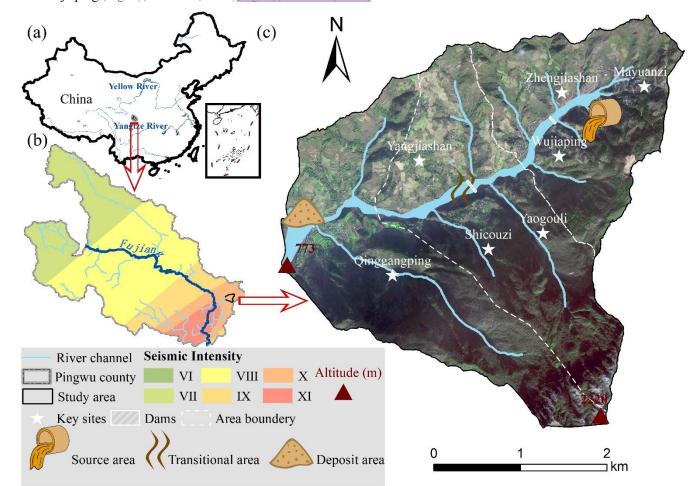


Figure 1: Overview<u>An overview</u> of the study area. (a) Location<u>The location</u> of <u>the</u> study area; (b) <u>SeismicA seismic</u> intensity map of
 the Wenchuan earthquake within <u>the</u> Pingwu <u>countyCounty</u>; (c) <u>TheA</u> schematic image of the study area.

101 **2.2 Historical hazards and intervention measures**

102 Six group debris flow-flash flood disaster chainschain groups have been found in the Xingping valley over athe decade after 103 the earthquake.- Based on the published work of SKLGP (State Key Laboratory of Geohazard Prevention and Geoenvironment 104 Protection) and the local states' geological survey before 2018 and our biannual field surveys since 2012, we catalogued the 105 time of occurrence, total rainfall of each event, and corresponding disaster details (Table S1). -The massive sediment was 106 transported quickly after the devastating quakeearthquake in 2008 and 2009, and the extreme rainfall in 2013 and 2018 trig-107 gered prosperous the deposition of extensive loose material deposited in the channel. Considering the landslide processes, we 108 divided the study area into three regions: the source area, the transitional area, and the deposit area (the. The white dashed 109 lines in Fig. 1c), which means Fig. 1c, indicate that the loose solid material would becan easily be transported from the source 110 area to the deposit one area through the transitional zone.

111 An engineering control project was constructed to intercept the upriver material in October 2010. The project included two

112 check dams, one in the upper source area and the other in the transitional zone (Feng et al., 2017) (Fig. 1c(Fig. 1c)). The upper

dam has a storage capacity of 5.78×10^4 m³ and a height of 10.0 m. The transitional area dam has a storage capacity of 7.2×10^4

114 m³ and a height of 9.0 m. With the reservoirs gradually filling with deposits, the first dredging work was subsequently done-

115 <u>performed</u> in 2013.- Nearly three years later, the storage capacity behind the upper dam remained at 50% in 2016, while the

116 transitional area dam <u>cancould</u> no longer retain sediment.

117 **3 Materials and Methods**

In this study, we examined the intervention effectiveness through the morphological response and sediment yield in the Xingping valley, which was simulated using the C-L model. The research entailed four main steps: 1) setting three scenarios with different intervention compositions, 2) preprocessing the model input data, including three groups of DEMs, the rainfall data, and <u>the m</u> value of the C-L, 3) calibration of the hydrological component, and 4) simulating landscape changes and analysing the intervention effectiveness in 2011-2013.

123 3.1 <u>Scenarios</u>Scenario settings

The abundant source material triggered by landslides should be controlled to prevent the threat of disasters downstream. Therefore, we designed three scenarios by incorporating engineering and biological measures referenced to current facilities to assess the effectiveness of intervention measures. Scenario UP: Unprotected landscapes meant the <u>sedimentsediment</u> would <u>transportbe transported</u> without anthropogenic intervention. Scenario PP: Present protected landscapes implied that only the present two check dams trapped <u>depositssediment</u> in 2011-2013 without dredging work over the period (see <u>sectionSection</u> 2.2). Scenario EP: Enhanced protected landscapes emphasised the <u>plusaddition of</u> vegetation revetments in the source area and levees in the deposit area based on the two check dams in Scenario PP.

- Fig. 1eFigure 1c shows the locations of the existing two check dams in both Scenario PP and Scenario EP. We determined the placements of additional facilities in Scenario EP according to the field survey, which demonstrated that the continuous supply of <u>sedimentssediment</u> was mainly from the source area. Therefore, the vegetation revetments <u>likesuch as</u> tree planting would be carried out in-upstream to prevent erosion by stabilising the topsoil and enhancing the soil's infiltration capacity with itsyia
- 135 roots (Lan et al., 2020).
- 136 Considering the damages damage caused by flash-flood floods to the residential area downstream, the levees (see Fig. S1 and
- 137 Section 3.2.2) are artificial barriers to protect agricultural land and buildings, which helpedhelp to prevent water and sediment

138 from overflowing and flooding surrounding areas. Table 1 shows the scenario descriptions, initial model conditions and input

139 rainfall series. The details about <u>the model input data are introduced below</u>.

| 140 | Table 1: Scenarios settingScenario settings | | | | |
|-----|---|---|-----------|-----------------------------------|----------------------------|
| | Scenario | Descriptions | Period | DEM (10m<u>10</u> m) | Rainfall data |
| | UP | no anthropogenic intervention | | UP DEM | downscaled hourly pre- |
| | | | | UP bedDEM | cipitation inover the pe- |
| | PP | the present two check dams upstream | 2011-2013 | PP DEM | riod |
| | | without dredging work | | PP bedDEM | (lumped) |
| | EP | additional vegetation revetments in the source area and levees in the deposit area based on Scenario PP | (3 years) | | downscaled hourly pre- |
| | | | 9 | EP DEM | cipitation in over the pe- |
| | | | l I | EP bedDEM | riod |
| | | | | | (spilt) |

141

142 3.2 CAESAR-Lisflood

143 The C-L integrated the Lisflood-FP 2D hydrodynamic flow model (Bates et al., 2010) with the CAESAR landscape evolution

model (LEM) (Coulthard et al., 2002; Van De Wiel et al., 2007), which is described in detail by Coulthard et al. (2013). The

catchment mode of C-L was applied in this study, withinin which the surface digital elevation model (DEM), the bedrock DEM,
 the grain size distribution, and a rainfall time series are required to simulate the sediment transport and geomorphic changes.

147 There are four primary modules within C-L operated as follows:

148 (1) a hydrological module generates surface runoff from rainfall input using an adaptionadaptation of TOPMODEL (Topogra-

149 phy-topography-based hydrological model) (Beven and Kirkby, 1979),

(2) a hydrodynamic flow routing module based on the Lisflood-FP method (Bates et al., 2010) <u>which</u> calculates the flow depths
 and velocities,

(3) an erosion and deposition module uses hydrodynamic results to drive fluvial erosion by either the Einstein (1950) or the

153 Wilcock et al. (2003) equationequations applied to each sediment fraction over nine different grain sizes,

154 (4) and a slope model moves of the movement of material from the hillslope to the fluvial system by considering both the mass

movement when a critical slope threshold is exceeded, and soil creep processes whereby sediment flux is linearly proportional to the surface slope.

The C-L model updates variable values stored in square grid cells at intervals, such as DEM, grain size and proportion data, water depth, and velocity. For the three scenarios, the initial conditions, such as DEMs and bedrock DEMs, the rainfall data,

and the m values_a were preprocessed as follows.

160 **3.2.1** Surface<u>The surface</u> and bedrock digital elevation model<u>models</u>

161 To clearly describe clearly the control process, especially the two dams and levees in the catchment, we unified grid cell scales to 10 m for all input data of the C-L. The GlobalDEM product with a 10 m × 10 m resolution and 5 m (absolute) vertical 162 163 accuracy waswere used to form three types of initial DEMs (UP DEM, PP DEM, and EP DEM). Before rebuilding the initial 164 DEMs, we filled the sinks of the original GlobalDEM based on the Environmental Systems Research Institute's (ESRI's) 165 ArcMap (ArcGIS, 10.8) to eliminate the 'walls' and the 'depressions' in the cells and thus avoided the intense erosion or depo-166 sition in the early run time. Then, the non-sinkssink DEM was used as the surface DEM in Scenario UP (UP DEM) without 167 any facilities. According to the engineering control project described in Section 3.2.2, the surface DEM of Scenario PP (PP 168 DEM) included the dams by raising the grid cell elevations by 10 m for the dam in the upper stream and 9 m for the dam in 169 the transitional area.-Similarly, the surface DEM in Scenario EP (EP DEM) included the dams in the PP DEM. In addition, two

- 170 levees were produced by raising <u>the grid eells'cell</u> elevation by 2 m-that were represented, representing at selected locations.
- For scenario EP, the placement and setting of <u>the vegetation revetments</u> in <u>Scenario EP wereare</u> introduced in Section 3.2.2.
- 172 The spatial heterogeneity of <u>the source material</u> (Fig. 1c) indicates the discrepancy of <u>in the</u> erodible thickness, which
- equals the difference between the surface DEM (DEM) and the bedrock DEM (bedDEM). We divided the study area into five
- regions according to the erodible thickness (Fig. S1) by checking out the relative elevation of the foundations of buildings, the exposed bedrock, and the <u>depositeddeposition</u> depth of landslides to <u>the</u> ground level. The average thicknesses of upstream
- 176 low_ and high-altitude areas were set to 10 m and 3 m, respectively, and the thickness of the erodible layer in the downstream
- area was set to 3 m. For the river channel and outlet, <u>as</u> there would be a large amount of deposition $\frac{1}{2}$, the thickness of erodible
- sediment was set to 5 m and 4 m, respectively. As the dams in Scenario PP and the levees in Scenario EP were non-erosive
- concrete, we set the erodible thickness of these features to 0 m. Eventually, <u>DEMsthe DEM data</u> were formatted to ASCII
- 180 raster <u>data</u> as required by C-L. The divided regions varied in erodible thickness, the placement of additional levees and vege-
- table revetments in Scenario EP, and the generation process of DEMs and bedDEMs wereare shown in Fig. S1.

182 **3.2.2 Vegetation settings**

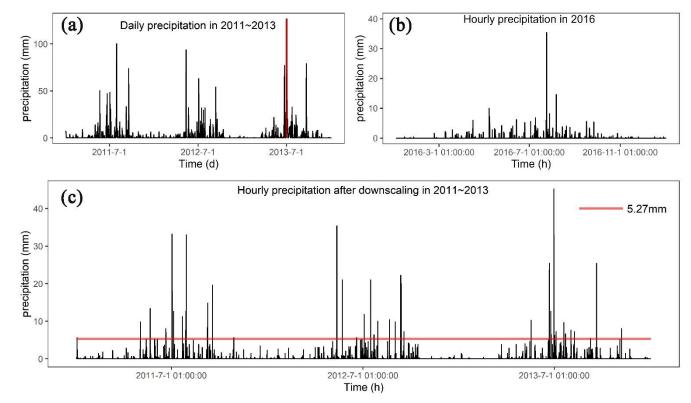
183 Another parameter required in each scenario simulation was the m value of the hydrological model (TOPMODEL) within C-184 L, which controls thean exponential decline of in transmissivity with depth (Beven, 1995, 1997) and influences the peak and 185 duration of the hydrograph in response to rainfall. The m value effectively imitates the effect of vegetation on the movement 186 and storage of water within the soil. The lower the m value is, the lower the vegetation coverage, and the flashier higher the 187 flash flood peak and the shorter the duration are reflected inof the flood hydrograph is reflected (Coulthard et al., 2002). The 188 m value is usually determined by the landcoverland cover (e.g., 0.02 for the forest, forests and 0.005 for the grasslands) (Coulthard and Wiel, Van De J., 2017). In our study, we set the m value as 0.008 in our smaller catchment (14 km²) in Scenar-189 190 ioScenarios UP and PP, which resembles the m value of farmland covered with lower vegetation coverage in the same catch-191 ment studied by-Xie et al. (2018) and Li et al. (2018). As mentioned earlier, the upstream-low elevation area covered by the 192 biological measures in the EP scenario was assigned a higher m value of 0.02. It has been This m value was calibrated inby the 193 more extensive catchment containing our study area by replicating in the flood event inof 2013 (Xie et al., 2018).

194 3.2.3 Rainfall The rainfall data

- 195 In this research, we compared three scenarios with identical by matching precipitation data between 2011 and 2013, as men-196 tioned in section Section 3.1. The source data of precipitation in 2011-2013 (Fig. 2a) was(Fig. 2a) were obtained from the China 197 Meteorological Administration (http://data.cma.cn)(http://data.cma.cn) with daily temporal resolution. The intensity and fre-198 quency of extreme rainfall events affect patterns of erosion and deposition (Coulthard et al., 2012b; Coulthard and Skinner, 199 2016). Therefore, we used the stochastic downscaling method to generate hourly data to better capture the hydrological events 200 introduced by Li et al. (2020) and Lee and Jeong (2014). The referenced hourly precipitation was observed from the pluviom-201 eter located 20 km from the study area in 2016 (Fig. 2b), with an annual total precipitation of 684 mm. The observed 202 rainfall in 2016 was characterised by: (1) hourly precipitation was from between 1.1 mm to and 35.4 mm, and (2) the maximum 203 and average durationdurations of a rainfall event wasevents as 24 h and 2.8 h, respectively. The main processes of the downscal-204 ing method are as follows:
- extracting the hourly rainfall of specific days in 2016 closest to the daily rainfall in 2011-2013 through the threshold
 setting and producing the genetic operators using the extracted hourly rainfall dataset;
- mixing on the genetic operators by <u>genetican</u> algorithm (Goldberg, 1989) composed of reproduction, crossover and mutation and repeating until the distance between the sum of hourly rainfall and the actual daily rainfall is was less than the set threshold;

• normalising the hourly precipitation to remainkeep the daily rainfall value unchanged.

Fig. 2eFigure 2c shows the downscaled rainfall series between 2011 and 2013. The downscaled hourly rainfall better captured the hydrological events at an hourly scale compared to the hourly-mean rain (5.27 mm) on the day with extreme rainfall (126.5 mm), which was far from the actual situation. Corresponding to the m value settings, the input of generated hourly precipitation iswas catchment lumped in Scenario UP and Scenario PP and divided into two separate but identical rainfall <u>events</u> in Scenario EP.



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Figure 2: (a) Daily precipitation in 2011-2013 (the red vertical line indicates <u>the maximum daily precipitation of 126.5 mm</u>); (b) Hourly precipitation in 2016; (c) Downscaled hourly precipitation in 2011-2013 (the red horizontal line indicates the hourly-mean precipitation <u>of 5.27 mm</u> on the day with <u>the maximum precipitation marked in (a)</u>).

220 **3.2.4 Other parameters**

221 The C-L model is sensitive to a set of input data introduced by Skinner et al. (2018) for a catchment with a grid cell size of 10 222 m, such as the sediment transport formula, slope failure threshold, and grain size set. -The grainsize grain size distribution of 223 sediment iswas derived from samplings at 14 representative locations in the same study basin by Xie et al. (2018). Given the 224 grainsize grain size distribution in this study, the Wilcock and Crowe formula was selected as the sediment transport rule, which 225 was developed from flume experiments using five different sand-gravel mixtures with grain sizes ranging between 0.5 and 64 226 mm (Wilcock et al., 2003). Considering the steep slopes on both sideseither side of deep gullies, a higher slope failure 227 threshold was determined to replicate the geomorphic changes between 2011 and 2013. Additionally, we found that the prob-228 ability of shallow landslides indeed accumulated increased from 20° to 50° in slope gradientgradients between 2011 and 2013 229 (Li et al., 2018). The slope angle was derivated erived from the DEM with a 30 m spatial resolution, which caused a lower 230 slope angle than that with a 10 m resolution. As such, we set the slope angle as 60°, which is lower than the 65° used in a 231 scenario without landslides (Xie et al., 2022) and higher than 50°. Some parameters were determined by repeated experiments. 232 such as the minimum Q value, and the other input values were referred to default values recommended by the developers (such 233 as the max erodemaximum erosion limit in the erosion/deposition module and the vegetation critical shear stress) in 234 https://sourceforge.net/p/caesar-lisflood/wiki/Home/. Table S2 in the supplemental material presented presents the model pa-235 rameters of C-L used in this study.

236 3.2.5 Model calibration

237 Considering the ungauged basins before 2015, we replicated the flash flood event in July 2018 using C-L simulations to cali-238 brate the hydrological components. Based on Scenario PP (with two checking dams), we input used the two-week hourly precipitation inof July 2018 as the input (Fig. S2a), which is was recorded by thea rain gauge located 2.5 km away from the 239 240 catchment (Fig. S2b). The simulation results (Fig. S2c and Fig. S2d) show the showed an erosion map and a maximum water 241 depth map in Scenario PP on July 15, 2018. We selected three locations to compare the deposition and inundation in the 242 simulation results, with satellite images and photos (Fig. S3). Additionally, the simulated sediment thickness and water depth 243 were close to those measured from pictures, which indicated that the flash flood event was well replicated by the C-L using 244 the input data.

245 **3.3 Output analysis**

246 The C-L model outputs in of each scenario include hourly water and sediment discharge at the basin outlet, and the difference 247 between DEMs at a specified time and initial DEMs (EleDiffs). We validated the model outputs by comparing the hourly 248 discharge and EleDiffs reflecting the depth of sediment deposition or erosion (> 0.1 m: deposition, < -0.1 m: erosion) with 249 field survey materials. The overall temporal and spatial geomorphic changes reflected by EleDiffs under three different sce-250 narios were used to assess the geomorphic response to interventions. To explore the geomorphic response to various control 251 measures, we focused on the key spots placed notable sites where the checking dams, levees, and vegetation revetments would 252 be located and recorded the depth of deposited accumulating sediment behind the two dams. To further explore the spatial 253 heterogeneity, we compared the volumes of deposition and erosion among three divided regions, including the source area, the 254 transitional area, and deposition the deposit area.

Based on the visual analysis and quantitative results, we defined two formulae to assess the effectiveness of <u>the</u> intervention. The conservation ability (*Ca*, Eq. (3)) was calculated based on variables in the sediment balance system (Fig. 3). (Fig. 3). The sediment volume of deposited sediment (D_n) and input sediment from the upper connected region (I_n) is equal to that of <u>the</u> eroded material (E_n) and <u>the</u> output sediment to the next part (O_n) over the same period (Eq. (1), Eq. (2)) in the system. A higher value of *Ca* in a specific region and scenario indicates <u>that</u> a more effective control system is <u>applied</u>.

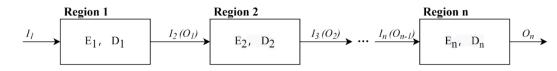


Figure 3: The sediment balance system in the study area (the Region *n* indicated indicates the source area, transitional area, and deposit area)

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$$I_n = \sum_{2}^{n} E_{n-1} - \sum_{2}^{n} D_{n-1},$$
(1)

$$I_n + E_n = O_n + D_n, (2)$$

$$Ca = \frac{D_n}{I_n + E_n} \tag{3}$$

265 Where, where *n* is the region number of the source area (=1), transitional area (=2), and deposit area (=3).

Additionally, we designed the relative efficiency (Re, Eq. (4)) to depict the efficiency of intervention measures in Scenario PP and EP in sediment loss, with the comparison to Scenario UP.

$$Re_{PP/EP,i} = \frac{Q_{UP,i} - Q_{PP/EP,i}}{Q_{UP,i}}$$

$$\tag{4}$$

Where where *i* is the sequence of the day; Q_{UP} is the daily sediment yield measured at the catchment outlet in Scenario UP₅. and $Q_{PP/EP}$ is the daily sediment yield measured at the catchment outletsame data in Scenario PP or Scenario EP of day *i*; and Re_{PP/EP} is the daily relative effectiveness of control measures in Scenario PP or Scenario EP.

4. Results

272 4.1 Model verification

Fig. 4<u>Figure 4</u> shows the input rainfall data and modelled discharge hydrograph between 2011 and 2013 (Fig. 4a(Fig. 4a)). The comparison of simulated mean discharge in April through July and the whole year with field survey materials in the two locations are also presented (Fig. 4b(Fig. 4b, c)). Concerning the discharge hydrograph, the peak discharges (63.7, 54.9, and 50.3 m³/s) correspond well with the peak rainfall intensities (31, 19.7 and 15 mm). The modelled water discharge from March to May in location A is slightly larger than the measured value reported by Feng et al. (2017). Additionally, an average annual discharge of 10.04 m³/s in location A is <u>lesslower</u> than that of 12.80 m³/s in the catchment outlet (location B), which has an area approximately three times the size of the study area.



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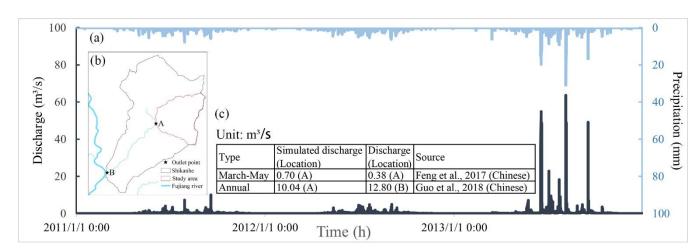


Figure 4: The input and output of the hydrograph. (a) The input hourly precipitation and simulated discharge in 2011-2013 in Scenario PP; (b) <u>LocationThe locations</u> of the specified outlet <u>pointpoints</u>; (c) <u>theA</u> comparison of the simulated average discharge to the recorded discharge.

Typical cross-sections are generated (Fig. 5)(Fig. 5) based on the replicated landscape changes in Scenario PP. The first site is located on the upriver road, which wasis eroded at a depth of 5.7 m according to the simulation results, while the photo shows a depth of no less than 4.0 m without an apparent eroded base. The cross-section #2 and the site photo of the gully depict that the eroded depth is approximately 1.0 m. Meanwhile, a clear sediment boundary is found in the building located at the deposited area (# 3), indicating a slightly lower deposition depth than the modelled one. model predicted.

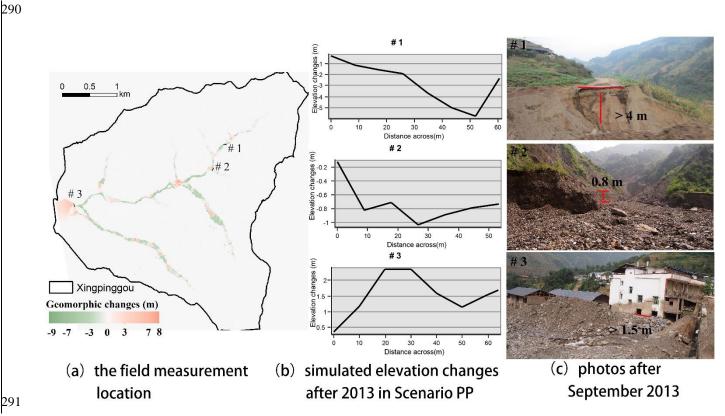


Figure 5: The comparison of cross-sections from the simulation results to the field measurements after 2013 in Scenario PP.

293 **4.2 Overall geomorphic changes**

Fig. 6aFigure 6a compares the three annual landscapes[andscape] changes in each scenario, which wereare classified into nine categories by natural breaks for EleDiffs: extreme erosion (<-7 m), heavy erosion (-7--3 m), moderate erosion (-3--1 m), light erosion (1-0.1 m), micro change (-0.1-0.1 m), light deposition (0.1-1 m), moderate deposition (1-3 m), heavy deposition (3-7 m), and extreme deposition (>7 m). A similar spatial pattern of erosion is observed in all three scenarios. More specifically, erosion mainly occurredemerges in the main channel and the branch valleys, among which the left branches wereare more severepronounced. In contrast, the deposition distribution appeared depositional zone appears to be varied vary in the three scenarios, especially in the area behind the two dams shown in <u>ScenarioScenarios</u> PP and EP.

The total area of affected grid cells representing erosion and deposition in each scenario wasfor three scenarios are calculated to revealcompare the difference (Fig. 6b).damages (Figure 6b). The affected area in Scenario UP was the largest at aboutis approximately 0.76 km² (5.4% of the total catchment), which wasis larger than that in Scenario PP (0.70 km², 5.0% of the whole catchment), and the affected area decreased decreases to 0.61 km² (4.4% of the total catchment) in Scenario EP. The total area of erosion and deposition reduced decreases gradually with more controlling measures established in this study.

Fig. 6cFigure 6c compares the extent of geomorphic changes in three situations using the areasranges that varied in depth. The erosion area of the light one and moderate erosion areas were more one is greater than the extreme and heavy oneserosion area for all three scenarios. The sizezone of each erosion degree in UP wasis more extensive than that in PP-and, followed by that in EP. In addition, the greater the deposition depth is, the lesssmaller the deposition coverage. Especiallycovers. In particular, the extreme deposition area was somewhat more greater than the area of the heavy deposition in the UP scenario. Further analysis shows that extreme, moderate, and light deposition areas decreased area decrease in the order of UP, PP, and EP. The

heavy deposition areas showarea shows the opposite trend, mainly attributed to the checking dams and vegetation revetments.

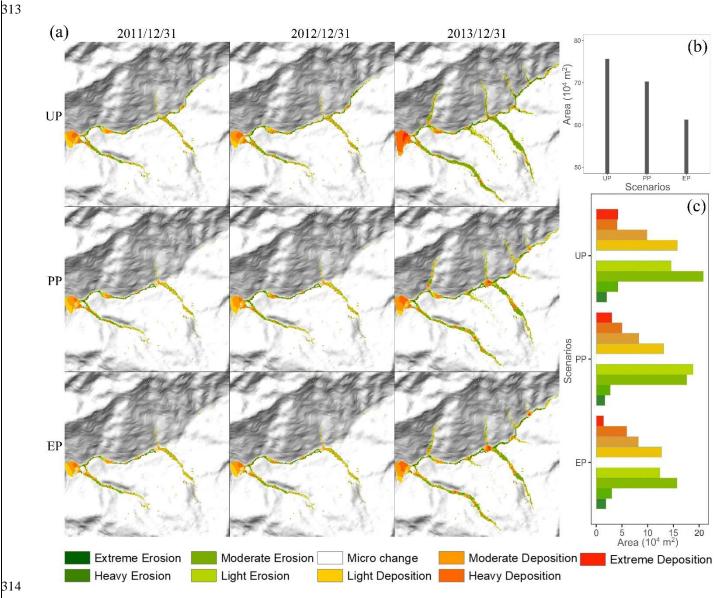


Figure 6: (a) Simulated geomorphic changes over time for <u>the</u> three scenarios; (b) <u>theThe</u> affected area of deposition and erosion for <u>the</u> three scenarios; (c) <u>The</u> columnar distribution of different erosion and deposition levels.

317 **4.3 Details of key spots** locations

318 As shown in Fig. 7, Fig. 7, the controlling measures and surroundings for the three scenarios wereare further investigated. 319 Behind the two dams upriver in Scenarios PP and EP, the evident orange clusters indicate that the deposition occurred in 320 Scenario PP and EP. In contrast, these locations were are dominated by erosion, shown in green in scenario UP. Further analysis 321 of the sediment depth shown in Figure 8 showedFig. 8 shows that the deposited depth behind the dams in Scenario EP wasis 322 lower than those that in Scenario PP. Additionally, in Scenario PP, sediment trapped by dam 1 wasis less than that by of dam 2, 323 but both have deposite the dams' heights (dam 1's height is 324 10 m, dam 2's height is 9 m). As for For the simulation results in Scenario EP, the values of -deposition depth behind the two 325 dams wereare nearly 8 m, which wereis lower than the dams' heights.

- The <u>The additional biological protection measure alters the</u> material produced from <u>the</u> upriver tributary gullies varied due to the additional biological protection measures in three scenarios. A sediment volume of 14.4×10^4 m³ sediments was is trans-
- ported from EP'sthe biological protection area in the EP scenario (solid lines in Fig. 7). A total of 27.1×10^4 m³ and
- 16.9×10^4 m³ of loose material wereare produced in the same region without biological protection in <u>ScenarioScenarios</u> UP

and PP, respectively. The vegetation revetment enhanced the enhances sediment conservation based on the role of dam 1. -Com-

pared with the deposition in UP and PP without levees in the downriver area (shown in the bottom row of <u>Fig. 7)</u>, Fig. 7), the

levees in EP <u>blockedblock</u> debris in the bend of the channel and <u>playedplay</u> an essential role in protecting the residents and

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333 cultivated land behind the levees.

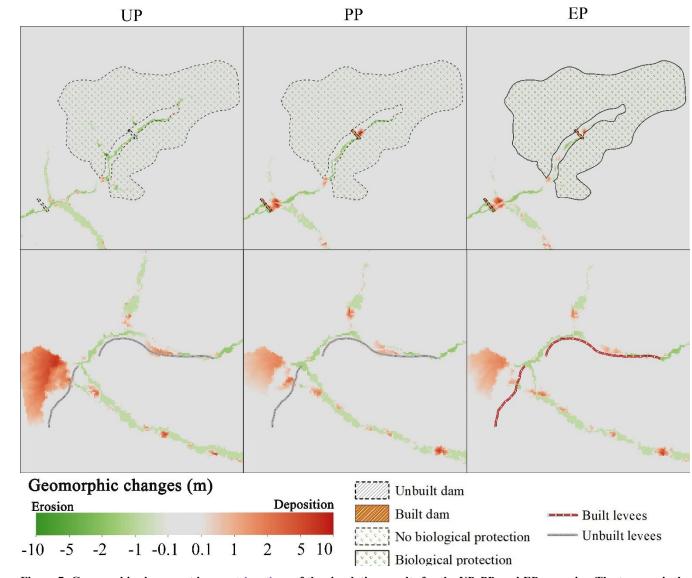
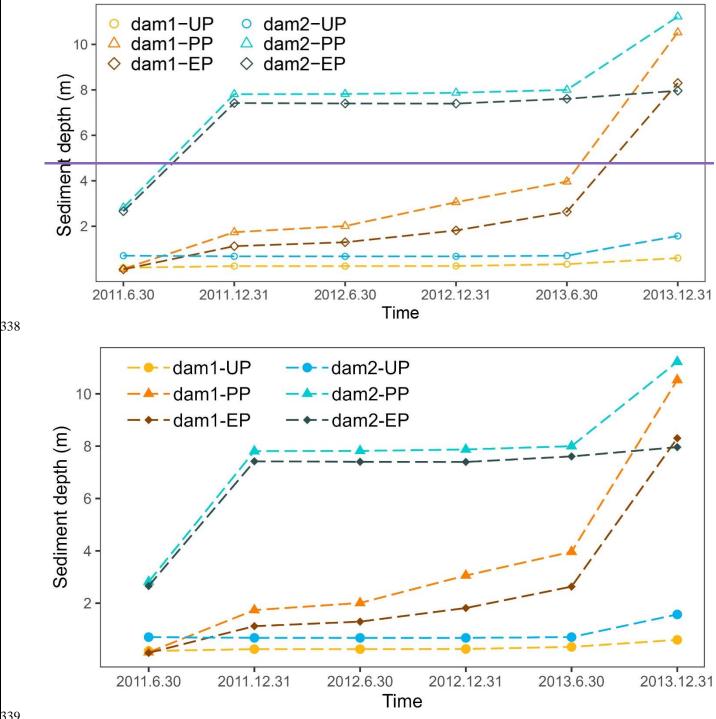


Figure 7: Geomorphic changes at key <u>spotslocations</u> of the simulation results for the UP, PP, and EP scenarios. The top row is the upriver extent containing dam 1, dam 2 and the vegetation revetment. The bottom row is the downriver extent containing levees.



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340 Figure 8: The depth of deposited sediment in the dams' placements.

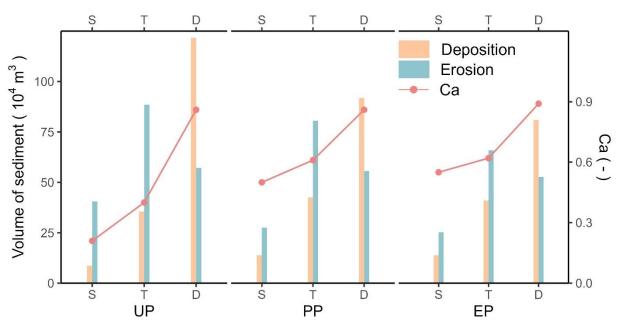
341 4.4 Effectiveness assessment of the intervention measures

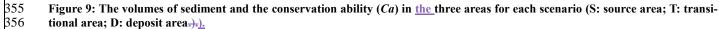
342 Fig. 9Figure 9 shows the erosion and deposition volumes in the source, transitional, and deposit areas and compares the con-343 servation ability (Ca) in each scenario. For all three scenarios, the deposition volume in the source area wasis less than that in 344 the transitional area, and the largest amount of sediment was deposited is accumulated in the deposit area. Regarding the eroded sediment, the largest volume wasis in the transitional area, followed by the transitional area, and the source area present-345 346 edpresents the least over, sediment transport wasis best controlled in the deposit area and worst contained 347 in the source area under any intervention conditions.

Compared with the *Ca* of the source area in Scenario UP, the value was increased increases by 138.1% in Scenario PP, which wasis attributed to the dam1. Likewise, dam 2 in the transitional area reduced effectively reduces sediment loss effectively, which wasis reflected by a 52.5% increase in *Ca*. Furthermore, the mitigation measures in Scenario PP with vegetation revetment and levees in Scenario EP worked better. act best. The conservation ability in the source area increased by 161.9% due to the dam retainment and vegetation revetment, and the levees helped increase the *Ca* by 3.49% in the deposit area.



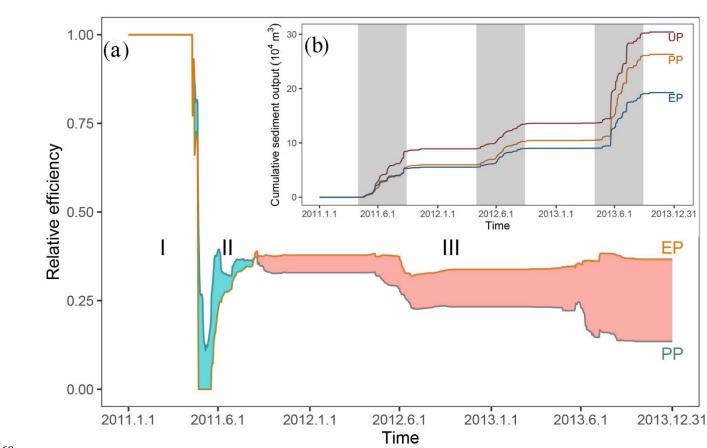
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The cumulative sediment yield time series for each scenario and the relative efficiency of <u>scenarioscenarios</u> UP and EP are presentpresented in Fig. 10bFig. 10b and Fig. 10aFig. 10a, respectively. The steep curve of <u>the</u> output cumulative sediment meansindicates a significant increase in the deposition. Three increasing stages are consistent with the rainfall intensity in <u>the</u> three monsoons (May-<u>SeptemberSept</u>). The total sediment output in UP <u>wasis</u> the largest of <u>at</u> \sim 30.4 \times 10⁴ m³; followed by <u>the</u> sediment yield <u>inof</u> PP (at 26.3 \times 10⁴ m³); and EP <u>presented produced</u> the least figure (material at 19.3 \times 10⁴ m³);.

The relative efficiency over the period of controlling measures by human intervention in PP and EP (Fig. 10b(Fig. 10a) indicates three distinct stages. Stage I shows that the intervention measures in both scenarios prevented the completely prevent sediment transport completely. Later stage II isshows a peculiar period when the effect of enhanced protective measures in EP was not as good aspales in comparison with that in PP through repeated experiments. For stage III, the relative efficiency of the intervention measures in EP wasis greater than that in UP for a more prolonged stage III, which could achieveachieves the long-term effect and stable conservation of solid material.



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Figure 10: (a) <u>cumulative sediment yield over time (grey region highlighting three monsoons), (b) relativeRelative</u> efficiency of <u>scenarioScenarios</u> UP and EP compared with the UP (cyan shading represents when PP is more effective than EP and red shading represents the opposite}); (b) Cumulative sediment yield over time (grey region highlighting three monsoons).

373 5. Discussion

374 **5.1 Model calibration and uncertainty**

375 The calibration Calibration and uncertainty are essential issues in the CAESAR-Lisflood (C-L) simulation of the geomorphic 376 response to intervention measures based on the CA framework (Yeh and Li, 2006). A preliminary calibration was carried out 377 by replicating reproducing the geomorphic changes and water depth driven by an extreme rainfall event that occurred in 2018. 378 The results (Fig. S3) demonstrated that the C-L model successfully replicated the flash flood event using the initial conditions 379 and model parameters. Actually, And the calibration of the replicating ability of the geomorphic response to the intervention 380 measures was derived from a direct comparison between the model results and direct measurements (Fig. 4 and Fig. 5). Fig. 5). As a result, the simulated water discharge was more than the measured one discharge but with the same order of 381 382 magnitude. Moreover, the errors of erosion and deposition depth between the simulation in Scenario PP and photographic 383 evidence inat three locations were at mostless than 20%. The results suggest the robustness of the model settings and parame-384 terisation.

The source of uncertainty is mainly from the model parameters and driving factors. Skinner et al. (2018b) provided a detailed sensitivity analysis of C-L, indicating that the sediment transport formula significantly influences a smaller catchment modelled by 10 m-_grid cells. The sediment transport law₅ and the Wilcock and Crowe equations (Wilcock et al., 2003) have been proven suitable in the Xingping valley (Xie et al., 2018, 2022a, b; Li et al., 2020). Nevertheless, the empirical models of sediment transport-would overpredict bedload transport rates in steep streams (gradients greater than 3%) (D'Agostino and Lenzi, 1999; Yager et al., 2012). Additionally, the driving factor, the input hourly rainfall data downscaled from the daily sequence, is an unrealistic situation. Various sediment transport equations and downscaled hourly rainfall data need to be tested in the C-L model to determine the further decrease uncertainty further.

5.2 Intervention <u>The intervention</u> effects

- 394 The-In this study, more facilities equivalent to create more comprehensive intervention systems in this study which aim to
- control sediment delivery. The C-L simulation of model simulated the geomorphic responseres to intervention measures
 suggests and suggested the considerable influence of intervention measures on spatial modification modifications and sediment
 yield. The relative systematic intervention measures lead to fewer total affected areas (7.9%-19.7%) and lower sediment yieldy-
- 398 <u>ields</u> (16.7%-%-36.7%), which are suggested in <u>the</u> overall evidence (see Fig. 6 and Fig. 10). SuchFig. 6 and Fig. 10). The model's prediction of the overall catchment-scale performance disturbed by the dynamics due to extreme eventevents is in line
- 400 with the viewpoints of other authors (Chen et al., 2023; Lan et al., 2020; Chen et al., 2015).
- 401 The mitigation measures considerably changed change the soil conservation ability in the three sub-regions, espe-402 cially in the source area. Herein, We hypothesise that the two main reasons whyfor the decreased erosion material is less-in the 403 source area than in another compared to the other two sub regions are subregions can be inferred from the interactions of loose 404 material and topographic constraints. First, the abundant loose solid material formed by the strong earthquake havehas stabi-405 lised overall since 2008's the 2008 debris flow (details in Table S1). Second, the long and deep gullies are mainly located in the 406 transitional area (Yaogouli, Shicouzi, Yangjiashan) and deposit area (Qinggangping), which provide more sediment supply 407 than the source area. As shown in Fig. S4, the movement of the material occurredoccurs mainly in the branch valleys in the 408 transitional and deposit areazones.
- Moreover, <u>comparingmorphological</u> details and <u>the</u> conservation ability <u>withof the</u> three scenarios <u>stressedshow</u> the unique role played by different intervention measures. For example, <u>the</u> check dams are most effective in blocking sediment, and <u>the</u> vegetation revetments strengthen the conservation ability. The <u>synergysynergetic</u> effect of <u>the</u> soil conservation ability of <u>checksincreases by more than two-fold due to the combination of the check</u> dams and <u>vegetablethe vegetation</u> coverage-is
- 413 ereated with an increase of more than two times. The levees are barriers with a discernable impact on sediment conservation
 414 but with a special specific object-oriented protection.
- 415 The effectiveness of mitigation measures detected will decrease decreases over time with a smaller downward trend. We sup-416 plementsupplemented a ten-year experiment to reveal the decreasingdeclining trend over a morean extended period. We ran-417 domly selected one of the 50 repeated rainfall datasets (year 2016-year 2025) downscaled by Li et al., 2020, which were 418 generated from the NEX-GDDP product (spatial resolution: 0.25°×0.25°, temporal resolution: daily) under the RCP 4.5 emis-419 sion scenario. The extracted rainfall sequence was then input to the C-L model to simulate the effectiveness of the three 420 intervention scenarios. The result (Fig. 11) (Fig. 11) illustrates that stage III (the stable stage that started on the 161st day, in 421 which Scenario EP's intervention measures were more effective) lasted longer than stages I and II, which were only at the start. 422 The relative effectiveness in both the PP and EP scenarios decreased gradually, while the curve fell faster in PP the PP scenario 423 (slope: -1.65×10^{-5}) than in the EP- scenario (slope: -1.31×10^{-5}).
- The storage capacity of <u>the checking dams fades as with</u> the accumulation of sediment <u>deposits accumulated</u>, which necessarily
- 425 leadleads to thea gradual decrease of in intervention effectiveness. Additionally, the vegetation revetments remain operationally
- effective in reducing sediment transport by stabilising topsoil over the period when the role of dam reservoirs gradually fails due to the lack of dredging work. Therefore, the vegetation protection strategy is vital for "green development" to reduce sediment loss but requires further efforts.

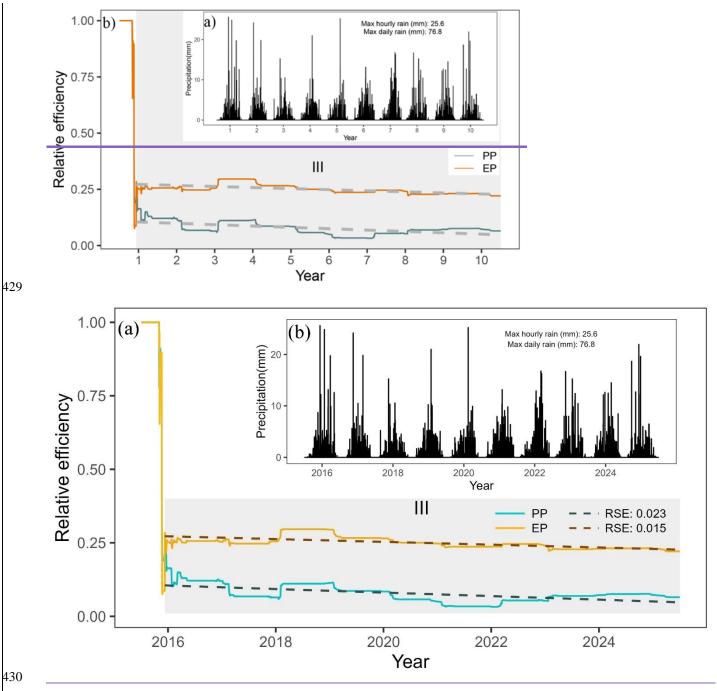


Figure 11: <u>Future rainfallRainfall</u> input <u>of ten years</u> and relative efficiency of sediment intervention measures. (a) rainfall downscaled from stochastic future rain; (b) the relative(a) Relative efficiency changes over ten years (<u>the grey</u> region highlighting stage III, and the <u>grey</u>-dashed lines <u>indicatingindicate</u> the linear fitting <u>eurve</u>).<u>curves</u>); (b) Rainfall downscaled from NEX-GDDP (NASA Earth Exchange Global Daily Downscaled Projections) product.

435 **5.23** Limitations and applications

436 We built the dams and levees in our simulations by increasing the elevation in the expected location and assuming that it could 437 not be eroded (see https://sourceforge.net/projects/caesar-lisflood/). This method proved experimentally feasible (Poeppl et al., 438 2019; Gioia and Schiattarella, 2020). The rigid dam and levee body embedded in the model wouldwere not be broken or 439 weakened over time so that the simulation result could underestimate the geo hazardgeohazard risk. Considering the complex-440 ity of the geo-hazard mechanism, the abovementioned tools could not cannot simulate the occurringoccurrence process of geo-441 hazard chain links. They would ignore the fierce attack on possible instantaneous damage to the environment and facilities downstream. Some typical geo-hazard geohazard chains were have focused on the specified event events in athe short time term 442 443 and recreated the hazard lifecycle using physical and mechanical models (Fan et al., 2020).

444 The methods applied in the study further demonstrate that the C-L model is an effective tool for understanding the short- to 445 medium-term or long-term geomorphologygeomorphological changes (Ramirez et al., 2022; Li et al., 2020; Coulthard et al., 446 2012a) and observing the effectiveness of natural hazard interventions intervention measures under different rainfall patterns. 447 Our simulations indicate that the mitigation facilities in this study wereare effective, especially engineering efforts ecooperating 448 withincorporating vegetation revetments in the upstream area, which would help decision-makers to optimise the management 449 strategies to control mountain disasters. Geotechnical engineering has disadvantages, even though it is a mature technology 450 that identifies and fixes problems quickly (Cui and Lin, 2013), such as the greater workneed for extensive labour and expense 451 and the difficulty of maintenance. While the "green development", the planting and maintenance of vegetation cover was 452 effective in preventingcan effectively prevent erosion by strengthening topsoil and absorbing excess rainwater with itsyia roots 453 (Reichenbach et al., 2014; Stokes et al., 2014; Forbes and Broadhead, 2013; Mickovski et al., 2007). Alternatively, thethese 454 methods couldcan be used to study the tree planting patterns on different slopes.

455 6. Conclusions

456 In this study, the scenarios intervented by involving check dams, biological measures and artificial barriers are were simulated 457 using the C-L model to outline the erosion and deposition area, measure the impacts of blocking sediment, and examine how 458 the vegetable vegetation revetments helped tohelp stabilise the slopes lopes. Four key findings are concluded. First, the engi-459 neering measures inused for controlling sediment transport are efficient, and the performance in protecting the fragile environ-460 ment would can be improved combining these engineering efforts with other intervention measures-like, such as 461 vegetation revetmentrevetments and artificial barriers. Second, the effectiveness of mitigation measures would de-462 ereased decreases over time. Third, the characteristics of the sediment transport patterns changed alter considerably caused of due 463 to the intervention measures. The stabilising sediment ability in the source area increased by 161.9% with the additional effect 464 of vegetation revetments. At last Finally, the present intervention measures are inadequateneed to be revised to reduce erosion 465 and should be combined with dredging work.

466 **Declaration of interest statement**

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

469 Author contribution

- 470 Di Wang: Conceptualisation, Methodology, Software, Writing-original draft preparation. Ming Wang Kai Liu and Jun Xie:
- 471 Supervision, Methodology, Writing- Reviewing and Editing, Validation.

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- 476

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