



1           **Towards an Automatic Early Warning System of Flood**  
2           **Hazards based on Precipitation Forecast: The case of the**  
3           **Miño River (NW Spain)**

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18    **Abstract:** An Early Warning System for flood prediction based on precipitation forecast  
19 is presented. The system uses rainfall forecast provided MeteoGalicia in combination  
20 with a hydrologic (HEC-HMS) and a hydraulic (Iber+) models. The upper reach of the  
21 Miño River and the city of Lugo (NW Spain) are used as a study area. Starting from  
22 rainfall forecast, HEC-HMS calculates the streamflow and Iber+ is automatically  
23 executed when a certain threshold is exceeded for some previously defined risk areas.  
24 The analysis based on historical extreme events shows that the system can provide  
25 accurate results in less than one hour for a forecast horizon of 3 days and report an alert  
26 situation to decision-makers.

27    **1. Introduction**

28    According to Noji (2000), floods are one of the most dangerous natural hazards in the  
29 world. Jonkman (2005) estimates that more than 100,000 deaths in the last century were  
30 caused by floods. From 1940 to 2018 the number of deaths related with flood events  
31 (8138) is only surpassed by the lightning fatalities (9386) in the U.S.  
32 (<https://www.nws.noaa.gov/om/hazstats.shtml>). Furthermore, the effect of the Climate  
33 Change will increase the number of flood events and their negative impact to people and  
34 properties (Dankers and Feyen, 2008; Alfieri et al., 2017). Therefore, the ability to predict  
35 these extreme events and prevent their consequences is a challenge for the scientific  
36 community worldwide.



37 In this context early warning systems (EWS) play a key role. UNISDR (2009) defines  
38 early warning systems as “the set of capacities needed to generate and disseminate timely  
39 and meaningful warning information to enable individuals, communities and  
40 organizations threatened by a hazard to prepare and to act appropriately and in sufficient  
41 time to reduce the possibility of harm or loss”. A complete EWS is divided into four steps:  
42 (1) risk knowledge, (2) monitoring, forecasting and warning, (3) communication of an  
43 early warning system and (4) response capability [UN, 2006]. The first two steps are  
44 related to the field of physical sciences while the two last steps are associated to social  
45 science aspects. There are several works related to the impact of the early warning system  
46 in the prevention of floods. Baudoin et al. (2014) and UNISDR (2015) show some  
47 interesting examples on how early warning systems can save lives and reduce the damage  
48 to the people. Borga et al. (2011) developed an early warning system methodology for  
49 flash floods in Europe through the HYDRATE project. The authors enhance the  
50 capability of flash flood forecasting in ungauged basins by exploiting the extended  
51 availability of flash flood data and the improved process understanding. Alfieri et al.  
52 (2012) analyse several early warning systems applied to detect surface water flooding,  
53 flash floods, debris flows, land-slides induced by extreme rainfall events, river and coastal  
54 floods. The authors proposed several tasks to palliate the main drawbacks of some of  
55 these systems. Also, Hossain et al. (2014) and Cools et al. (2012) where a satellite-based  
56 forecast system is applied to measure the water depth of the river at the “Valley of Death”  
57 and an early warning system to detect flash flood is developed to the Sinai Peninsula,  
58 respectively. In Europe a very interesting example of an early warning system is the EWS  
59 applied to the region of Flanders (Schelfaut et al., 2012 and CIW, 2013). In this work, the  
60 different steps are analysed under the FREEMAN project (Flood RESilience  
61 Enhancement and MANagement). The European Flood Awareness System (EFAS) is  
62 also another example of an EWS developed to the sponsorship of the European  
63 Commission. This system provides daily streamflow forecast for Europe starting from up  
64 to 10-days weather forecast (medium-term forecast). More details of this model can be  
65 shown in Thielen et al. (2009), Pappenberger et al. (2011), Cloke et al. (2013) and Alfieri  
66 et al. (2014). Using this model Dottori et al. (2017) develop a methodology to adapt EFAS  
67 to real time forecasting. Demerit et al. (2013) analyse the problems derived from the use  
68 of the early warning system to medium and long-term flood forecast, mainly the  
69 dissemination of the information to people potentially affected by these events. They  
70 reveal that flood forecasters usually wait the confirmation from local institutions



71 (Hydrologic Confederations...) instead of acting based on the information provided by  
72 the early warning systems. These local systems are focused in short-term forecast (0 to  
73 48 h) that are more suitable to evacuation than fore damage mitigation. The latter is  
74 associated to the long and medium-term forecasts provided by the European early  
75 warning systems.

76 In this paper, a flood early warning system based on precipitation forecast is presented.  
77 The system, which is being developed in collaboration with the Hydrographic  
78 Confederation of Miño-Sil River, consists of three steps: i) precipitation forecast; ii) use  
79 of a hydrologic model to detect extreme flows; iii) use of a hydraulic model that is applied  
80 at certain areas only under extreme flows. Starting from 1-day, 2-day and 3-day  
81 precipitation forecast windows provided by the Regional Meteorological Office  
82 (MeteoGalicia), the outflows associated to the catchment of the Miño River (NW Spain)  
83 were obtained using the HEC-HMS model (U.S. Army Corps of Engineers, 2018). This  
84 model was previously calibrated for the area of study by means of series of historical  
85 flood events detected over the last decade. The numerical model Iber (Bladé et al., 2014)  
86 was used to obtain water depth and velocity under extreme flow conditions for some risk  
87 areas where previous events have caused damages or material loses. Both models (i.e.,  
88 HEC-HMS and Iber) are freely available software so the system can be applied at any  
89 location without costs derived from the licences of commercial codes.

90 The paper, which aims to describe the steps followed to develop the EWS, is organized  
91 as follows. First, a description of the area of study (the upper reach of Miño River and the  
92 city of Lugo, NW Spain) is shown. Then the methodology to obtain the weather forecast,  
93 the computation of the run-off and the hydraulic processes are briefly presented. Also the  
94 communication among all the models (Precipitation Forecast - Run-Off - Hydraulic  
95 processes) is explained. Next, the results of the precipitation and outflow forecast of a  
96 series of historical flood events are presented along with a statistic analysis of their  
97 accuracy. Finally, the numerical water depth obtained for a particular flood event at the  
98 city of Lugo is shown and compared with field data measured during the event.

## 99 **2. Study area**

100 The area of study is located in north-western Spain (Figure 1). It corresponds to the upper  
101 reach of the Miño River. This catchment area is about 2200 km<sup>2</sup> and the elevation ranges



102 from 360 to 980 m.a.s.l. The average annual precipitation ranges from 144 to 1300 mm  
103 year<sup>-1</sup>.

104 Figure 1 (upper-left panel) shows the catchment of the upper reach of the Miño River,  
105 which is divided into three main sub-basins according to their topographic characteristics.  
106 Seven rain gauges operated by MeteoGalicia are located in the entire catchment. Table 1  
107 shows the location and the elevation of each of the rain gauges located in the upper reach  
108 of the Miño River. The outlet of this catchment is located in the city of Lugo (Figure 1,  
109 lower panel). This area is usually flooded during the events of extreme precipitations in  
110 the upper reach of the Miño River. The absence of dams in the catchment to regulate the  
111 flow also affect the high frequency of these events.

### 112 **3. Methodology**

113 In this work, an automatic EWS is proposed. This system is composed of several elements  
114 as shown in Figure 2. All these components are orchestrated by a Python script that is the  
115 responsible of gather and transform the data properly in order to feed the models used in  
116 the system. First of all, the rainfall forecast performed with the Weather Research and  
117 Forecasting model is provided by the weather agency (MeteoGalicia). Details are  
118 provided in next section. Forecasted data are automatically downloaded and the rainfall  
119 relative to each sub-basin is extracted to feed the hydrological model HEC-HMS. When  
120 the catchment outflow obtained with HEC-HMS surpasses the 90<sup>th</sup> percentile of historical  
121 data, it is considered as a possible extreme event and the following steps will be applied.  
122 In that case, this outflow will be used as inlet condition for the hydraulic simulation using  
123 the model Iber+ to provide flood maps with water depths and velocities at certain risk  
124 areas (the city of Lugo in this particular case). Data provided by Iber+ are processed for  
125 hazard evaluation. At this stage the system checks if there is a risk condition in the areas  
126 accessible by pedestrians. These areas are user defined and can be changed depending on  
127 seasonal events. In order to emit a warning alert, the criteria of Cox et al. (2010) are used  
128 to define safety limits for children since they are the most vulnerable population group.  
129 Following this criterion, a warning will be emitted if there is a zone where any of the  
130 following thresholds are surpassed: the water depth ( $h$ ) is higher than 0.5 m, the water  
131 velocity ( $v$ ) is higher than 0.2 ms<sup>-1</sup> or the product ( $h \cdot v$ ) excess 0.4 m<sup>2</sup>s<sup>-1</sup>. This warning is  
132 sent in form of report to a decision maker, so an expert can validate the resulting data and  
133 discard false positives.



134 The details of the components of the EWS, the data sources, and the calibration processes  
135 are shown in the following sections.

### 136 **3.1 Precipitation data**

#### 137 **3.1.1 Forecasted precipitation data**

138 Forecasted precipitation data were obtained from the Regional Meteorological Office  
139 (MeteoGalicia, <http://www.meteogalicia.gal/>). MeteoGalicia publishes weather forecast  
140 results based on the Weather Research and Forecasting (WRF) Model (Skamarock et al.,  
141 2005) (<http://www.wrf-model.org>). The WRF model is a numerical weather prediction  
142 system at regional mesoscale designed mainly for forecasting applications. WRF is run  
143 operationally since 2008 providing daily data until the end of 2012 (00 UTC) and twice  
144 a day (00 UTC and 12 UTC) from then on, with a 72- hour forecast window, a temporal  
145 resolution of 1 hour and maximum spatial resolution of 4 km (Sousa et al., 2013). Data  
146 provided by MeteoGalicia are freely available at its THREDDS (Thematic Realtime  
147 Environmental Distributed Data Service) server, also maintaining an historical archive of  
148 past forecast since 2008. The model outputs provide several variables related to weather.  
149 In the case of this study, precipitation information was automatically obtained for the  
150 areas under interest at the 00 UTC of each day during the period 2008-2018.

#### 151 **3.1.2 Measured precipitation data**

152 Real precipitation data at hourly scale were obtained from the rain gauges managed by  
153 MeteoGalicia, which is responsible of their maintenance and data quality control. Data  
154 from these rain gauges will be used to assess the performance of the MeteoGalicia  
155 Weather Forecast to predict extreme rain events. The rain gauges selected for this study  
156 were shown in Figure 1 and their location and elevation is detailed in Table 1.

### 157 **3.2 River discharge data**

158 Daily discharge data of the Minho River were provided by the corresponding river Basin  
159 Authority (Confederación Hidrográfica del Miño-Sil, <https://www.chminosil.es>). In this  
160 case of study, Miño flow data at Lugo station covering the period 2008-2018 were  
161 selected. River data were used to calibrate and validate the hydrologic model system used  
162 during the development of this study.



### 163 3.3 HEC-HMS & Iber+

164 Here the hydrological and hydraulic models used in the study will be briefly described  
165 along with the methods to analyze their accuracy.

166 The distributed model HEC-HMS (Feldman, 2000 and U.S. Army Corps of Engineers,  
167 2018) was used to analyse the rain-runoff processes and the numerical code Iber (Bladé  
168 et al., 2014) was used to compute the hydraulic processes.

169 The HEC-HMS is a model developed by the US Army Corps of Engineers that is applied  
170 to simulate continuous hydrological processes. The HEC-HMS model can be used to  
171 analyse various hydrological aspects, such as flooding events, reservoir capacity,  
172 stormwater warnings, and stream restoration (U.S. Army Corps of Engineers 2008).  
173 HEC-HMS is divided into four components: (i) an analytical model: calculation of direct  
174 runoff and channel routing; (ii) a basin model: representation of hydrological elements in  
175 a watershed; (iii) a system to manage input data and store data; (iv) a post-processing tool  
176 to report and illustrate simulation results.

177 Taylor diagrams (Taylor, 2001) were used to compute the accuracy of the results obtained  
178 with HEC-HMS by means of the normalised standard deviation (Eq. 1), centred root-  
179 mean square difference (Eq. 2) and correlation (Eq. 3).

180

$$181 \quad \sigma_{n,A} = \frac{\sqrt{\frac{\sum_{i=1}^N (A_i - \bar{A})^2}{N}}}{\sigma_B} \quad (1)$$

182

$$183 \quad E_{n,A} = \frac{\sqrt{\frac{\sum_{i=1}^N [(A_i - \bar{A}) - (B_i - \bar{B})]^2}{N}}}{\sigma_B} \quad (2)$$

184

$$185 \quad R_A = \frac{\sum_{i=1}^N [(A_i - \bar{A})(B_i - \bar{B})]}{N \sigma_A \sigma_B} \quad (3)$$

186

187 where  $A$  is a numerical variable and  $B$  a reference variable. The subscript  $i$  refers to the  
188 different samples,  $N$  is the number of samples, barred variables refer to mean values and  
189  $\sigma$  is the standard deviation.

190 The hydraulic simulations were carried out using the numerical model Iber (Bladé et al.  
191 2014). Iber is a numerical code that solves the 2D Shallow Water Equations by means of  
192 finite volume schemes (FVS). The software package is formed by three elements: pre-



193 processing tool, numerical model and post-processing tool. The first and the last modules  
194 are based in the software GID (GID, 2018). It provides a user friendly graphical interface  
195 (GUI) to create the case and edit the parameters that define the problem to solve. It also  
196 provides tools to analyse the results of the numerical simulations. The pre-processing and  
197 post-processing tools were used only during the modelling and testing of the study area.  
198 However, the automatic EWS runs the model in batch mode without user interaction. Iber  
199 was recently improved in terms of efficiency becoming Iber+ (García-Feal et al. 2018).  
200 This new parallel implementation of the Iber model takes advantage of GPU computing  
201 using the Nvidia CUDA (NVIDIA CO., 2019) platform. Using this technology, the new  
202 implementation is able to run up to 100 times faster. This fact makes Iber+ especially  
203 suitable for the implementation of an EWS where the response times can be crucial to  
204 issue an early alert. The accuracy of the water depth results computed with Iber+ at  
205 several control points was assessed by means of the *bias* and the *RMSE* (Root Mean  
206 Square Error) relative to the values measured *in situ* during the extreme event recorded  
207 on January 2013.

## 208 **4. Results and discussion**

### 209 **4.1 Accuracy of MeteoGalicia Precipitation Forecast**

210 The capability of MeteoGalicia Weather Forecast system to predict rain events was  
211 evaluated by means of the comparison with real precipitation data provided by the rain  
212 gauges in the area of study. For that purpose, the predicted (numerical) precipitation was  
213 obtained at the closest grid points to the location of the rain gauges. The correlation  
214 between predicted and measured precipitation was calculated for each rain gauge during  
215 the available period (2008-2018). For this calculation, Spearman rank correlation was  
216 used due to its robustness to deviations from linearity, as well as its strength to the  
217 influence of outliers. This procedure was carried out for 3 forecast windows (1-24 h, 25-  
218 48 h and 49-72 h; 1-day, 2-day and 3-day forecast from now on) to determine the accuracy  
219 of the forecast at different temporal scales.

220 The values of the correlation for each rain gauge are shown in Table 2. In general,  
221 precipitation prediction offers a good representation of the registered values. In fact,  
222 correlations above 0.8 were obtained for the first two windows (1-day and 2-day forecast),



223 although with a higher correlation for the first one. The correlation is slightly lower for  
224 the 3-day forecast, although it is still close to 0.8.

225 Therefore, it can be concluded that the precipitation forecast provided by MeteoGalicia  
226 offers results very close to the real rain events for the entire time series of precipitation  
227 data (2008-2018). This shows the accuracy of MeteoGalicia models to forecast  
228 precipitation events up to three days in advance.

#### 229 **4.2 Calibration and validation of hydrological processes using HEC-HMS**

230 A set of 15 extreme flood events registered during the period 2008-2018 were used to  
231 calibrate and validate the rain-runoff model HEC-HMS by comparing the outflows  
232 measured at the gauge station located at Lugo with the flows obtained with HEC-HMS  
233 using the 1-day forecast of precipitation.

234 Calibration was carried out using the specific calibration tools implemented in HEC-HMS  
235 (Feldman, 2000) in order to choose two independent parameters, the curve number ( $CN$ )  
236 and lag time ( $L_g$ ), for each sub-basin of the domain. Eleven flood events were used for  
237 calibration purposes and the rest of cases were used to validate the model. Table 3 shows  
238 the values of the  $CN$  and  $L_g$  for each sub-basin obtained for each event used in the  
239 calibration step.

240 The mean values of  $CN$  and  $L_g$  of each sub-basin were used to validate the model in four  
241 flood events (01/2013, 01/2014, 02/2016 and 03/2018) by means of a Taylor diagram  
242 (Figure 3).

243 The values of normalised standard deviation range from 0.8 to 1.2, the values of the  
244 root mean squared difference range from 0.3 to 0.6 and the correlation of the numerical  
245 results range from 0.85 to 0.95. These values show that the mean values of  $CN$  and  $L_g$   
246 obtained in the calibration step characterise the behaviour of the basin with a high  
247 accuracy.

248 Figure 4 compares the numerical and measured streamflow for the event that happened  
249 in January 2013 using the three forecast windows. The left panel shows that time series  
250 of the flows predicted by the model are similar to those measured at the gauge station.  
251 The right panel is the Taylor diagram corresponding to the three forecast windows. The  
252 standard deviation is observed to range from 0.8 to 1.2 for the three forecasts. RMSD  
253 values for 1-day and 2-day forecasts are around 0.3, being around 0.6 for the 3-day  
254 forecast. Finally, the correlation coefficient for 1-day and 2-day forecasts are close to  
255 0.95, being around 0.85 for the 3-day forecast.





### 256 4.3 Case of study

257 Once the predicted water flow showed to reproduce the real events with a high accuracy  
258 ( $E_n \sim 0.8$ ,  $\sigma_n \sim 0.3$  and  $R \sim 0.95$ ), the water depth and velocity during the flood event that  
259 affected Lugo on 20<sup>th</sup> January, 2013 were computed using the numerical code Iber+  
260 (Garcia-Feal et al., 2018). Figure 5 shows the numerical domain at Lugo, where seven  
261 land uses were defined to model the characteristics of the terrain. The Manning's  
262 coefficient associated to each land use are shown in Table 4. Figure 5 also shows the  
263 location of the inlet and outlet boundary conditions.

264 The topography of the area of study was obtained from raster files freely downloaded  
265 from the Instituto Geográfico Nacional website (<https://www.ign.es/web/ign/portal>). The  
266 computational domain was discretised using a mesh with near 200,000 unstructured  
267 triangular elements, with an average area of 2 m<sup>2</sup>.

268 Five control points were defined at the area of study (see Figure 6) to analyse the accuracy  
269 of the numerical results. Points from 1 to 4 are located in places next to the riverbank  
270 usually frequented by pedestrians while the last one is located in the riverbed. Therefore,  
271 the first four points are of special interest to issue an alert.

272 Figure 7 shows the values of the water depth obtained in the numerical simulations along  
273 with the water depth measured at the control points during the flood event. The range of  
274 the values of the numerical water depths correspond to 3 times of the standard deviation  
275 of the values obtained from the 12 p.m. to 4 p.m. of January 20<sup>th</sup>, 2013 and the dot  
276 corresponds to the mean value of the water depth during the range of hours defined.  
277 Visually, the numerical results are quite similar to the field data when considering the 1-  
278 day forecast, especially if one considers that the accumulation of the small inaccuracies  
279 of the three models involved can give rise to biases. The values are slightly less accurate  
280 when considering the 2-day forecast and worse for the 3-day forecast due to lower  
281 accuracy in rainfall forecast.

282 Table 5 shows the values of the *bias* and the *RMSE* between measured and computed  
283 water elevations using the three different forecast windows. The minimum values of *bias*  
284 and *RMSE* are obtained with the 24h forecast (0 and 21 cm, respectively). The accuracy  
285 decreases with the forecast window, although results are still good for a 2-day forecast  
286 and acceptable for a 3-day forecast. The *RMSE*, which is a measure of the deviation from  
287 real values, was calculated for the three forecast windows being smaller than 0.5 m, which  
288 is the critical height indicated by Cox et al. (2010). Especially remarkable is the



289 simulation obtained with 1-day forecast, with a deviation of just 21 cm respect to real data  
290 and a null *bias*. The good agreement between the measured and computed values indicates  
291 that the system can be used to issue alert up to 3 days in advance.

292 Figure 8 shows the maximum water depth and maximum velocity obtained for 1-day  
293 forecast. Hazard maps (Figure 9) can be computed from these data according to the  
294 criterion of Cox et al. (2010). Several recreation areas near the riverbanks show to have  
295 surpassed the aforementioned hazard threshold. Therefore, decision-makers can use the  
296 map to restrict activities in these areas, in order to mitigate the consequences of floods.

## 297 **5. Conclusions**

298 In this paper an Early Warning System for flood prediction using precipitation forecast  
299 was presented. This system starts automatically using rain forecast data retrieved from  
300 Regional Meteorological Office (MeteoGalicia) and concatenates two freely available  
301 software packages (HEC-HMS and Iber+). The upper reach of the Miño River (NW  
302 Spain) and, in particular, the city of Lugo were used as a benchmark.

303 A Python script was developed to deal with all the components involved in the system  
304 without user interaction. First, the precipitation forecast provided by MeteoGalicia is  
305 automatically obtained for the area of study. Second, rain forecast is provided to HEC-  
306 HMS as an input to compute the streamflow in the catchment area. When the streamflow  
307 obtained with HEC-HMS surpasses the 90th of the historical percentile at some  
308 previously selected risk area (the city of Lugo in this particular case), the possibility of  
309 an extreme event is detected and that streamflow is automatically defined as an inlet  
310 condition for Iber+. Finally, data obtained from Iber+ are processed for risk assessment  
311 and, if applicable, decision makers are reported.

312 The accuracy of the different models was assessed to analyse the capability of the system  
313 to provide reliable results. First, the accuracy of the precipitation forecast provided by  
314 MeteoGalicia was analysed for the period 2008-2018 showing that the 1-day forecast is  
315 slightly more accurate than the 2-day forecast, being the 3-day slightly worse, although  
316 the three forecast windows showed a reasonable agreement with field data. As a second  
317 step, the accuracy of HEC-HMS to reproduce extreme flows was assessed by means  
318 fifteen flood events recorded over for the period 2008-2018. Taylor diagrams were used  
319 to compute the accuracy of the numerical streamflow compared with field data obtained  
320 at the control station located near Lugo. Once again, results were satisfactory for the three



321 forecast windows, especially for the 1-day and 2-day forecast. Finally, a historical flood  
322 event recorded in January, 2013 was used to assess the accuracy of Iber+ to reproduce  
323 real water elevation at 5 control points located at the riverbank and riverbed. Both the  
324 *RMSE* and the *bias* between the measured and computed elevations were satisfactory,  
325 especially for the 1-day forecast.

326 The system needs less than 1 hour to run the models for a 3-day forecast horizon. While  
327 data can be downloaded in a few seconds and the hydrologic model can be run in less  
328 than a minute, no matter the extent of the area, the real bottleneck in the system is the  
329 hydraulic model. Fortunately, the execution time does not necessarily increase with the  
330 number of risk areas since different areas can be run concurrently when the available  
331 hardware resources allow it. Taking into account that meteorological data are available  
332 every day at 5:00 a.m. the system can provide an alert report to decision makers before  
333 6:00 a.m. Additional improvements can be applied without additional cost in term of  
334 runtime. For example, an ensemble approach can be applied when rain forecasts from  
335 different sources are used as an input condition for HEC-HMS, in such a way that Iber+  
336 is only executed when at least one of the hydrological realizations indicates a possible  
337 extreme event.

338 Additional research is still needed to cover the entire Miño river basin, where other  
339 problems may arise from the presence of dams. The system, when fully developed, can  
340 even help to manage dams intelligently, maximizing energy production and dampening  
341 floods at the same time.

342 The Early Warning System can be easily adapted for any area of the world since the  
343 required input data can be obtained freely from public institutions and the models to  
344 compute the hydrological and the hydraulic processes (HEC-HMS and Iber+,  
345 respectively) are both freely available. Therefore, the EWS is especially interesting for  
346 developing countries where the acquisition of commercial software is not sustainable.

347

348

349 *Code and data availability.* Freely available data and software (HEC-HMS and Iber+)  
350 were used for this work. The detailed processing flowchart is shown in Fig. 2 (Section 3  
351 – Methodology).

352

353 *Author contributions:* JGC, OGF and DFN designed the research, conducted the analysis  
354 and wrote the paper, ; JMMDA and MGG supervised the research and revised the paper.



355

356 *Competing interests.* The authors declare that they have no conflict of interest.

357

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#### 469 **Figure Captions**

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471 **Figure 1.** Area of study. The rain gauges ( $rg_1, \dots, rg_7$ ) located in the catchment (upper-  
472 left panel) and the area of study in Lugo (lower panel) are also shown. (PNOA courtesy  
473 of © Instituto Geográfico Nacional).

474 **Figure 2.** Flowchart of the proposed EWS.

475 **Figure 3.** Taylor diagram of the validation cases (01/2013, 01/2014, 02/2016 and  
476 03/2018).

477 **Figure 4.** Time series of the outflow at the control point obtained in the gauge station  
478 (dashed line) and calculated using the three forecast windows (left panel) and Taylor  
479 diagram for the same cases (right panel).

480 **Figure 5.** Numerical domain at Lugo. The land uses and the location of the boundary  
481 conditions (red lines) are also shown. (PNOA courtesy of © Instituto Geográfico  
482 Nacional).

483 **Figure 6.** Location of the five control points at the area of study in Lugo. (PNOA courtesy  
484 of © Instituto Geográfico Nacional).

485 **Figure 7.** Comparison between water depth ( $h$  in meters) between the numerical model  
486 (.) and the field data (x) for the three forecast windows 1-day (left), 2-day (middle) and



487 3-day (right). The range of the numerical values correspond to 3 times the standard  
488 deviation of the elevations obtained from the 12 a.m. to 4 p.m. of January 20<sup>th</sup>, 2013.

489 **Figure 8.** Maximum water depth (upper panel) and maximum velocity (lower panel)  
490 obtained with Iber+ for the 1-day precipitation forecast. (PNOA courtesy of © Instituto  
491 Geográfico Nacional).

492 **Figure 9.** Areas where hazard criterion is surpassed. (PNOA courtesy of © Instituto  
493 Geográfico Nacional).

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496 **Table 1.** Location and elevation of the rain gauges located in the area of study (The  
497 system of reference for latitude and longitude is the EPSG: 4326).

498 **Table 2.** Values of the correlation (Spearman's  $r$ ) of the precipitation forecast using the  
499 measured data as reference at each rain gauge. The averaged values for each precipitation  
500 forecast are also shown.

501 **Table 3.** Curve number ( $CN$ ) and lag time ( $L_g$ ) values for each sub-basin for different  
502 flood events. The mean value and the standard deviation are provided in lower rows.

503 **Table 4.** Manning's coefficients of the numerical domain.

504 **Table 5.** Values of the  $RMSE$  and  $bias$  for three forecast windows.

505





506 **Table 1.** Location and elevation of the rain gauges located in the area of study (The  
 507 system of reference for latitude and longitude is the EPSG: 4326).  
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Rain gauge id.	Name	Latitude	Longitude	Elevation (m.a.s.l.)
rg <sub>1</sub>	Labrada	43.4054	-7.50205	662
rg <sub>2</sub>	Lanzós	43.3746	-7.64468	470
rg <sub>3</sub>	Guitiriz-Mirador	43.2266	-7.78307	684
rg <sub>4</sub>	Sanbreixo	43.1457	-7.79112	496
rg <sub>5</sub>	Castro de Rei Lea	43.1559	-7.48588	428
rg <sub>6</sub>	Pol	43.1626	-7.28258	647
rg <sub>7</sub>	Corno do Boi	43.0374	-7.89265	731

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**Table 2.** Values of the correlation (Spearman's  $r$ ) of the precipitation forecast using the  
 measured data as reference at each rain gauge. The averaged values for each precipitation  
 forecast are also shown.

Rain gauge	Forecast window (h)		
	1-24	25-48	49-72
rg <sub>1</sub>	0.84	0.82	0.77
rg <sub>2</sub>	0.84	0.82	0.79
rg <sub>3</sub>	0.83	0.81	0.77
rg <sub>4</sub>	0.81	0.79	0.75
rg <sub>5</sub>	0.81	0.80	0.76
rg <sub>6</sub>	0.84	0.83	0.79
rg <sub>7</sub>	0.83	0.81	0.77
Mean value	0.83	0.81	0.77

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**Table 3.** Curve number ( $CN$ ) and lag time ( $L_g$ ) values for each sub-basin for different  
 flood events. The mean value and the standard deviation are provided in lower rows.

Date of the flood event	Sb <sub>1</sub>		Sb <sub>2</sub>		Sb <sub>3</sub>	
	$CN$	$L_g$ (min)	$CN$	$L_g$ (min)	$CN$	$L_g$ (min)
12/09	92	1154	97	2700	98	2770
11/10	80	1140	84	2702	80	2781
03/13	79	1157	96	2701	99	2774
11/13	80	1148	86	2685	83	2778
01/14	78	1155	96	2700	98	2767
03/14	81	1153	88	2706	92	2764
01/15	96	1153	99	2701	99	2773
03/15	81	1151	91	2700	98	2771
02/16	81	1155	88	2700	98	2767
03/16	82	1153	80	2711	84	2764
03/18	80	1152	82	2691	93	2769
Mean	85	1152	90	2700	93	2771
$\sigma$	6	4	6	7	7	5

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526 **Table 4.** Manning's coefficients of the numerical domain.

Land's uses	Manning's coefficient ( $\text{s m}^{-1/3}$ )
River	0.025
Brush	0.050
Trees	0.120
Sparse vegetation	0.080
Infrastructure	0.020
Industrial	0.100
Residential	0.150

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531 **Table 5.** Values of the *RMSE* and *bias* for three forecast windows.

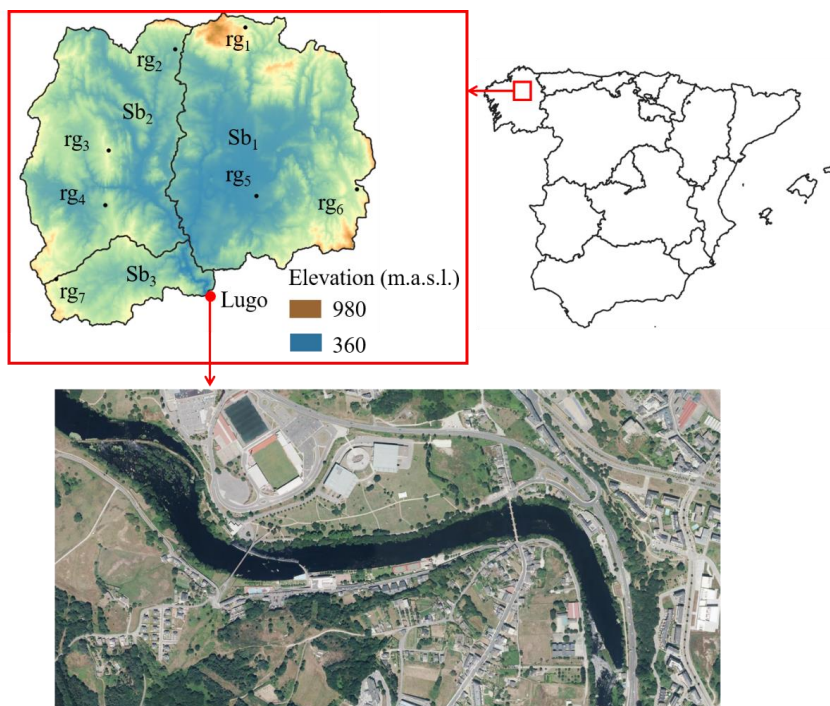
	<i>RMSE</i> (cm)	<i>bias</i> (cm)
1-day	$21 \pm 5$	$0 \pm 5$
2-day	$28 \pm 6$	$4 \pm 6$
3-day	$41 \pm 5$	$-35 \pm 5$

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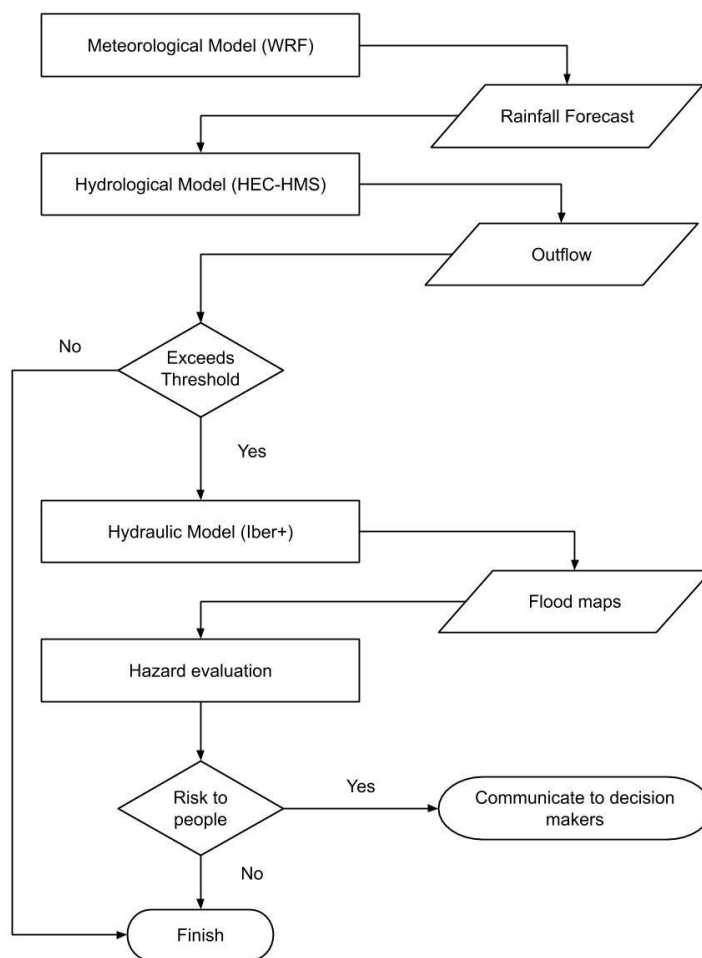
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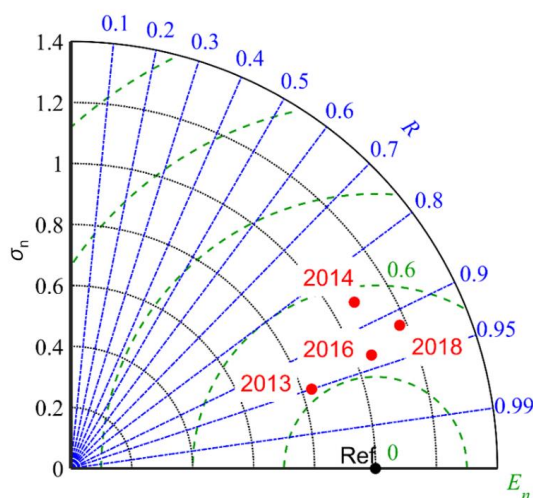


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547 **Figure 2.** Flowchart of the proposed EWS.

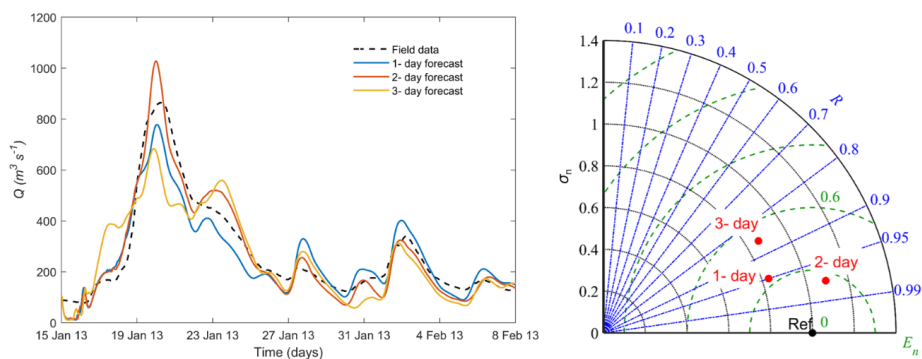
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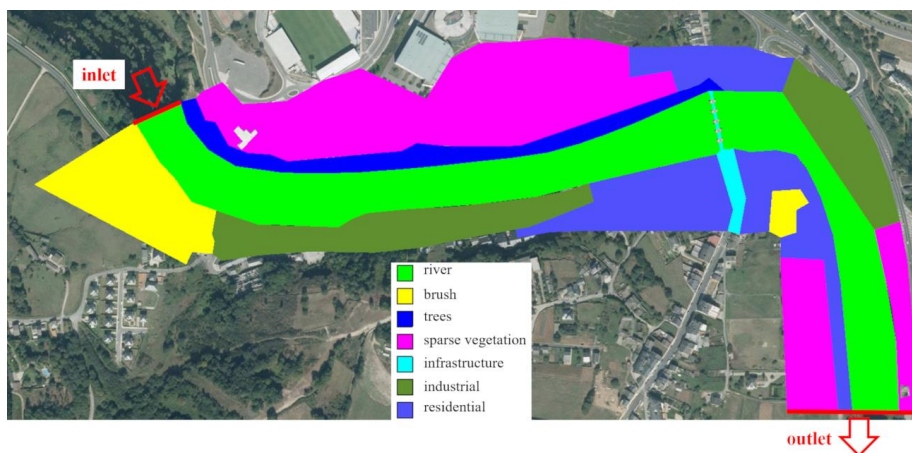
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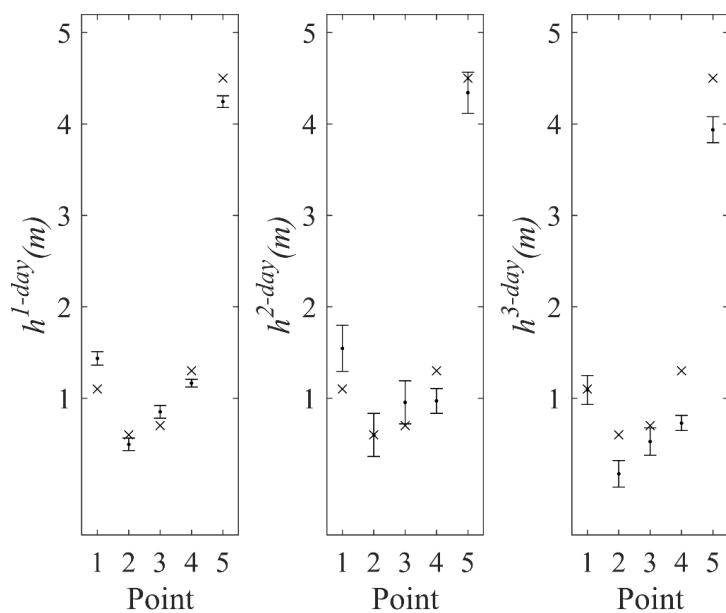


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573 **Figure 6.** Location of the five control points at the area of study in Lugo. (PNOA courtesy  
574 of © Instituto Geográfico Nacional).

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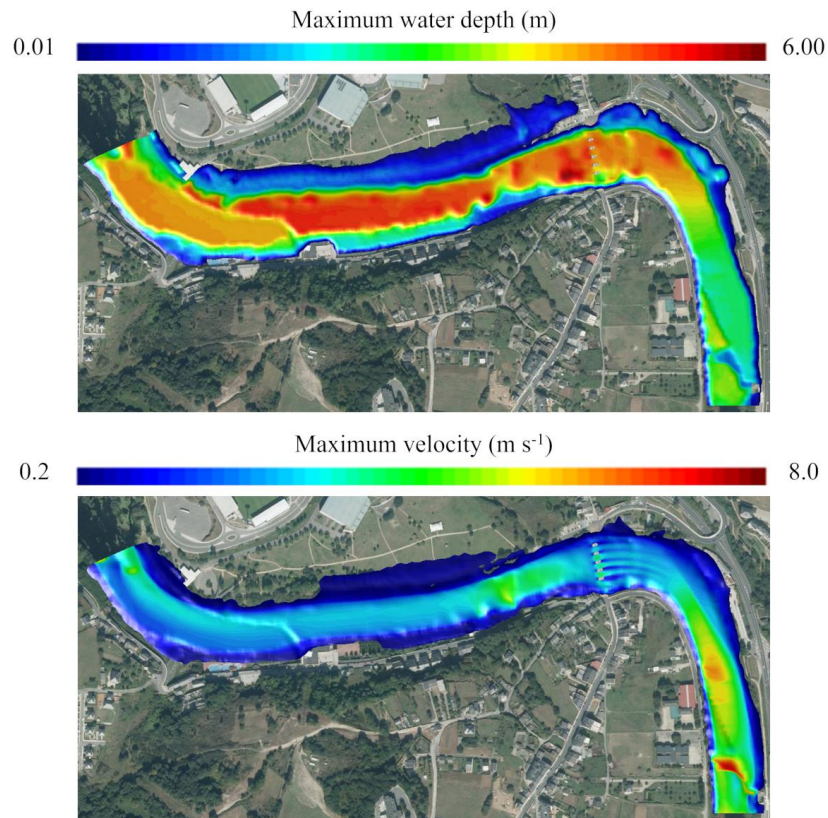
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