

# Interactive comment on "Multilayer-HySEA model validation for landslide generated tsunamis. Part I Rigid slides" by Jorge Macías et al.

Anonymous Referee #1

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## General Comments:

This is an informative paper on state of the art tsunami modeling for land-slide generated tsunamis. The study presents results of performing simulations for 3 benchmark problems provided by the National Tsunami Hazard Mitigation Program (NTHMP) with the numerical code Landslide-HySEA. The topic and results presented in the paper are within the scope NHESSD topics. The paper provides a sufficiently detailed description of both, the governing equations modeled in the code and the numerical algorithm implemented to resolve the system. Additional references are provided for readers interested in additional details. The authors provide an adequate literature review of pre-existing validation efforts in the introductory section of the report and with a few necessary improvements also provide a clear and understandable description of the implementation of the laboratory experiments used for the validation. The results are presented in a clear and concise manner. The first part of the paper could benefit from a thorough English language and stylistic review, particularly (Sections 1, 2). The style seems to improve after those two sections. It should also be reviewed for some typos: Some examples typos are provided in the Specific Comments below.

*Authors comment: As suggested by the reviewer, we have sent the abstract and the first two sections for professional English language revision. This revised text has been included in the current version of the paper, now uploaded (These corrections are not marked in red in the revised version).*

*First of all, note that the reviewer must have used for the revision an older version of the submitted paper as most of the typos he/she is mentioning are not present in the version that was uploaded in the NHESS system. Also, the numbering he/she is using does not correspond to that of the (up to today) current version of the paper.*

## Specific comments:

- pp1 Please correct the sentence: "The US National Tsunami Hazard and Mitigation Program (NTHMP) has proposed the experimental data used Hazard and Mitigation Program (NTHMP) and established for the NTHMP Landslide Benchmark Workshop, held in January 2017 at Galveston." to "The US National Tsunami Hazard and Mitigation Program (NTHMP)..."

*This sentence was not present in the version uploaded at the NHESS system, corresponds to an older version.*

- pp2. l. 9; Please, provide reference for "Catalina Island" 2006 workshop.

*The reference of Liu et al (2008) [7] has been included.*

- pp3. l. 33; Fifteen or twenty?, please specify.

*Again, this is not in the version we are taking from NHESS system. In that version, it can be read "Twenty years ago, at the beginning of the century,..."*

- pp.4. Please, clarify the type of approximation the Landslide-HySEA uses to model the physical system. Are vertical pressure and velocity gradients modeled linearly within each layer with matching values at the interphase between layers?

*The system is derived under the assumption of a linear vertical profile within each layer for the total pressure. The horizontal and vertical velocities are assumed to have a constant vertical profile within each layer. More details on the derivation of the system (1) can be found in [5] (model LDNH<sub>0</sub>).*

*An alternative deduction of the same system (1) is performed in [3] assuming linear vertical profiles for pressure and vertical velocity, and constant vertical profile for the horizontal velocity, as well as some extra hypothesis for the case of two layers.*

*Concerning the continuity of variables at the interphase between layers:*

*The system is derived from Euler equations after a Galerkin approach at z-direction. At the discrete level on z, the total pressure matches at interphases and velocities satisfies a discrete jump condition (See [5] or [3]).*

This clarifications have been added in the first two paragraphs of Section 3.

- What is exactly meant in line 74 by "The multilayer model is able to take into account the full vertical structure" isn't this an overstatement, please clarify.

*We wanted to express that the multi-layer model is able to better approximate the vertical structure than a standard one-layer depth-averaged model. Considering a richer vertical structure provides better approximations of more complex 3D effects that may occur in the simulated flow. In particular, increasing the number of layers, the linear dispersion relation of the model converges towards the exact dispersion relation from the Stokes linear theory (see [5] for a proof of the result).*

Three sentences, including the text above, have been added at the end of the paragraph in order to clarify this point.

- pp. 5 Please, label equations throughout the paper.

*Done.*

- pp. 5 (Equation System 1). There seems to be a lack of symmetry in the discretization of the continuity equation. Is this meant to be one-sided discretization? Please, check.

*The system (1) is equivalent to the model LDNH<sub>0</sub> given in [5] for a given number of layers L.*

*The system LDNH<sub>0</sub> contains exactly L equations corresponding to the incompressibility condition at each layer (see eq. (3.18a) in [5]). However, given a layer  $\alpha \in \{1, \dots, L\}$ , the incompressibility eq. (3.18a) involves the presence of the spatial derivatives of  $u_1, u_2, \dots, u_{\alpha-1}$ , as well as  $u_\alpha$ , that makes the design of the numerical method less efficient.*

*In the present paper, we have circumvented that difficulty by doing some algebraical manipulations.*

*Let us show the equivalence between incompressibility equations given in (1), and the incompressibility equations of system LDNH<sub>0</sub>, given in eq. (3.18a) [5].*

- Procedure to obtain the incompressibility equation for the lower layer  $\alpha = 1$  in (1): Equation (3.18a) given in [5] for the lower layer  $\alpha = 1$  and written with the notation used in this reviewed paper reads:

$$w_1 + \partial_t H - u_1 \partial_x (-H + \Delta sh) + \frac{1}{2} \partial_x (\Delta sh u_1).$$

Now, if we divide by  $\Delta sh > 0$  at both sides of the previous equation and after arranging terms, we obtain:

$$\frac{1}{2} \partial_x u_1 + \frac{1}{h \Delta s} u_1 \partial_x \left( H - \frac{1}{2} h \Delta s \right) + \frac{1}{h \Delta s} (w_1 + \partial_t H) = 0,$$

that coincides with the incompressibility equation given in (1) for the lower layer  $\alpha = 1$ :

$$\partial_x u_{1/2} + \sigma_{1/2} \partial_z u_{1/2} + \partial_z w_{1/2} = 0,$$

where,  $u_{1/2}$ ,  $\sigma_{1/2}$ ,  $\partial_z u_{1/2}$  and  $\partial_z w_{1/2}$  are given in eqs. (2), (3) and (5):

$$u_{1/2} = \frac{u_1 + u_0}{2} = \frac{u_1 + 0}{2}, \quad \sigma_{1/2} = \partial_x \left( H - \frac{1}{2} h \Delta s \right),$$

$$\partial_z u_{1/2} = \frac{1}{h \Delta s} (u_1 - u_0) = \frac{1}{h \Delta s} (u_1 - 0),$$

$$\partial_z w_{1/2} = \frac{1}{h \Delta s} (w_1 - w_0) = \frac{1}{h \Delta s} (w_1 + \partial_t H).$$

- Procedure to obtain the incompressibility equation for a given layer  $\alpha > 1$  in (1): Equation (3.18a) given in [5] for the layer  $\alpha$  and  $\alpha - 1$ , and written with the notation used in this reviewed paper, respectively reads:

$$w_\alpha + \partial_t H - u_\alpha \partial_x (-H + (\alpha - 1/2) \Delta sh) + \partial_x (\Delta sh u_1) + \dots + \partial_x (\Delta sh u_{\alpha-1}) + \frac{1}{2} \partial_x (\Delta sh u_\alpha) = 0,$$

and

$$w_{\alpha-1} + \partial_t H - u_{\alpha-1} \partial_x (-H + (\alpha - 1 - 1/2) \Delta sh) + \partial_x (\Delta sh u_1) + \dots + \partial_x (\Delta sh u_{\alpha-2}) + \frac{1}{2} \partial_x (\Delta sh u_{\alpha-1}) = 0.$$

Now, subtracting both equations yields

$$\Delta sh \partial_x \left( \frac{u_\alpha + u_{\alpha-1}}{2} \right) + w_\alpha - w_{\alpha-1} + (u_\alpha - u_{\alpha-1}) \partial_x (H - (\alpha - 1) \Delta sh) = 0.$$

If we divide at both sides of the previous equation by  $\Delta sh > 0$ , then we can re-write it using the notation introduced in the present reviewed paper:

$$\partial_x u_{\alpha-1/2} + \sigma_{\alpha-1/2} \partial_z u_{\alpha-1/2} + \partial_z w_{\alpha-1/2} = 0$$

that coincides with the expression given in (1).

Therefore, if we consider the matrix operator associated with the set of incompressibility equations, then it is clear that this operator (from eq (3.18a) in [5], consists of a lower triangular matrix.

However, with the procedure followed here, we can pre-compute a triangularization of the original operator, that can be solved later in a more efficient way.

The above explanation has not been included in the corrected version of the paper now uploaded, nevertheless we could include it as a Remark or Appendix if the reviewer considers it is appropriate.

- pp 6. l. 109; Linearization around what “lake”?

*The word “lake” does not appear in the current version. It was in an older version.*

- pp. 8 Table 1. Please, include expression for Phase Velocity from Airy linear theory for reference. Why is only Phase Velocity approximations shown? What about Group Velocity and Shoaling Gradient?

*We have included the expression for Phase Velocity from Airy linear theory as requested (see eq (7)).*

*Concerning Group Velocity and Shoaling Gradient, we have considered that the expressions are too tedious to be given here. Instead, we present the relative errors of phase and group velocities as well as linear shoaling with respect to the Airy theory in Figure 2.*

- pp. 8 l. 145-147, Please, check if expected values of  $kH$  for your numerical experiment fall within the range properly modeled in your approximations ( $5 < kH < 15$  pp7-8, l.144...), the paper would benefit from a brief discussion on this topic.

*We agree with the reviewer’s comment. We have included a discussion on this topic for the benchmark problem 2, where it was clear how to measure the experiment’s wave number.*

- pp. 11. l. 168-174. Please, from the explanation on how the solution proceeds, the elliptic operator for the continuity equation seems to be computed implicitly, the pressure terms calculated with the solution from the continuity equation and then the discharge field updated in time explicitly? If this is the case, a bit more detail explanation would be appreciated. Otherwise, please clarify how the solution proceeds.

*We have detailed the explanation in the present reviewed paper.*

*The procedure is based on the Chorin’s projection method, a standard and well-known approximation for dispersive systems (see, for instance, [1, 3, 4, 6, 9, 11]).*

- pp. 14, Figure 5. From the curves, the motion of the block seems to stop abruptly. Is this correct?

*Is correct. We use the prescribed motion for the block given in eq (17). Moreover, the block stops at time  $t = t_0 = 1.677$  s. This is part of the benchmark description provided by the NTHMP. For the workshop we presented results with a non-stopping slide but we were simulating a different experiment. This information has been included in the reviewed paper.*

- pp. 14, 223. Please, specify where in the domain outflow conditions are imposed.

*Done. In the case of this 2D experiment, outflow boundary conditions were imposed at  $x = -1$ ,  $x = 10$ .*

- pp. 14 & 23. Please, clarify how a Smagorinsky turbulent model for the Reynolds stresses is used in this context. Do the field equations preserve the classic Navier-Stokes viscous stress tensor for the resolved scales and a Smagorinsky model is then used for the Reynolds stresses? The text seems to confuse these two terms as if they are the same one, but both are present separately in the Reynolds averaged Navier-Stokes equations.

*We do not pretend to perform Navier-Stokes simulations. We understand that this is not clear in the present wording and a new subsection has been included to better explain this issue (see Subsection 3.2. Wave breaking and wetting and drying).*

*It is well known that dispersive systems can not correctly represent breaking waves, and a breaking mechanism has to be included to account for these breaking effects. In the current*

*work, we add to the equation a dissipation term in momentum equations that accounts for the dissipation of the energy associate with a breaking bore. The key idea is that, in the presence of a breaking bore, a hydrostatic regime can better represent the physics.*

*To do that, we have included the diagonal part of the stress tensor for the horizontal momentum equation, and a breaking criteria is used to switch on and off such dissipation terms near to breaking bores. This is a standard technique when dealing with such type of dispersive problems and breaking waves (see [3, 4, 6, 11] and references therein.)*

This is detailed in the new Subsection 3.2 "Modeling of breaking waves and wetting and drying treatment".

- pp. 17 Table 4. Please, define all variables in the column 1 of Table 4.

*Done.*

*Some of the parameters appearing in Table 4 in the former version of this paper have been removed since they were expendable for the experiment's description. However, the interested reader is referred to the original paper [2].*

- pp 23. l. 313; Please specify if  $\Delta x = \Delta y$ .

*Done.*

- pp.23. Figure 12, please specify units in geometry parameters.

*Done in the caption. It also appears in the axis labels.*

- pp.26 l. 335; "...homogeneous, inviscid, and..." is it inviscid, or have viscous terms been included as stated in pages 14 and 23? Please. correct.

*It is inviscid. The included "Viscous terms" consist of a standard technique to simulate the dissipation of energy associated with breaking waves that allow correct treatment of breaking bores.*

- pp.26 l. 355-356; The last sentence should be supported with results from full N-S models, otherwise I suggest to eliminate.

*Done.*

- A couple of examples of typos that need correction: *No need to correct them, as they were not in the previous version of the paper*

- pp. 1, Abstract; "The US National Tsunami has proposed the experimental data used Hazard and Mitigation Program (NTHMP) and established for the NTHMP Landslide Benchmark Workshop, held in January 2017 at Galveston."

*Not present in the version at the NHESS system. Corresponds to an older version*

- pp. 2 l. 29; "...Multilayer-HySEA..."

*Same thing. Not in the current version.*

- pp.10 l. 163; "...non-conservative hyperbolic system underlying system..."

*Not present in the current version.*

- pp. 21 l. 278; "Tesla P100 GPU In can be.."

*Not present in the current version.*

Anonymous Referee #2

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Regarding Figure 6 description in the text (now is Figure 5) we agree with the reviewer comment, and we have changed "excellent" by "good" agreement.

About the more fundamental observation regarding "Code availability", the version of the code actually used to perform all the benchmarks presented in the present study can be downloaded from our web page (as we already do with the open-source of Tsunami-HySEA since 2016). The section "Code and data availability" now stands as follows:

"The numerical code used to perform the numerical simulations in this paper is available at HySEA codes web page at <https://edanya.uma.es/hysea/index.php/download>.

All the data used in the present work and necessary to reproduce the experiments set-up of the numerical experiments and the laboratory measured data to compared with, can be downloaded from [8] at the web site <http://www1.udel.edu/kirby/landslide/>. Finally, the NetCDF files containing the numerical results obtained with the Multilayer-HySEA code can be found and download from [10]."

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