



1 **Investigating beach erosion related with its recovery at Phra Thong Island, Thailand caused by**
2 **the 2004 Indian Ocean tsunami**

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22 **Abstract**

23 The 2004 Indian Ocean Tsunami and the 2011 Great East Japan earthquake and tsunami caused large-
24 scale topographic changes in coastal areas. Whereas much research has focused on coastlines that have
25 or had large human populations, little focus has been paid on coastlines that have little or no
26 infrastructure. The importance of examining erosional and depositional mechanisms of tsunami events
27 lies in the rapid reorganisation that coastlines must undertake immediately after an event. Through
28 understanding the precursor conditions to this reorganisation is paramount to the reconstruction of the
29 coastal environment. This study examines the locations of sediment erosion and deposition during the
30 2004 Indian Ocean Tsunami event on the relatively pristine Phra Thong Island, Thailand. Coupled with
31 satellite imagery, we use numerical simulations and sediment transportation models to determine the
32 locations of significant erosion and the areas where much of that sediment was redeposited during the
33 tsunami inundation and backwash processes. Our modelling approach confirms that beaches on Phra
34 Thong Island were significantly eroded by the 2004 tsunami, predominantly during the backwash phase
35 of the first and largest wave to strike the island. Although 2004 tsunami sediment deposits are found on
36 the island, we demonstrate that most of the sediment was deposited in the shallow coastal area,
37 facilitating quick recovery of the beach when normal coastal processes resume.

38



39 **1. Introduction**

40 The 2004 Indian Ocean Tsunami and the 2011 Great East Japan earthquake and tsunami caused large-
41 scale topographic changes in coastal areas (Pari et al., 2008; Goto et al., 2011a; Tanaka et al., 2011;
42 Haraguchi et al., 2012; Hirao et al., 2012; Udo et al., 2013; Imai et al., 2015). Since the two tsunami
43 events, long-term topographic changes ranging from years to over a decade have been confirmed in
44 areas affected by the two events (Choowong et al., 2009; Ali et al., 2015; Udo et al., 2016; Mieda et al.,
45 2017; Koiwa et al., 2018), but knowledge regarding the processes of topographic recovery remain
46 poorly understood. Long-term topographic changes in the coastal area have not considered the
47 perspective of early restoration and reconstruction in areas affected by the 2011 tsunami. Structural
48 measures, such as levee construction are moving forward, creating the potential for future problems.
49 Coastal areas that have undergone large-scale topographic changes in a tsunami do not necessarily
50 return to their original topographies. In cases where topographic changes continue without recovery
51 (Udo et al., 2016; Koiwa et al., 2018), it is important to take structural measures that consider future
52 topographic scenarios.

53 Because reconstruction plans must be formulated in a short time after the tsunami while recovery
54 may take several years, it is difficult to predict the recovery process of coastal areas from field surveys
55 and reflect this in structural measures. It is therefore necessary to clarify in advance the response
56 mechanism as to how the coastal area will recover from large-scale topographic changes caused by a
57 tsunami. To clarify the response mechanism of tsunami-affected topography requires a thorough
58 understanding of the sediment budget in the sedimentary system after the event. Defining the conditions
59 of sediment transport during the tsunami is also key for the initial response process.

60 Prior studies have mainly estimated sediment transport conditions, such as erosion and sediment
61 deposition through remote sensing (e.g. Fagherazzi & Du 2008, Choowong et al 2009; Liew et al 2010),
62 and sedimentological and stratigraphic analysis (e.g. Paris et al 2007; Hawkes et al 2007; Switzer et al
63 2012); however, the information obtained regarding the final results of the sediment transport process
64 is limited. It is difficult to obtain information on where sediment has eroded and deposited and whether
65 topographic changes caused by the local sediment runoff or deposition are the results of action from
66 inflow or backwash (e.g. Pham et al 2018). This information determines the sediment budget in the
67 system before and after the tsunami and is therefore important for considering topographic recovery.
68 Therefore, in addition to information from remote sensing and sedimentological data, analyzing
69 numerical simulation results to reproduce spatial-temporal phenomena is effective when discussing the
70 sediment transport process. In recent years, the movable bed model for simulating tsunami sediment
71 transport has been developed, improved, and applied in the field (Takahashi et al., 1999; Takahashi et
72 al., 2008; Takahashi et al., 2011; Takahashi et al., 2012; Morishita et al., 2014; Yamashita et al., 2015;
73 Arimitsu et al., 2017; Yamashita et al., 2018), and reproducibility has been confirmed by comparison
74 between the calculated and measured values.

75 An important consideration in the recovery process following catastrophic marine events (e.g.
76 typhoon and tsunami) is the degree of development and human modification of the coastal zone prior



77 to the event. Artificial structures, such as sea walls, roads and buildings interfere with overwash
78 processes, and these areas are often targeted from reconstruction and rehabilitation through rapid
79 engineering reconstruction. Little is known about the recovery processes in sparsely developed and
80 populated areas, and Phra Thong Island, western Thailand is an ideal location to examine the recovery
81 processes following a major tsunami event.

82 Examining the sediment transport processes on Phra Thong Island is expected to elucidate
83 phenomena, improve numerical calculation models for the future and is applicable to other areas.
84 Furthermore, many palaeotsunami deposits were identified in areas impacted by the 2004 IOT on Phra
85 Thong Island (Jankaew et al., 2008; Sawai et al., 2009; Fujino et al., 2009; Fujino et al., 2010; Brill et
86 al., 2012a, b; Pham et al., 2017; Gouramanis et al., 2017). Thus, clarifying the sediment transport
87 conditions of the 2004 tsunami will be important for future estimations of history, scope and cause of
88 older tsunamis in Indian Ocean coastal areas.

89 This study investigates the conditions of sediment transport and considers the factors involved in early
90 recovery of the Phra Thong Island beaches after the 2004 tsunami. We used tsunami sediment transport
91 calculations to spatio-temporally reproduce the sediment transport processes occurring during the
92 tsunami.

93

94 **2. Conditions and method**

95 **2.1. Phra Thong Island, Thailand**

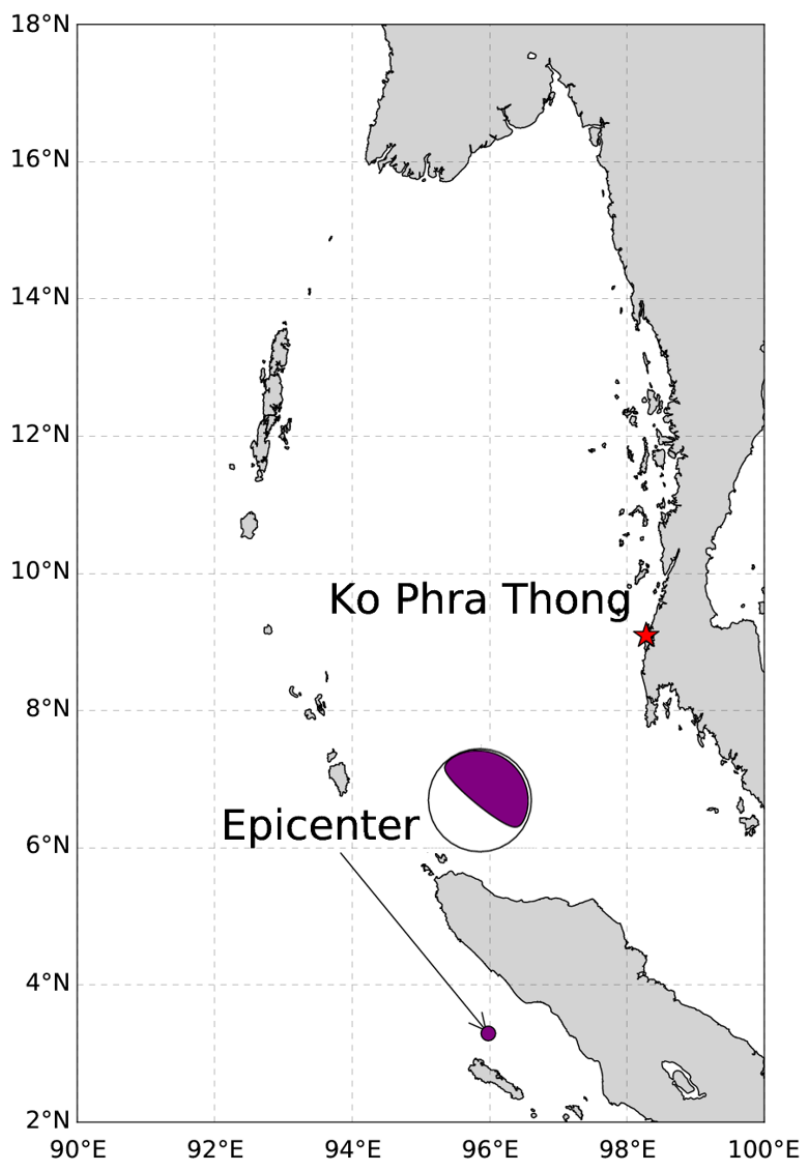
96 During the 2004 Indian Ocean tsunami, a wave exceeding 20 m at its highest was observed at the
97 southernmost tip of Phra Thong Island (Fig. 1). Over 70 people were lost and a village of 100 households
98 disappeared. Geomorphologically, the western coast of the island has a beach ridge sequence trending
99 parallel to the coast, which formed during the sea level regression following mid-Holocene sea level
100 highstand at *ca.* 6,000 years ago (Brill et al. 2015). The eastern shore of the island is extensively covered
101 by mangroves along the shores of tidal channels. The island has a tropical climate. Additionally,
102 palaeotsunami deposits are preserved in swales in the beach ridge system along the western coast of
103 Thailand (e.g. Jankaew et al. 2008; Gouramanis et al. 2017). Furthermore, although local beaches were
104 lost in the 2004 tsunami, satellite photography showed recovery within 18 months (e.g. Choowong et
105 al. 2009).

106 Although this study used tsunami sediment transport calculations for analysis, other uncertainties
107 remain, such as the effects of artificial features on the calculations. Because of its natural topography
108 with few artificial features, Phra Thong Island is a rare case that is useful for verifying tsunami sediment
109 transport calculations with less uncertainty.

110

111 **2.2. Topography and bathymetry data**

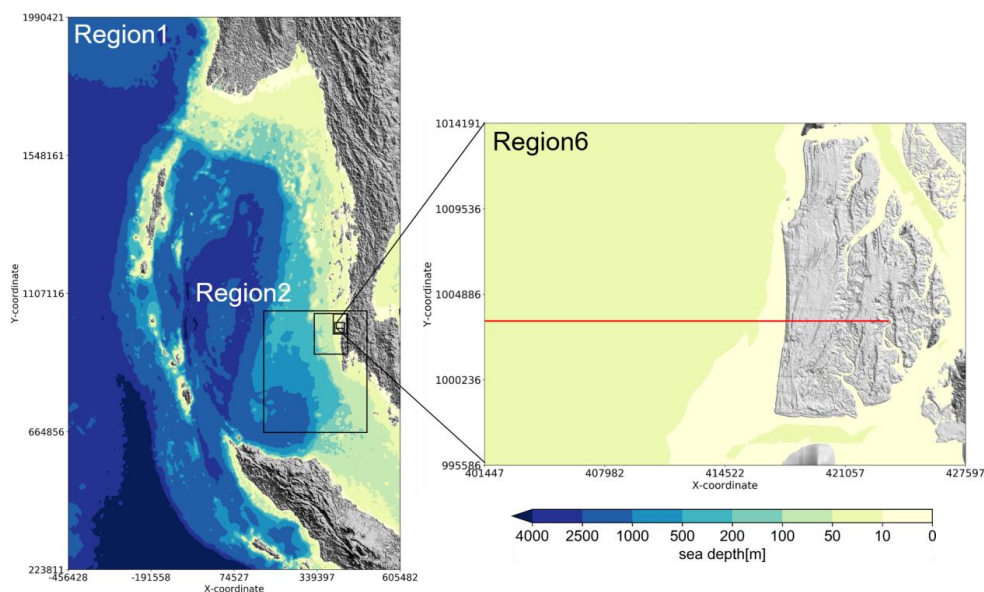
112 Topography and bathymetry data used for the tsunami sediment transport calculations were created
113 based on various water depths and elevations. Figure 2 shows the terrain data that were created.
114 Topographic data were created from Region 1, which includes the Andaman Sea, to Region 6, which



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Figure 1 Location of Phra Thong Island

118 includes all of Phra Thong Island. The grid spacing from Region 1 to Region 6 is 1,215 m, 405 m, 135
119 m, 45 m, 15 m, and 5 m, respectively. In the tsunami sediment transport calculation, plane calculation
120 was performed using an orthogonal coordinate system; the coordinate system of the target area Phra
121 Thong Island is UTM 47N. Region 1 is the projection of depth data of the 30-second grid provided by
122 GEBCO (2014) on the Cartesian coordinate system UTM 47N. Regions 2–4 use a digital marine chart
123 with 300 m resolution based on a survey by the Thai Navy. Regions 5 and 6 use an original 5 m (terrain



124

125 Figure 2 Terrain data (The black frame shows Region 1 to Region 6, and the red line in Region 6
126 shows the cross-section where calculation was performed.)

127

128 data) and 15 m (sea depth data) grid spacing to create mean terrain and water depth data based on
129 analysis of satellite image by EOMAP and elevation data provided by the Land Development
130 Department of Thailand. The terrain data of Region 4, created from the digital marine chart of 300 m
131 resolution, showed discontinuity at the boundary with Region 5, which had a higher resolution. The
132 discontinuity was therefore removed to the extent possible by interpolation with an inverse distance
133 weighting method using all terrain data.

134

135 2.3. Tsunami source model

136 The fault model proposed by Suppasri et al. (2011) was used as the tsunami source of the 2004 Indian
137 Ocean Tsunami. The fault model is divided into six small faults from satellite image analysis and survey
138 results, and it is assumed that each small fault slides simultaneously and instantaneously. For the
139 tsunami source, the vertical tectonic displacement in each fault was calculated according to Okada
140 (1985). Table 1 shows the fault parameters of each fault and Figure 3 shows the initial water level.

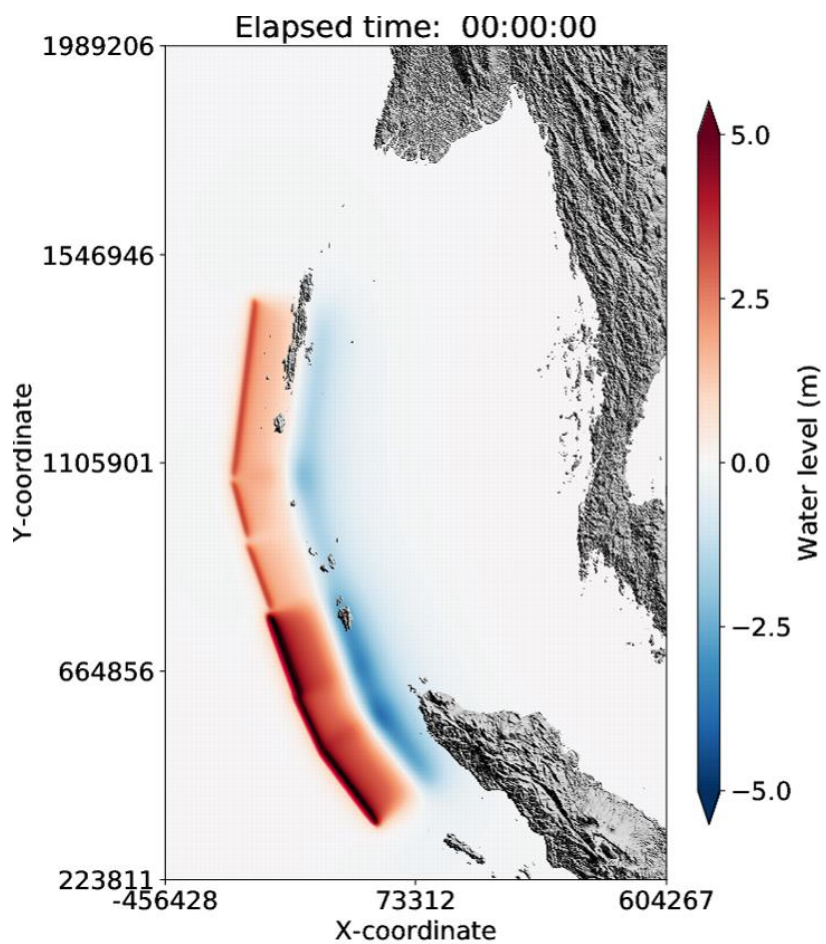


Figure 3 Initial water level

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 142
 143
 144

Table 1 Fault parameters (Suppasri et al., 2011)

Segment No.	1	2	3	4	5	6
Latitude(N)	3.03	4.48	5.51	7.14	8.47	9.63
Longitude(E)	94.40	93.32	92.87	92.34	91.88	91.57
Strike(deg)	323	335	340	340	345	7
Dip(deg)	15	15	15	15	15	15
Slip(deg)	90	90	90	90	90	90
Length(km)	200	125	180	145	125	380
Width(km)	150	150	150	150	150	150
Dislocation(m)	14	12.6	15.1	7	7	7
Depth(km)	10	10	10	10	10	10

145



146 **2.4. Tsunami sediment transport calculation**

147 **2.4.1. Tsunami propagation and run-up model**

148 Tohoku University's Numerical Analysis Model for Investigation of Near-field tsunamis, No. 2
149 (TUNAMI-N2) is based on the nonlinear long wave theory and was used as the tsunami propagation
150 and run-up model.

151
$$\frac{\partial \eta}{\partial t} + \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} = 0 \quad (1)$$

152

153
$$\frac{\partial M}{\partial t} + \frac{\partial}{\partial x} \left(\frac{M^2}{D} \right) + \frac{\partial}{\partial y} \left(\frac{MN}{D} \right) + gD \frac{\delta \eta}{\delta x} + \frac{gn^2}{D^{\frac{7}{3}}} M \sqrt{M^2 + N^2} = 0 \quad (2)$$

154

155
$$\frac{\partial N}{\partial t} + \frac{\partial}{\partial x} \left(\frac{MN}{D} \right) + \frac{\partial}{\partial y} \left(\frac{N^2}{D} \right) + gD \frac{\delta \eta}{\delta y} + \frac{gn^2}{D^{\frac{7}{3}}} N \sqrt{M^2 + N^2} = 0 \quad (3)$$

156

157 Here, η is the change in water level from the still-water surface, D is the total water depth from the
158 bottom to the water surface, and g is the acceleration of gravity. The bottom friction is expressed
159 according to the Manning formula, where n is Manning's roughness coefficient. M and N are the total
160 flow fluxes in the x and y directions, respectively, and are given by integrating the horizontal flow
161 velocity u , v from the water bottom h to the water surface η . It is assumed that the horizontal flow
162 velocity is uniformly distributed in the vertical direction.

163 The nonlinear long wave theory consists of a continuous equation that is derived from (1) the
164 principle of conservation of mass (continuity equation) and (2) the conservation of momentum
165 (equation of motion). These two equations are obtained by vertically integration from the seabed to the
166 water surface.

167 When the water depth is about 50 m or less, the effects of the 2nd, 3rd and 5th terms of the advection
168 and seabed friction terms (Equations 2 and 3) are reduced, therefore wave theory that omit these terms
169 is often used at depths shallower than 50 m. Meanwhile, the Message Passing Interface (MPI) parallel
170 was implemented in the model for highly efficient calculations. Both the advection term and the bottom
171 friction term were therefore considered in the calculations without reducing accuracy in deeper waters.

172

173 **2.4.2. Tsunami movable bed model**

174 For the tsunami movable bed model, we used the numerical sediment transport model (STM)
175 proposed by Takahashi et al. (2000), which solves the time evolution of sediment transport considering
176 the exchange sediment volume of the bed and suspended load layers according to the flow conditions
177 of the nonlinear long wave theory-based TUNAMI-N2 model.

178 This model divides sediment transport by the tsunami into a bed load layer, where sediment grains pull,



179 and a suspended load layer, where sediment grains float. The governing equations consist of continuous
 180 equations for the bed load layer and the suspended load layer, which are shown below.

181

$$182 \quad \frac{\partial Z_B}{\partial t} + \frac{1}{1-\lambda} \left(\frac{\partial q_{Bx}}{\partial x} + \frac{\partial q_{By}}{\partial y} + \omega_{ex} \right) = 0 \quad (4)$$

183

$$184 \quad \frac{\partial \bar{C}_s M}{\partial x} + \frac{\partial \bar{C}_s N}{\partial y} - \omega_{ex} + \frac{\partial \bar{C}_s h_s}{\partial t} = 0 \quad (5)$$

185

186 Equation (4) is a continuous equation for within the bed load layer. The first term is the exchange
 187 sediment volume with the bottom, the second term is the balance of sediment flow volume moving in
 188 a tractive form in the flow direction, and the third term defines the balance of suspension flux, caused
 189 by diffusion, and sedimentation flux, caused by gravity, as the exchange sediment volume between the
 190 bed load layer and the suspended load layer. ω_{ex} is expressed by the following equation.

191

$$192 \quad \omega_{ex} = \epsilon_z \frac{\partial C}{\partial z} - \omega_0 C \quad (6)$$

193

194 Here, ρ_s is the sediment grain density, λ is the sediment grain porosity, Z_B is the bottom height from the
 195 reference plane, q_B is the amount of bed load sediment, ϵ_z is the diffusion coefficient in the vertical
 196 direction, C is the concentration in the vicinity of the boundary between the bed load layer and the
 197 suspended sediment layer, ω_0 is the sedimentation velocity of the sediment grains, C_B is the average bed
 198 load sediment concentration, h_B is the bed load layer thickness, C_s is the average suspended load layer
 199 concentration, h_s is the suspended load layer thickness, and M is the bed load flux. w_0 is the
 200 sedimentation velocity of the sediment grains. Equation (5) is a continuous equation for within the
 201 suspended load layer. The first and second terms are bed load sediment moving in a suspended state in
 202 the flow direction, the third term is the exchange sediment volume between the bed load layer and the
 203 suspended load layer, and the fourth term is the increase or decrease of the sediment flow in the
 204 suspended load layer.

205 In Equations (4) and (5), the equation defining the bed load sediment volume q_B and the equation
 206 defining the exchange sediment volume w_{ex} of the bed load layer and suspended load layer are necessary,
 207 but according to Takahashi et al. (1999), they are obtained by the following.

208

$$209 \quad q_B = \alpha \sqrt{sgd^3} (\tau_* - \tau_c)^{\frac{3}{2}} \quad (7)$$

210

$$211 \quad \omega_{ex} = \beta \sqrt{sgd} (\tau_* - \tau_c)^2 - \omega_0 \bar{C}_s \quad (8)$$

212



213

214

$$\tau_* = \frac{u_*^2}{sgd} \quad (9)$$

215

216 Here, α is the coefficient of the bed load sediment volume equation, β is the coefficient of the
217 suspension volume equation, s is specific gravity in water, g is the acceleration of gravity, d is grain
218 diameter, τ_* is the Shields number, τ_c is the limit Shields number, u_* is the friction velocity obtained
219 from the Manning formula.

220

221 In the model comprised of Equation (4) and Equation (5), the bottom height Z_B from the reference
222 plane and the average suspended sediment concentration C_S are the initial values before the tsunami and
223 the flow flux M , respectively. Because suspended sediment thickness h_S is given by the equation of
224 motion of a fluid and the continuous equation, sea level fluctuation can be determined over time.
225 Further, the MPI parallel was implemented according to Yamashita et al. (2016) in this model to enable
226 relatively efficient wide area calculations.

226

227 2.5. Calculation conditions

228

229 Here we explain the conditions for the numerical calculations. Figure 3 was used for the tsunami
230 source, while Figure 2 was used for terrain data. The calculations were performed using a 3:1 nested
231 grid that increased the resolution a 1215 m grid to a 5 m grid. Additionally, the target region of the
232 sediment transport calculation was limited to Region 6, with a grid spacing of 5 m.

232

233 The simulations were calculated over a 0.05 second increment with a 6 hour period in which the
234 suspended sediment concentration in the vicinity of the shoreline decreased and stabilized. For the
235 bottom conditions, the Manning's roughness coefficient was fixed at $n = 0.025$, and the entire area
236 of Region 6 was considered the movable bed. The grain size was based on one sediment data set
237 (Gouramanis et al., 2017) from the locally eroded region, and was considered as a representative value
238 for all of the tsunami sediment grain sizes. A uniform grain size of $D_{50} = 0.127$ mm was used.

238

239 The limit Shields number τ_c in Equations (7) and (8) was obtained using Equations (10) and (11)
240 according to Iwagaki et al. (1954), as shown below.

240

241

$$\tau_c = u_c^2 \rho \quad (10)$$

242

243

$$u_c^2 = 8.41d^{\frac{11}{32}} \quad (11)$$

244

245 Here, u_c is the friction velocity and ρ is the density of water.

246

247

248

Table 2 shows each parameter set used for sediment transport calculations in this study.



249

Table 2 Set parameters for sediment transport calculations

Variable	Set Value
Coefficient of bed load sediment volume equation α	6.55
Coefficient of suspension sediment volume equation β	9.1×10^{-5}
Friction speed u_c	0.01353 m/s
Bottom slope correction factor ε	2.5
Sedimentation velocity of sediment grains w_0	0.1353 m/s
Maximum suspended sediment concentration C_{max}	37.7%
Specific gravity of sediment grains in water s	1.65
Void ratio λ	0.4

250

251 3. Result

252 3.1. Verification of reproducibility

253 3.1.1. Tsunami trace height

254 The reproducibility of the calculated results is based on the tsunami trace height data (IUGG;
 255 available at <http://www.nda.ac.jp/fu-jima/TMD/index.html>) for the 2004 Indian Ocean Tsunami is
 256 discussed using geometric mean K and geometric standard deviation κ proposed by Aida (1978).
 257 Figure 4 shows results of calculation of the maximum inundation depth of trace height data at seven
 258 available sites on Phra Thong Island. The geometric mean K and the geometric standard deviation κ can
 259 also be obtained using the following formula (Aida, 1978).

260

$$261 \log K = \frac{1}{n} \sum_{i=1}^n \log K_i \quad (12)$$

262

$$263 \log \kappa = \sqrt{\frac{1}{n} \left\{ \sum_{i=1}^n (\log K_i)^2 - n(\log K)^2 \right\}} \quad (13)$$

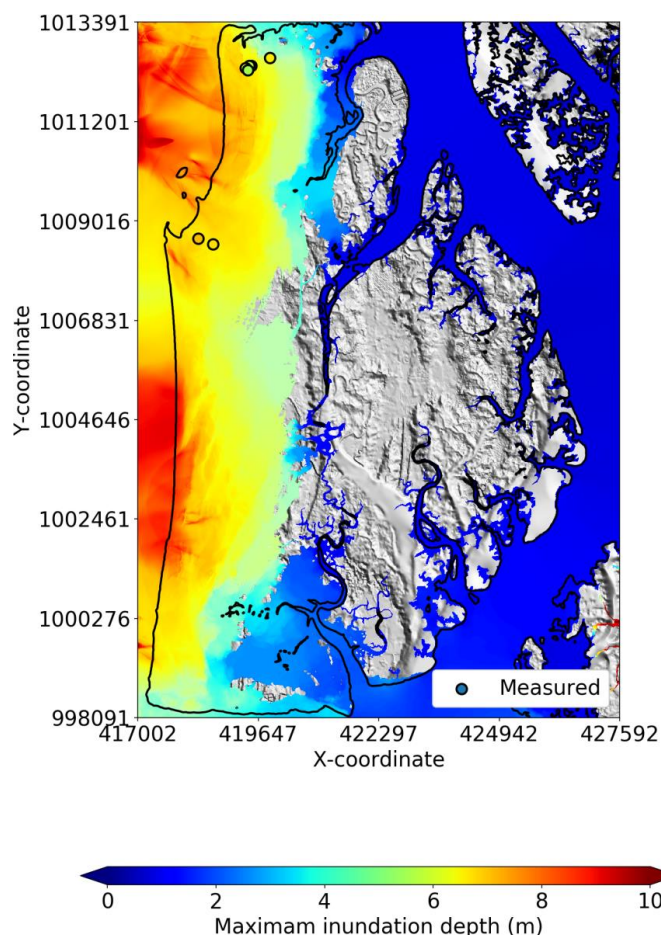
264

265 Here, n is the number of points, R_i is the trace height at the i th point, H_i is the calculated value at the i th
 266 point, and $K_i = R_i/H_i$. From Equations (12) and (13), $K = 0.96$ and $\kappa = 1.10$ are obtained. Additionally,
 267 the source model used in this calculation gives $K = 0.84$ and $\kappa = 1.30$ for reproducibility of tsunami
 268 trace height in the wide area along the coast of Thailand (Suppasri et al., 2011). The Japan Society of
 269 Civil Engineers (2012) consider $0.95 < K < 1.05$ and $\kappa < 1.45$ as guides for evaluating reproducibility
 270 of tsunami numerical calculations. Therefore, it can be said that this calculation has good tsunami
 271 reproducibility.

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Figure 4 Comparison of calculated and measured maximum inundation depth

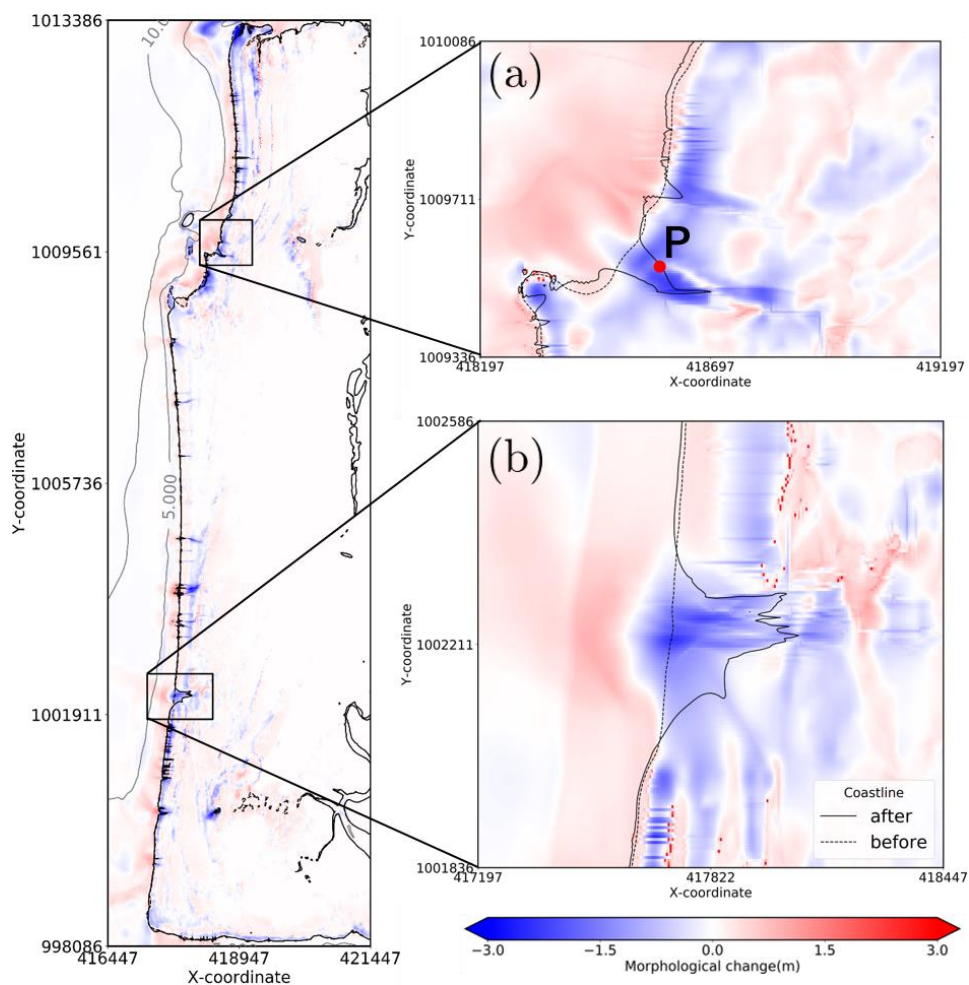
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278 3.1.2. Change of shoreline

279 Our sediment transport models reproduce the locations of sediment erosion and these are confirmed
280 from satellite images. First, Figure 5 shows topographical changes caused by the tsunami and the
281 shoreline before (dashed line) and after (solid line) the tsunami in this calculation. As shown in Figure
282 5, local erosion was largely observed in regions (a) and (b). Comparison with the satellite image shows
283 that the position of erosion in both regions is consistent (Figure 6). Although the actual amount of
284 erosion is unknown, this indicates that the planar spread of the eroded part can be relatively well
285 reproduced relatively by the calculation. Region (a) was further investigated in detailed as the area
286 corresponds to the point where sediment outflow was confirmed by Jankaew et al. (2008) in the
287 following section.

288

289

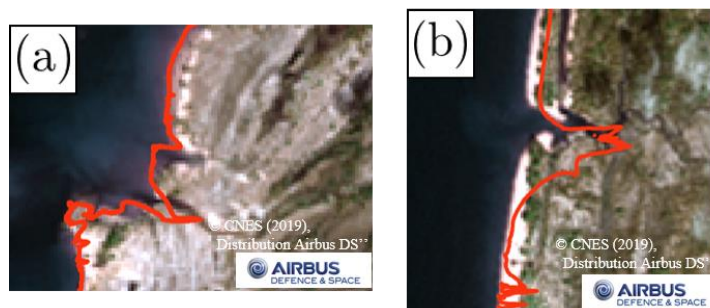


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291

Figure 5 Topographic change and shoreline position immediately after the tsunami

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293

294

Figure 6 Comparison of shoreline position in satellite image and calculation results (© CNES, 2019, Distribution Airbus DS)

295



296 **3.1.3. Sediment layer**

297 Here we discuss the distribution of sediment thickness from the sediment transport models based on
298 sediment data from prior studies. Figure 7 compares sediment layer thickness in this calculation with
299 sediment data from 148 points (Jankaew et al., 2008; Gouramanis et al., 2017).

300 Although the calculated value of sediment thickness is slightly overestimate in general, Figure 7
301 shows that the inland thinning tendency is reproducible. Because overestimation is a result of
302 considering the entire area as a movable bed in the calculation, ground which is not easily eroded in
303 reality may appear excessively eroded.

304 The grain size in this calculation is based on using sediment data (Gouramanis et al., 2017) from one
305 point in region (a) of Figure 5 as a representative value of the entire area. It is possible that the grain
306 size may not be representative of the sediment within region (a). Therefore, Figure 8 shows the result
307 of calculations with the larger grain size $D_{50} = 0.3$ mm as a representative value.

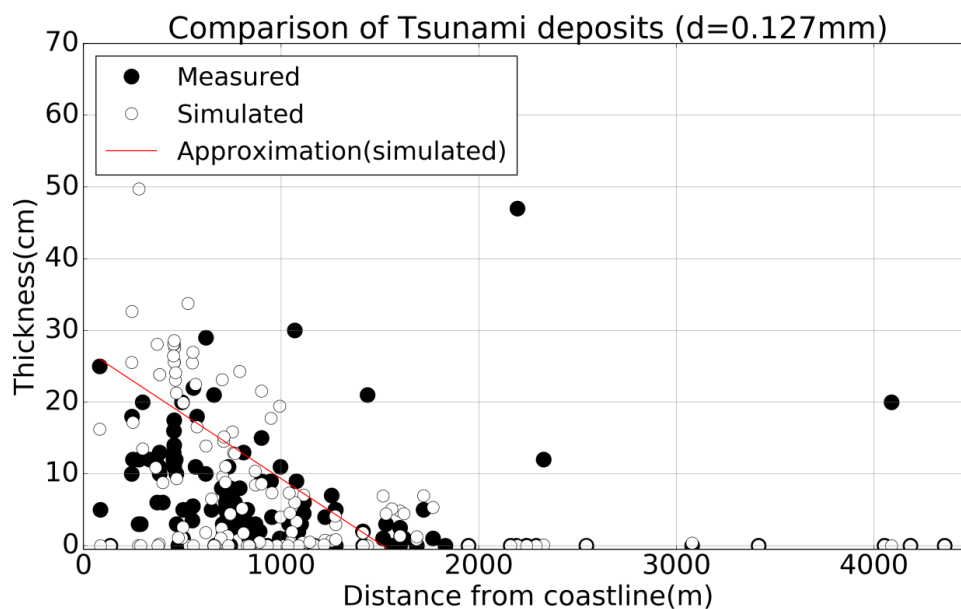
308 Figure 8 confirms the improved reproducibility through smaller variation of calculation results
309 compared with $D_{50} = 0.127$ mm. Future studies should consider that the grain size considered
310 representative in region (a) may not be representative of the wider area, and further sediment grain size
311 analysis of the 2004 IOT sediment deposits from elsewhere on the island may improve tsunami sediment
312 transport modelling onto the island.

313 In addition, Figures 7 and 8 confirm that tsunami inundation of Phra Thong Island exceeded 2,000
314 m, and the grain size had no influence to the simulated inundation distance. In areas where the
315 inundation distance exceeded 2,000 m, i.e. near the inundation limit and along the large tidal channels
316 in the east, the measured tsunami deposits of 10 cm or more exist could not be reproduced by the
317 simulation. There are two possible reasons for this. (1) In the Great East Japan Earthquake tsunami,
318 sandy sediments were deposited up to 57–76% of the inundation limit, and muddy sediments were
319 deposited further inland (Goto et al., 2011b; Goto et al Abe et al., 2012; Chague'–Goff et al., 2012).
320 The same phenomenon may therefore have occurred. However, there is not much mud in this system.
321 The beach ridges are mostly medium to coarse sand as is the nearshore and offshore environment.
322 Therefore, this assumption may not be applicable to Phra Thong Island (2) It is possible that the tsunami
323 eroded sediment within the tidal channels as the tsunami flowed out of these channels. This suggests
324 that finer grain sizes were deposited beyond 2,000 m of the western coast.

325

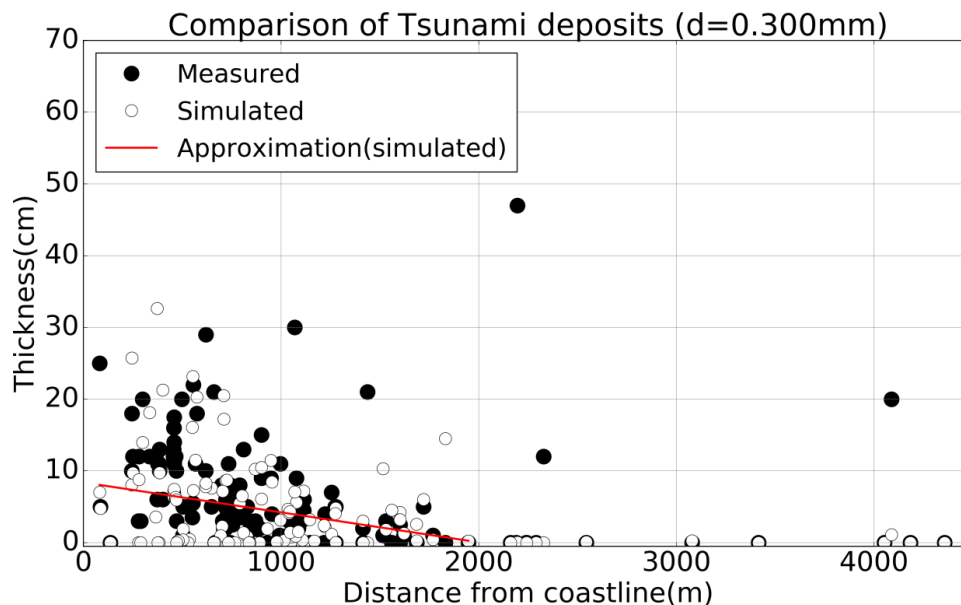
326 **3.2. Sediment transport process**

327 Figure 5 shows the local erosion caused by the sediment transport processes in region (a). The
328 calculated time series changes of water level and ground height at point P in region (a) are shown in
329 Figure 9. It is apparent from Figure 9 that the first wave arrived 2 hours 40 minutes after the earthquake,
330 and backwash was generated 10 minutes later. At Point P. the ground elevation increased by about 50
331 cm through sediment deposition during the first inflowing wave and was largely eroded during the
332 backwash, so beach loss in region (a) is considered to be a result of erosion during the backwash.



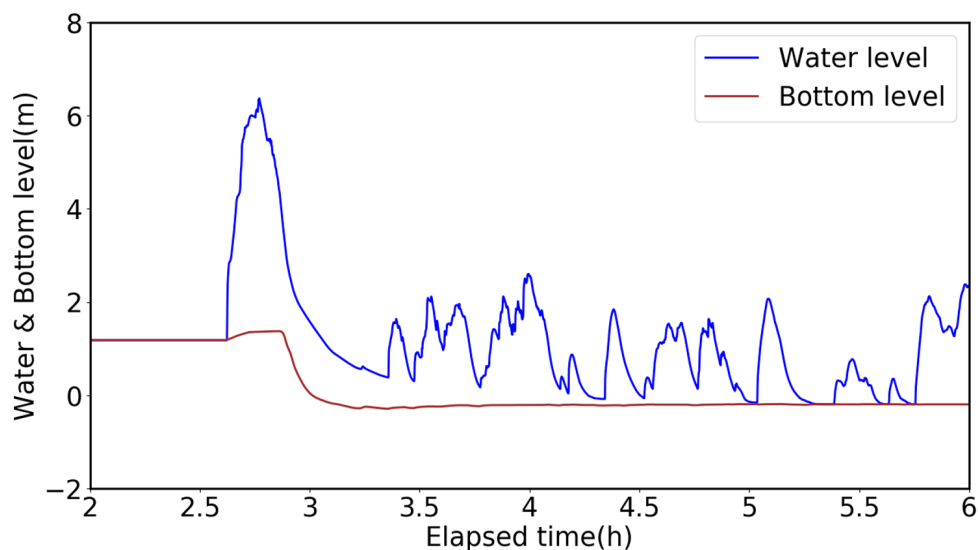
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Figure 7 Comparison of tsunami deposit thickness with representative grain size $D_{50} = 0.127$ mm (calculated value and measured value)



337
338
339
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Figure 8 Comparison of tsunami deposit thickness with representative grain size $D_{50} = 0.300$ mm (calculated value and measured value)



341

342 Figure 9 Chronological change of water level and ground height at point P in region (a)

343

344 Additionally, based on the waveform (which assumes a flat surface), a cross section calculation was
345 carried out along the survey line in Figure 2. Figure 10 shows the chronological changes in ground
346 height, water level, suspended sediment concentration and saturation of suspended sediment
347 concentration on the survey line at each unit of time. As shown in Figure 10, seabed erosion was
348 observed at a depth of about 20 m or less during the first inflowing wave because of increased suspended
349 sediment concentration and decreased of sea depth. The eroded sediment was transported into the
350 shallow water area thereafter, and the concentration of suspended sediment far exceeded the saturation
351 of suspended sediment concentration in the vicinity of the shoreline. Sedimentation was therefore
352 considered predominant near the shoreline. In other words, it is estimated that sediment eroded in the
353 shallow water area during the first lead wave, and much sediment was transported inland. After the run-
354 up, suspended sediment concentration decreased, and most of the sediment that eroded in the shallow
355 water area was deposited near the shoreline, while the remainder was transported inland. Inland, it was
356 found that erosion and deposition occurred according to topographical conditions.

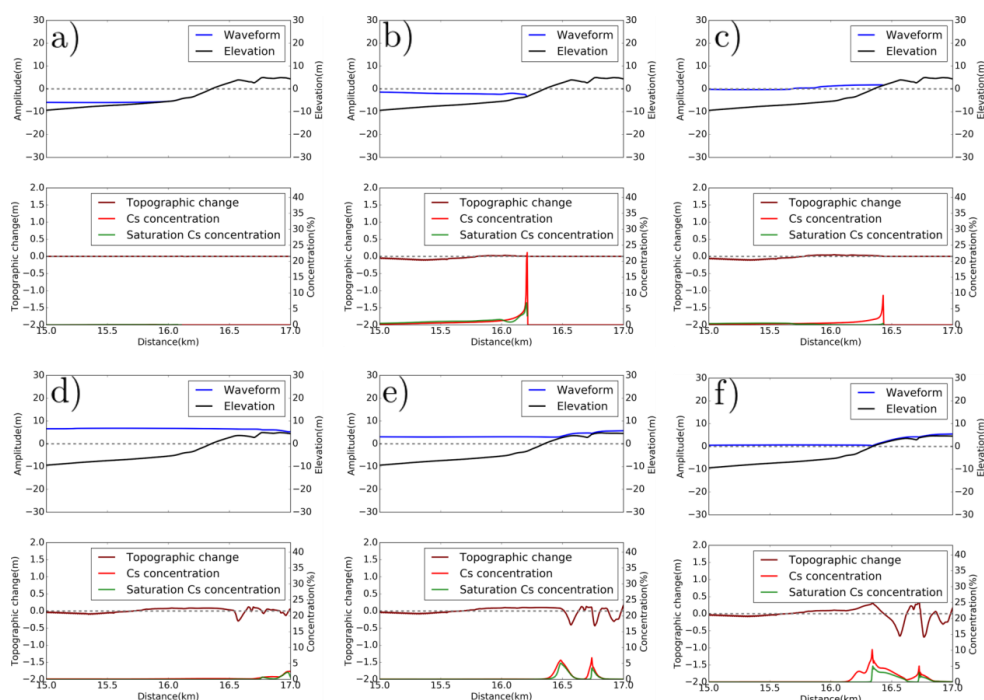
357 During the backwash, the suspended sediment concentration near the shoreline rises as the backwash
358 progresses offshore, thus the beach near the shoreline was eroded by the backwash and flowed out to
359 sea.

360

361 4. Discussion

362 4.1. Sediment transport process and beach recovery factors

363 Region (a) in Figs 5 and 6 were selected for detailed investigation of the simulation results and
364 discussion. In the sediment transport process on Phra Thong Island, a tsunami wave large enough to

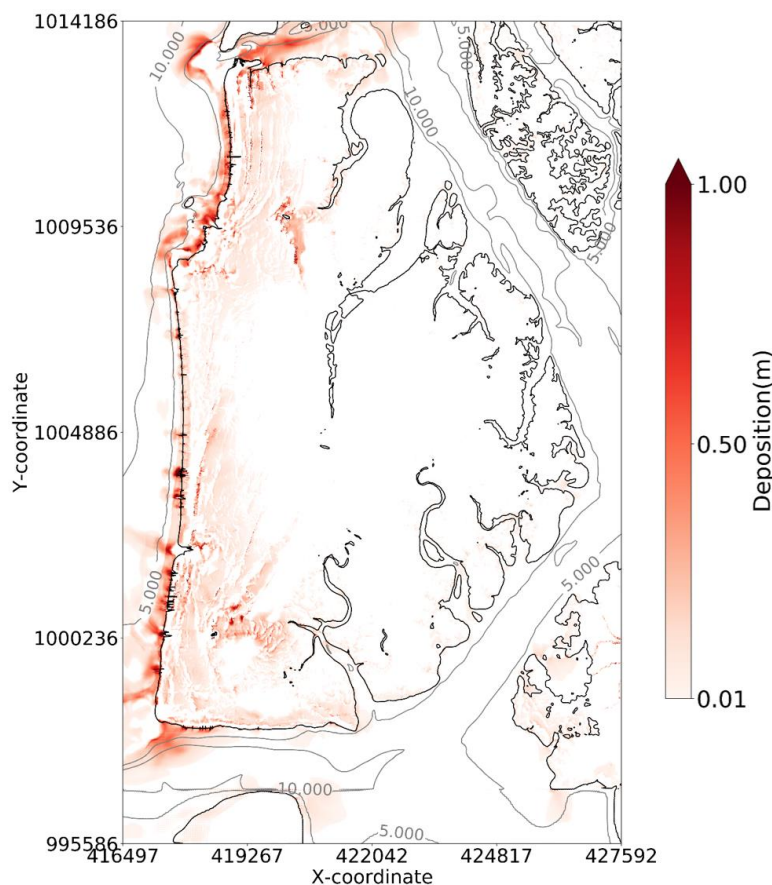


365

366 Figure 10 Change in water level, flow velocity, ground height, suspended sediment concentration, and
367 saturation suspended sediment concentration by section calculation along the survey line in (a) 1st
368 backwash, b) Prior to 1st leading wave run-up, c) Start of 1st leading wave run-up, d) Advance of
369 1st leading wave run-up, e) Start of 2nd backwash, f) Advance of 2nd backwash

370

371 expose the nearshore sediments ran up the exposed nearshore area while retaining sediment from the
372 shallow water. The sediment concentration gradually increases while running up the relatively long
373 distance of the exposed nearshore, and became sediment-saturated as the wave reached the shoreline,
374 making it difficult for new sediment to be eroded further. This can explain why the degree of beach
375 erosion is small during the leading wave, and may be a characteristic sediment transport property of
376 shallow beaches like those on Phra Thong Island. In other words, numerical simulation results suggest
377 that there is little transportation of sediments from the shoreline by the first inflowing wave and that
378 inland deposits were formed by sediment transported from the sea. Similarly, analysis of microfossils
379 (Sawai et al., 2009) from preserved 2004 IOT tsunami deposits inland suggests that tsunami deposits
380 on Phra Thong Island originated from shallow nearshore zone. Pham et al. (2018) suggested that
381 sediment grain sizes and mineralogy were most similar to those of nearshore sediments, but that
382 geochemically the 2004 IOT sediments were a combination of nearshore and onshore sources, but that
383 quantifying the contributions from different environments remains a challenge. The sediment transport
384 modelling suggests that most sediment comes from the shallow offshore and nearshore environment.
385 Figure 11 shows the results of the calculated sediment deposition onshore and offshore Phra Thong



386

387 Figure 11 Sediment distribution (showing depth contours at 5 m intervals in the sea area)

388

389 Island. From the modelling results, most of the eroded sediment in region (a) was deposited in shallow
390 nearshore environments in water less than approximately 5 m deep.

391 Therefore, the calculations show that the sediment that flowed from the lost beach was deposited in
392 relatively shallow water, which would facilitate rapid recovery of the coastal environment shortly after
393 the tsunami, when normal coastal conditions return. This study considered only sediment transport and
394 topographic change caused by the tsunami to determine the initial condition of the recovery process.
395 However, our results show that sediment flowing out from the beach were deposited in relatively
396 shallow water, allowing for rapid sediment transport to the shoreline in subsequent coastal conditions.
397 Future studies can build on these findings to determine the offshore extent of sediment transport and
398 deposition, and identify the processes of coastal recovery on Phra Thong Island. The erosion of the
399 beaches changed the sediment budget significantly, with large volumes of sediment relocated into the
400 nearshore. The removal of sediment from the coastal zone also generated accommodation space which
401 was rapidly infilled upon normal wave and tidal conditions.



402 Geomorphologically, the Sendai Plain, which was inundated by the March 11, 2011 Great East Japan
403 tsunami, is similar to the beach ridge plain on Phra Thong Island (refs needed), but most of the tsunami
404 sediment deposited onshore came from terrestrial sources (Goto et al., 2012; Szczucin'ski et al., 2012;
405 Takashimizu et al., 2012; Sugawara et al., 2014). However, the Great East Japan tsunami differed from
406 the 2004 IOT as the Japanese event had a much smaller receding wave (Nationwide Ocean Wave
407 information network for Ports and HARbourS, NOWPHAS). As such the Japanese tsunami may not
408 have achieved sediment saturation as the wave approached the shoreline, thereby containing a lower
409 sediment concentration and allowing large volumes of sediment to be entrained from the beach for
410 subsequent formation of inland deposits. The different sources of deposited sediment in the two areas
411 reflects contrasting characteristic sediment transport properties on shallow beaches, and may be useful
412 for estimating paleotsunami from coast recovery and geological records.

413

414 **4.2. Limits of calculation results**

415 This study analyzed tsunami sediment transport on Phra Thong Island using numerical calculations
416 and assumed that the island was unvegetated and lacked topography. However, the western half of the
417 island has an undulating surface caused by the beach ridge and swale system, and is extensively
418 vegetated with trees and dense grasses on the ridges and thick grasses within the swales. The eastern
419 half of the island has wide tidal channels and an extensive fringing mangrove system. Both topography
420 and differing vegetation types add complexity to the inundation and backflow sediment transport
421 models not captured here. In future, it is necessary to consider the influence of vegetation on tsunami
422 sediment transport.

423 Another potential limitation of the model is the selection of a single (median) grain size for the
424 sediments. As shown in previous studies (e.g. Sugawara et al., 2014a), the assumption of transport of
425 single grain sized sediment differs from actual situations because of the distribution of grain sizes
426 mobilised and deposited by tsunami. Therefore, it is important to set representative grain sizes and fully
427 study how grain size affects tsunami sediment transport. Future modelling may consider simulating the
428 suite of grain sizes individually or simulating a population of grain sizes that are identified in the modern
429 environment and in preserved tsunami deposits.

430 Furthermore, although the calculation was performed considering the entire area a movable bed, the
431 existence of fixed beds, such as rocky areas, should be considered. We consider this a minor component
432 of this research as the rocky headlands that serve as fixed beds are relatively small in area and would
433 contribute little to the overall simulations in our models.

434 Sugawara et al. (2014b) considers the simulation result of sediment layer thickness using the tsunami
435 sediment transport calculation to be affected by grain size, bottom conditions and topographic data.
436 Their study showed that the layer thickness increases as grain size becomes finer and the layer thickness
437 distribution tendency was unchanged regardless of grain size. Similar results were obtained in this study.
438 Additionally, because bottom surface roughness greatly affects sediment transport near the shoreline,
439 varying bottom surface conditions may influence future modelling results on Phra Thong Island.



440 **5. Conclusion**

441 Because of insufficient knowledge about the topographic recovery process after a tsunami, this study
442 used sediment transport modelling to identify the erosional and depositional processes affecting the
443 beach at Phra Thong Island, Thailand during the 2004 Indian Ocean Tsunami.

444 First, it was confirmed by comparing the measured and calculated values of the sediment layer
445 thickness that the location of beach runoff identified on Phra Thong Island was reproducible and
446 consistent with sediment transport results. Based on the sediment transport results we conclude that the
447 processes of sediment erosion and deposition on Phra Thong Island are characterized by the following
448 sequence:

- 449 • erosion caused by the inflowing waves occurred at a relatively shallow location in the offshore
450 area and the transported sediment was deposited near the shoreline;
- 451 • the inflowing waves caused minimal erosion of the shoreline;
- 452 • onshore sediment deposition is due to onshore topographical features trapping sediments prior
453 to backwash; and,
- 454 • erosion of the shoreline was largely caused by backwash resulting in onshore sediments
455 deposited in the shallow nearshore zone.

456 Rapid beach recovery on Phra Thong Island is facilitated due to the large volume of sediment deposited
457 in the nearshore zone and the large accommodation space available for remobilization and redeposition
458 of sediments when normal coastal conditions resume soon after the tsunami causing a re-equilibration
459 of the beach.

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470

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