

The authors thank the reviewers for a very detailed reading of the paper and substantive comments that have clearly improved the research and its presentation. Below are the original comments in italics and our responses below them.

Anonymous Referee #1

Received and published: 3 March 2020

This paper compiles historic datasets on land cover, topography and coastal water levels and combines these with statistical and coastal models of extreme water levels and storm tides to understand how human modifications have changed the signal of extreme water levels in Jamaica Bay between 1870 and now. The paper is well-written and addresses a highly relevant topic.

My main comments on the paper are:

1. the authors should include at least 1 paragraph outlining the underlying processes incorporated by the seCOM model. While this information exists in the cited publications (e.g. Orton et al., 2016), it will be helpful to have some of this information in this paper as well.

Change made – We have added a paragraph that elaborates on the model:

“The Stevens Estuarine and Coastal Ocean Model (seCOM) is a free-surface, hydrostatic, primitive equation model, with terrain-following (sigma) vertical coordinates, set on an orthogonal, curvilinear Arakawa C-grid (Georgas and Blumberg, 2010; Blumberg et al., 1999). The model has been further developed with regard to wind stress formulations (Orton et al., 2012), coupled wave modeling (Georgas et al., 2007), and land wetting and drying (Blumberg et al., 2015). It has been used to provide validated and accurate ensemble 3D storm tide predictions as part of the NY Harbor Observation and Prediction System (NYHOPS; Georgas and Blumberg, 2010) and the Stevens Flood Advisory System (Jordi et al., 2018). Typical errors in hindcasts of extreme storm tides (e.g. Hurricane Sandy) are 0.15-0.20 m (Orton et al. 2016).”

2. In Section 2.3, the authors should include a few sentences describing how the synthetic storm set from Orton et al., 2016b was abbreviated for the purposes of this study. How were the random tide permutations for the ETCs or the storm tide events for the TCs abbreviated?

Changes were made to give more detail, revising the text to read:

“The abbreviated set of 80 ETCs includes all the same storm events, but fewer random tide permutations for each storm. Instead of 50 simulations for the top 19 historical ETC storm tide events, there were 5 or 10 simulations each for the 11 highest ETC storm tides that are most relevant for the 5-year and higher return periods. The abbreviated set of 64 TCs includes a range of storm tide events from low to high magnitude (1.5 to 6.0 m). Model results for simulated TC events at a given magnitude are then used as a proxy for all the events at that magnitude, thus representing all 606 storms.”

3. I recommend moving the results from the leverage experiments described in Section 4.3. to Section 3, Results.

Change made – I kept hearing this and capitulated – see Section 3.3. The methods were also moved to the methods section (Section 2.4).

4. Sentence on Page 3, L13 is incomplete.

Change made, fixing the error.

The authors thank the reviewers for a very detailed reading of the paper and substantive comments that have clearly improved the research and its presentation. Below are the original comments in italics and our responses below them.

Carmine Donatelli (Referee)

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Received and published: 20 April 2020

I have read with great interest the paper entitled: ‘Storm Tide Amplification and Habitat Changes due to Urbanization of a Lagoonal Estuary’, by Orton et al.

The manuscript is very well written and organized, the used methodology is robust and supported by the clearness of the presented data. Previous works are referenced appropriately.

I think this study represents an important contribution to our understanding of the mechanisms by which geomorphic changes alter the physical response of back-barrier estuaries to tides and low frequency actions. I recommend publication with minor revisions.

My minor comments/suggestions are listed below.

Pages 10-11: ‘The most dramatic land cover change is from large areas of fringing wetlands (light blue) to urbanized areas (red), but also the center of the bay has shifted from marshes to open waters (1 dark blue)’.

The influence of marsh loss on water levels is strongly related to the setting: marsh loss associated with lateral erosion vs. marsh loss associated with reclamation projects. Reductions in the basin planform area (wetland reclamation) increase water levels, while marsh retreat due to lateral erosion may have the opposite effect (in agreement with the analytical model of Keulegan, 1967 and 3D numerical modelling investigations, Picado et al., 2010; Donatelli et al., 2018). I would highlight/expand this point in the text.

Text was added to address this useful point –

These results are also consistent with prior studies that showed that the influence of lagoonal wetland loss on water levels is different when it comes to lateral erosion versus landfill reclamation. Reductions in the tidally-wetted area through wetland reclamation increase storm tides, while wetland retreat due to lateral erosion has the opposite effect (e.g., Donatelli et al., 2018; Picado et al., 2010).

Page 15: ‘It was previously established that the bay’s tide ranges have grown substantially (Swanson and Wilson, 2008), and we find similar results. Averaging high and low waters for daytime minima and maxima in 1878 over 37 days gives an observed tide range of 1.35 m, while observations for the entire year 2015 show a tide range

of 1.73 m. This increase of 28% is smaller than the prior estimate of the tide range change from 1899 to 2000 from Swanson and Wilson (2007), which was 1.16 m to 1.64 m or 41%. However, the 1878 measurements are for a location at mid-bay (Holland House), whereas the 1899 measurements are for the easternmost end of the bay (Inwood or Norton Point), where tide attenuation (e.g. due to narrow, shallow channels and wetlands) was likely more pronounced.'

I would move these lines into the Discussion section.

This paragraph actually gives results – it is the first time tide range changes are presented. Moreover, the discussion and primary paper focus is on the topic of storm tides. Thus, we have not made this change.

Page 16 (lines 11-14): I would expand these lines. Are the results for Jamaica Bay translatable to other systems? What systems?

Text was added to address this suggestion:

“Systems with likely impacts include those with substantial changes to inlets, mean estuary depths, or wetland landfill/reclamation, and may be detected by long-term changes to tides (Talke and Jay, 2020).”

Page 18 (lines 1-19): I would move the description of the idealized numerical experiments into the Methods section.

Change made – I kept hearing this and capitulated – see Section 2.4. The results were also moved to the results section (Section 3.3).

Page 21: I would mention Englebright [1975] and Harting et al., [2002], who show how inlet modifications have reduced the movement of offshore sediments into the backbarrier basin.

This suggested change was not made, as these studies were speculative about changes to the inlet's role in sediment import to the bay. I'd rather not further the speculation, because there is a study of sediment fluxes into the bay that I hear is in review.

The authors thank the reviewers for a very detailed reading of the paper and substantive comments that have clearly improved the research and its presentation. Below are the original comments in italics and our responses below them.

Anonymous Referee #3

Received and published: 27 April 2020

General comments: The paper entitled “Storm Tide Amplification and Habitat Changes due to Urbanization of a Lagoonal Estuary” by Philip M. Orton et al. analyzes the impacts of historic landscape changes within the 20th century in Jamaica Bay, New York City on present-day storm tide water levels. The results of this study reveal considerable effects of especially channel deepening on storm tide peak water levels within the bay, which is comparable to, and even exceeding, global mean sea level rise during the same period. The work carried out by Orton et al. is scientifically solid, well written and the presented results are highly relevant not only to Jamaica Bay, New York City, but also to many other highly populated and developed coastal areas around the globe. The methods are generally sound (some issues are listed below) and the conclusions are supported by the presented data. I recommend publication of this article with minor revisions.

My detailed comments are listed below:

Page 7, lines 15 – 19: I think this part needs some clarification. I would doubt that the landward edge of a saltmarsh equals the extent of high tide flooding. This would mean that the marsh gets completely flooded during most of the tides, which should not be the case. The upper edge of the high salt marsh is usually only flooded during storm tides or the highest spring tides. What are the implications of this approach to the validity of the results? Something, which could also be taken up in the discussion.

The text was unclear, and changes have been made to clarify. We actually did use the annual highest astronomical tide (HAT) as the elevation of the upper edge of the high salt marsh. HAT was estimated using 1840s tide data from a nearby location with a similar tide range (Governor’s Island, New York Harbor). Text has been revised to change “high tide flooding” to read “highest astronomical tide flooding”.

Page 7, line 29: How was the digitized bathymetric and topographic data resampled in order to meet the named 30 m grid resolution (line 2 page 6)? Which resampling technique was used (e.g. bilinear, nearest or cubic etc.)?

Change made to clarify – Bilinear interpolation was used, and this word is added to the text at that location.

Page 8, lines 7 – 9: Briefly outlining the methodology used to simulate the ensemble of storm tides would help the reader. You could still write that a detailed description is

given in Orton et al. 2016b.

Change made - the detailed description is actually given in the subsequent section, and the text now refers to Section 2.3 for that information: "A hydrodynamic model was applied to the historical and modern "landscapes" (land surface elevation and roughness) and used to simulate an ensemble of storm tide events described in Section 2.3."

Page 8, lines 9-12: I would appreciate some more information on the functioning and structure of the model sECOM. What exactly does accurate mean? Can you provide an estimate of the error associated with it?

Changes made –

"The Stevens Estuarine and Coastal Ocean Model (sECOM) is a free-surface, hydrostatic, primitive equation model, with terrain-following (sigma) vertical coordinates, set on an orthogonal, curvilinear Arakawa C-grid (Blumberg et al. 1999; Georgas and Blumberg, 2010; Orton et al. 2012) ... Typical errors in hindcasts of extreme storm tides (e.g. Hurricane Sandy) are 0.15-0.20 m (Orton et al. 2016)."

Page 8, lines 39-42: Does this mean you have assigned a single Manning n coefficient to both eelgrass and saltmarsh vegetation? In the literature there are many studies suggesting Manning n coefficients of 0.07 (Lawrence et al. 2004) or up to 0.08 for saltmarsh surfaces (Stark et al. 2016, 2017; Temmerman et al. 2012) and I assume that the roughness of seagrass beds should be considerably less. What was the decision to take a value of 0.045 based on? What is the sensitivity of your model to variations in these coefficients?

A model simulation was performed to quantify the uncertainty. We were unable to find a Manning's-n number in the literature for eelgrass (*Zostera Marina*). As eelgrass and other macrophytes are widely accepted to reduce flow rates, we chose a simple route and set the Mannings number to be the same as *Spartina Alterniflora*. In retrospect, I agree that a lower value could have been better. To address the resulting possible bias, I ran an experiment to quantify the effect on one sample 100-year storm tide event, a hurricane, and found the maximum difference occurred in the northern bay and was a reduction of 8 millimeters for peak storm tide. This is because the eelgrass area is only 32% of the bay interior benthic substrate (below MSL elevation), and the flow during a 100-year storm tide event is 3-4m deep over this roughened surface. I conclude that the choice of a high eelgrass mannings-n value does not significantly alter our results, nor the main conclusions of the paper.

I think answering these questions is important, since you state that the "most dramatic land cover change is from large areas of fringing wetlands (light blue) to urbanized areas (red)"

(page 10, lines 43 – 44) and because artificially recovering the wetlands in your model has only resulted in a reduction of peak storm surge heights of -2% (page 18 lines 26-28). On the other hand, increasing Manning n coefficients to 0.025 for scattered areas of lost eelgrass resulted in a peak reduction of 3%. This needs some further explanations.

You are correct in your expectation that recovering fringing wetlands would reduce storm tides significantly and that is shown in the paper (Fig. 8) -- the experiment you are referring to where there was a reduction of only 2% was for “interior” wetlands in the center of the bay, not fringing wetlands. This is explained in the manuscript as being a result of the deep channels running around these wetlands, so that storm tides do not need to pass over them to reach neighborhoods. The experiment restoring fringing wetlands actually reduced the hurricane storm tide more, by 13% (see same section of text). The experiment where bottom roughness was raised to 0.025 across all seabed areas within the bay led to a reduction in the hurricane storm tide of 3%, but I note that this was not just scattered restoration of eelgrass, this was across-the-bay increase in benthic roughness.

The manuscript was modified to be clearer on all these points:

“For example, extensive wetland restoration in the center of the bay (not the fringing wetlands) leads to a change in peak storm tide of only -2%, because deep shipping channels around the wetlands are the primary conduit for flood waters (Orton et al., 2015). A small rise in Mannings-n across the entire bay’s seabed from 0.020 to 0.025 (mimicking scattered areas of lost eelgrass, sand bedforms or shells) reduced the peak by -3%. The other changes also had relatively minor effects.”

Page 14, lines 17-20: Please consider moving this sentence to the discussion section, as you start interpreting your results here.

Change accepted – this text was moved to the end of section 4.1.

Page 15, lines 25 – 33: This part should be moved into the discussion too.

This paragraph actually gives results – it is the first time tide range changes are presented. Moreover, the discussion and primary paper focus is on the topic of storm tides. Thus, we have not made this change.

Page 20, lines 40-41: I suggest rephrasing this sentence to make it a little clearer: It is not the sunlight that is reduced but due to increased turbidity, the light penetration into the water column is reduced.

Change made, revising to:

“They are known to decline in eutrophic conditions due to the reduced sunlight that results from increased turbidity”

Figure 4: Perhaps it is just due to the system that created the pdf file, but the legends of both maps are very hard to read. Please check and increase the size of the key.

Change made, increasing the legend on each panel by 25% in size.

Literature

Lawrence, D.S.L.; Allen, J.R.L.; Havelock, G. M. (2004): Salt Marsh Morphodynamics: an Investigation of Tidal Flows and Marsh Channel Equilibrium. In: Journal of Coastal Research 20 (1); p. 301-316

Stark, Jeroen; Plancke, Yves; Ides, Stefaan; Meire, Patrick; Temmerman, Stijn (2016): Coastal flood protection by a combined nature-based and engineering approach. Modeling the effects of marsh geometry and surrounding dikes. In: Estuarine, Coastal and Shelf Science 175; p. 34-54.

Stark, J.; Smolders, S.; Meire, P.; Temmerman, S. (2017): Impact of intertidal area characteristics on estuarine tidal hydrodynamics. A modelling study for the Scheldt Estuary. In: Estuarine, Coastal and Shelf Science 198; p. 138-155.

Temmerman, Stijn; Vries, Mindert B. de; Bouma, Tjeerd J. (2012): Coastal marsh dieoff and reduced attenuation of coastal floods. A model analysis. Global and Planetary Change 92-93; p. 267-274.

1 **Storm Tide Amplification and Habitat Changes due to Urbanization of a Lagoonal Estuary**

2
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1 **Abstract**

2 In recent centuries, human activities have greatly modified the geomorphology of coastal
3 regions. However, studies of historical and possible future changes in coastal flood extremes
4 typically ignore the influence of geomorphic change. Here, we quantify the influence of 20th
5 Century manmade changes to Jamaica Bay, New York City, on present-day storm tides. We
6 develop and validate a hydrodynamic model for the 1870s, based on detailed maps of
7 bathymetry, seabed characteristics, topography, and tide observations, for use alongside a
8 present-day model. Predominantly through dredging, landfill, and inlet stabilization, the
9 average water depth of the bay increased from 1.7 to 4.5 m, tidal surface area decreased from
10 92 to 72 km², and the inlet minimum cross-sectional area expanded from 4800 to 8900 m².
11 Total (freshwater plus salt) marsh habitat area has declined from 61 to 15 km² and intertidal
12 unvegetated habitat area from 17 to 4.6 km². A probabilistic flood hazard assessment with
13 simulations of 144 storm events reveals that the landscape changes caused an increase of 0.28
14 m (12%) in the 100-year storm tide, even larger than the influence of global sea level rise of
15 about 0.23 m since the 1870s. Specific anthropogenic changes to estuary depth, area and inlet
16 depth and width are shown through targeted modeling and dynamics-based considerations to
17 be the most important drivers of increasing storm tides.

18

19 **Keywords:** Estuary; storm surge; geomorphology; habitat; hazard assessment; dredging;
20 landfill; Jamaica Bay, New York

21

22 **1. Introduction**

23

24 The characteristics of storm tides and the probability of flooding depend on both far-field
25 forcing (meteorological, tidal) and on local characteristics (bathymetry, bottom roughness,
26 floodplain size). Therefore, changes to local mean sea level, shipping channel depths, wetland
27 land cover, and storm intensities, sizes, speeds, and tracks can all potentially alter system
28 response and flood probabilities. Recent non-stationary, probabilistic hazard assessments have
29 demonstrated spatially coherent variability in common storm tides (Marcos et al., 2015), as well
30 as extreme storm tides (Wahl and Chambers, 2016), and have begun revealing the climate
31 modes (e.g., NAO and ENSO index) that modulate storm tides in some regions. Similarly, long
32 term cycles in astronomic forcing (e.g., the 18.6-year nodal cycle) affect both nuisance flooding
33 (Ray and Foster, 2016) and the probability of high impact events (Talke et al., 2018). In some
34 estuaries, such as Boston Harbor, flood hazard remains statistically stationary after accounting
35 for sea-level rise and tidal variability (Talke et al., 2018). In others, flood hazard is non-
36 stationary. For example, a recent study of New York Harbor (NYH) showed an increase in the
37 10-year storm tide of 0.28 m since the mid-1800s in addition to the local relative sea level rise
38 of 0.44 m (Talke et al., 2014).

39

40 Climatic and astronomical variability in hydrodynamic forcing coincides with several centuries
41 of human-induced geomorphic change to estuaries and harbors (e.g., Sanderson, 2009;
42 Grossinger, 2001; Talke et al., 2018; Jaffe et al., 1998). Wetlands have been reclaimed; in NYH, a

1 typical case, approximately 80% of pre-development wetlands have been lost (USACE, 2009).
2 Harbors and estuaries have been deepened, with the controlling depth of channels often
3 doubled or even tripled (Orton et al., 2015; Familikhalili and Talke, 2016; Ralston et al., 2019;
4 Helaire et al., in press; Chant et al., 2011). Coastal boundaries have been hardened and raised,
5 preventing overland flooding except in extreme cases. Natural wave breakers have been
6 destroyed, including oyster reefs that may have once reduced coastal wave energy in New
7 York's outer harbor by between 30 and 200% (Brandon et al., 2016).

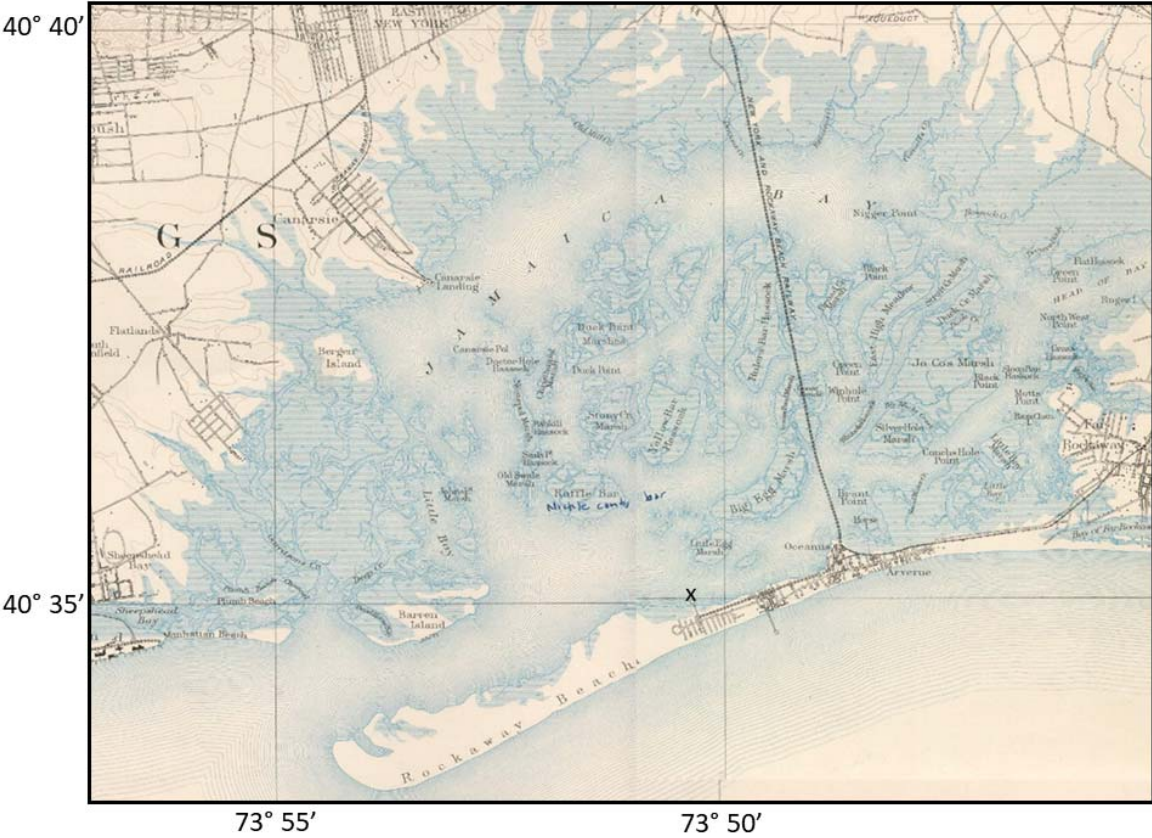
8
9 The sum effect of changing bathymetry is an altered hydrodynamic regime, with effects on
10 astronomical tides, storm surges, and morphodynamic feedbacks (e.g., de Jonge et al., 2014;
11 Chernetsky et al., 2010; Talke and Jay, 2020). A study of the Cape Fear Estuary showed that tide
12 range had doubled since the 1880s in Wilmington, NC, due to a doubling of the shipping
13 channel. Moreover, idealized modeling showed ~~that~~ a ~0.5 to 2 m storm surge increase at
14 Wilmington across a variety of hurricane intensities (Familikhalili and Talke, 2016). Model
15 simulations of Hurricane Katrina's flooding with present-day versus estimated historical
16 conditions (ca. 1900) suggest that wetland loss exacerbated flooding well beyond the influence
17 of sea level rise (Irish et al., 2014). Within the Hudson River estuary, Ralston et al. (2019)
18 showed that a doubling of channel depth near Albany (NY) more than doubled tide range and
19 increased the magnitude of storm surge compared to 19th century conditions. Within New York
20 Harbor, deepening of the inlet produced a smaller shift in the lunar semidiurnal tidal
21 constituent amplitude of 7% at The Battery (Ralston et al., 2019). Within nearby Newark Bay
22 and the Passaic River, tides have been amplified by ~10% over the past century, reflecting a
23 change in the controlling channel depth at some locations from ~3 to 15 m (Chant et al., 2011).
24 In parts of Jamaica Bay, another sub-embayment of New York Harbor, tide range changes are
25 much larger and have grown by 41%, from 1.16 m in 1899 to 1.64 m in 2007 (Swanson and
26 Wilson, 2008). Numerical experiments within Jamaica Bay suggest that individual storm tide
27 events such as Hurricane Sandy are quite sensitive to depth modifications (Orton et al., 2015).
28 However, the implications of historical channel deepening and land cover changes on flood
29 hazard have not yet been quantified through a probabilistic assessment.

30
31 In this contribution, we investigate the influence of extreme changes in bathymetry and
32 wetland cover on storm tide hazard. Jamaica Bay, New York, was a back-bay lagoonal system
33 that was converted to a deepwater port (Sanderson, 2016; Swanson and Wilson, 2008; Seavitt
34 et al., 2015; Swanson et al., 2016). Although the system's morphology was evolving in the 18th
35 and 19th centuries and possibly earlier, the most dramatic alterations occurred in the early 20th
36 century (Black, 1981). The Jamaica Bay Improvement Commission (1907) proposed to
37 reconfigure the bay into a port (**Figs. 1-2**), and The River and Harbor Acts of 1910 and 1925 set
38 in motion a plan to reconfigure the entrance channel to a depth of at least 9 m and width of
39 450 m, protected by jetties. Groins were placed along the seaward-side of the Rockaway
40 Peninsula (labeled in Fig. 1 as "Rockaway Beach") and a jetty constructed at the tip to stabilize
41 the barrier island (Hess and Harris, 1987). The bay's perimeter channels were extensively
42 dredged for several decades, and dredged sediments were used for landfill development over
43 the fringe wetlands surrounding the bay, creating neighborhoods and the Floyd Bennett Field
44 airport (Black, 1981). At mid-century, additional dredging and landfill occurred at the

1 northeastern end of the bay, for creation of John F. Kennedy (JFK) International Airport, leaving
2 “borrow” pits that today are up to 15 m deep. As the 20th Century progressed, the port was
3 never realized, and the primary port for the region ended up across New York Harbor in Newark
4 Bay.

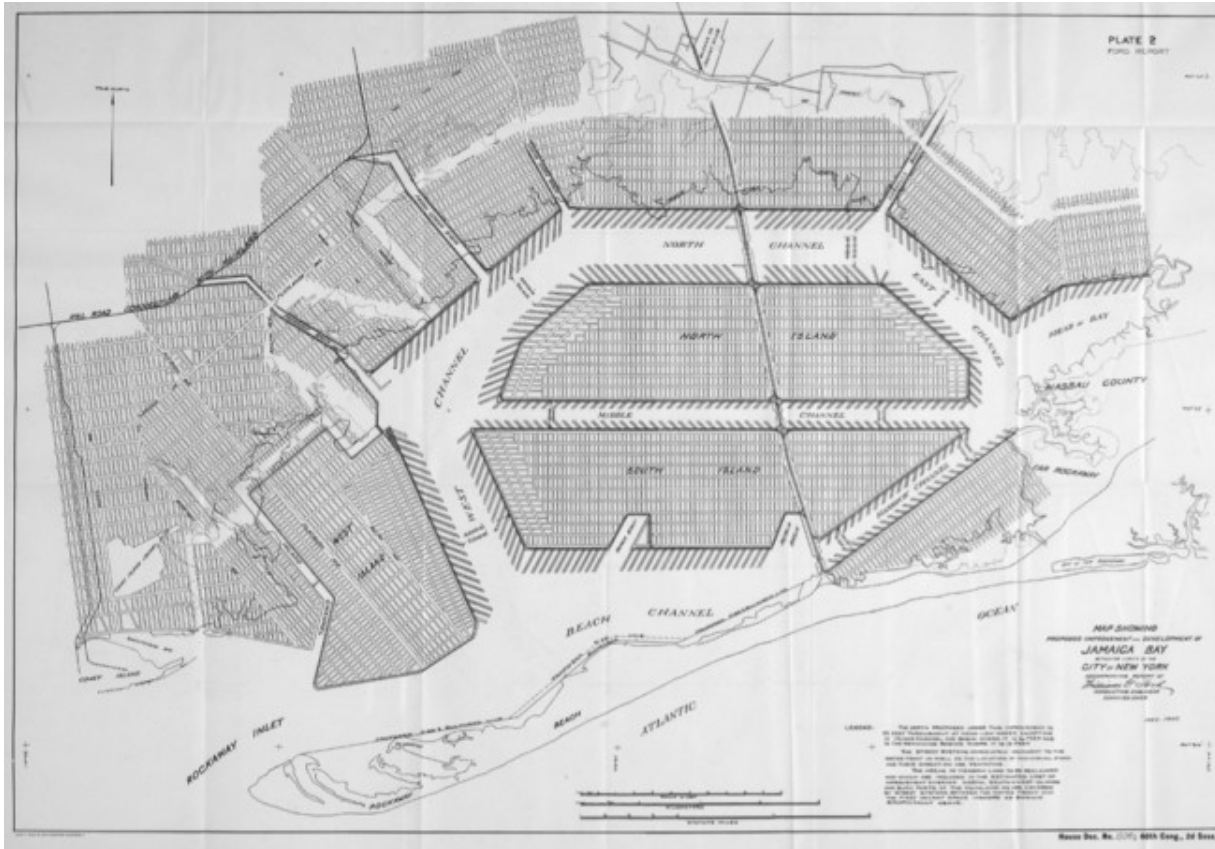
5
6 Here we present a quantitative assessment of Jamaica Bay landscape changes and use
7 retrospective modeling to estimate the impacts on storm tides and flooding. A detailed
8 hydrodynamic model of the 1870s was developed based on maps of bathymetry and seabed
9 characteristics, for use alongside an existing present-day model. Modeling of 144 storm tide
10 events for both the 1870s landscape and the present-day landscape is used to develop a
11 probabilistic flood hazard assessment. We show that manmade geomorphic changes in Jamaica
12 Bay have produced an important and heretofore under-appreciated and unquantified increase
13 in storm tides. Given the environmental and societal value of the Jamaica Bay wildlife refuge,
14 JFK Airport, the Gateway National Recreation Area, several city and state parks, and the lives of
15 the hundreds of thousands of people in flood zones around the bay, our results have
16 implications for the future management of the system.

17



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20 **Figure 1:** An 1888-1889 survey map of Jamaica Bay, in southeast New York City, portraying the
21 morphology and marsh cover (blue hatching). The map is excerpted from Powell (1891) and the
22 “X” marks the Holland House pier tide measurement location.

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4 **Figure 2:** Plan for converting Jamaica Bay into a port (Jamaica Bay Improvement Commission,
5 1907)

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8 **2. Methods**

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To evaluate how and why flood hazard has changed due to landscape changes in Jamaica Bay (see Results), we applied a quantitative approach—the use of numerical models to produce a probabilistic hazard assessment (e.g., Orton et al., 2016)—to both the historical (1870s era) and modern bathymetries and landscapes of Jamaica Bay. Below, we describe our landscape reconstruction (2.1), our modeling approach (2.2), and our hazard assessment methodology (2.3), and the set of experiments designed to isolate the specific landscape changes that result in growing storm tides (2.4).

16

17 **2.1 Jamaica Bay landscape reconstructions**

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Although maps and charts of the Jamaica Bay landscape extend back to the 17th century (Sanderson, 2016), the first thorough bathymetric and topographic maps were made by the US Coast Survey between the 1840s and 1870s. The first tidal measurements also date from this period (e.g., Talke and Jay, 2013). Because the 1870s time period pre-dates most channel deepening, this period constitutes a good proxy for conditions prior to major 20th century anthropogenic modifications.

1
2 To develop numerical models of the “present-day” and 1870s conditions, we first created
3 digital elevation models and land cover maps at 30 m resolution. The domain extends eastward
4 and northward to land up to 6 m navd88 elevation, and extends westward past Coney Island.
5 The landscape reconstruction from the 1870s forms a way-point between the pre-European
6 landscape of c. 1609 and modern conditions (Sanderson, 2016). Since no bathymetric data are
7 available from before the 19th century, comparisons between the 1600s and 1800s are
8 qualitative (See **Sect. 4.3**).

9
10 *2.1.1 Present-day landscape*

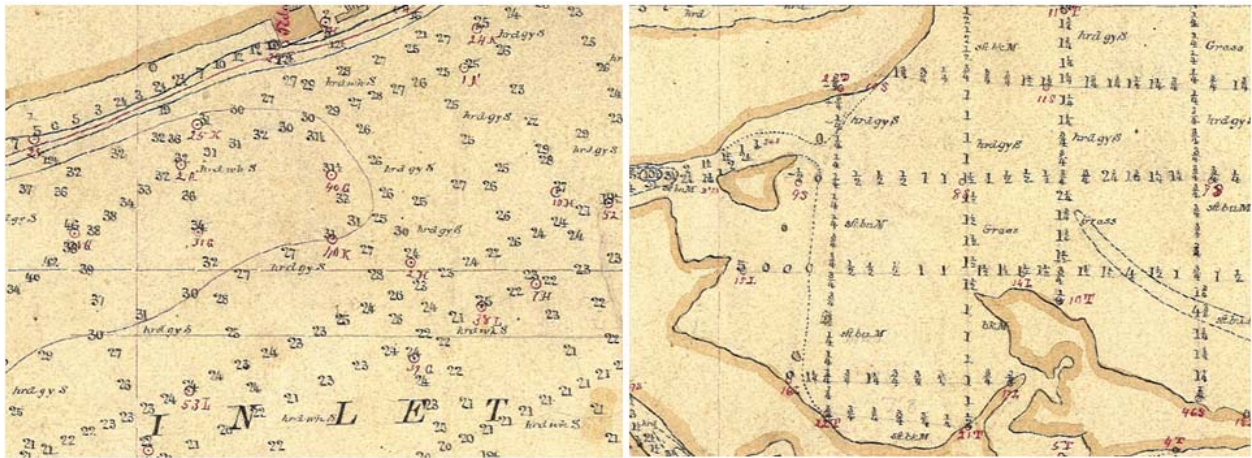
11 The present-day digital elevation model is based (by order of preference) on United States
12 Geological Survey (USGS) bathymetric/topographic data collected by LIDAR in 2013–2014,
13 slightly older data collected in 2007-2008 by Flood (2011), and older National Oceanic and
14 Atmospheric Administration bathymetric survey data for a few remaining small areas of the
15 Bay. The LIDAR data cover dry land, marsh islands, and shallow waters (shallower than
16 approximately 2 m) and the Flood (2011) data cover the navigation channel and other deep-
17 water regions. Bare-earth land elevations in populated areas are based on 2010 New York City
18 LiDAR data. Present-day land cover data for the Jamaica Bay watershed at 30 m resolution are
19 from the 2011 National Land Cover Dataset (NLCD), as described in Homer et al. (2015).

20
21 *2.1.2 Historical landscape data*

22 Bathymetric and benthic character data for the 1870s model are from a pair of H-sheets from
23 1877 and 1878 for Jamaica Bay: Maynard (1877) and Moore (1878). The Maynard (1877) survey
24 was drawn at 1:5,000 scale, while the Moore (1878) survey was drawn at a scale of 1:10,000.
25 Both show grids of depth surveys, with parallel lines approximately 100 m apart, and with
26 sounding data approximately every 20 m (**Fig. 3**). Moore (1878) includes depth contour lines
27 that mark out channels between the marshy islands and other underwater features. While
28 earlier H-sheets depicted the bathymetry of Rockaway Inlet and Broad Channel, the Maynard
29 (1877) and Moore (1878) manuscript maps are the first to depict the bathymetry of the entirety
30 of Jamaica Bay. Approximately 20,000 individual sounding points were digitized to describe the
31 interior of the bay. Raw data were corrected for tidal stage and reduced to the Mean Low
32 Water datum, based on local tide gauge measurements. Since we have recovered and digitized
33 these hand-collected tide records from the US National Archives (see e.g., Talke and Jay, 2017),
34 we are able to validate our model results for the historical model against contemporary 1870s
35 data (see **Sect. 2.2**).

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37 Topographic and land-cover data were digitized and synthesized from T-sheets and other
38 surveys drawn by Bien and Vermule (1891b), Bache (1882), Bien and Vermule (1891a), Dorr
39 (1860), Gilbert (1855), Gilbert (1856a), Gilbert (1856b), Gilbert and Sullivan (1857), Jenkins
40 (1837b, a), Powell (1891), and Wilson (1897). Historic maps and charts were georeferenced
41 using a first order rectification to the modern city grid with less than 50 m root mean square
42 error, using control points located at road intersections, buildings, railroads, or other features
43 that are present historically and can be located today. To reduce to a common datum and

- 1 assess temporal evolution, we tracked the datum of each map or chart and the publication
- 2 date.



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5 **Figure 3:** Detail view of two portions of the 1877 survey dataset (left) at Rockaway Inlet (at
6 bottom left of **Figs. 1-2**) and (right) a shallow bay area with mud, sand and grass areas
7 (Maynard, 1877). Shown are measured depths (in feet) and bottom characterization notes (e.g.
8 “sft” for soft, “hrd” for hard, “gy” for gray, “S” for sand, “M” for mud, and “Grass” likely for
9 eelgrass beds), with typical spacing of 100-150 m. The mapped area on the right is now covered
10 by fill and a former airport, Floyd Bennett Field.

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13 Because historical surveys usually neglected intertidal areas, we use inferential techniques to
14 approximate the historical elevations within this region, using known plant-cover data.
15 Specifically, the present-day vertical zonation of salt marshes around New York City was used to
16 approximate the historical elevation of marshes. The seaward extent of salt marsh was
17 assumed to represent the mean sea level (the lower edge of the low salt marsh; Edinger, 2014),
18 while the landward edge was assumed to represent the extent of highest astronomical tide
19 flooding (the upper edge of the high salt marsh; Edinger, 2014). Locations where maps showed
20 a contour between low and high salt marsh were assigned an elevation equal to mean high
21 water.

22 Vertical datum adjustments were made by relating the topographic zero of each map and chart
23 to the relative sea level reconstruction (RSL) provided by Kemp & Horton (2013). They studied
24 foraminiferal assemblages over the past two centuries from salt marsh sediment in nearby
25 Barnegat Bay, New Jersey. Their results were used to identify RSL in the southern coastal New
26 York City at the time the map or chart represents. To estimate the NAVD88 elevation of the
27 topographic zero for the map, we noted that the Kemp & Horton (2013) study places the 0 level
28 of their RSL reconstruction at 0.10 meter above mean sea level in Barnegat Bay, which was
29 converted to NAVD88 using NOAA Tides & Currents adjustment values for Barnegat Inlet
30 (Station 8533615).

1 Raster digital elevation models (DEM) were created in ArcGIS 10.3 with the “Topo to Raster”
2 interpolation method to create hydrologically correct DEMs (ESRI, 2016). In addition to contour
3 line and point elevation data, historical stream and pond data were also added. To preserve the
4 winding characteristics of marsh creeks during the interpolation, creek beds were converted to
5 point features and their elevation was set at the Mean Low Water datum of the appropriate
6 date.

7 **2.2 Flood and tide modeling and validation**

8 A hydrodynamic model was applied to the historical and modern “landscapes” (land surface
9 elevation and roughness) and used to simulate an ensemble of storm tide events described in
10 Section 2.3 following the methodology of Orton et al. (2016b). The Stevens Estuarine and
11 Coastal Ocean Model hydrodynamic model (sECOM) is a free-surface, hydrostatic, primitive
12 equation model, with terrain-following (sigma) vertical coordinates, set on an orthogonal,
13 curvilinear Arakawa C-grid (Georgas and Blumberg, 2010; Blumberg et al., 1999). The model has
14 been further developed with regard to wind stress formulations (Orton et al., 2012), coupled
15 wave modeling (Georgas et al., 2007), and land wetting and drying (Blumberg et al., 2015). It
16 provides has been used to provide validated and accurate (Georgas et al., 2014; Orton et al.,
17 2012) ensemble 3D storm tide predictions as part of the NY Harbor Observation and Prediction
18 System (NYHOPS; Georgas and Blumberg, 2010) and the Stevens Flood Advisory System (Jordi
19 et al., 2018). Typical errors in hindcasts of extreme storm tides (e.g. Hurricane Sandy) are 0.15-
20 0.20 m (Orton et al. 2016).

21
22
23 The Jamaica Bay model grid was a 30 by 30 meter, square-cell grid (Orton et al., 2015). This grid
24 was doubly-nested inside two larger model domains that represent (1) the regional coastal
25 ocean and estuaries from Maryland to Cape Cod, and (2) the Atlantic Ocean from Cape Hatteras
26 to Nova Scotia (Orton et al., 2016b). Storm meteorological forcing for the regional and large-
27 scale grids was spatially and temporally variable, and is described in Orton et al. (2016b) and
28 the next section.

29
30 Simplifying assumptions are used for the model simulations on the Jamaica Bay grid for
31 computational efficiency in simulating a large number of storms. While the regional coastal and
32 estuary modeling used 3D simulations, the model’s two-dimensional (2D) mode was used for
33 Jamaica Bay (e.g., Orton et al., 2015). This is a common practice in estuary storm tide modeling
34 (Familkhalili and Talke, 2016; Kennedy et al., 2011). While stratification can have a small
35 influence on storm tides in stratified estuaries (Orton et al., 2012), Jamaica Bay has limited
36 freshwater input and weak stratification (Marsooli et al., 2018). A wave model is not coupled
37 with the Jamaica Bay hydrodynamic modeling, for computational efficiency and because our
38 focus here is on storm tides and “still water” elevations. The broad shallow continental shelf at
39 the Apex of New York Bight leads to relatively small impacts of waves on estuary storm tide
40 temporal maxima (e.g. due to wave set-up; Marsooli and Lin, 2018; Lin et al., 2012). Lastly, the
41 time-varying meteorological forcing was assumed spatially constant on the Jamaica Bay grid,
42 because the bay is only ~10 km wide.

1 The gridded land elevation and land cover type datasets for the 1870s and present-day were
2 interpolated onto the model grid to create land elevation and Mannings-*n* roughness model
3 input files. The 30-meter resolution modeling does not resolve fine-scale features such as
4 elevated seawalls, though they are rare in this area. In 2D tide and storm surge modeling
5 studies, a common simplified approach (Irish et al., 2014; Mattocks and Forbes, 2008; Szpilka et
6 al., 2016) to representing the effects of wetlands and other natural features is to treat them as
7 enhanced landscape roughness features, through a variable called Mannings-*n*. Reasonable
8 estimates for Mannings-*n* values are 0.045 for intertidal wetlands and eelgrass (*Zostera Marina*)
9 beds, 0.020 for unvegetated continental shelf and estuary substrate, and 0.10 and 0.13 for
10 medium and high intensity developed land, respectively (Mattocks and Forbes, 2008). This
11 approach has previously been applied to Jamaica Bay (Orton et al., 2015).

12
13 Depending on purpose, different mean sea-levels were used in the study. To determine habitat
14 and tidal datum changes, we run tide-only simulations using the mean sea level that existed for
15 a given landscape year. Storm simulations for both the modern and historic (1870s) period use
16 2015 mean sea level, to quantify the effect of landscape change on flood hazard and isolate this
17 process from the effect of sea level change. Mean sea level for the 1870s was -0.28 m (Kemp
18 and Horton, 2013) and in 2015 was +0.09 (based on smoothed recent trends), both relative to
19 the 1983-2001 MSL datum at The Battery (NOAA station 8518750). These values are -0.37 and
20 0.00 m NAVD88, respectively, based on conversions for the Jamaica Bay Inwood tide gauge
21 (USGS station 01311850). An elevated (or reduced) mean sea level was imposed as a constant
22 offset to a given simulation's offshore elevation boundary conditions at the edge of the Jamaica
23 Bay grid. This is a reasonable simplification here because recent work showed virtually no
24 change to tides at nearby Sandy Hook (NOAA station 8531680) when there is sea level rise
25 (below a 1% change to tide range per meter of sea level rise Kemp et al., 2017).

26
27 Tide-only simulations for 1878 were run for a 40-day period that overlapped with water level
28 observations made from 13 August 1878 through 21 September 1878 at a pier on the north side
29 of the Rockaway Peninsula (**Fig. 1**). The tide simulation for the present-day covers a 35-day
30 period from 1 August 2015 through 5 September 2015. Since wind-forcing during the late
31 summer is typically weak, these tide-only simulations are useful for direct validation of the
32 model.

33
34 Model validations were performed for the 1870s era model, and the present-day model was
35 previously validated (Orton et al., 2015). The prior storm validation of the present-day model
36 for Hurricane Sandy showed a time series RMSE of 20 cm and high water mark RMSE of 19 cm
37 (Orton et al. 2015). The tidal validations here use summertime periods without strong wind
38 influences, and modeled time series were compared to observations for both 1878 and 2015
39 using RMS error and the Willmott skill (e.g., Warner et al., 2005). The 2015 period included
40 7920 samples taken at 6-minute intervals over a 33-day period at the Inwood USGS gauge
41 station. The 1878 period included only daytime measurements, with 2438 samples taken at 10-
42 minute intervals over a 37-day period at the Holland House pier on the north side of Rockaway
43 Peninsula. The mean error is subtracted before computing statistics to account for possible
44 remote sea level anomalies or steric sea level variations, and because the 1878 tide staff datum

1 is poorly known. The results for the tide modeling time series validation for 1878 were 0.09 m
2 RMS error and 0.991 skill, while the results for the 2015 period were 0.09 m RMS error and
3 0.989 skill.

4
5 Historic and modern tidal datums, tidally wetted area and intertidal zones were assessed by the
6 following methodology. First, simulated water levels after a 2 day spin-up period were
7 harmonically analyzed (Pawlowicz et al., 2002) at historic gauge locations. A year-long synthetic
8 tide time series was then produced, using appropriate nodal corrections, and once and twice-
9 daily water level minima and maxima were compiled and averaged to compute tidal datums
10 such as MLLW and MHHW. The tidally-wetted area was then defined as the area wetted at high
11 tide in Jamaica Bay after MHHW conditions at Rockaway Inlet. The intertidal area is similarly
12 defined as the difference between the tidally-wetted area and the area flooded at the low tide
13 occurring after a predicted MLLW tide at Rockaway Inlet.

14 15 **2.3 Probabilistic flood hazard assessment**

16 A probabilistic flood hazard assessment was used to quantify the annual probabilities of
17 exceedance (or inversely, the return periods) for any given storm tide. We applied the storm set
18 and statistical framework utilized by Orton et al. (2016b), which employed a joint probability
19 method of flood hazard assessment that is an ensemble simulation of a diverse set of possible
20 storms (the storm climatology) including both synthetic tropical cyclones (TCs; e.g. hurricanes)
21 and historical extratropical cyclones (ETCs; e.g. nor'easters). The synthetic TCs spanned all
22 combinations of a complete range of intensities (6 bins), sizes (3), speeds (3), landfall locations
23 (5) and angles (3), and each simulated TC had an estimated annual frequency of occurrence
24 based on an extensive simulation with a statistical-stochastic TC model (Hall and Yonekura,
25 2013). The wind and pressure meteorological forcing for ETCs was historical reanalysis data
26 from Oceanweather, Inc., whereas the forcing for TCs came from simplified parametric TC
27 models. The assessment methods were validated by comparison to historical data at multiple
28 levels of the study, demonstrating unbiased storm tide simulations and storm tide hazard
29 estimates (versus return period), relative to historical events (Orton et al., 2016b). Additional
30 details of the assessment, including historical data, validations, storm climatology development,
31 statistical analysis and uncertainty quantification are given in Orton et al. (2016b). The storm
32 tide modeling results from the larger-scale model grids in this prior study were applied as
33 offshore boundary conditions to the Jamaica Bay domain simulations for the present study.

34
35 Some simplifications of the application of the Orton et al. (2016b) flood hazard assessment to
36 our Jamaica Bay submodels are noted here. The prior flood hazard assessment included 1516
37 storm simulations (606 TCs, and ~~96140~~ ETCs), but we use an abbreviated storm set to reduce
38 the computational expense. The abbreviated set of 80 ETCs includes all the same storm events,
39 but fewer random tide permutations for each storm. Instead of 50 simulations for the top 19
40 historical ETC storm tide events, there were 5 or 10 simulations each for the 11 highest ETC
41 storm tides that are most relevant for the 5-year and higher return periods. The abbreviated set
42 of 64 TCs includes a range of storm tide events from low to high magnitude (1.5 to 6.0 m).
43 Model results for simulated TC events at a given magnitude are then used as a proxy for all the
44 events at that magnitude, thus representing all 606 storms. A statistical comparison of the

1 abbreviated versus full storm set showed minor differences of less than 5% across 5-year to
2 500-year storm return periods, validating our approach. The historic and modern model
3 landscapes are subjected to the same set of storms, and therefore any differences in storm tide
4 hazard reflect geomorphic changes rather than artifacts of the simplified hazard assessment.

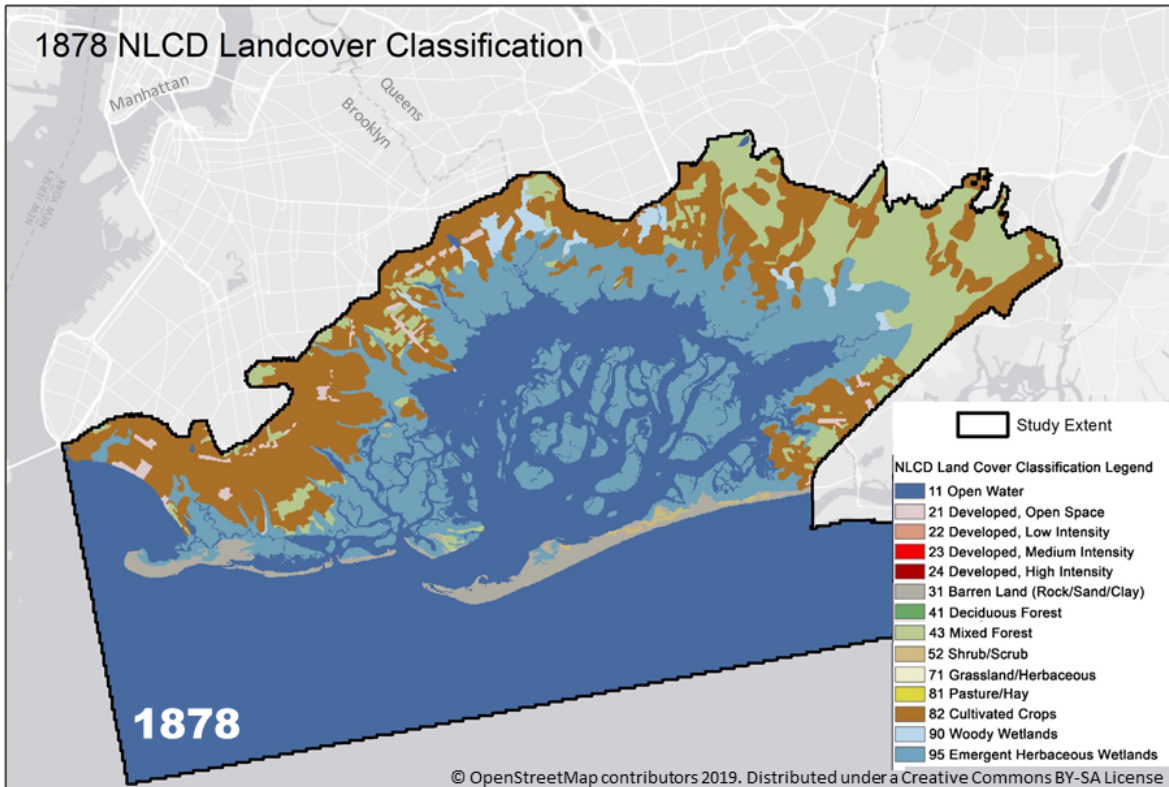
6 **2.4 Hurricane storm surge leverage experiments**

7 Simple “leverage experiments” were next used to isolate the effects of specific historical
8 landscape changes on the simulated water levels during a fast-moving, Category-3 hurricane
9 that approximates an event from 1821 (Orton et al., 2015). The storm surge from this hurricane
10 (3.4 +/- 0.4 m) likely exceeded the surge in hurricane Sandy (2.76 m), and produced water levels
11 of ~3m above 1821 mean sea-level despite occurring near low tide (Orton et al., 2016b).
12 Meteorological forcing for the simulations was created from parametric models (Orton et al.,
13 2015). The following experiments were performed using modifications to the modern-day
14 landscape to mimic the historical landscape’s main features one-by-one:

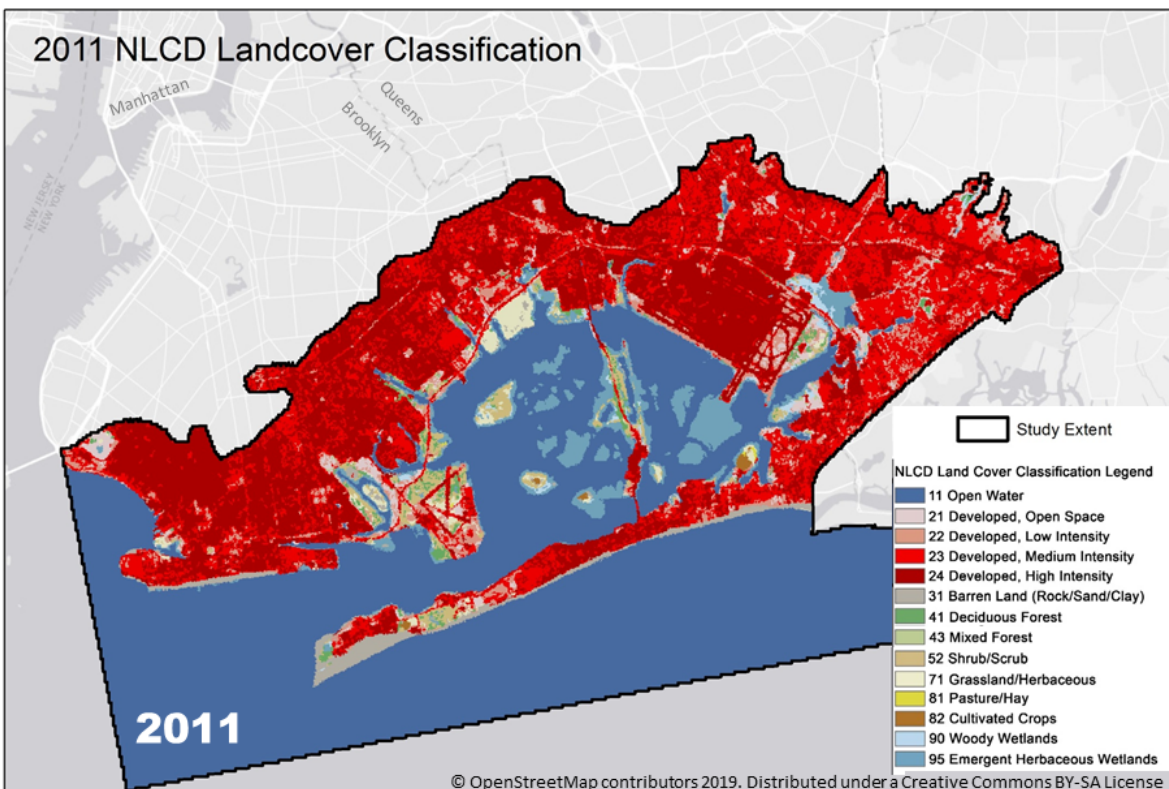
- 15 • Tapered shallowing of the channel depth from offshore (8 m) into the inlet (5 m) and
16 into the innermost areas of the bay (1 m depth)
- 17 • Narrowing of the inlet so that its narrowest point is reduced by 50%
- 18 • Bay perimeter floodplain/wetland restoration, including reducing elevation and altering
19 friction coefficients to represent wetland land cover
- 20 • Wetland restoration in the center of bay to the 1870s footprint
- 21 • Inclusion of additional roughness, to mimic effect of eelgrass and oyster shells
- 22 • Restoration of a shoal off the west end of Rockaway Peninsula
- 23 • Shallowing the deep borrow pit area on the northeast side of the bay
- 24 • Restoration of the landform to the north of the inlet to wetlands
- 25 • Narrowing channels on the interior of the bay

28 **3. Results**

29
30 Our digitization of the historical landscape shows that changes to Jamaica Bay land cover and
31 elevation since the 1870s are dramatic, with widespread urbanization of upland areas and
32 marshlands that once surrounded the bay. Maps of estimated Jamaica Bay area land cover for
33 the present-day and 1870s periods are shown in **Fig. 4**. The most dramatic land cover change is
34 from large areas of fringing wetlands (light blue) to urbanized areas (red), but also the center of
35 the bay has shifted from marshes to open waters (dark blue). Mapped land elevations
36 (topography, bathymetry) and Mannings-n roughness values are shown in **Fig. 5**. Obvious
37 geomorphic changes include a lengthening of Rockaway Peninsula and reconfiguration of the
38 inlet (bounded by red lines). The land roughness (Mannings-n) change reflects the widespread
39 change from marshes (light blue) to urbanized land (red) or open water (dark blue). These
40 changes in habitat type are quantified in **Sect. 3.1**, below.



1



2

3 **Figure 4:** Land cover of the Jamaica Bay watershed (top) reconstructed for the 1870s, and
 4 (bottom) for present-day.

1 Simulations suggest that the mean water depth in Jamaica Bay has increased by either 2.8 or
 2 3.1 m, with the exact result dependent on how calculations are made. If only wetted regions
 3 are included in the average, water depth in Jamaica Bay increased from 1.7 m to 4.5 m between
 4 the 1870s and 2015; of this change, 0.37 m can be attributed to sea-level rise. If the entire
 5 tidally-wetted bay area is used in an average (with dry grid cells included as zero depth), a
 6 historical and modern mean depth of 1.1 m and 4.2 m is found. Our values are consistent with,
 7 and improve upon, the approximate estimate of a historical change from 1 m to 5 m made by
 8 Swanson et al. (1992). In conclusion, our results show a large historical change in bay-wide
 9 mean depth, but slightly smaller than prior studies have suggested. ~~A detailed analysis of areal~~
 10 ~~changes to various types of habitat is given in Sect. 3.2.~~
 11

12 **3.1 Habitat changes**

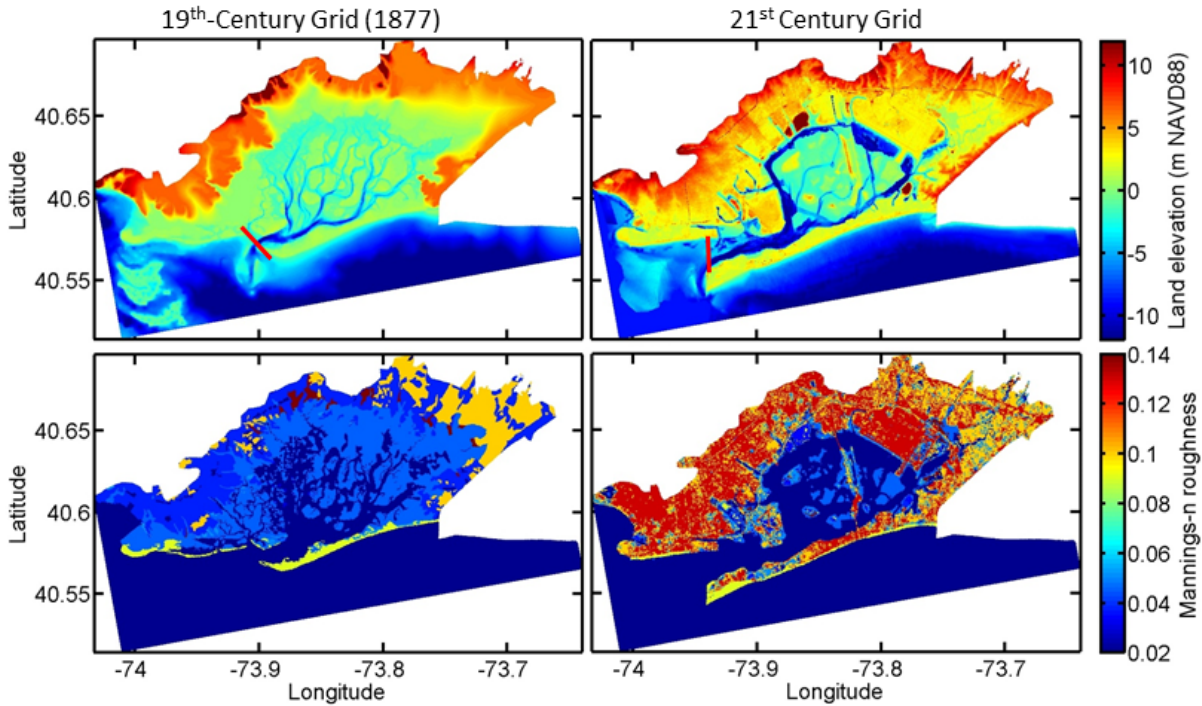
13 The surface areas of many habitat types have changed dramatically since the 1870s, in spite of
 14 an only 23% reduction in interior bay area wetted by average daily high tides (**Table 1**). The
 15 reduction in total area is caused by the reclamation of fringing flood-plain and marshlands, but
 16 is partially offset by a growth of the bay westward due to an increase in inlet length.
 17

18 Total marsh area has declined by 76%, eelgrass area by 100%, intertidal unvegetated area by
 19 72%, and total intertidal area by 73%. The deepwater area (>4 m) has increased by 314% (or
 20 alternatively, the 1870s had 76% less deepwater area than the present). The estimates for
 21 wetland area and loss are nearly identical to the prior estimate of a loss of 75% from 64 km² to
 22 16 km² (NYC-DEP, 2007), but here we provide greater context of changes to other habitat types.
 23 The habitat type changes are computed within the differing bay interiors for the 1870s and
 24 present-day, as enclosed by red line inlet boundaries shown in the top panels of **Fig. 5**.
 25
 26

27 **Table 1:** Estuarine habitat types and their area for the 1870s and present-day
 28

Landscape	Total marsh area ^a (km ²)	Eelgrass area (km ²)	Intertidal-unvegetated (km ²) ^b	Total intertidal area ^b (km ²)	Deep area (>4 m) (km ²)	Interior bay area ^c (km ²)
Basis	map data	map data	map data, tide simulation	tide simulation	map data	map data
1870s	61.3	16.5	17.3	51.5	6.6	92.4
Present-day	14.9	0	4.9	14.0	27.7	71.5
Change	-46.5 (-76%)	-16.5 (-100%)	-12.4 (-72%)	-37.5 (-73%)	20.9 (314%)	-20.9 (-23%)

29
 30 a: Includes all saline marsh and freshwater marsh within the model domain, some not tidal
 31 b: Intertidal area is the difference in area wetted by MHHW and MLLW, based on modeling
 32 (**Sect. 2.2**)
 33 c: Interior bay area is the wetted area at MHHW, based on modeling (**Sect. 2.2**)



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Figure 5: 1870s and early twenty-first century landscape data used as inputs to the hydrodynamic model. On the **top** are land elevation maps, and on the **bottom** are land-cover roughness (Mannings-n) maps. The **left column** shows the 1870s and the **right column** shows the present-day landscape. Red lines delineate the inlet boundary for defining the interior of the bay and tidal prism.

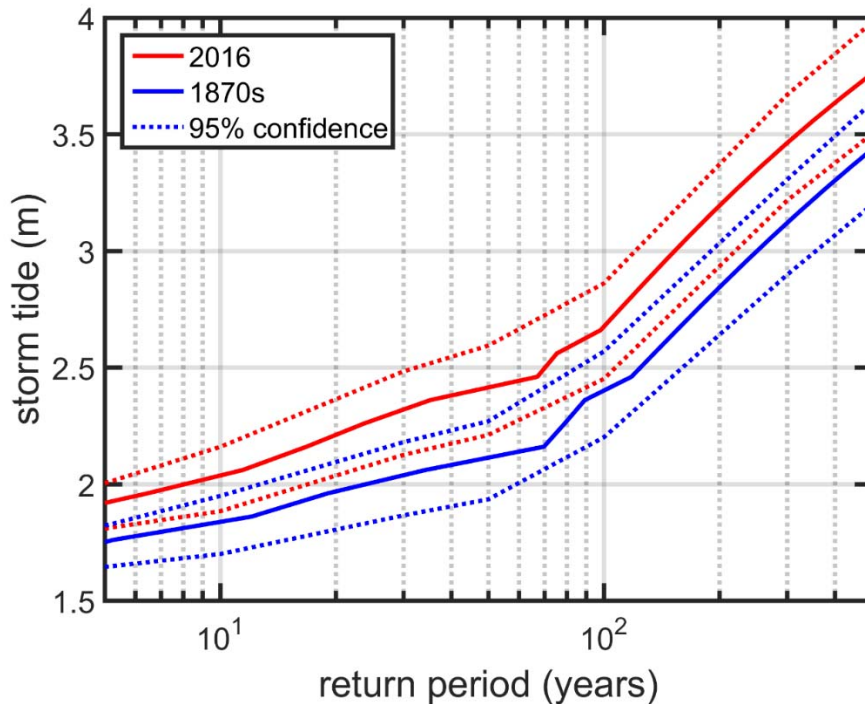
3.2 Storm tide changes

The flood hazard assessment shows similar basic features as found in the prior study of New York Harbor from which methods and offshore model boundary conditions were taken (Orton et al., 2016b). The estimated storm tide for return periods below 30 years is determined predominantly by the relatively frequent extratropical cyclones, and the curve (**Fig. 6**) has a relatively small slope of storm tide with increasing return period. For return periods above 30 years, tropical cyclones become increasingly important and the slope abruptly increases at about the 70-year return period.

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The results reveal that storm tides are markedly larger on the present-day landscape than the historical landscape across a wide range of return periods (**Fig. 6; Table 2**). Holding sea-level constant at 2015 levels, the modern 10-year and 100-year storm tides of 2.02 and 2.66 m are larger than historical simulations by 0.20 m and 0.28 m, respectively, at the eastern end of the bay (Inwood). By contrast, sea-level rise effects are small; when we simulate storms on the 1870s landscape with the 1870s sea level, the 100-year storm tide difference increases by 0.02 m to 0.30 m. The increase in storm-tides is attributable to decreased frictional effects, which scale as $1/H$ (e.g., Friedrichs & Aubrey, 1994). Because the ~ 3 m increase in average depth

1 caused by landscape changes is much larger than the ~0.37 m increase in sea-level, landscape
 2 changes dominate long term changes to flood hazard.
 3



4
 5 **Figure 6:** Storm tide exceedance curves for the 1870s and present-day Jamaica Bay landscapes,
 6 for Inwood. Storm tide is the water level above mean sea level (MSL), and storms for both cases
 7 were simulated with 2015 MSL.

8
 9 **Table 2:** Storm tide elevation and flood area for 1870s versus present-day landscapes^a

Landscape	10-year Storm tide (m)	100-year Storm tide (m)	10-year Flood area (km ²)	100-year Flood area (km ²)
1870s	1.82	2.38	279	284
Present-day	2.02	2.66	226	243
Change	0.20 or 11%	0.28 or 12%	-53 or -19%	-41 or -14%

11
 12 a: These are tallied across the entire model domain
 13

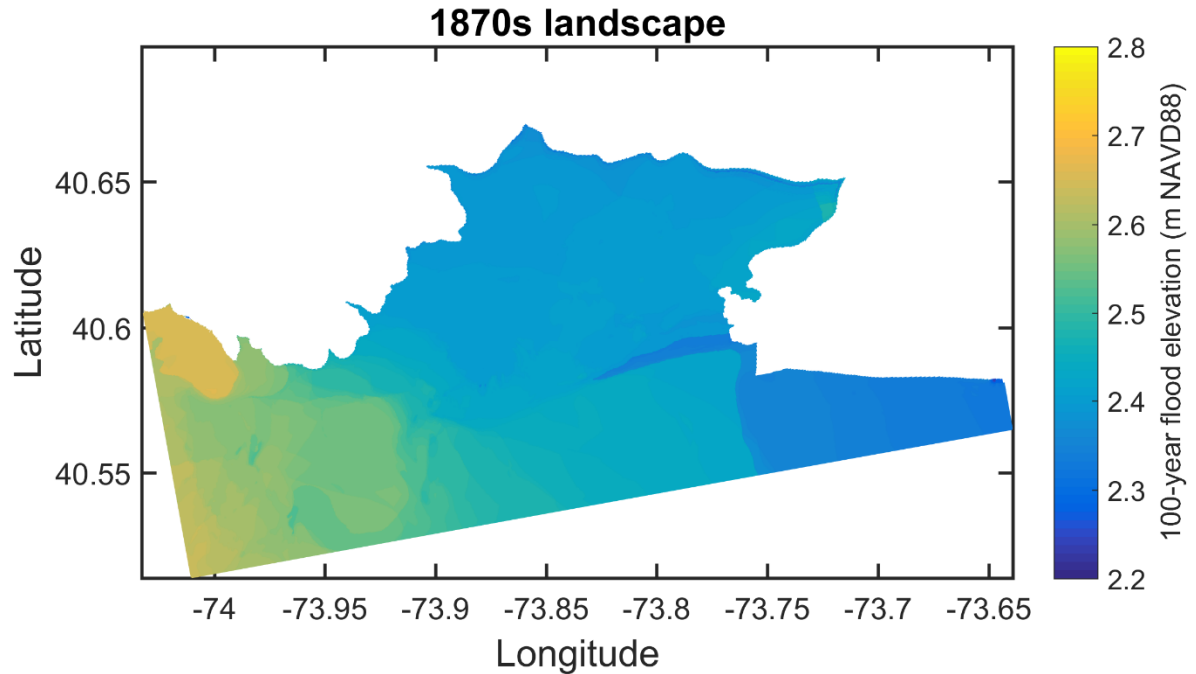
14
 15 Storm tides for the 1870s landscape are seen to clearly decrease with distance into the bay,
 16 with the 100-year flood elevation declining from 2.54 m outside the inlet to 2.42 m in the
 17 eastern part of the bay (**Fig. 7**). By contrast, present-day storm tides (and tides) amplify within

1 the bay, and therefore the 100-year flood hazard increases from 2.56 (outside the inlet) to 2.70
2 m (eastern bay).

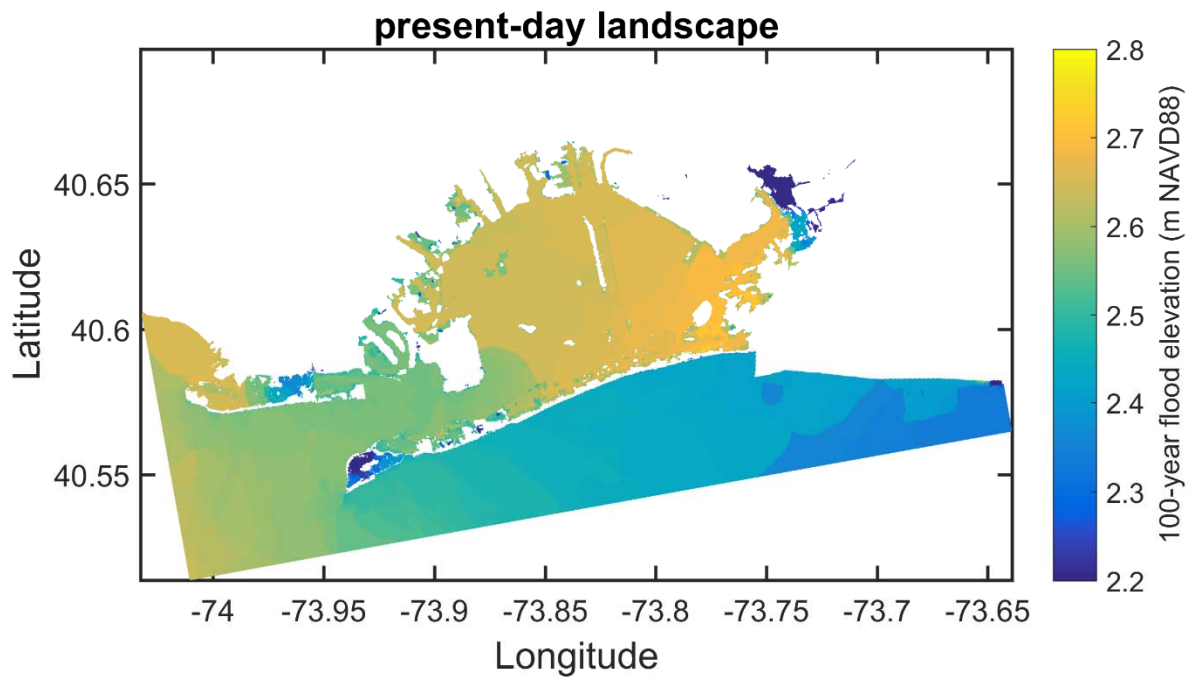
3 Increases in storm tide magnitudes in the bay do not necessarily lead to increases in flooding
4 extent. While **Fig. 6** shows that storm tides are increased substantially by the landscape
5 changes from the 1870s to present, **Fig. 7** demonstrates that the flooded area has substantially
6 decreased for the 100-year flood. **Table 2** shows that the 100-year flood area decrease is 41
7 km² and the 10-year flood area decrease is 53 km² across the model domain (both including the
8 Coney Island and the Jamaica Bay areas). The simple explanation for this is that fringing
9 marshes across the region that were -0.25-0.50 m navd88 elevation in the 1870s were
10 converted using landfill into elevated neighborhoods and airports at 1.5-3.0 m NAVD88, and
11 thus are above this extra 0.20-0.28 m of storm tide. Similarly, for the United Kingdom the
12 frequency of extreme sea level events increased over the last 100 years, yet coastal flooding
13 hasn't increased (Haigh and Nicholls, 2017) because of improvements in forecasting/warning
14 and flood defenses.

15 It was previously established that the bay's tide ranges have grown substantially (Swanson and
16 Wilson, 2008), and we find similar results. Averaging high and low waters for daytime minima
17 and maxima in 1878 over 37 days gives an observed tide range of 1.35 m, while observations
18 for the entire year 2015 show a tide range of 1.73 m. This increase of 28% is smaller than the
19 prior estimate of the tide range change from 1899 to 2000 from Swanson and Wilson (2007),
20 which was 1.16 m to 1.64 m or 41%. However, the 1878 measurements are for a location at
21 mid-bay (Holland House), whereas the 1899 measurements are for the easternmost end of the
22 bay (Inwood or Norton Point), where tide attenuation (e.g. due to narrow, shallow channels
23 and wetlands) was likely more pronounced.

24



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3 **Figure 7:** Maps of the 100-year flood for the present-day and 1870s landscapes. In both cases,
 4 floods were simulated with a 2016 mean sea level.

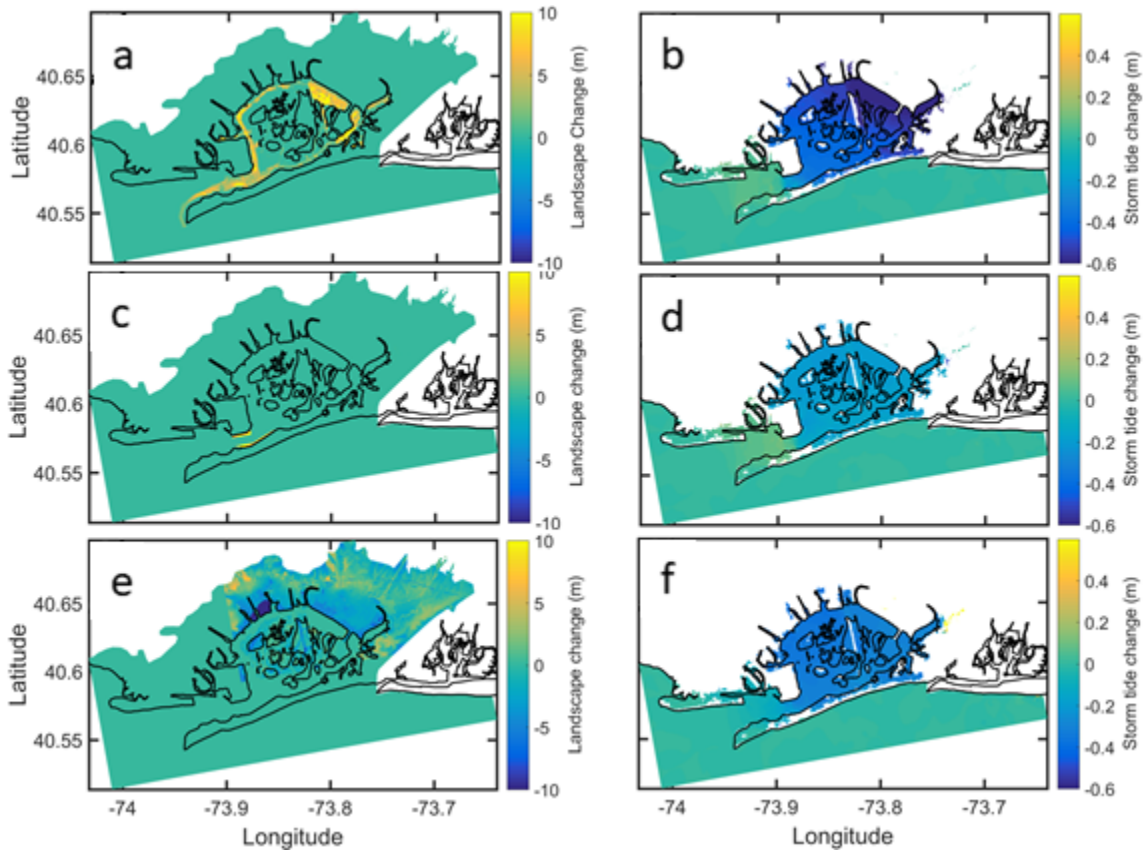
5

6 **3.3. Leverage experiment results**

7 Three of the leverage experiments led to large reductions in hurricane storm tide. The tapered
 8 shallowing leads to a change in the peak hurricane storm tide of -56 cm or -23% (**Fig. 8ab**). The
 9 inlet narrowing leads to a change of -19 cm or -8% (**Fig. 8cd**). Bay perimeter floodplain/wetland

1 restoration results in a change of 31 cm or -13% (Fig. 8ef). All the other landscape changes
 2 showed smaller impacts, indicating that they likely play little role in the long-term changes to
 3 storm tides. For example, extensive wetland restoration in the center of the bay (not the
 4 fringing wetlands) leads to a change in peak storm tide of only -2%. A small rise in Mannings-n
 5 across the entire bay's seabed from 0.020 to 0.025 (mimicking scattered areas of baywide lost
 6 eelgrass, sand bedforms or shells) changed the peak by -3%.

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11 **Figure 8:** Results of “leverage experiments” used to isolate the effects of specific historical
 12 landscape changes, testing their influence on the storm tide for a Category-3 hurricane. The left
 13 panels (a,c,e) show the imposed changes made to the present-day landscape, where the black line shows the present-day coastline. The right panels (b,d,f) show the resulting modeled storm
 14 tide changes. The top row is channel shallowing, middle row inlet narrowing, and bottom row
 15 interior floodplain restoration.

16

18 4. Discussion

19

20 In recent centuries, human activities have greatly modified the geomorphology and ecology of
 21 coastal regions, yet studies of historical and possible future changes in coastal flood extremes
 22 typically ignore the influence of geomorphic change (e.g., Lin et al., 2016; Orton et al., 2019).
 23 Jamaica Bay exemplifies an extreme case of “estuary urbanization” marked by land-fill, diking,

1 channel deepening, and wetland loss (e.g., Marsooli et al., 2018). The upland changes reflected
2 in **Figs. 4-5** and **Table 1** include widespread landfill and urbanization of fringe wetlands, the
3 most visible result of these activities. Our results show that urbanization extends below the
4 estuary water surface, with deepening of channels for shipping and excavation of borrow pits
5 for landfill. The primary insight from this study that estuary urbanization amplifies storm tides
6 likely applies to many urban sub-embayments worldwide, since basin engineering and wetland
7 landfill for port development is globally a common and ongoing process (e.g., Murray et al.,
8 2014; Paalvast and van der Velde, 2014; Schoukens, 2017). Systems with likely impacts include
9 those with substantial changes to inlets, mean estuary depths, or wetland landfill/reclamation
10 (Talke and Jay, 2020), and could potentially be identified by observed long-term changes to
11 tides(Talke and Jay, 2020).

12
13 Further analyses described below (**Sect. 4.1**) demonstrate that the specific changes to the bay
14 that amplify storm tides (channel, inlet depths and widths, landfill) were all directly imposed by
15 humans. Some contribution of the landscape and storm tide changes, such as the wetland
16 erosion in the center of the bay, may be influenced by natural erosion or changing sediment
17 supply (Peteet et al., 2018; Hu et al., 2018; Wang et al., 2017). However, the complex
18 morphologic study required to separate these human and natural factors is beyond the scope
19 of the present study. A broader discussion of the influence of the landscape changes on
20 estuarine conditions and processes is given below (**Sect. 4.2**). Broader discussions of the multi-
21 century landscape change at Jamaica Bay (**Sect. 4.3**) and the general implications of these
22 results for dredged harbors and urbanized estuaries (**Sect. 4.4**) are also included herein.

23 24 **4.1 Anthrogeomorphic amplification of storm tides**

25 The 1870s landscape mitigates storm tide elevations (**Fig. 6**) and damps them as they propagate
26 into the bay (**Fig. 7**) by several ~~potential~~ mechanisms identified in the leverage experiments
27 (Fig. 8). First, the natural floodplain and its wetlands acts as a storage reservoir, allowing a given
28 volume of water to spread over a larger area, but rising to a lesser vertical extent, than a
29 confined (modern) system (**Fig. 8ef**). Second, as also pointed out in Orton et al., (2015), the
30 shallower historical channels ~~and larger regions with marsh vegetation~~ produced a more
31 frictional environment that ~~can damp~~ed long-waves such as tides and storm surge (**Fig. 8ab**).
32 Third, the narrower (Fig. 8cd) and shallower and narrower inlet ~~may have altered~~ the
33 impedance of the storm surge ~~into entering~~ the estuary.

34
35 As has been shown previously, extensive wetland restoration in the center of the bay (not the
36 fringing wetlands) leads to a change in peak storm tide of only -2%, because deep shipping
37 channels around the wetlands are the primary conduit for flood waters. (Orton et al., 2015;
38 Marsooli et al., 2016). These results are also consistent with prior studies that showed that the
39 influence of lagoonal wetland loss on water levels is different when it comes to lateral erosion
40 versus landfill reclamation. Reductions in the tidally-wetted area through wetland reclamation
41 increase storm tides, while wetland retreat due to lateral erosion has the opposite effect (e.g.,
42 Donatelli et al., 2018; Picado et al., 2010).

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2
3 Scaling suggests that the conveyance of long waves (e.g. storm surges, tides) through an inlet
4 into a lagoonal estuary depends on the inlet choking number $P = \left(\frac{gb^2H^3T^2}{C_dL\eta A_e^2} \right)^{1/2}$, i.e., on the drag
5 coefficient (C_d), inlet width (b), length (L), depth (H), tide or surge amplitude (η), the long-wave
6 period (T), and estuary surface area (A_e) (e.g., MacMahan et al., 2014; Stigebrandt, 1980). For
7 decreasing value of P , the inlet is increasingly “choked”, meaning that long-wave amplitudes
8 strongly decrease entering the lagoon. For low values of P (below 5), choking becomes
9 important, and for high P (above 10), the inlet geometry is unimportant (Stigebrandt, 1980).
10 The dependence of P on $H^{3/2}$ conveys a strong sensitivity to water depth, and dependencies on
11 b and A_e convey modest sensitivities to inlet width and estuary area.

12
13 Our landscape reconstruction and numerical results suggest that the choking of long waves at
14 Rockaway Inlet has been strongly reduced. For typical tides, we estimate that P increased from
15 4.5 in the 1870s to 13 at present. For a large amplitude, short-timescale storm surge such as the
16 1821 hurricane, P has changed from 0.69 to 2.0. These changes are driven by a 41% increase in
17 inlet’s average depth (from 6.0 to 8.5 m), and 50% increase in average width (from 1000 to
18 1500 m), and a 23% reduction in bay area. A lengthening of the inlet (from 6600 to 9900 m) due
19 to the growth of Rockaway Peninsula slightly counteracts these effects on choking number,
20 however. Measured at its minimum along-inlet location, there is an 85% increase in the cross-
21 sectional area of the inlet, from 4800 to 8900 m². Reflection and possibly resonance likely play a
22 role in the amplification of tides in the present-day estuary, whereas the shallow water depths
23 and frictional effects of fringing wetlands would also reduce these effects in the 1870s system.

24
25 The dependence of the inlet choking number on both geometric properties and long-wave
26 characteristics helps interpret numerical results. Changes to inlet geometry and channel depth
27 have most strongly changed the large impact, high amplitude storm surges caused by TCs such
28 as the 1821 event. Smaller amplitude events caused (e.g. ETCs) are less likely to be affected by
29 inlet geometry; this is one of the reasons that there is a lesser change in the 5-year storm tide
30 than the 100-year storm tide (**Fig. 6**). The difference between the 500-year storm tide for 1877
31 and present-day landscapes is not larger than that of the 100-year storm tide. This may arise
32 because overtopping of Rockaway Peninsula becomes important, circumventing the inlet and
33 invalidating the above scaling arguments.

34
35 Similarly, the tide or surge time-scale (wave period) T impacts the conveyance of surge or tide
36 into estuaries and back-bays (Aretxabaleta et al., 2017; Kennedy et al., 2011), and the damping
37 that occurs within them (Orton et al., 2015). Slow surge events such as Hurricane Sandy (e.g.,
38 those building to a peak over more than 18 hours) are less affected by hydrodynamic drag (due
39 to smaller flow velocity), potentially producing more severe estuarine floods (Familkhalili and
40 Talke, 2016; Orton et al., 2015). These considerations suggest that modeling flood hazard or
41 designing infrastructure using a representative “storm of record” can produce bias; instead,

1 using an ensemble approach (such as used here) with both small and large time-scale events
2 produces better results.

3
4 The primary reasons for increased storm tides – the floodplain (bay area) reduction, inlet width
5 and depth increases, and bay channel depth increases (**Fig. 8**) – were all imposed by human
6 activities such as landfilling, dredging, inlet stabilization (e.g. with the jetties) and shoreline
7 hardening. Moreover, sea level rise of 37 cm since the 1870s raised total water levels during
8 storms but only changed the storm tide by 2 cm. Because the ~3 m increase in average depth
9 caused by landscape changes is much larger than this increase in mean sea level, landscape
10 changes dominate the long-term changes to flood hazard. Therefore, we conclude that the
11 amplification in storm tides is primarily of anthropogenic origin.

12 13 14 **4.2 Ecological importance of landscape changes since the 1870s**

15 The present-day landscape of Jamaica Bay supports a highly eutrophic, but in many ways
16 healthy estuarine ecosystem with oxygen levels slowly rising over recent decades (Walsh et al.,
17 2018; NYC-DEP, 2018). However, various indicator species, particularly those that depend on
18 intertidal habitats (e.g. diamondback terrapin) have continued declining in abundance (Walsh
19 et al., 2018). Here, we note some likely ecological influences of the landscape and habitat
20 changes summarized in **Figs. 4-5** and **Table 1**.

21
22 Our landscape reconstruction confirms that the bay’s eelgrass beds have disappeared
23 completely, and wetland area has declined dramatically since the 1800s. The wetland decline
24 may be stopped with marsh island restoration/ reconstruction activities which have been
25 occurring over the past decade (Seavitt et al., 2015). Eelgrass beds provide many similar
26 ecological services in estuaries, including nursery and refuge for a diverse and dense faunal
27 community, trapping of sediment, and erosion prevention (Orth et al., 2006). They are known
28 to decline in eutrophic conditions due to the reduced sunlight that results from increased
29 turbidity (Vaudrey et al., 2010; Orth et al., 2006). Salt marshes are widely-known for their
30 ecological importance, including many of the same roles as eelgrass beds, but including
31 intertidal habitat. At Jamaica Bay, this habitat serves diamondback terrapin and birds such as
32 the sharp-tailed sparrow, egrets, herons and geese.

33
34 Our landscape reconstruction shows that unvegetated intertidal area has decreased by 12.7
35 km², a loss of 74%. This change is of equal magnitude in km² to the loss of eelgrass beds (**Table**
36 **1**). Mudflats, sandbars, oyster and mussel reefs, and other unvegetated intertidal areas are
37 forms of “shallows”, and provide important habitat for benthic invertebrates like polychaetes,
38 snails, clams, crabs, and blue mussels, as well as birds that feed on them such as the
39 oystercatcher and willet. They are also used by terrapins for feeding and by horseshoe crabs for
40 reproduction.

41
42 The center of the bay (inside the channels that circle the bay today) has not only lost marsh
43 islands, it has had its land elevation drop substantially, most areas by about 1 m since the 1800s
44 (**Fig. 5**). What were once large expanses of intertidal unvegetated area have shifted to being

1 subtidal. This drop may reduce the sediment supply to the remaining marsh islands' substrate
2 during storms (Wang et al., 2017). Also, an increased depth in front of the marsh can increase
3 wave energy and promote lateral erosion (Fagherazzi et al., 2006). As a result, the loss of
4 intertidal zones and associated increased water depths may be detrimental to the sustainability
5 of the remaining marsh islands and their critical habitat.

6
7 The increase from 7 to 28 km² of deep habitat areas (**Table 1**) may attract more large fish such
8 as striped bass due to increased swimming space, the reduction in thermal variability caused by
9 a deep water column, or stratified deep water's lower temperature in summertime. It is
10 unknown whether there were more or less striped bass in Jamaica Bay in the 1800s, but their
11 presence today has the benefit of supporting a small fleet of fishing charter boats. However,
12 there are several square kilometers of poorly-flushed deepwater regions, predominantly in
13 Grassy Bay immediately southwest of Kennedy Airport, that are prone to hypoxia and even
14 anoxia in late summer, providing compromised habitat area for many organisms (NYC-DEP,
15 2018).

16
17 Our landscape reconstruction and modeling suggest that the residence time of water within the
18 bay has more than doubled between the 1870s and today, with potential adverse ecological
19 implications. The residence time of water in an estuary that receives large wastewater-derived
20 nutrient inputs like Jamaica Bay is an important control on hypoxia, with longer residence times
21 often leading to worsened hypoxia (e.g., Sanford et al., 1992). A simple model of the residence
22 time of a lagoonal-type estuary system is the volume of the bay divided by the tidal flux rate
23 which is the tide prism (volume of water between mean high water and mean low water) over
24 the tide period (12.42 hours) (e.g., Sanford et al., 1992). For the 1870s landscape and sea level,
25 the average modeled tidal prism of the bay was 80 million m³ and volume was 97 million km²,
26 leading to a residence time of 0.62 days. For the 2015 landscape and sea level, the average
27 modeled tidal prism of the bay was 102 million m³ and volume was 290 million m³, leading to a
28 computed residence time of 1.5 days. This simple model was shown for the modern landscape
29 to underestimate residence times (relative to modeled tracer releases), but nevertheless shows
30 that the changes in bay morphology lead to a substantial increase in residence time of a factor
31 of 2-3 mainly due to the much greater volume of the present-day bay. More detailed analyses
32 of water quality and residence time have been performed in other recent studies, and these
33 results are being reported on in separate papers but generally support this interpretation
34 (Marsooli et al., 2018; Fischbach et al., 2018).

35 36 **4.3 Earlier Jamaica Bay landscapes: The estimated 1609 landscape**

37 The 1870s landscape of Jamaica Bay was already influenced by humans. Prior to European
38 colonization, Jamaica Bay was likely more open to the ocean, with an actively migrating inlet
39 located further to the east, a barrier island system, extensive fringing marshlands, but far fewer
40 marsh islands than in the 1870s (Black, 1981; Sanderson, 2016). A less well-constrained model
41 for the pre-European landscape was also produced for this study, and modeling suggests storm
42 tide reductions (from offshore into the bay) were caused by the landscape of the 17th century
43 (Orton et al., 2016a). The model was based on 17th and 18th century maps that showed
44 coastlines and major features, such as an inlet which was in the center of today's Rockaway

1 Peninsula, and a general absence of marsh islands in the bay, calling the bay “Jamaica Sound”.
2 However, the maps did not show bathymetry measurements, and therefore the actual
3 hydrodynamic behavior of the system is highly uncertain relative to the 1870s and present-day
4 landscape (Orton et al., 2016a). Ongoing research is helping improve our understanding of the
5 landscape of the 1600s and long-term evolution through analyses of sediment cores from the
6 western-central area and eastern ends of the bay (Peteet et al., 2018). That study showed that
7 European settlement led to increases of inorganic sediment delivered to the bay, likely due to
8 forest clearance for agriculture and subsequent erosion, and this may explain the increase in
9 marsh island area in the 1700s and 1800s. These considerations suggest that on century
10 timescales, hard to quantify factors such as the anthropogenically mediated sediment supply
11 may also exert an important influence on long-term system evolution.
12

13 **4.4 Broader context**

14 Remarkably, despite the visions of the Jamaica Bay Improvement Commission (1907) and The
15 River and Harbor Acts of 1910 and 1925, the present-day commercial shipping activity through
16 this largely man-made 1 km wide, 8-16 m deep shipping channel (measured at Floyd Bennett
17 Field, the narrowest part) is limited to an average of 3 one-way trips per day servicing
18 gravel/sand companies, sewage treatment plants and bulk fuel companies (USACE, 2016). Our
19 results show that maintaining these shipping channels leads to higher storm tides in the bay,
20 even though the economic activity that justified their construction is largely absent.
21

22 Globally, common development approaches such as dredging for port development and
23 landfilling for neighborhood development can have major economic benefits, but can also raise
24 vulnerability as they did for Jamaica Bay (Talke and Jay, 2020). The movement towards “New-
25 Panamax” and larger ships is leading major harbors to dredge wider channels and depths of
26 approximately 16 m (Briggs et al., 2015). Other dredged estuaries have been shown to cause
27 enhanced inland propagation of storm tides, such as with the Cape Fear estuary (Familkhalili
28 et al. 2016). The Mississippi Gulf River Outlet canal was originally created through dredging, and
29 recently was de-authorized and blocked in part because of a debate over whether it increased
30 storm surge penetration inland (Shaffer et al., 2009). Within the St Johns River, Florida, channel
31 deepening to a controlling depth of >14m is continuing, despite model results that showed
32 increases in tide range and storm surge of 0.1-0.2 m in some locations (USACE, 2014).
33

34 The results presented here suggest that evaluating changes to flood hazard should be part of
35 the cost-benefit analysis of any environmental impact study or restoration study, particularly
36 projects that propose altering inlet geometry or channel depth. Our results can help inform
37 debates about whether to continue maintaining under-used ports, since allowing inlets and
38 channel depths to return to pre-development geometry is potentially a way to mitigate against
39 future sea-level rise effects. Given adequate sediment supply, many systems quickly return
40 towards pre-development depths; for example, the lower Passaic River in New Jersey has
41 accumulated as much of 5 m of sediment after maintenance dredging ceased in the early 1980s
42 (Chant et al., 2011).
43
44

5. Conclusions

This study applied a historical reconstruction approach for a case study of how natural and urbanized estuary systems modify coastal storm tides. A Jamaica Bay flood model for the 1870s was developed and simulation results were contrasted with those from a present-day model to quantify the influences of 20th Century changes in bathymetry and habitat on storm tide hazard. The hydrodynamic model landscape (land elevation and friction) for the 1870s was estimated from detailed maps of topography, bathymetry and seabed characteristics, and validated using tide observations. The models were used for tide simulations, supplementing map data with tidal datums for additional analysis of habitat change (e.g. estuary intertidal area), and for coastal storm flood modeling and probabilistic hazard assessment.

Major changes to land elevation and land cover were quantified and translated into habitat area changes, more precisely constraining previous estimates of mean depth change and previously-reported estimates of marsh loss. Predominantly through dredging, landfill and inlet stabilization, the average water depth of the Jamaica Bay has increased from 1.7 to 4.5 m, tidal surface area diminished from 92 to 72 km², and the inlet cross-sectional area was expanded from 4800 to 8900 m². Total (freshwater plus salt) marsh habitat area was estimated to decline by 74%, intertidal area by 73%, and intertidal unvegetated habitat area by 72%, both by about a factor of four. Deepwater habitat increased by 314%, also about a factor of four. Submerged grasses (e.g. eelgrass) disappeared completely.

A probabilistic flood hazard assessment with simulations of 144 storm events revealed that the landscape changes caused an increase of 0.28 m (12%) in the 100-year storm tide, similar to the separate effect of a global sea level rise of 0.23 m (Church and White, 2011; Hay et al., 2015) and local sea level rise of 0.37 m from the 1870s to 2015 (Kemp and Horton, 2013). The 10-year storm tide increased by 0.20 m (11%). In spite of these rising storm tides, flood area for the 10-year and 100-year storm tides is smaller than it was in the 1870s, by 19 and 14%, respectively, due to landfill conversion of fringing wetlands into elevated neighborhoods.

Specific anthropogenic changes to estuary depth, area and inlet depth and width were shown through targeted modeling and dynamics-based considerations to be important drivers of these changing storm tides, with depth changes being the strongest factor. The dependence of inlet choking of a long-wave such as tide or surge depends on estuary area squared, inversely on inlet width squared, and inversely on inlet/estuary depth cubed. These choking effects are also enhanced with short-duration sea level anomalies, such that a rapid-pulse storm surge rising in a matter of a few hours is damped more than a semidiurnal tide or long-duration storm surge event. Similar scaling shows that damping within the estuary has also decreased.

Our study highlights that anthropogenic changes to estuary geomorphology can affect storm tide hazard to a degree that is comparable to historical sea-level rise. An improved understanding of historical estuarine landscapes, as well as their hydrodynamic and sedimentary processes, can help inform nature-based flood and climate mitigation efforts.

1 Studies such as this one that reconstruct the historical landscape can be used to assess
2 strategies to minimize floods into the future, as demonstrated on the broader nature-based
3 adaptation study (Orton et al. 2016) website and flood adaptation mapper tool
4 (<http://AdaptMap.info>). These results have influenced adaptation considerations after
5 Hurricane Sandy spurred a strong interest in flood adaptation. Concepts of bay shallowing and
6 inlet narrowing were considered as options in a stakeholder-driven study of nature-based
7 options for flood and hypoxia mitigation, with narrowing being one of the more deeply-
8 evaluated alternatives (Fischbach et al., 2018).

9
10

11 *Data availability.* Model DEMs, still-water elevation data, and animations of model simulations
12 for the 1870s and present-day are available by download from the project’s flood mapper
13 <http://AdaptMap.info/jamaicabay/> (5-year through 1000-year still-water elevation, in GeoTIFF
14 and CSV formats). Observed tide data for 1877-1878 are available at the US National Archives in
15 College Park, MD, in Record Group 23, Entry 148, PI. 105. Tide data used for 2015 are available
16 from the United States Geological Survey (station 01311850) via <https://waterdata.usgs.gov>.

17

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22

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24

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30

31

32

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