Stability evaluation and potential failure process of rock slopes characterized by non-persistent fractures

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Abstract. Slope failure, which causes destructive damage and fatalities, is extremely common in mountainous areas. Therefore, the stability and potential failure of slopes must be analyzed accurately. For most fractured rock slopes, the complexity and random distribution of structural fractures make the aforementioned analyses considerably challenging for engineers and geologists worldwide. This study aims to solve this problem by proposing a comprehensive approach that combines the discrete fracture network (DFN) modeling technique, synthetic rock mass (SRM) approach, and statistical analysis. Specifically, a real fractured rock slope in Laohuding Quarry in Jixian County is studied to show this comprehensive approach. DFN simulation is performed to generate non-persistent fractures in the cross section of the slope. Subsequently, SRM approach is applied to simulate the slope model using 2D particle flow code software (PFC2D). A stability analysis is carried out based on the improved gravity increase method, emphasizing the effect of stress concentration throughout the formation of the critical slip surface. The collapse, rotation, and fragmentation of blocks and the accumulation distances are evaluated in the potential failure process of the rock slope. 100 slope models generated with different DFN models are used to repeat the aforementioned analyses as the result of a high degree of variability in DFN simulation. The critical slip surface, factor of safety, and accumulation distance are selected by statistical analysis for safety assurance in slope analysis and support.

Keywords. Fractured rock slope, Synthetic rock mass, Statistical analysis, Stability evaluation, Potential failure

1 Introduction

Rockslides are common geological hazards in mountainous areas. This phenomenon seriously threatens human lives and properties worldwide every year. Therefore, the analyses of rock slopes, especially their stability and failure process, are necessary for civil and mining engineering. Generally, rockslides are controlled by discontinuities (such as beddings, faults,

and structural fractures). Discontinuities in rock slopes were formerly assumed in slope analysis as through-going and fully persistent planes. However, many researchers have suggested that discontinuities are generally not fully persistent (Eberhardt et al., 2004; Scavia, 1995; Terzaghi, 1962) and that failure surface is a combination of preexisting non-persistent discontinuities and newly propagated cracks (Brideau et al., 2009; Einstein et al., 1983; Frayssines and Hantz, 2006; Lajtai, 35 1969; Zhang et al., 2017). Non-persistent fractures are highly complex and come in various sizes and properties, and their locations and characteristics are difficult to determine. Thus, the influence of non-persistent fractures on slope analysis poses a great challenge (Fan et al., 2015; Wasantha et al., 2014).

Several researchers showed that non-persistent fractures play vital roles in the stability and failure process of fractured rock slopes (Gao et al., 2017; Huang et al., 2015; Jiang et al., 2015; Li et al., 2009; Zhang et al., 2015; Zhou et al., 2017). 40 However, these non-persistent fractures were artificially specified by researchers as having the same sizes and orderly arranged locations. The complexity and random distribution of non-persistent fractures in rock slopes should be considered in reflecting and modeling the stability and failure process of real rock slopes in nature.

According to a major research work on fractured rock masses, the discrete fracture network (DFN) modeling technique maximizes the use of discontinuity data from exposed surfaces and can become the best option for simulating realistic 45 fractured rock masses (Bonilla-Sierra et al., 2015; Chen, 2001; Elmo et al., 2013; Pine et al., 2006). By coupling the DFN technique with continuum, discontinuum, and hybrid modeling approaches, synthetic rock mass (SRM) models can be set up to investigate the mechanical properties of fractured rock masses (Elmo and Stead, 2009; Mas Ivars, 2010; Pierce et al., 2007). SRM approach has been widely used to determine the representative elementary volume size of a fractured rock mass (Esmaieli et al., 2010), reproduce rock mass properties and behaviours (Mas Ivars et al., 2011), and simulate fracture 50 propagation in a fractured rock mass (Zhang and Stead, 2014). SRM models have been primarily used to simulate failure and deformation of fractured rock slopes (Bonilla-Sierra, 2015; Elmo and Stead, 2013). DFN simulation included in SRM modeling program exists a high degree of variability. The variability of DFN simulation means there are an infinite number of possible realizations of 2D fracture systems exist given specified input parameters (Pine et al., 2006). The results of SRM model analyses that incorporate different DFN models may vary significantly (Elmo et al., 2018; Zhang et al., 2012). 55 Therefore, rock slope analyses based on only one DFN model can lead to erroneous results (Elmouttie and Poropat, 2014; Mas Ivars, 2006). A statistical analysis based on a large number of DFN models may reduce the aforementioned errors and provide reasonable results for rock slope analysis and support (Ferrero et al., 2016; Zhang et al., 2013; Zhang et al., 2017).

The current study proposes a comprehensive approach that combines several well-established methods to conduct a stability evaluation and failure process analysis of a fractured rock slope in Tianjin City. First, 100 DFN models are 60 generated on the basis of the fractures collected in the field. Second, slope models are constructed using SRM approach. Third, the improved gravity increase method is employed to determine the stability of a single-slope model. Fourth, the potential failure processes of the fractured rock slope models are simulated. Fifth, the final critical slip surface, factor of safety, and accumulation distance are determined on the basis of the statistical analysis of 100 slope models generated with different DFN models.

2 Study area and data acquisition

2.1 Study area

A rock slope in Laohuding Quarry, which is located north of Jixian County, Tianjin, is analyzed in this study (Fig. 1). The quarry was originally used for mining stromatolites, and this activity seriously damaged vegetation. After the mining area was closed, many steep slopes with internally developed discontinuities were formed. These slopes may become hidden dangers (e.g., geological disasters) and pose potential threats to people and nearby equipment.

The Laohuding Quarry area is higher in the north than in the south, with a monoclinal mountain situated in the south–north direction. The average slopes of the eastern and western sides are 25° and 30°, respectively. The highest altitude is over 160 m, whereas the lowest is 60 m, with a relative elevation of approximately 100 m (Fig. 1b).

This region has a continental climate with an average annual precipitation of 770.20 mm. The flood season is from June to August, and it accounts for 77.3 % of the annual precipitation. During this period, slope failures are frequently triggered. The average annual evaporation is 1867.30 mm, which is 2.42 times the amount of precipitation. These conditions indicate that the region is arid.

The lithology in this area is characterized by limestone of the middle-upper Proterozoic erathem, which exhibits a powder crystal–mud crystal structure. The limestone is moderately thick, and the karst phenomena in the mining area are not obvious. Faults and weak interlayers are not observed, and thus, this area is tectonically stable. Discontinuities in outcrops are not persistent but intermittent (Fig. 1c). Therefore, slope stability and potential failure process are controlled by non-persistent discontinuities (fractures).

2.2 Data acquisition and DFN generation

The investigated rock slope is 20 m high and is oriented at a trend of 200° with an approximately vertical angle (Fig. 1c). Fracture characteristics, such as orientation, trace length, spacing, roughness, aperture, filling, and termination, in the exposed surface were systematically surveyed using a rectangular sampling window measured 62 m long and 6m high (Kulatilake and Wu, 1984). Exactly 169 fractures were collected, and the 2D trace map is shown in Fig. 2. The mechanical properties of the different rock mass structures vary, and thus, an evaluation of the homogeneity of the fractured rock mass was conducted (Zhang et al., 2011). The result shows that this region can be considered as a statistically homogeneous area. As shown in Figure 3, the fractures can be divided into three sets (Chen et al., 2005). Fractures in set 1 with an average orientation of 39.5°/87.3° (dip direction/dip angle) are rare. Fractures in sets 2 and 3 with an average orientation of 307.4°/44.7° and 110.2°/31.7°, respectively, host the most fractures and constitute the dominant sets (Table 1). The Fisher constants (K) ranging from 9.1 to 17.1 imply the high dispersion of fracture orientations (Fisher, 1953; Priest, 1993).

The sampling window method is characterized by the following: (a) only one end of a fracture is measured, (b) both ends of a fracture are measured, and (c) no end of a fracture is measured. Therefore, the measured trace lengths were biased.

The mean value and probability density function (PDF) of the corrected trace lengths for each fracture set can be determined according to the methods proposed by Kulatilake and Wu (1984) (Table 1).

A 2D analysis was performed in this study. The cross section normal to the exposed surface was used to perform the 2D stability analysis and potential failure process of the rock slope. A fracture plane intersected by the cross section with a small angle acted as the surface of separation, which will not influence the results of stability analysis. Therefore, the fractures intersected by the cross section with an angle smaller than 20 ° were artificially deleted prior to the stability analysis. We derived the characteristics of the fractures (location, orientation, trace length, and density) in the cross section from those features measured from the exposed surface. Subsequently, the 2D fracture traces were generated using Monte Carlo simulation by synthesizing the aforementioned characteristics. The specific processes are clearly described in the research of Zhang et al. (2017) and are briefly introduced as follows. The locations of the fractures were assumed to follow Poisson's distribution. P_{21} (the 2D fracture density) in the cross section was proved to be $\tan\eta_i$ times that of the exposed surface (where η_i is the acute angle between the mean normal vector direction of fracture set i and the NS direction). The 2D orientation of a fracture is reflected by its trace gradient k, which can be expressed as $\sin\alpha/\cot\beta$ (where α and β are the dip direction and dip angle of a 3D fracture, respectively). Empirical distribution was followed to generate the 3D fracture orientations based on the fracture orientation frequency, and then k in the cross section can be determined. The results of Zhang et al. (2017) revealed that the mean [$E(ch^2)$] and variance [$V(ch^2)$] values of the trace length square are constant. $E(ch^2)$ and $V(ch^2)$ of the collected fracture traces in the cross section can be determined according to those features on the exposed surface. The rooted numbers result in the trace lengths in the cross section. The cross section of the investigated rock slope was 20 m high, and the smallest mean dip angle of the three fracture sets was 31.7 °. Thus, the length of the cross section was 30 m [20 × cot (31.7 °)]. Finally, we used Monte Carlo simulation to merge the aforementioned parameters to generate the 2D DFN model in a 30 m × 20 m cross section.

More than one DFN model can be generated with the same fracture data. For example, Fig. 4 exhibits four DFN models with different fracture characteristics. Therefore, the rock slope analyses based on only one DFN model can lead to wrong results (Mas Ivars, 2006; Xu et al., 2014). To solve this problem, we generated and verified the validity of numerous DFN models by applying the following method. Initially, we intersected the fractures in the exposed surface with lines extending along the dip direction. Doing so produced a series of intersection points for an individual line. Subsequently, we intersected the DFN models using the exposed surface and consequently generated a series of intersection points for an individual network. We compared these two sets of intersection points by using their probability density curves. The DFN models generated in the cross section proved reasonable when the results were identical to one another. Finally, we selected 100 reasonable DFN models to construct different slope models and conduct stability analysis and potential failure process simulation.

3 SRM model for rock slope analysis

SRM approach is used to construct fractured rock slope models. In the present study, the SRM model used was a combination of two well-established models, namely, the bonded-particle model (BPM) in PFC2D and the DFN model
130 (details are available in the research of Pierce et al. (2007). SRM approach is widely used to simulate the mechanical properties of fractured rock masses, perform rock masses stability analysis, and simulate the failure and deformation of fractured rock slopes.

3.1 Parameter determination for SRM model

The SRM model in PFC2D is defined by many parameters that cannot be directly identified via laboratory and field
135 experiments. Therefore, the parameters of the model should be predetermined according to the macroscopic characteristics of rock slopes. In particular, several numerical tests should be performed to ascertain and quantify the input parameters of the BPM and DFN model. In PFC2D, a material is considered an assemblage of bonded rigid circular particles, and particle size distribution dramatically influences modeling behaviour (Mas Ivars et al., 2011). Therefore, determining the particle size of a numerical specimen remains a challenge. Generally, the ratio between the maximum and minimum radii of particles is 1.66
140 (Potyondy and Cundall, 2004). A small particle size is indicative of accurate simulation results. However, the number of particles of rock models increases with a decrease in particle size. A large amount of particles will result in a long calculation time and low computational efficiency. In the present study, particles with radii between 0.05 and 0.083 m were finally selected to fill rock models after repeatedly changing the particle size. In that case, the size of particles is small enough for the comparatively reasonable results and the calculation time is acceptable.

145   The BPM parameters are calibrated against laboratory uniaxial and biaxial compression tests. The specimens (the height-to-diameter ratio is 2:1) for the numerical uniaxial and biaxial compression tests are set up to reproduce the macro-properties of real rock materials, such as uniaxial compressive strength (σ_c), elastic modulus (E), Poisson's ratio, friction angle, and cohesion obtained in laboratory tests. Different macro-properties are influenced by different parameters. Specifically, E is mainly controlled by several parameters, including particle contact modulus (E_c), particle normal/shear
150 stiffness ratio (k_n/k_s), parallel bond modulus (E_b), and parallel bond normal/shear stiffness ratio (k_{nb}/k_{sb}); Poisson's ratio is influenced by k_n/k_s and k_{nb}/k_{sb}; σ_c is influenced by normal strength, internal friction angle and cohesion of parallel bonds; and cohesion and friction angles are influenced by the friction coefficient (Bahaaddini et al., 2013). The values of the aforementioned parameters are empirically assigned in advance, and then the numerical uniaxial and biaxial compression tests are carried out. When the macro-properties of the numerical tests correspond to the results from the laboratory tests, the
155 parameters are considered reasonable. Otherwise, the parameters are adjusted until the rock specimens have the same macro-properties as real rock materials (Park and Song, 2009; Yang et al., 2006). The calibrated parameters of particles and bonds are listed in Table 2. The macro-properties of the rock specimens for the numerical tests and those of the real rock materials for the laboratory tests are listed in Table 3.

In PFC2D, a smooth joint (SJ) model is commonly adopted to generate fractures. In this model, two particles that lie on the opposite sides of the intended fracture plane can overlap and pass through each other instead of moving along their perimeters, thereby reproducing the real physical and mechanical properties of fractures (Bahaaddini et al., 2013). The SJ parameters are normal stiffness ($\bar{k}_{nj}$), shear stiffness ($\bar{k}_{sj}$), and coefficient of friction (μ_j). To determine these parameters, we built a numerical specimen (with a width-to-height ratio of 1:1) for the direct shear tests and normal deformability tests to simulate macro-properties, including shear stiffness, normal stiffness, and friction angle. The SJ parameters can be obtained as long as the test results approximate those of the laboratory tests. Specifically, $\bar{k}_{nj}$ was obtained by the numerical normal deformability tests; $\bar{k}_{sj}$ and μ_j were determined by the numerical direct shear test. Table 4 lists the values of the SJ parameters and the results of the normal deformability and direct shear tests of the numerical and laboratory tests. The specific calibration procedures are complex and are thus not introduced in this paper in detail. Additional details about the calibration can be found in the works of Bahaaddini et al. (2013), Cheung et al. (2013), and Duan et al. (2016).

3.2 Model generation

The investigated rock slope with a relatively low height is located on a ground surface with a relatively flat terrain. The study area is dry, crustal movement is not obvious, and no active fault exists nearby (Sect. 2.1). Thus, the effects of ground stress, water, and earthquake on the slope analysis were not considered in the current work.

The size of the slope section is 20 m (height) × 30 m (length). The bottom and right sides of the slope section were expanded by 10 m as the boundary section (Fan et al., 2004). Ultimately, the size of the SRM model was determined to be 30 m (height) × 40 m (length) (Fig. 5). The upper boundary of the model was free. Moreover, the left, right, and bottom boundaries were assumed to be smooth rigid walls.

The particles with the same radii (0.05 to 0.083 m) as those reported in Sect. 3.1 were applied to fill the 20 m × 30 m slope section. Considering the small effect of boundary section on the slope analysis, we filled the boundary section with particles with larger radii (0.1 to 0.15 m) to improve computational efficiency (Fig. 5). A total of 48,947 particles were generated, and the parameters presented in Table 2 were adopted for the bonds and rock particles.

Gravity was applied to the model, and the model was calculated (cycled) until the particle assemblage reached an equilibrium state (i.e., the unbalanced forces reached the required standard of 10^{-6}). Then, the generated DFN model reported in Sect. 2.2 was added to the slope section by defining the FISH functions, thereby forming the SRM model (Fig. 5, with the DFN model in Fig. 4a as an example). The SJ parameters presented in Table 4 were adopted for the fractures. This process ignored the stress concentration at the tips of the structural fractures generated by tectonic stress. Nevertheless, the process was considered reasonable in this study because the stress concentration was intensely reduced after the long-term stability of the rock slope.

The slope was formed within one operation. Therefore, the left boundary (smooth rigid wall) was removed to simulate a one-time excavation of the slope.

4 Stability analysis

4.1 Determining the factor of safety

To trigger instability, an improved gravity increase method is used in this study. The improved gravity increase method was proposed by Meng et al. (2015). This method leads to the failure of a slope in PFC2D by slowly increasing gravity
195 acceleration and reducing the friction coefficient of particles while keeping other parameters constant. The amplitude of reduction of the friction coefficient is the same as that of the increase in gravity acceleration to ensure an approximate invariance of the resisting force. When the slope model is in a limit equilibrium state, i.e., fractures in the slope are propagated and coalesced until a through-going slip surface (i.e., the critical slip surface) is initially formed, the factor of safety F can be defined as the ratio of the gravity acceleration in the limit equilibrium state (g') to that in the initial state (g),
200 i.e., $F= g' / g$. Taking the model in Fig. 5 as an example, we calculate the factor of safety by using the calculation procedure shown in Fig. 6. The simulation results indicate that the factor of safety of the slope model using the improved gravity increase method is 25. Additional details on the factor of safety can be found in Sect. 7 of this paper.

4.2 Initiation and propagation of fractures

When the factor of safety is determined, the critical slip surface is simultaneously obtained. To get an in-depth understanding
205 of the fracture propagation mechanism, the propagation process of fractures and the evolution of force chains during the formation of the critical slip surface are recorded (Fig. 7). The force magnitude is proportional to the thickness of the line in the force chain plots (lower right corner of Fig. 7), in which the blue and green lines denote compressive and tensile forces, respectively. The color of the line segments is obvious in the region where the stress concentration is strong.

Non-homogeneous stresses are distributed throughout the slope owing to the heterogeneity of the slope model. After
210 2,000 time steps, the compressive stress, which slowly increases from top to bottom under the action of gravity, is initially distributed throughout the slope. The tensile stress exists only in the tips of the fractures (Fig. 7a). Then, the degree of tensile stress concentration increases at the fracture endpoints (Fig. 7b). The fractures (black lines surrounded by a pink circle in Fig. 7) propagate from the tips of the original fractures (red lines) where the tensile stress is concentrated (Figs. 7a and 7b). After the initiation of fracture propagation, the tensile stress (green markings) at the tips of the original fractures dissipates (lighter
215 green markings). A new tensile stress concentration is found at the tips of the propagated fractures, as shown in the force chain plots in Figs. 7b and 7c. The propagated fractures continuously expand downward to the tips of the neighboring fractures (or rock surface) accompanied by the concentration and release of tensile stress. The orientation of the yellow arrows in Fig. 7 corresponds to the fracture propagation direction. Finally, a decrease in forces, especially the compressive forces (lighter color) throughout the slope, is observed; furthermore, a through-going surface, i.e., the critical slip surface, is
220 formed when the propagated fractures arrive one after another to the tip of the original fractures (Fig. 7d).

5 Potential failure and accumulation process

According to the aforementioned results of stability analysis, the factor of safety is extremely high such that the investigated rock slope is highly stable. Nonetheless, the potential failure and the accumulation process are simulated in the present study to obtain good knowledge of the failure mechanism of fractured rock slopes and provide references for similar slope projects.
225   To maintain coherence of analysis, we use the model in Fig. 5 as an example. Section 4 presents an analysis of the formation process of the critical slip surface of the gravity-increased model. Subsequently, another round of analysis is performed to determine the failure process after forming the critical slip surface.

Figure 8 presents the displacement field images of the slope model in different time steps. In the displacement field plots, particles are colored according to their relative displacement magnitude. Figure 8a, which corresponds to Fig. 7d,
230   represents the displacement field of particles when the critical slip surface is initially formed. The displacement field image indicates the occurrence of a small deformation in the slip mass above the critical slip surface; the bedrock remains stable without a distinguished gap with the slip mass. The displacements of the slip mass continuously increase, and the largest displacement of the particles (red particles in Fig. 8b) is nearly 0.2 m, which indicates the aggravation of rock failure (Fig. 8b). After 60000 time steps, the slip mass is slowly fractured into many rock blocks along the non-persistent fractures (Fig.
235   8c). The displacement and size of these blocks vary from one another. The block fragmentation is apparent near the critical slip surface because of the newly propagated fractures, whereas most of the rock blocks far from the critical slip surface remain intact (Fig. 8d). Ultimately, the slip mass is completely separated from the bedrock (Fig. 8d).

As soon as the slip mass is detached from the bedrock, a large displacement and movement of blocks occurs. To reflect the actual failure and accumulation process of rock slopes in nature, the PFC2D procedure should be manually interrupted to
240   make corresponding adjustments (when the time steps are 80,000, which correspond to Fig. 8d). First, the particles in the bedrock are deleted to improve computational efficiency, and the critical slip surface is replaced with a rough rigid wall. The frictional properties of the rigid wall are the same as those of the propagated fractures. Then, the DFN model is removed, and the body force in the model is initialized to avoid splitting caused by the release of stress. Finally, the gravity acceleration is restored to 10.0, which corresponds to natural conditions. Figure 9 presents the computed results. In the figure, the blue
245   sections denote the assemblage of rock particles from a macroscopic level while the red lines represent the bonds (contacts) between particles. For a convenient description, we numbered several rock blocks from 1 to 6.

In Fig. 9a (5×10^4 time steps), except for block 2, the blocks rotate under inertia force and gravity and are separated from one another. The blocks near the slip surface are disintegrated into numerous sub-blocks, and even crushed particles. Rock blocks 1, 3, 4, and 5 rotate counterclockwise by approximately 60 °, 30 °, 260 °, and 40 °, respectively; whereas block 6 rotates
250   clockwise by 75 °(Fig. 9b) when the time steps are 2×10^5. Block 6 initially crashes to the ground, and the collision results in the bond breakage between particle blocks (red segment in Fig. 9c). Block 6 is divided into two sub-blocks and some crushed particles. Blocks 4, 5, and 2 successively crash to the ground one after another but their shapes are kept intact, whereas block 3 is split owing to the collision with block 6, as shown in Figs. 9c and 9d. As soon as all crushed particles and

blocks fall to the ground or the critical slip surface, the blocks and particles slide or roll forward as a whole and are
255   accompanied by a fragmentation of the block edges (Fig. 9e). Figure 9f presents the final shape of the rock model. The final
deposit is composed of relatively intact rock blocks and crushed particles, and the blocks pile up above the crushed particles,
presenting an inverse grading phenomenon. We also record the final accumulation distance, which is represented by the
farthest reach distance of intact blocks (bonds exist in particles in these blocks). The final accumulation distance of the rock
slope model shown in Fig. 5 is 28 m.

260   **6 Stability analysis**

The slope analysis in Sects. 4 and 5 are based on a SRM model with one DFN model. However, as mentioned in Sect. 2,
numerous DFN models can be generated because of the variability of DFN simulation, and the stability analysis of only one
SRM model may lead to erroneous results. In the present study, 100 SRM models on the basis of the different DFN models
(generated in Sect. 2), are built to conduct the aforementioned analysis. In particular, the critical slip surfaces and safety
265   factors of these models are calculated using the improved gravity increase method following the calculation procedures in
Figure 6. Then, the method mentioned in Sect. 5 is employed to simulate the potential failure and accumulation process.

The factors of safety and the critical slip surfaces of the 100 slope models based on 100 different DFN models
significantly vary. For example, Figure 10 exhibits the critical slip surfaces of the SRM models based on DFN models shown
in Fig. 4. According to the results, the locations and shapes of the four critical slip surfaces significantly vary, although they
270   all extend along the non-persistent fractures. The factors of safety of these models are 25, 28, 40.5, and 33.5.

Figure 11 illustrates the critical slip surfaces of the 100 SRM models on the basis of 100 different DFN models. Figs.
12a and 12b present the factors of safety of the 100 models, ranging from 25 to 73.5. Therefore, the variability of the
simulation results should be emphasized in the stability evaluation of fractured rock slopes. The outcome that considers
numerous model calculations may lead to a rational result. In the present study, a statistical analysis method is applied to
275   solve this problem. The final critical slip surface and factor of safety are attributed to conservative considerations. The
potential critical slip surface constitutes a large slip mass (Fig. 11). The final critical slip surface covers over 90 % of the slip
mass to guarantee safety in the rockslide analysis and support. Additional information on the critical slip surface can be
found in the research of Zhang et al. (2017). Critical slip surfaces are supposed to have an arc-shaped geometry that differs
from their actual linear or broken line morphologies. Arc morphology is easily defined and is convenient for practical
280   engineering designs. F_s is the final factor of safety of the rock slope when the F values of the other 90 models are greater
than F_s The result shows that the final factor of safety of the rock slope are 43.5.

Similarly, the results of the potential failure and accumulation process vary. Figure 13 presents the final accumulation
states of the models shown in Fig. 10. The plots indicate that the sizes and quantities of the fractured blocks, as well as the
rotating degrees, are significantly different. The final accumulation distances of the models are 28, 34, 35, and 40 m.

285   Finally, the different accumulation distances, with the minimum value of 15 m and the maximum value of 96 m, of the 100 SRM models based on 100 different DFN models are obtained (Fig. 12c). The potential failure and accumulation process based on one SRM model may obtain erroneous results. A statistical analysis method is also applied to solve this problem. To guarantee safety in the rock slope analysis, we attribute the final accumulation distance to conservative considerations. In particular, when the distance values of the other 90 models are lower than a certain value, then the value is

290   the final accumulation distance (D_a) of the rockslide. Therefore, the final accumulation distance is 87 m.

7 Discussion

Slope failure is a 3D stability problem. Thus, constructing a 3D SRM model for stability evaluation and failure process analysis is highly convincing and accurate. A 3D SRM model also combines rock masses in the BPM with DFN model. However, the quantity of rock particles in a 3D slope is extremely large to conduct an effective calculation in PFC. In

295   addition, the factor of safety obtained by 3D analysis is generally higher than that in 2D analysis. Given that many theories and technologies cannot be established and that their adoption cannot perfectly reflect rock masses at present, the accuracy of analyses may not satisfy engineering project requirements. Moreover, deriving a high factor of safety is sometimes unfavourable. Accordingly, 2D analysis, which is simple and commonly used in reality, is adopted in the present study for the stability evaluation and potential failure analysis of the investigated slope. The 2D analytical result can be regarded a

300   good reference, and it provides a theoretical and practical basis for future initiatives that utilize 3D analysis.

The factor of safety of the investigated slope is extremely high. In the field investigation, unlike that for various non-persistent fractures, weak interlayer and through-going discontinuities are not observed; thus, the non-persistent fractures play a vitally important role in the stability of the investigated slope. The strength of the rock bridges (intact rock) is considerably higher than that of the fractures. Therefore, the obtained factor of safety is extremely high and is thus

305   reasonable. In addition, the effects of water (rainfall) and earthquakes were ignored in the present study. However, the accuracy of the calculation result would increase if rainfall (seepage analysis) and earthquakes (kinetic analysis) are considered. This topic will be the direction of our future research.

The failure process is unlikely to occur in the investigated rock slope unless it is subjected to significant environmental changes, such as earthquakes, rainfall, unloading, or overloading. Nonetheless, the potential failure process is simulated in

310   this study to understand the rockslide mechanism and subsequently provide a good reference for similar slope projects. For example, the size and motion of rock blocks can be utilized to predict risk degree, and the final accumulation of deposits can contribute to hazardous area division. The final arrangement of deposits (a combination of blocks and crushed particles) provides a good explanation for the inverse grading of rock avalanche reported by Cruden and Hungr, (1986), Imre et al. (2010), and Wang et al. (2012).

315   DFN simulation presents a high degree of variability and may provide erroneous results. A statistical analysis based on numerous SRM models with different DFN models similar to those performed in the present study can reduce errors and

provide conservative results for slope support. Finally, although the final results of the factor of safety, critical slip surface, and accumulation distance can guarantee safety in the rockslide analysis and support, they are not the exact values. Statistical analysis provides a new method for deriving an in-depth understanding of solid earth, where specific locations and

320   characteristics of geological materials and structures remain unknown, such as discontinuities, especially for small-scale non-persistent fractures. Meanwhile, new theories and technologies are required to obtain precise forecasts with respect to the range values characterized by statistical methods.

8 conclusion

The present study combines several methods, namely, DFN simulation, SRM approach, and statistical analysis, to conduct

325   stability evaluation and potential failure process analysis of a fractured rock slope in Laohuding Quarry in Jixian County, Tianjin. The SRM technique is utilized to generate a slope model with non-persistent fractures in the form of a DFN. An innovative formula for the safety factor is deduced by considering stress concentration on the basis of the improved gravity increase and strength reduction methods. The formation of a critical slip surface is also investigated. The potential failure and accumulation processes are simulated to provide a reference for similar slope projects. Numerous slope models are

330   calculated, and the final results of the safety factor, critical slip surface, and accumulation distance are determined by statistical analysis. The major findings are summarized as follows.

        (1) The slope model with non-persistent fractures can be effectively constructed on the basis of SRM technology. The instability of the slope model can be attained by combining the improved gravity increase method or the strength reduction method, thereby obtaining the safety factor and critical slip surface. An innovative formula to calculate the safety factor is

335   proposed by considering stress concentration and the calculation principle of PFC2D.

        (2) Fracture propagation is closely related to stress concentration. Fractures initially propagate from the tips of the original fractures where the tensile stress is concentrated. Then, the stress is released, and a new stress concentration occurs at the tip of the propagated fractures when the fracture propagates downward to the neighbouring fractures. The critical slip surface is formed by the coalescence of preexisting fractures and newly propagated fractures.

340   (3) In the initiation of failure, the slip mass is fractured into rock blocks along the preexisting fractures. Then, most blocks rotate and collapse under inertia force and gravity. Several blocks are split into sub-blocks owing to the collision between the blocks and the ground. The final deposit is composed of intact blocks and crushed particles, presenting inverse grading phenomena.

        (4) The critical slip surfaces, factors of safety, and accumulation distances of the slope models with different DFN

345   models vary. Therefore, the final outcome is obtained by statistical analysis. It ensures engineering safety for rockslide analysis and support. The factor of safety (reserve) of the studied rock slope is determined to be 43.5. The critical slip surface is confirmed, as shown in Fig. 11. The final accumulation distance is 87 m.

Data availability. The data from the research findings cannot be shared now, because these data are also part of the future research.

350 **Author contributions.** WZ initiated this research, analysed the simulation results, and revised the manuscript. JW wrote software code and wrote this paper. PX, JL and BS conducted field investigation and recorded field data. FW and CC dealt with the field data. XC and JQ guided and collated the software code.

Competing interests. The authors declare that they have no conflict of interest.

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References

Brideau, M., Yan, M., and Stead, D.: The role of tectonic damage and brittle rock fracture in the development of large rock slope failures, Geomorphology, 103, 30–49, 2009.

365 Bahaaddini, M., Sharrock, G., and Hebblewhite, B. K.: Numerical investigation of the effect of joint geometrical parameters on the mechanical properties of a non-persistent jointed rock mass under uniaxial compression, Comput. Geotech., 49, 206–225, 2013.

Bonilla-Sierra, V., Scholtès, L., Donzé, F. V., and Elmouttie, M. K.: Rock slope stability analysis using photogrammetric data and DFN–DEM modeling, Acta Geotech., 10, 497–511, 2015.

370 Cruden, D. M. and Hungr, O.: The debris of the Frank slide and theories of rockslide-avalanche mobility, Can. J. Earth Sci., 23, 425–432, 1986.

Chen, J. P.: 3-D network numerical modeling technique for random discontinuities of rock mass, Chinese Journal of Geotechnical Engineering, 23, 397–402, 2001.

Chen, J. P., Shi, B. F., and Wang, Q.: Study on the dominant orientations of random fractures of fractured rock mass, 375 Chinese Journal of Rock Mechanics and Engineering, 24, 241–245, 2005.

Cheung, L. Y. G., O'Sullivan, C., and Coop, M. R.: Discrete element method simulations of analogue reservoir sandstones, Int. J. Rock Mech. Min., 63, 93–103, 2013.

Duan, K., Kwok, C. Y., and Pierce, M.: Discrete element method modeling of inherently anisotropic rocks under uniaxial compression loading, Int. J. Numer. Anal. Met., 40, 1150–1183, 2016.

380 Einstein, H. H., Veneziano, D., Baecher G. B., and O'Reilly, K. J.: The effect of discontinuity persistence on rock slope stability, Int. J. Rock Mech. Min., 20, 227–236, 1983.

Eberhardt, D., Stead, D., and Coggan, J. S.: Numerical analysis of initiation and progressive failure in natural rock slopes— the 1991 Randa rockslide, Int. J. Rock Mech. Min., 41, 69–87, 2004.

Elmo, D. and Stead, D.: An integrated numerical modelling–Discrete Fracture Network approach applied to the
385 characterisation of rock mass strength of naturally fractured pillars, Rock Mech. Rock Eng., 43, 3–19, 2009.

Elmo, D., Stead, D., Eberhardt, E., and Vyazmensky, A.: Applications of finite/discrete element modeling to rock engineering problems, Int. J. Geomech., 13, 565–580, 2013.

Elmo, D., Donati, D., and Stead, D.: Challenges in the characterisation of intact rock bridges in rock slopes, Eng. Geol., 245, 81–96, 2018.

390 Esmaieli, K., Hadjigeorgiou, J., and Grenon, M.: Estimating geometrical and mechanical REV based on synthetic rock mass models at Brunswick Mine, Int. J. Rock Mech. Min., 47, 915–926, 2010.

Elmouttie, M. K. and Poropat, G. V.: Quasi-Stochastic analysis of uncertainty for modeling structurally controlled failures, Rock Mech. Rock Eng., 47, 519–534, 2014.

Fisher, R.: Dispersion on a sphere, Proceedings of the Royal Society of London, 217, 295–305, 1953.

395 Fan, S. C., Jiao, Y. Y., and Zhao, J.: On modeling of incident boundary for wave propagation in jointed rock masses using discrete element method, Comput. Geotech., 31, 57–66, 2004.

Frayssines, M. and Hantz, D.: Failure mechanisms and triggering factors in calcareous cliffs of the Subalpine Ranges (French Alps), Eng. Geol., 86, 256–270, 2006.

Fan, X., Kulatilake, P. H. S. W., and Chen, X.: Mechanical behavior of rock-like jointed blocks with multi-non-persistent
400 joints under uniaxial loading: A particle mechanics approach, Eng. Geol., 190, 17–32, 2015.

Ferrero, A. M., Migliazza, M. R., Pirulli, M., and Umili, G.: Some open issues on rockfall hazard analysis in fractured rock mass: problems and prospects, Rock Mech. Rock Eng., 49, 3615–3629, 2016.

Gao, W., Dai, S., Xiao, T., and He, T. Y.: Failure process of rock slopes with cracks based on the fracture mechanics method, Eng. Geol., 231, 190–199, 2017.

405 Huang, D., Cen, D. F., Ma, G. W., and Huang, R. Q.: Step-path failure of rock slopes with intermittent joints, Landslides, 12, 911–926, 2015.

Imre, B., Laue, J., and Springman, S. M.: Fractal fragmentation of rocks within sturzstroms: insight derived from physical experiments within the ETH geotechnical drum centrifuge, Granular Matter, 12, 267–285, 2010.

Jiang, M. M., Jiang, T., Crosta, G. B., Shi, Z. M., Chen, H., and Zhang, N.: Modeling failure of jointed rock slope with two
410 main joint sets using a novel DEM bond contact model, Eng. Geol., 193, 79–96, 2015.

Kulatilake, P. H. S. W. and Wu, T. H.: Estimation of mean trace length of discontinuities, Rock Mech. Rock Eng., 17, 215–232, 1984.

Lajtai, E. Z.: Strength of discontinuous rocks in direct shear, Géotechnique, 19, 218–233, 1969.

Li, L. C., Tang, C. A., Zhu, W. C., and Liang, Z. Z.: Numerical analysis of slope stability based on the gravity increase
415   method, Comput. Geotech., 36, 1246–1258, 2009.

Mas Ivars, D.: Water inflow into excavations in fractured rock — a three-dimensional hydro-mechanical numerical study, Int.
J. Rock Mech. Min., 43, 705–725, 2006.

Mas Ivars, D. Bonded particle model for jointed rock mass, Ph.D. thesis, Royal Institute of Technology, Sweden, 2010.

Mas Ivars, D., Pierce, M. E., Darcel, C., Reyes-Montes, J., Potyondy, D. O., Young, R. P., and Cundall, P. A.: The synthetic
420   rock mass approach for jointed rock mass modelling, Int. J. Rock Mech. Min., 48, 219–244, 2011.

Meng, Y. D., Su, Q. M., Lu, W. P., and Xu, Z.: Research on improved grain flow gravity increase method, Chinese Journal
of Water Resource and Power, 33, 149–151, 2015.

Priest, S. D.: Discontinuity analysis for rock engineering, London : Chapman and Hall, 1993.

Potyondy, D. O. and Cundall, P. A.: A bonded-particle model for rock, Int. J. Rock Mech. Min., 41, 1329–1364, 2004.

425   Pine, R. J., Coggan, J. S., Flynn, Z. N., and Elmo, D.: The development of a new numerical modelling approach for naturally
fractured rock masses, Rock Mech. Rock Eng., 39, 395–419, 2006.

Pierce, M., Cundall, P., Potyondy, D., and Ivars, D. M.: A synthetic rock mass model for jointed rock, in: Proceedings of
First Canada/United States Rock Mechanics Symposium, Vancouver, 341– 349, 2007.

Park, J. W., and Song, J. J.: Numerical simulation of a shear test on a rock joint using a bonded-particle model, Int. J. Rock
430   Mech. Min., 46, 1315–1328, 2009.

Scavia, C.: A method for the study of crack propagation in rock structures, Géotechnique, 45, 447–463, 1995.

Terzaghi, K.: Stability of steep slopes on hard unweathered rock, Géotechnique, 12, 251–270, 1962.

Wang, Y. F., Cheng, Q. G., and Zhu, Q.: Inverse grading analysis of deposit from rock avalanches triggered by Wenchuan
earthquake, Chinese Journal of Rock Mechanics and Engineering, 1089–1106, 2012.

435   Wasantha, P. L. P., Ranjith, P. G., Xu, T., Zhao, J., and Yan, Y. L.: A new parameter to describe the persistency of non-
persistent joints, Eng. Geol., 181, 71–77, 2014.

Xu, Q., Chen, J. Y., Li, J., and Yue, H. Y.: A genetic algorithm for locating the multiscale critical slip surface in jointed rock
mass slopes, Math. Probl. Eng., 2014.

Yang, B., Jiao, Y., and Lei, S.: A study on the effects of microparameters on macroproperties for specimens created by
440   bonded particles, Eng. Computation., 23, 607–631, 2006.

Zhang, W., Chen, J. P., Liu, C. H., Ma, J. Q., and Zhang, C.: Application of chi-square test in structural homogeneity
dividing of fractured rock mass, Chinese Journal of Geotechnical Engineering, 33, 1440–1446, 2011.

Zhang, W., Chen, J. P., Liu, C., Huang, R., Li. M., and Zhang, Y.: Determination of geometrical and structural representative
volume elements at the Baihetan Dam Site, Rock Mech. Rock Eng., 45, 409–419, 2012.

445 Zhang, W., Chen, J. P., Zhang, W., Lv, Y., Ma, Y. F., and Xiong, H.: Determination of critical slip surface of fractured rock slopes based on fracture orientation data, Sci. China. Technol. Sc., 56, 1248–1256, 2013.

Zhang, W., Zhao, Q. H., Chen, J. P., Huang, R. Q., and Yuan, X. Q.: Determining the critical slip surface of a fractured rock slope considering preexisting fractures and statistical methodology, Landslides, 14, 1253–1263, 2017.

Zhang, Y. and Stead, D.: Modelling 3D crack propagation in hard rock pillars using a synthetic rock mass approach, Int. J.
450 Rock Mech. Min., 72, 199–213, 2014.

Zhou, Y., Chai, J. F., and Han, G.: Meso numerical study on the failure mechanism on rock slope with bedding intermittent joints, Engineering Review, 37, 272–280, 2017.

Zhang, K., Cao, P., Meng, J. J., Li, K. H., Fan, W. C.: Modeling the progressive failure of jointed rock slope using fracture mechanics and the strength reduction method, Rock Mech. Rock Eng., 48, 771–785, 2015.

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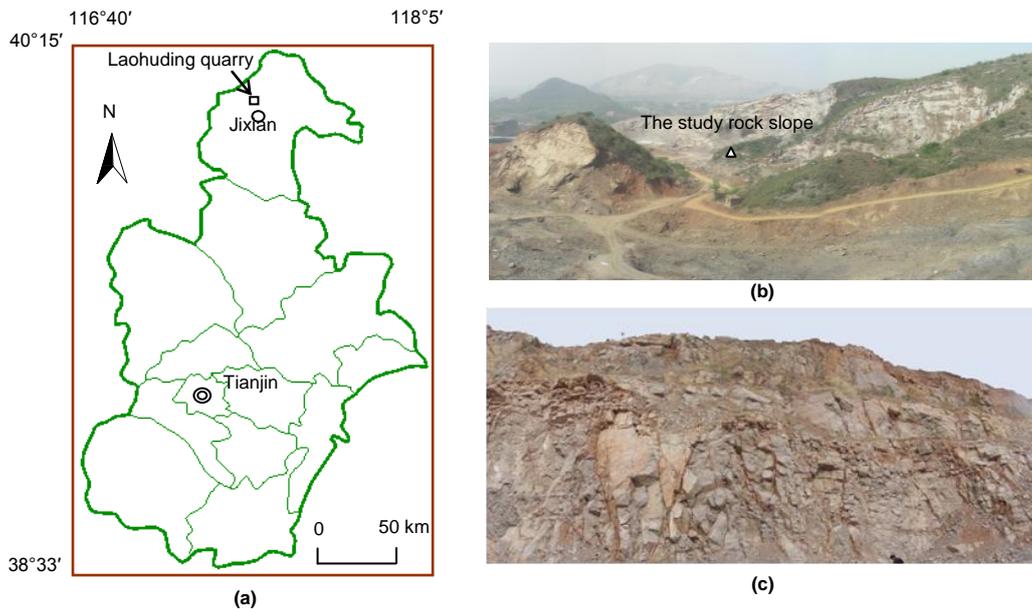
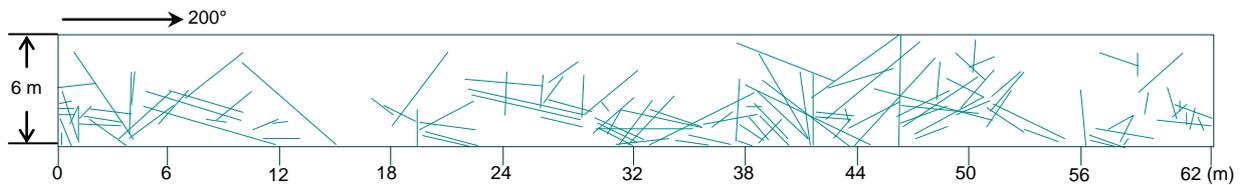


Figure 1: Location of the Laohuding Quarry and investigated rock slope. **(a)** location of Laohuding Quarry in Tianjin City; **(b)** image of Laohuding Quarry and the location of the investigated rock slope; **(c)** image of the investigated rock slope.

460 **Figure 2:** 2D trace chart of collected fractures

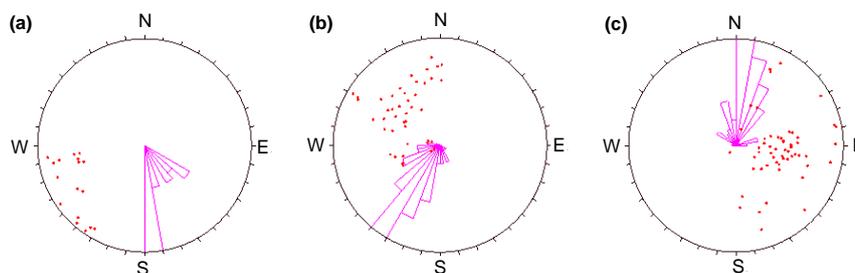



Figure 3: Poles and strike rose diagrams of the fracture sets. **(a)**–**(c)** are fracture sets 1, 2, and 3.

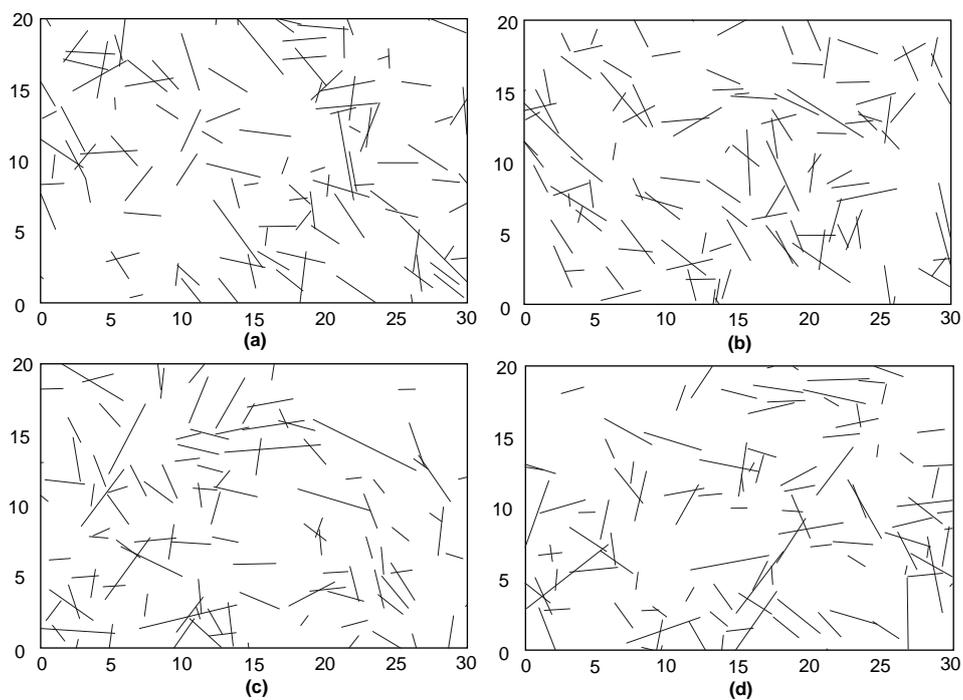



Figure 4: Variability of DFN simulation. **(a)**–**(d)** are the DFN models in four simulations. The line segments in the rectangle frame represent the fractures, and the left boundary of the frame represents the exposed surface.

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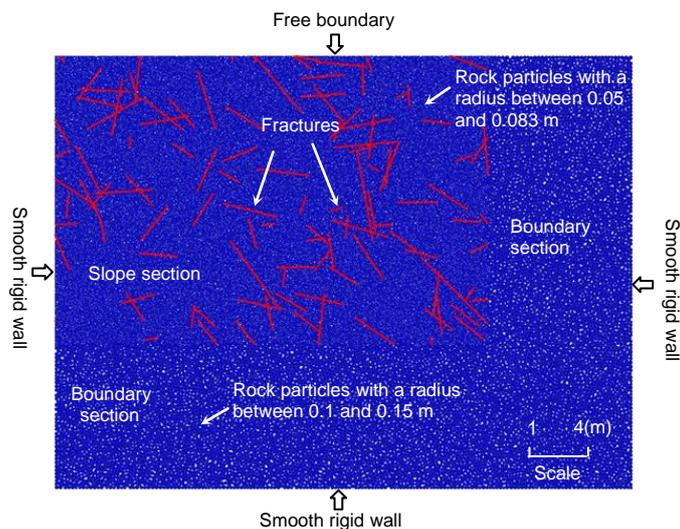


Figure 5: SRM model of the investigated fractured rock slope. The left boundary is the exposed surface.

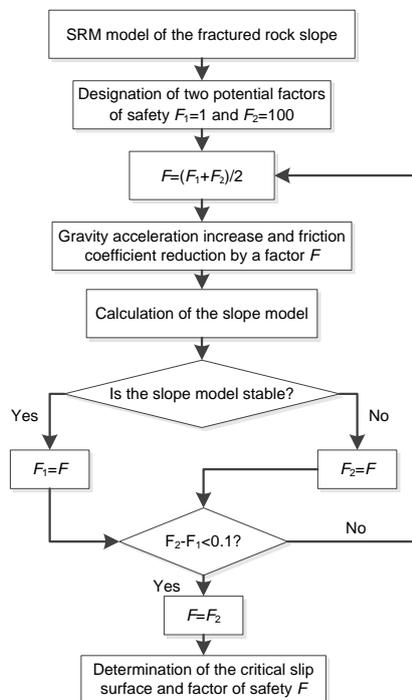



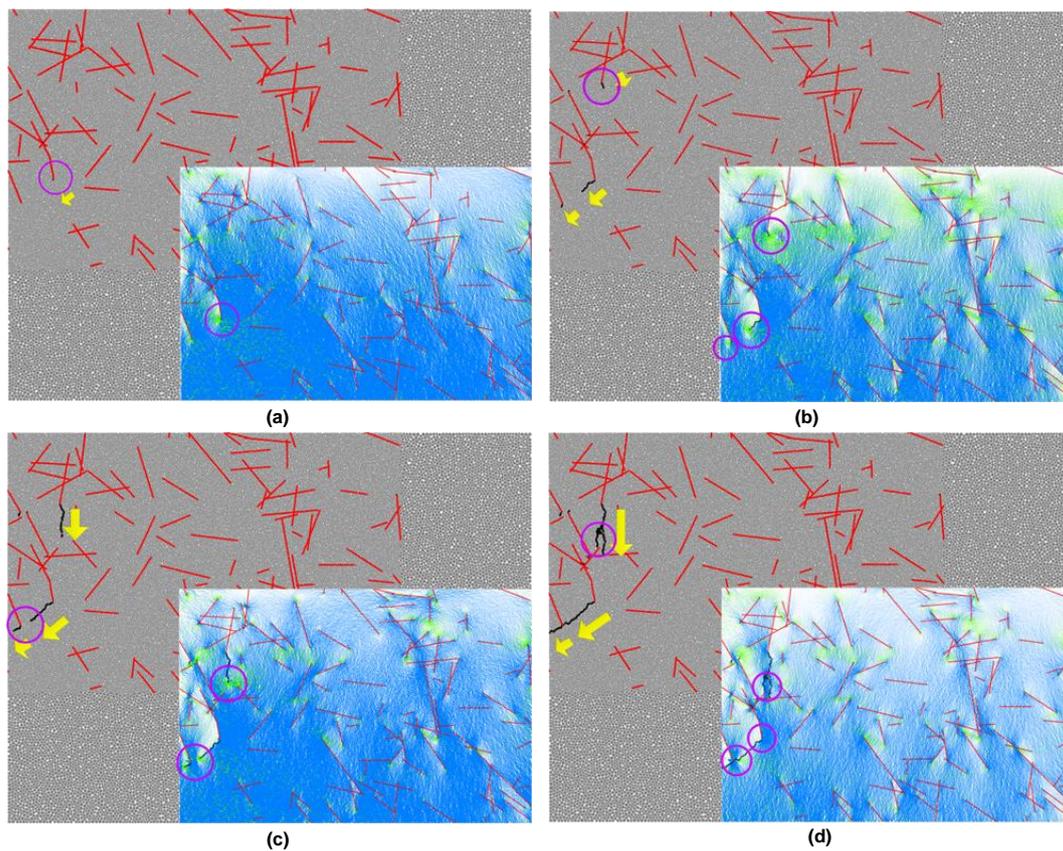
Figure 6: Program flow chart for the slope stability analysis.

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Figure 7: Program flow chart for the slope stability analysis. Formation process of the critical slip surface and force chain plots. The time steps of **(a)**–**(d)** are 2000, 5000, 10000, and 20000. Blue and green lines denote compressive and tensile forces, respectively.
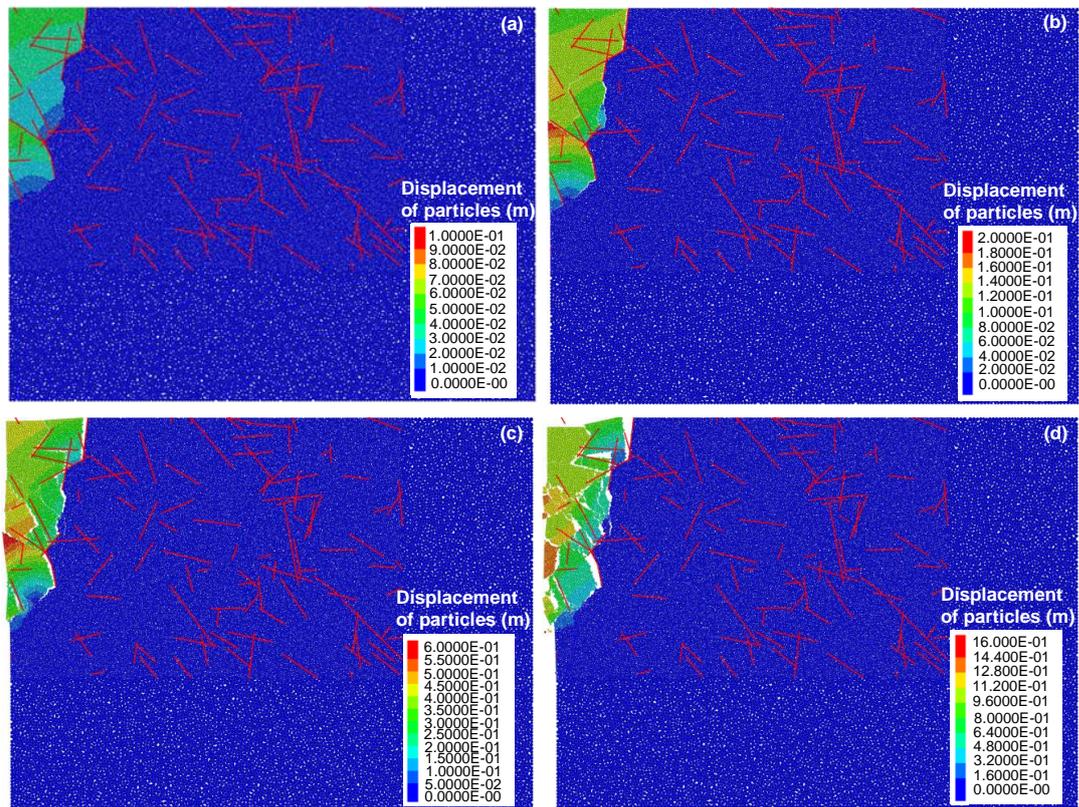
Figure 8: Particle displacement field of the fractured rock slope. The time steps of **(a)**–**(d)** are 20000, 40000, 60000, and 80000.
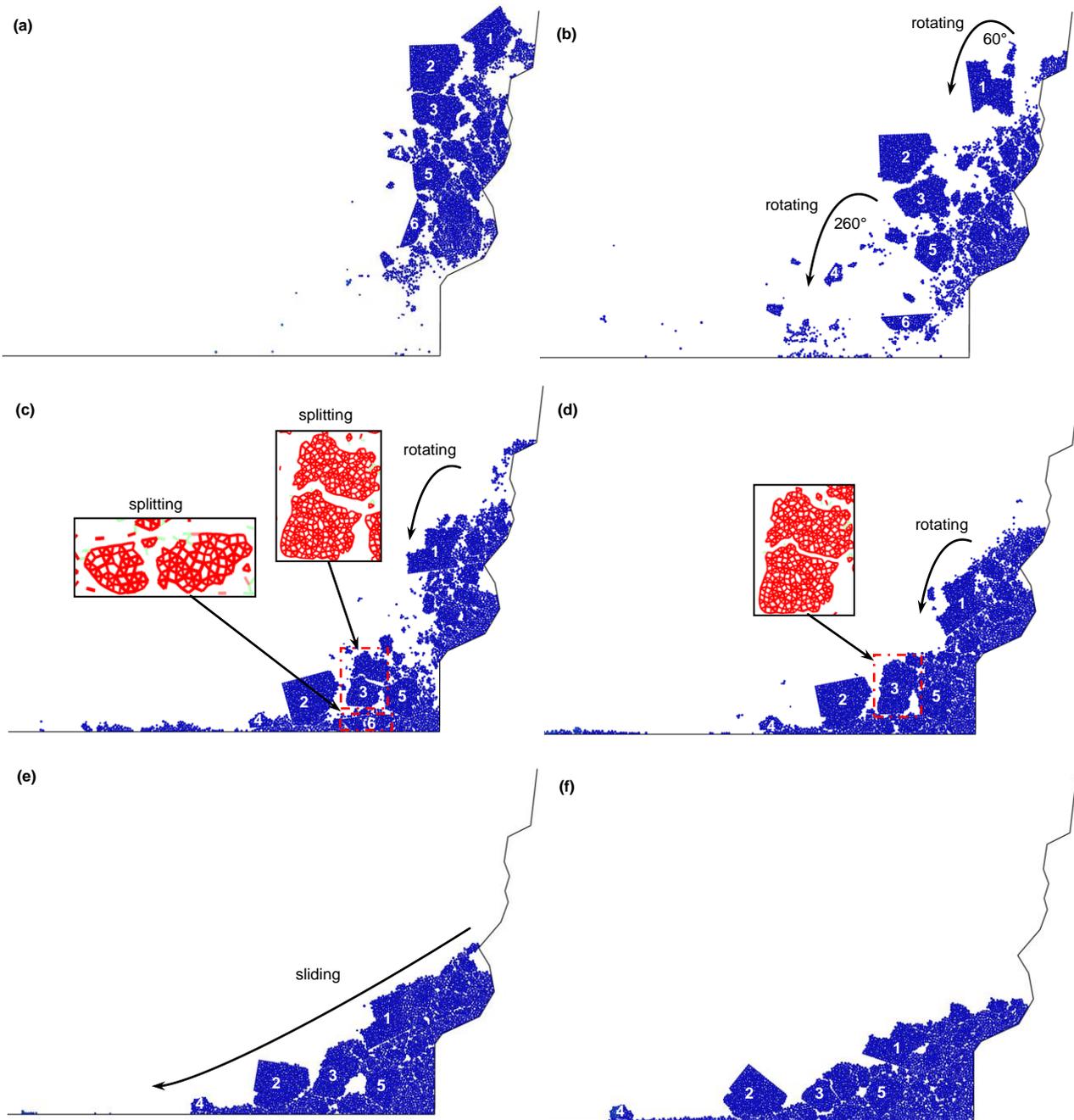
Figure 9: Failure and accumulation process of the rock slope. The time steps of **(a)**–**(f)** are 5×10^4, 2×10^5, 4×10^5, 8×10^5, 1.6×10^6, and 3.2×10^6.
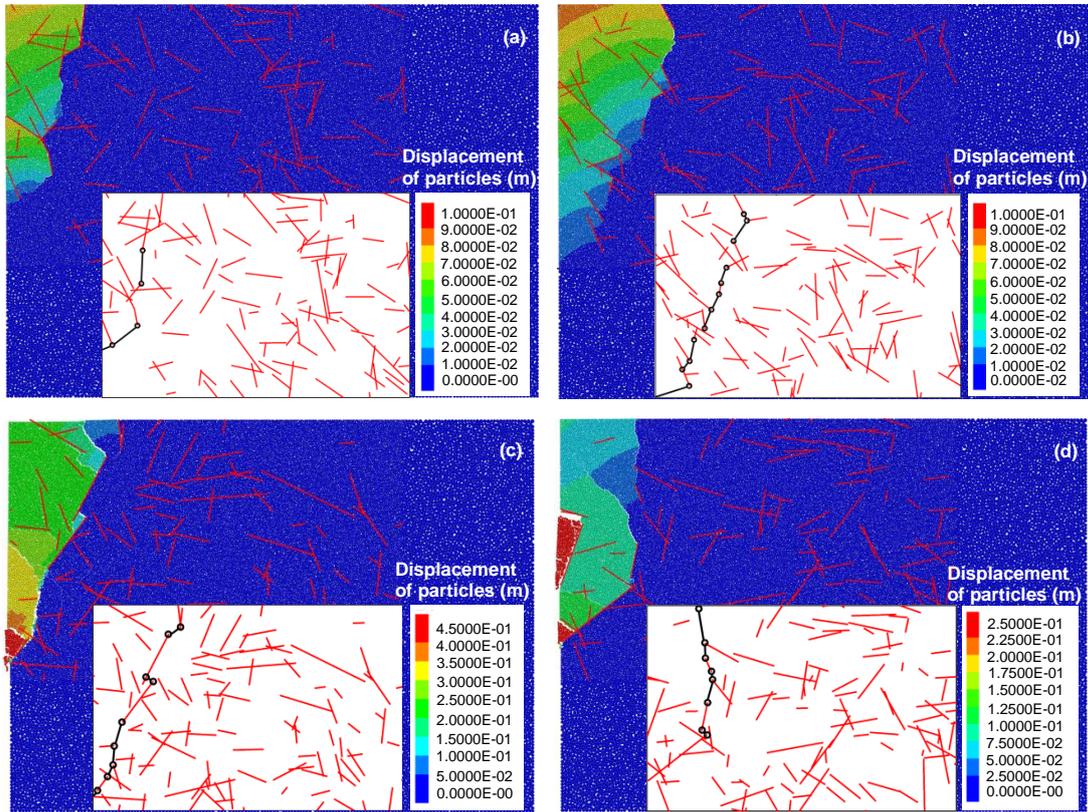
Figure 10: Four different critical slip surfaces of rock slopes with four different DFN models. The factors of safety of **(a)**–**(d)** are 25, 28, 40.5, and 33.5.
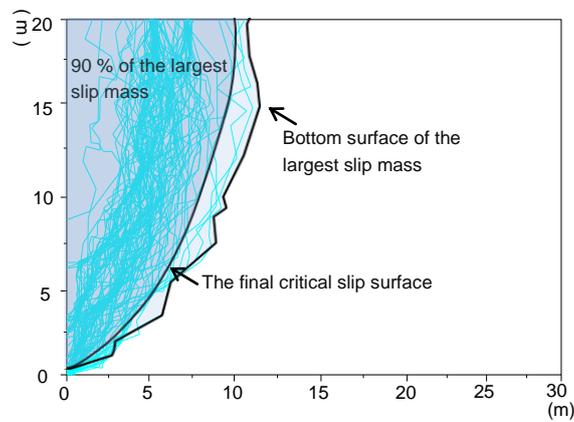
Figure 11: Potential critical slip surfaces of 100 models and the final critical slip surface of the investigated rock slope.
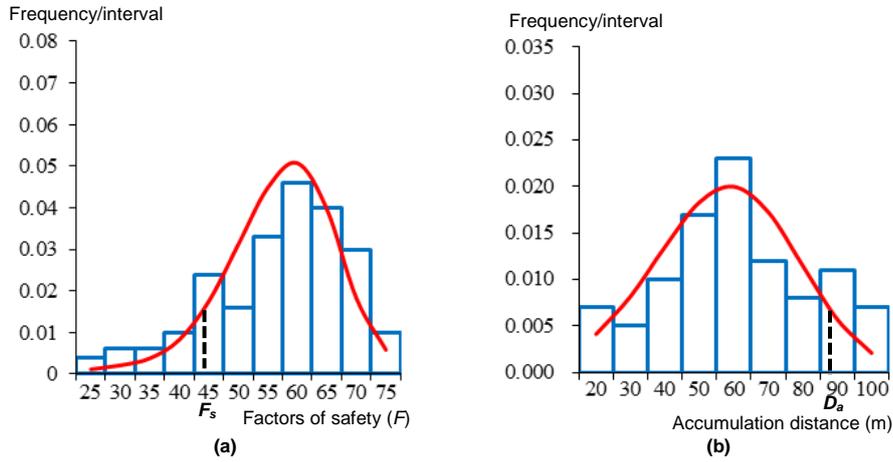
Figure 12: Statistical results of 100 slope models. **(a)** the final factor of safety F_s of the investigated rock slope; **(b)** the final accumulation distance D_a of the investigated rock slope.
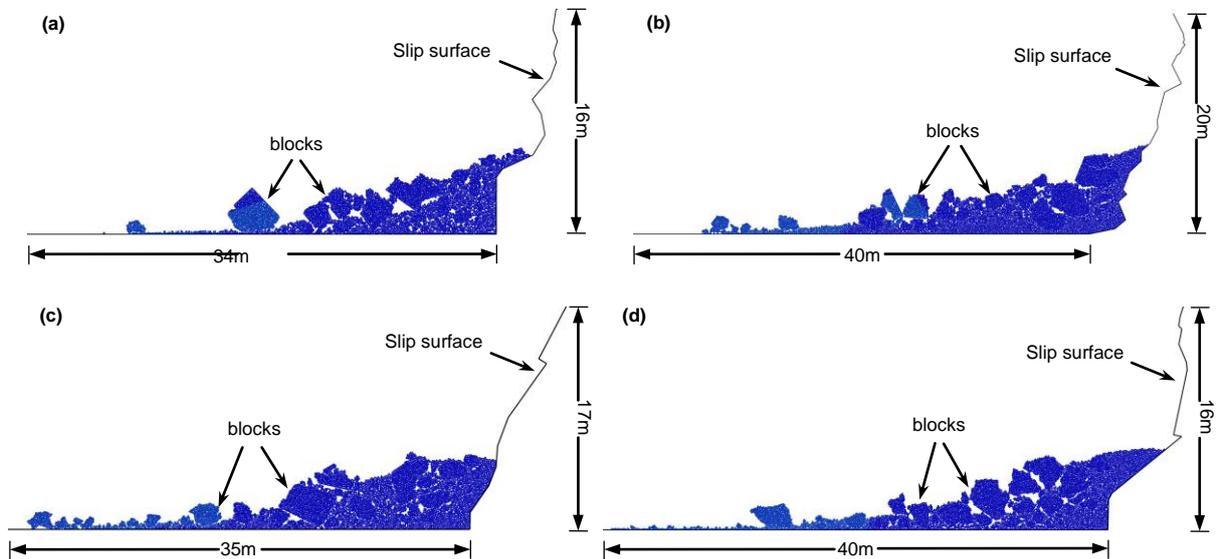
Figure 13: Ultimate accumulation states of rock slopes with different DFN models (partly). The final accumulation distances of **(a)**–**(d)** are 28, 34, 35, and 40m.

Table 1: Parameters for discrete fracture network (DFN) simulation.

Fracture set	Fracture number	Dip Direction (°)	Dip Angle (°)	Trace length surveyed (m)	Corrected (m)	Std. (m)	Distribution type	R_0	R_1	R_2	P_{21}(m/m²)	K
1	18	39.5	87.3	2.16	2.42	1.2	Gamma	0.89	0.11	0	0.11	17.1
2	58	307.4	44.7	2.71	2.84	1.7	Log-normal	0.83	0.14	0.03	0.45	10.3
3	93	110.2	31.7	2.33	2.49	1.2	Gamma	0.87	0.13	0	0.63	9.1

490   **Table 2:** Values of the BPM parameters.

Particle parameters		Parallel bond parameters	
Particle density (kg/m^3)	2650	E_b (GPa)	23
Minimum particle radius (m)	0.05	k_{nb}/k_{sb}	1.25
Radius ratio	1.66	Normal strength (MPa)	25
Friction coefficient	0.7	Internal friction angle (°)	38
k_n/k_s	1.25	Cohesion (MPa)	25
E_c (GPa)	23	Radius multiplier	1

Table 3: Comparison of macro-properties determined by numerical and laboratory tests.

Macro-parameters	E (Gpa)	Poisson's ratio	Friction angle (°)	Cohesion (Mpa)	σ_c (Mpa)
Numerical tests	35.7	0.23	23	12.68	37.8
Laboratory tests	35	0.24	25	12.25	38.3

Table 4: Calibrated smooth-joint parameters and results of numerical and laboratory tests

Smooth-joint parameters		Test results		
		Parameters	Numerical tests	Laboratory tests
Normal stiffness $\bar{k}_{nj}$ (GPa/m)	10	Friction angle (°)	17.87	18
Shear stiffness $\bar{k}_{sj}$ (GPa/m)	8	Shear stiffness (GPa/m)	3.415	3.4
Coefficient of friction μ_j	0.466	Normal stiffness (GPa/m)	7.042	7

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