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Probabilistic characteristics of narrow-band long wave run-up onshore

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Abstract

The run-up of random long wave ensemble (swell, storm surge and tsunami) on the constant-slope beach is studied in the framework of the nonlinear shallow-water theory in the approximation of non-breaking waves. If the incident wave approaches the shore from deepest water, runup characteristics can be found in two stages: at the first stage, linear equations are solved and the wave characteristics at the fixed (undisturbed) shoreline are found, and, at the second stage, the nonlinear dynamics of the moving shoreline is studied by means of the Riemann (nonlinear) transformation of linear solutions. In the paper, detail results are obtained for quasi-harmonic (narrow-band) waves with random amplitude and phase. It is shown that the probabilistic characteristics of the runup extremes can be found from the linear theory, while the same ones of the moving shoreline - from the nonlinear theory. The role of wave breaking due to large-amplitude outliers is discussed, so that it becomes necessary to consider wave ensembles with non-Gaussian statistics within the framework of the analytical theory of non-breaking waves. The basic formulas for calculating the probabilistic characteristics of the moving shoreline and its velocity through the incident wave characteristics are given. They can be used for estimates of the flooding zone characteristics in marine natural hazards.

Keywords: tsunami, storm surge, long wave runup, Carrier-Greenspan transform, statistical characteristics

1. Introduction

The flooded area size, the water flow depth and its speed on the coast, the coastal topography characteristics and the features of the coastal zone development determine the consequences of marine natural disasters on the coast. The catastrophic events of recent years are well known, when tsunami waves and storm surges caused significant damage on the coast and people's death. It is worth saying that only in 2018 two catastrophic tsunamis occurred in Indonesia, leading to the death of several thousand people (on Sulawesi Island in September and in the Sunda Strait in December). The calculations of the coast flooding in tsunamis and storm surges is mainly carried out within the framework of nonlinear shallow-water equations, taking into account the variable roughness coefficient for various areas of the coastal zone (Kaiser et al,

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2011; Choi et al, 2012). The characteristics of the coastal destruction is determined either by using fragility curves (Macabuag et al, 2016; Park et al, 2017) or by using a direct calculation of the tsunami forces (Qi et al, 2014; Ozer et al, 2015a, b; Kian et al, 2016; Xiong et al., 2019).

The computation accuracy was tested on a series of benchmarks, including the idealized problem of the wave run-up onto the impenetrable slope of a constant gradient without friction (Synolakis et al, 2008). The nonlinear shallow water equations for the bottom geometry of this kind are linearizedby using the hodograph (Legendre) transformations. This step makes it possible to obtain a number of exact solutions describing the run-up on the coast. This approach, first suggested in (Carrier and Greenspan, 1958), was later on used to analyze the run-up of single and periodic waves of various shapes (Synolakis, 1987; Pelinovsky and Mazova, 1992; Tinti and Toniti, 2005; Madsen and Fuhrman, 2008; Madsen and Schaffer, 2010; Antuano and Brocchini, 2008, 2010; Didenkulova, 2009; Dobrokhotov et al, 2015; Aydin and Kanoglu, 2017). Moreover, such approach made it possible to determine the conditions for the wave breaking. The latter means the presence of steep fronts (gradient catastrophe) within the hyperbolic shallow water equation framework. The Carrier-Greenspan transformation was further generalized for the case of waves in an inclined channel of an arbitrary variable cross section (Rybkin et al, 2013; Pedersen, 2016; Shimozone, 2016; Anderson et al, 2017; Raz et al, 2018). In a number of practical cases, its use proves to be more efficient than the direct numerical computation within the 2D shallow water equation framework (Harris et al, 2015, 2016).

Due to bathymetry variability and shoreline complexity, diffraction and scattering effects lead to an irregular shape of the waves approaching the coast. Moreover, very often not the leading wave turns out to be the maximum one. Such typical tsunami wave records on tide-gauges are well known and are not shown here. It is applied even more to swell waves, which in some cases approach the coast without breaking (Huntley et al, 1977; Hughes et al, 2010). As a result, statistical wave theory can be applied to such records and with their help, nonlinear shallow water equations in the random function class can be solved. This approach was used to describe the statistical moments of the long wave run-up characteristics in (Didenkulova et al, 2008, 2010, 2011). Special laboratory experiments were also conducted on irregular wave run-up on a flat slope, the results of which are not very well described by theoretical dependencies (Denissenko et al, 2011, 2013). As for field data, we are acquainted with two papers: (Huntley et al, 1977; Hughes et al, 2010), where the statistical characteristics of the moving shoreline on two Canadian and one Australian beaches were calculated. They confirmed the fact that the wave process on the coast is not Gaussian. In our opinion, the main problem in the theoretical model of describing the irregular wave run-upon the shore is associated with the use of two hypotheses: 1)

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the small amplitude wave field (in the linear problem) is Gaussian; 2) waves run-up on the shore without breaking. It is obvious, however, that in the nonlinear wave field some broken waves can always be present. They affect the distribution function tails and, thus, the statistical moments of the run-up characteristics as well.

The connection of the run-up parameters at the nonlinear stage with the linear field at a fixed point is described either in a parametric form or implicitly in a nonlinear equation (Didenkulova et al. 2010). This does not allow using the standard methods of random processes. At the same time, it is known that this implicit equation is equivalent to a partial first-order differential equation (PDE), that is, to the simple or Riemann wave equation (Rudenko and Soluyan, 1977). In statistical problems, this equation arises in nonlinear acoustics. This equation or its generalization, the nonlinear diffusion equation called the Burgers equation (Burgers at al, 1974) is the model equation in the hydrodynamic turbulence theory (Frisch, 1995). It should be noted that for the one-dimensional Burgers turbulence, as well as its three-dimensional version, used for the model description of the large-scale Universe structure (Gurbatov et al, 2012). It is possible to give an almost comprehensive statistical description for certain initial conditions (Gurbatov et al, 1991, 1997, 2011; Gurbatov and Saichev, 1993; Molchanov et al, 1995; Frisch, 1995; Woyczynski, 1998; Frisch and Bec, 2001; Bec and Khanin, 2007). In particular, single-point and two-point probability distributions of the velocity field and even N-point probability distributions and, accordingly, multi-point moment functions were found. This partially allows using a mathematical approach developed in statistical nonlinear acoustics. An experimental study of the nonlinear evolution of random quasi-monochromatic waves and the probability distributions and spectra analysis have been carried out in acoustics more than once. They confirmed theoretical conclusions; see, for example (Gurbatov et al, 2018, 2019).

This paper is devoted to the analytical study of the probabilistic characteristics of the long narrow-band wave run-upon the coast. Section 2 gives the basic equations of nonlinear shallow water theory and the Carrier-Greenspan transformation, with the latter making it possible to linearize the nonlinear equations. Section 3 describes the moving shoreline dynamics when the deterministic sine wave climbs on the slope. The probability characteristics of the deformed sine oscillations of the moving shoreline with a random phase are described in Sect. 4. Section 5 contains the probabilistic characteristics on the vertical displacement of the moving shoreline if the incident narrow-band wave has a random amplitude and phase. The discussion of the wave breaking effects and their influence on the distribution of the run-up characteristics is given in Sec. 6. The results obtained are summarized in Sect. 7.

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2. Basic equations and transformations

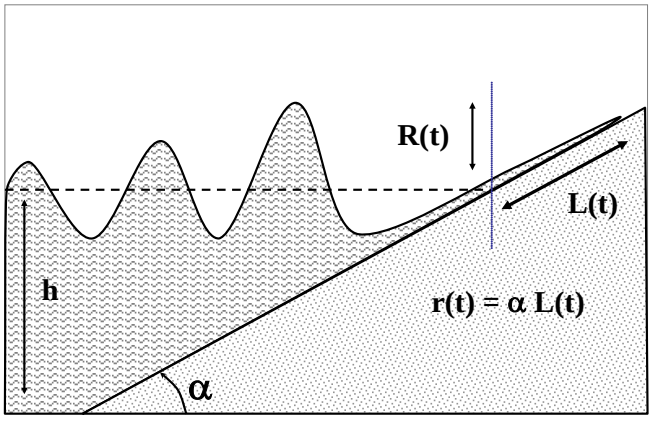

Fig. 1. The problem geometry

Here we will consider the classical formulation of the problem of a long wave run-upon the constant-gradient slope in an ideal fluid (Fig. 1). The wave is one-dimensional and propagates along the *x*-axis directed onshore. The basin depth is a linear depth function: $h(x) = -\alpha x$, where α is the inclination angle tangent and point $x = 0$ corresponds to a fixed unperturbed water shoreline. *L(t)* and *r(t)* describe horizontal and vertical displacement of the moving shoreline, and *R(t)* is the water level oscillations at $x = 0$. The bottom and the shore are assumed impenetrable. The long wave dynamics is described by nonlinear shallow water equations:

$$\frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} + g\frac{\partial \eta}{\partial x} = 0, \tag{2.1}$$

$$\frac{\partial \eta}{\partial t} + \frac{\partial}{\partial x}\left[(-\alpha x + \eta)u\right] = 0. \tag{2.2}$$

Here, $\eta(x,t)$ is the free surface elevation above the undisturbed water level, and $u(x,t)$ is the depth-averaged flow velocity (within the shallow water theory, the flow velocity is the same on all horizons), and *g* is the gravity acceleration. Obviously, after introducing total depth

$$H(x,t) = -\alpha x + \eta(x,t), \tag{2.3}$$

equations (2.1) and (2.2) are a hyperbolic system with constant coefficients. This fact makes it possible to transform the system into a linear equation one by using a hodograph (Legendre) transformation, which was done in the pioneering work (Carrier and Greenspan, 1958). As a

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result, the wave field is described by a linear wave equation in the 'cylindrical' coordinate system

$$\frac{\partial^2\Phi}{\partial\lambda^2}-\frac{\partial^2\Phi}{\partial\sigma^2}-\frac{1}{\sigma}\frac{\partial\Phi}{\partial\sigma}=0, \tag{2.4}$$

and all variables are expressed in terms of an auxiliary wave function $\Phi(\sigma,\lambda)$ using explicit formulas

$$\eta=\frac{1}{2g}\left(\frac{\partial\Phi}{\partial\lambda}-u^2\right), \tag{2.5}$$

$$u=\frac{1}{\sigma}\frac{\partial\Phi}{\partial\sigma}, \tag{2.6}$$

$$x=\frac{1}{2\alpha g}\left(\frac{\partial\Phi}{\partial\lambda}-u^2-\frac{\sigma^2}{2}\right), \tag{2.7}$$

$$t=\frac{1}{\alpha g}(\lambda-u). \tag{2.8}$$

It should be noted that the variable σ is proportional to the total water depth.

$$\sigma=2\sqrt{gH}=2\sqrt{g(-\alpha x+\eta)}, \tag{2.9}$$

so, the wave equation (2.4) is solved on the semi-axis $\sigma\geq 0$, and this coordinate plays the radius role in the cylindrical coordinate system. We would like to emphasize that the point $\sigma=0$ corresponds to a moving shoreline, and therefore, the original problem, solved in the area with a unknown boundary, is reduced to a fixed area problem.

It is important to note that the hodograph transformation is valid if the Jacobian transformation is non-zero

$$J=\frac{\partial(x,t)}{\partial(\sigma,\lambda)}\neq 0. \tag{2.10}$$

It is the case when a gradient catastrophe, identified in the framework of the shallow-water theory with the wave breaking, does not occur. The necessary condition for the wave breaking absence is the boundedness and smoothness of all solutions; this question will be discussed further on.

We will assume that the wave approaches the coast from the area far from the shoreline ($x\to-\infty$), where the wave is linear. Then it is obvious that the function $\Phi(\sigma,\lambda)$ can be completely found from the linear theory. The difficulty in finding the wave field in the near-

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shoreline area is due to the implicit transformation of the coordinates *(x,t)* to (σ, λ). However, for the most interesting point of the moving shoreline $\sigma = 0$ (its dynamics determines the size of the flooded area on the coast) all the formulas become explicit. In particular, from (2.5) and (2.6) follows

$$r(t) = R\left[t + \frac{u(t)}{\alpha g}\right] - \frac{u(t)^2}{2g}, \tag{2.11}$$

$$u(t) = U\left[t + \frac{u(t)}{\alpha g}\right], \tag{2.12}$$

where *r(t)* and *u(t)* are the vertical displacement of the moving shoreline and its speed, and the functions *R(t)* and *U(t)* determine the field characteristics at the fixed point *(x = 0)* from the linear theory

$$R(t) = \frac{1}{2g}\frac{\partial \Phi(\sigma = 0, \lambda)}{\partial \lambda}\bigg|_{\lambda = \alpha g t}, \qquad U(t) = \frac{1}{\sigma}\frac{\partial \Phi(\sigma, \lambda)}{\partial \sigma}\bigg|_{\sigma = 0, \lambda = \alpha g t}. \tag{2.13}$$

Then we add the obvious kinematic relations for the vertical displacement and velocity of the last sea point along the slope.

$$u(t) = \frac{1}{\alpha}\frac{dr(t)}{dt}, \qquad U(t) = \frac{1}{\alpha}\frac{dR(t)}{dt}. \tag{2.14}$$

Let us note that formula (2.12) is identical to the so-called Riemann wave or a simple wave in a nonlinear non-dispersive medium (in particular, in nonlinear acoustics), if we consider the parameter $1/\alpha g$ to be a 'coordinate'; see, for example, (Rudenko and Soluyan, 1977, Gurbatov et al, 1991, 2011). Moreover, formula (2.13) describes the integral over the Riemann wave. This analogy proves to be very useful when transferring the already known results in the wave nonlinear theory to the run-up characteristics described by the ODE.

Detailed calculations of the long wave run-up on the coast were carried out repeatedly; see, for example (Carrier and Greenspan, 1958; Synolakis, 1987; Pelinovsky and Mazova, 1992; Tinti and Toniti, 2005; Madsen and Fuhrman, 2008; Madsen and Schaffer, 2010; Antuano and Brocchini, 2008, 2010; Didenkulova, 2009; Dobrokhotov et al, 2015; Aydin and Kanoglu, 2017).

It is worth mentioning that the nonlinear time transformation in (2.11) and (2.12) leads to the shoreline oscillation distortion in comparison with the linear theory predictions. So, for large amplitudes the wave shape becomes multi-valued (broken). The first moment of the wave

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breaking on the shoreline (the gradient catastrophe) is easily found from (2.12) by calculating the first derivative of the moving shoreline velocity

$$\frac{du}{dt} = \frac{dU/dt}{1 - \frac{dU/dt}{\alpha g}}, \tag{2.15}$$

from it follows the wave breaking condition

$$Br = \frac{\max(dU/dt)}{\alpha g} = \frac{\max(d^2R/dt^2)}{\alpha^2 g} = 1, \tag{2.16}$$

where we have introduced the breaking parameter – *Br* to designate the left-hand side in (2.16), which characterizes the nonlinear wave properties on the shoreline. The condition (2.16) can be given a physical meaning, that the breaking occurs when the last sea particle acceleration ($\alpha^{-1}d^2R/dt^2$) exceeds the component of gravity acceleration along the shoreline ($g\alpha$). As shown in (Didenkulova, 2009), condition (2.16) coincides with (2.10) for Jacobian. It is important to emphasize that the breaking condition is unequivocally found through solving the linear problem of the wave run-up on the shore. It is determined only by the particle acceleration value on the shoreline; but it is not determined separately by the shoreline displacement or its velocity.

A similar Carrier – Greenspan transformation is obtained for waves in narrow inclined channels, fjords, and bays (Rybkin et al, 2013; Pedersen, 2016; Anderson et al, 2017; Raz et al, 2018); only the wave equation (2.4) and relations (2.5) - (2.8) change. However, the moving shoreline dynamics is still described by equations (2.11) and (2.12), valid for arbitrary cross-section channels.

3. The moving shoreline dynamics at an initially monochromatic wave run-up

The monochromatic wave run-up on a flat slope by using the Carrier – Greenspan transformation has been studied in a number of papers cited above. Let us reproduce here the main features of the moving shoreline dynamics necessary for us to draw a statistical description further on. Mathematically, the monochromatic wave run-up is described by an elementary solution of equation (2.4)

$$\Phi(\sigma,\lambda) = QJ_0(l\sigma)\cos(l\lambda), \tag{3.1}$$

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where Q and l are arbitrary constants, and J_0 is the zero-order Bessel function. Far from the shoreline ($\sigma \to \infty$) the Bessel function decreases, so the wave function Φ becomes small. In this case, in (2.5) - (2.8) one can use approximate expressions (the 'linear' Carrier – Greenspan transformation)

$$\eta = \frac{1}{2g}\frac{\partial \Phi}{\partial \lambda}, \qquad u = \frac{1}{\sigma}\frac{\partial \Phi}{\partial \sigma}, \qquad x = -\frac{\sigma^2}{4\alpha g}, \qquad t = \frac{\lambda}{\alpha g}, \tag{3.2}$$

and using the asymptotic representation for the Bessel function, reduce (3.1) to the expression for the water surface displacement

$$\eta(x,t) = a(x)\left\{\sin\left[\omega\left(t - \int \frac{dx}{\sqrt{gh(x)}}\right)\right] - \frac{\pi}{4}\right\} + \sin\left[\omega\left(t + \int \frac{dx}{\sqrt{gh(x)}}\right) + \frac{\pi}{4}\right], \tag{3.3}$$

where

$$a(x) = \frac{Q}{2g}\sqrt{\frac{l}{\pi\sqrt{gh(x)}}}, \qquad \omega = gl\alpha \ . \tag{3.4}$$

The wave field away from the shoreline is a superposition of two waves of the same frequency and a variable amplitude *a (x)*, which together form a standing wave. It immediately shows that the wave amplitude varies with depth according to the Green law ($h^{-1/4}$), as it should be far from the coast. The same asymptotic result follows from the exact solution of linear shallow water equations.

$$\eta(x,t) = R_0 J_0\left(\sqrt{\frac{4\omega^2 |x|}{g\alpha}}\right)\sin(\omega t), \tag{3.5}$$

where R_0 is the wave amplitude at the fixed shoreline ($x = 0$), identified with the maximum run-up height in the linear theory. By connecting (3.4) and (3.5), we obtain the formula for the run-up height obtained through the incident wave amplitude far from the coast

$$\frac{R_0}{a(x)} = \sqrt{\frac{2\omega}{\alpha}\sqrt{\frac{h(x)}{g}}} \ . \tag{3.6}$$

Formula (3.6) allows working further with the run-up height R_0 instead of the wave amplitude far from the coast *a(x)*, considering it to be given. Having determined Q and l through the incident wave parameters, we can calculate the run-up characteristics in the nonlinear theory, considering the limit of formula (3.1) with $\sigma \to 0$ and using the Carrier – Greenspan transformation formulas (2.5) - (2.8). The moving shoreline movement is determined by the parametric dependence

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$$t = \frac{\lambda}{\alpha g} - \frac{\omega R_0}{\alpha^2 g}\cos\left(\frac{\omega\lambda}{\alpha g}\right), \tag{3.7}$$

$$r = R_0 \sin\left(\frac{\omega\lambda}{\alpha g}\right) - \frac{\omega^2 R_0^2}{2\alpha^2 g}\cos^2\left(\frac{\omega\lambda}{\alpha g}\right). \tag{3.8}$$

It is convenient to introduce dimensionless variables

$$z = \frac{r}{R_0}, \quad \tau = \omega t. \quad \varphi = \frac{\omega\lambda}{\alpha g}, \tag{3.9}$$

and calculate the breaking parameter

$$Br = \frac{\omega^2 R_0}{\alpha^2 g}, \tag{3.10}$$

so the formulas (3.7) and (3.8) are finally rewritten in the form

$$\tau = \varphi - Br\cos(\varphi), \tag{3.11}$$

$$z = \sin(\varphi) - \frac{Br}{2}\cos^2(\varphi), \tag{3.12}$$

what is another record for the formulas (2.11) and (2.12), if we take

$$R(t) = R_0 \sin(\omega t), \tag{3.13}$$

arising from (3.5) with $x = 0$. Let us note that the function $z(\tau, Br)$ is set in a parametric form, but after expressing φ from (3.12) and substituting it in (3.11), we can obtain the explicit expression for the function $\tau(z; Br)$. In the paper, we will use both explicit and implicit expressions of the functions describing the moving shoreline dynamics.

Fig. 2 shows the moving shoreline dynamics at different wave height values in terms of the breaking parameter up to the limiting value ($Br = 1$). In the limit of small parameter values, the oscillations are close to sinusoidal (it is almost a linear problem). Then, with the increasing amplitude, the moving shoreline velocity gets a steep leading front, while at the moving shoreline vertical displacement a peculiar feature is formed at the wave run-down stage. As it is known, at the time of the Riemann wave breaking, a peculiarity like $u \sim t^{1/3}$ is formed (Pelinovsky et al, 2013). Then, in the integral over the Riemann wave (at the moving shoreline displacement), this peculiar feature will have the form $z \sim t^{4/3}$. Thus, with the wave amplitude increase, the first breaking occurs at sea (at the run-down stage), and not on the coast. Then the breaking zone expands and moves on to the coast, but at this stage, analytical solutions based on the Carrier-Greenspan transformation become inapplicable.

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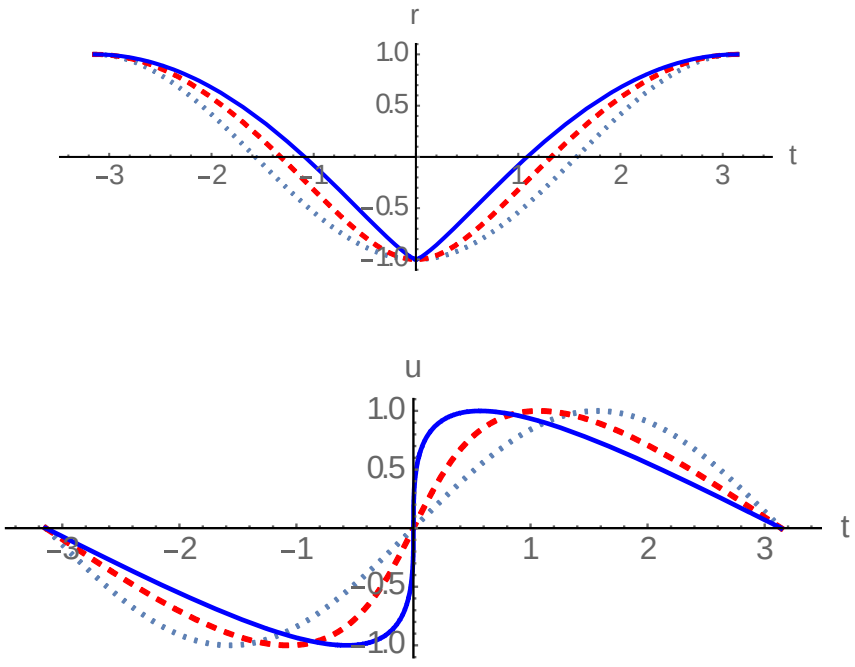

Fig. 2. The moving shoreline dynamics (top) and its velocity (below) for different breaking parameter values *Br* (0 –the dotted line, 0.5 –the dashed line and 1 – the solid line).

4. Probabilistic characteristics of the initially sine wave run-up with a random phase

Let us now consider the probabilistic characteristics of the initially sine wave run-up with a random phase on the shore, assuming it to be uniformly distributed over the interval $[0-2\pi]$. These characteristics are found by using the geometric probability methods (Kendall and Stuart, 1969), so that for ergodic processes the probability density of the moving shoreline vertical displacement coincides with the relative location time of the function $\xi(t)$ in the interval (ξ, $\xi+d\xi$)

$$W(\xi)=\frac{1}{2\pi}\sum_{n=1}^{N}\left|\frac{dt_n}{d\xi}\right|, \tag{4.1}$$

where the summation takes place at all intersection level $\xi(t)$. For harmonic disturbance, it is enough to restrict ourselves to considering the field on a half-period. So, for the moving shoreline vertical displacement in dimensionless variables, the derivative $d\tau/dz$ of the

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273 parametric curve (3.11) and (3.12) can be calculated through the ratio of the derivatives $d\tau / d\varphi$
274 и $dz / d\varphi$

275 $$W_z^{\sin}(z;Br) = \frac{1}{\pi}\frac{1+Br\sin\varphi}{\cos\varphi + Br\cos\varphi\sin\varphi} = \frac{1}{\pi\cos\varphi}\ , \tag{4.2}$$

276 we indicated here that the probability density depends on *Br* as a parameter. Finding $\cos\varphi$ from
277 the formula (3.12) for the vertical displacement, we obtain the final expression for the
278 probability density

279 $$W_z^{\sin}(z;Br) = \frac{1}{\pi}\frac{1}{\sqrt{1-\frac{1}{Br^2}\left[1-\sqrt{1+2zBr+Br^2}\right]^2}}\ , \tag{4.3}$$

280 which in the linear problem for a purely sinusoidal perturbation transforms into a well-known
281 expression for the probability distribution of a harmonic signal with a random phase (Kendall
282 and Stuart, 1969)

283 $$W_z^{\sin}(z;0) = \frac{1}{\pi}\frac{1}{\sqrt{1-z^2}}\,. \tag{4.4}$$

284 The probability distribution (4.3) for the three values of the parameter *Br*is shown in Fig.
285 3. As you can see, the probability density becomes an asymmetric function with a greater
286 probability in the area of positive values corresponding to the wave run-up on the coast than at
287 the run-down stage. At the ends of the interval, the probability density is unlimited throughout
288 the entire range change of *Br*, since the shoreline oscillations near the maximum have a zero
289 derivative (the moving shoreline velocity in it becomes zero).

290 The obtained probability density function can be used to calculate the statistical moments
291 of the shoreline oscillations. Technically, however, it is easier to use the parametric equations
292 (3.11) and (3.12) and calculate all the moments.

293 $$M_n^z = \frac{1}{2\pi}\int_0^{2\pi} z^n(\tau)d\tau = \frac{1}{2\pi}\int_0^{2\pi} z^n(\varphi)\frac{d\tau}{d\varphi}d\varphi\ . \tag{4.5}$$

294 So, the first moment

295 $$M_1^z = \frac{Br}{4} \tag{4.6}$$

296 determines the average water level rise on the coast when the waves approach the shore (set-up
297 phenomenon), which is commonly observed (Dean and Walton, 2009).

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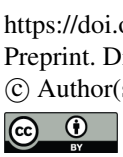

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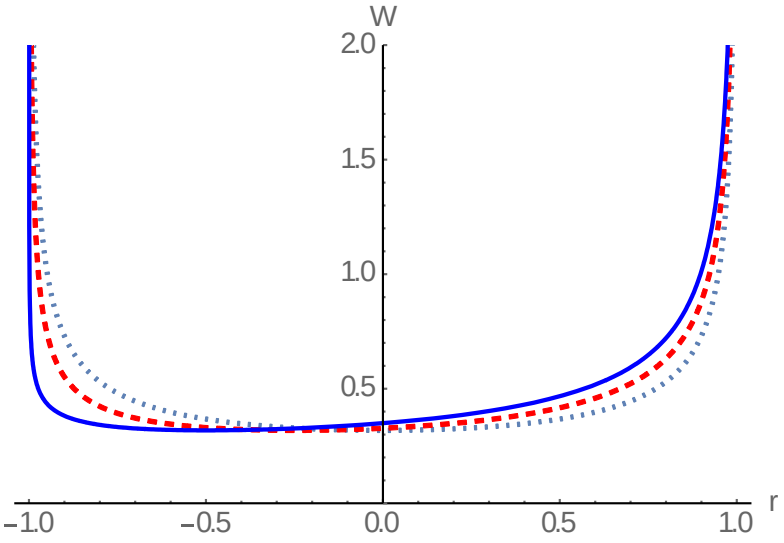

Fig. 3. The probability density of the moving shoreline vertical displacement for the initially sine wave run-up at *Br* = 0 (the dotted line), 0.5 (the dashed line) and 1 (the solid line).

The second moment determines the dispersion

$$\delta^2 = \frac{1}{2\pi}\int_0^{2\pi}(z - M_1^z)^2 d\tau = \frac{1}{2} - \frac{3}{32}Br^2, \tag{4.7}$$

characterizing the fluctuation range relative to the average value; it relatively weakly decreases with the growth of the parameter *Br* (less than 10% for non-breaking waves).

Finally, the total flooding time and its drainage time are easy to find from (3.11) and (3.12), finding from the equation mentioned last, the value φ, at which $z = 0$, and substituting the obtained values in (3.11)

$$T_{flood} = \pi - 2\arcsin\left[\frac{\sqrt{1+Br^2}-1}{Br}\right] + 2\sqrt{2}\sqrt{\sqrt{1+Br^2}-1}, \tag{4.9}$$

$$T_{dry} = \pi + 2\arcsin\left[\frac{\sqrt{1+Br^2}-1}{Br}\right] - 2\sqrt{2}\sqrt{\sqrt{1+Br^2}-1},$$

Both times change almost linearly with the increasing wave amplitude (parameter *Br*), see Fig. 4.

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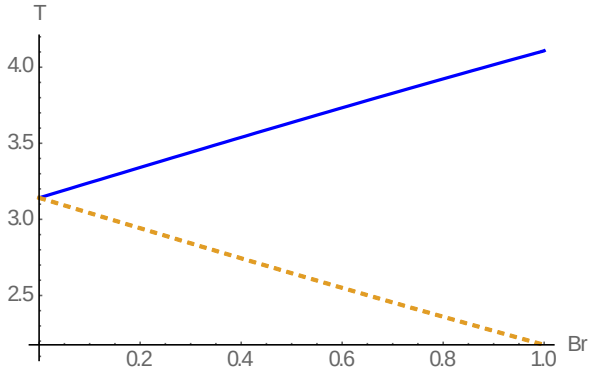

Fig. 4. The total flooding time (the solid curve) and the drainage time (the dashed curve) depending on the parameter *Br*.

It is worth noting that, in contrast to the vertical displacement, the moving shoreline velocity distribution [$u = (\omega R_0 / \alpha)v$], as it is easy to show, does not depend on the breaking parameter and probability density function is determined by the simple formula

$$W_v^{\sin}(v) = \frac{1}{\pi}\frac{1}{\sqrt{1-v^2}}. \qquad (4.10)$$

The distribution independence on the degree of nonlinearity is well known for the Riemann waves and is explained by the compensation of compression and rarefaction areas (Gurbatov et al, 1991, 2011).

5. Probabilistic characteristics of a narrow-band wave run-up with a random amplitude and phase

Let us consider the run-up of a quasi-harmonic wave with a random amplitude and phase on a flat slope. To do this, we will first rewrite formulas (4.3) and (4.10) for them to include the wave amplitude. It is convenient to enter the maximum height R_{max} as the amplitude scales at which the breaking parameter turns into 1

$$Br = \frac{\omega^2 R_{\max}}{\alpha^2 g} = 1, \qquad (5.1)$$

And to use dimensionless displacement ($y=r/R_{max}$). Then the dimensionless amplitude is

$$A = \frac{R_0}{R_{\max}} \le 1\ , \qquad (5.2)$$

and formula (4.3) is converted to the form $(-A < y < A)$

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$$W_y^{\sin}(y;A)=\frac{1}{\pi}\frac{1}{\sqrt{A^2-\left[1-\sqrt{1+2y+A^2}\right]^2}}\ . \tag{5.3}$$

Assuming now that the wave amplitude A is a random variable, we average (5.3) by using the amplitude distribution density $W_A(A)$

$$W(y)=\int_y^\infty W_y^{\sin}(y;A)\,\mathrm{W}_A(A)dA\,. \tag{5.4}$$

Formula (5.4) has an important practical meaning: by the measured distribution of the wave amplitudes far from the coast (re-computed on run-up amplitudes in the linear theory), it is possible to obtain the distribution of the wave run-up characteristics on the coast. The only requirement imposed on the wave ensemble is that it should not contain breaking waves, which should be somehow removed from the record. It immediately follows that the Gaussian field containing large amplitude tails does not fit this requirement, and it should be modified. Therefore, we assume the amplitude distribution to be finite for $A<A_{max}=1$. In this case, the breaking will not be implemented in any way, and the random wave run-up will take place without any breaking. Further calculations depend on the specific type of the amplitude distribution.

Let us construct the finite amplitude distribution at which the linear field distribution is close to the Gaussian form and modify the Rayleigh distribution in the area $A<A_{max}=1$ (Fig. 5)

$$W_A(A;A_{\max},A_s)=\frac{1}{1-\exp(-2A_{\max}^2/A_s^2)}\frac{4A}{A_s^2}\exp\left(-2\frac{A^2}{A_s^2}\right),\ A\le A_{\max}\,, \tag{5.5}$$

to make the density function distribution normalized. Here, A_s is the so-called significant wave run-up height (an averaged value of 1/3 highest amplitudes). We would like to note here, that it follows from (2.11) and (2.12) that the extremal run-up characteristics in the nonlinear theory remain the same as in the linear theory. This means that the significant wave run-up height remains the same as in the nonlinear theory.

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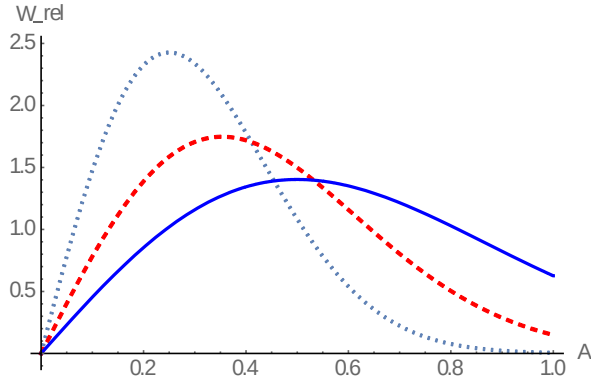

Fig. 5. The modified Rayleigh distribution (5.5) for different distribution values A_s/A_{max}; 0.5 –the dotted curve, 0.7 –the dashed line, 1 –the solid line.

When $A_s<<A_{max} = 1$, distribution (5.5) transforms into the Rayleigh one, which is characteristic of the Gaussian initial distribution of a narrow-band random signal. With the help of (5.5), it becomes possible to calculate the distribution function of shoreline oscillations for the various wave energy. So, with the incident wave small amplitude ($A_s<<1$), distribution (5.3) can be replaced by a simpler expression (4.4) and the answer is the run-up distribution characteristics in the linear theory:

$$W_{lin}(y; A_{max}, A_s) = \frac{4}{\pi A_s^2 [1-\exp(-2A_{max}^2 / A_s^2)]} \int_y^{A_{max}} \frac{A}{\sqrt{A^2 - y^2}} \exp\left(-2\frac{A^2}{A_s^2}\right) dA. \quad (5.6)$$

Besides, if $A_s<<A_{max} = 1$, the integral (5.6) is reduced to the Gaussian distribution

$$W_{lin}(y; A_s) = \frac{2}{\sqrt{2\pi} A_s} \exp\left(-2\frac{y^2}{A_s^2}\right), \quad (5.7)$$

where, $A_s = 2\sigma_y$, and σ_y^2 is the moving shoreline oscillation dispersion.

Fig. 6 shows the distribution of the run-up characteristics for different ratios of A_s/A_{max} values by formulas (5.4) and (5.5); they are shown in solid lines. Here the dashed lines show the calculation results according to the linear theory (5.6). As one can see, with $A_s/A_{max} = 0.5$ (the top panel) and 0.7 (the middle panel), the linear distribution is close to the Gaussian one. Nonlinearity leads to the asymmetry of the distribution function density in the direction of positive values corresponding to the wave characteristics on the coast. If the undisturbed wave ensemble is made of relatively large waves ($A_s/A_{max} = 1$), their distribution is far from the Gaussian, both in the linear and in the nonlinear approximation.

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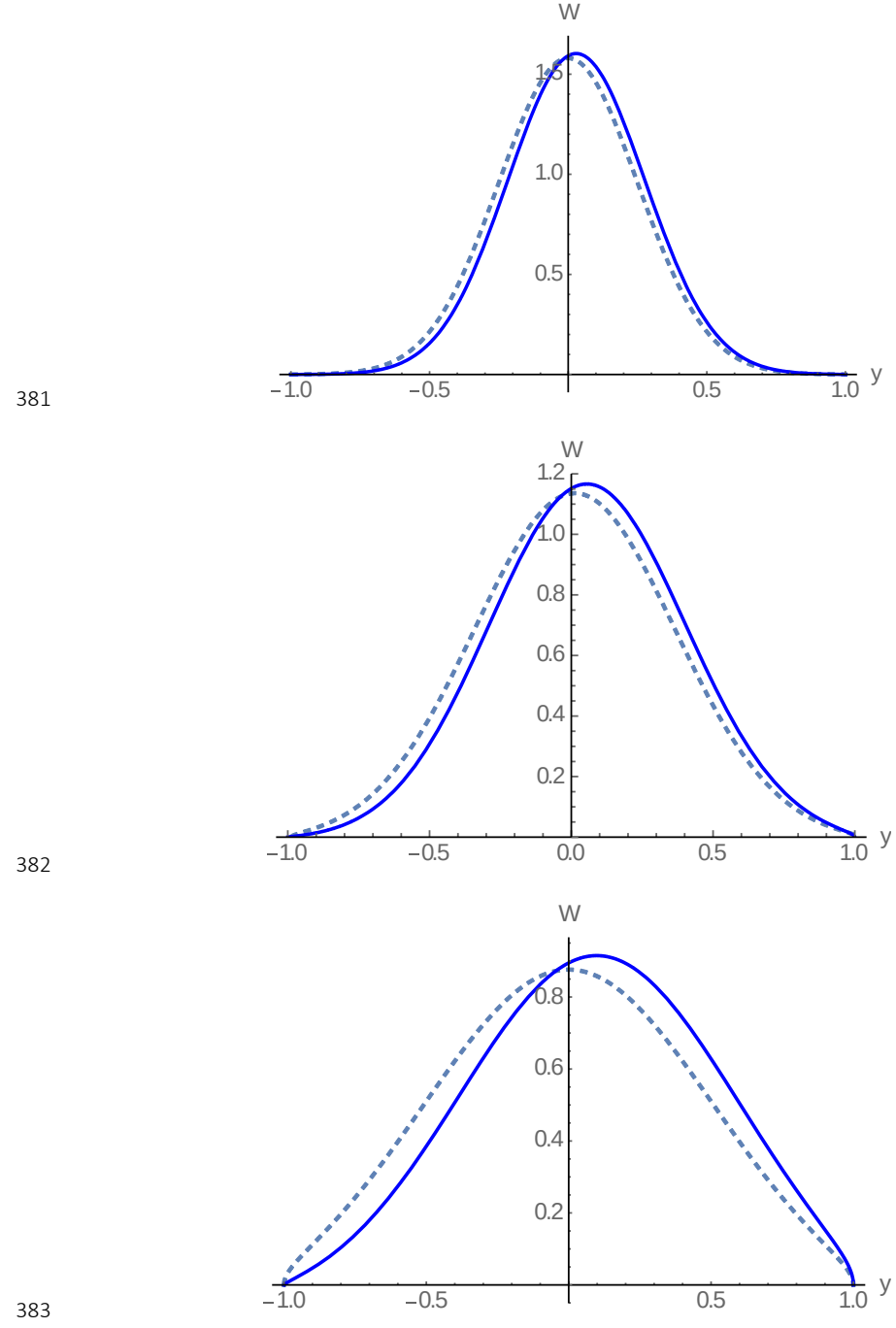

Fig. 6. The probabilistic density function of the vertical shoreline displacement in the nonlinear theory (solid lines) and in the linear theory (dashed lines) for different A_s/A_{max}: 0.5 values: (the upper panel), 0.7 (the middle panel) and 1 (the lower panel).

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The finite ($A<A_{max}$) power-law distribution concentrated mainly near the maximum amplitude A_{max} can be considered as another example of undisturbed large-amplitude waves.

$$W_A(A) = \frac{6A^5}{A_{\max}^6}. \tag{5.8}$$

Fig. 7 shows the graphs of the probabilistic density function of the moving shoreline displacement calculated by using formula (5.4) and (4.4) in the linear theory and (5.3) in the nonlinear theory. It is also seen in the figure that nonlinear effects lead to a strong asymmetry towards the positive values, that is, to the wave amplification at the run-up up stage than at the run-down stage.

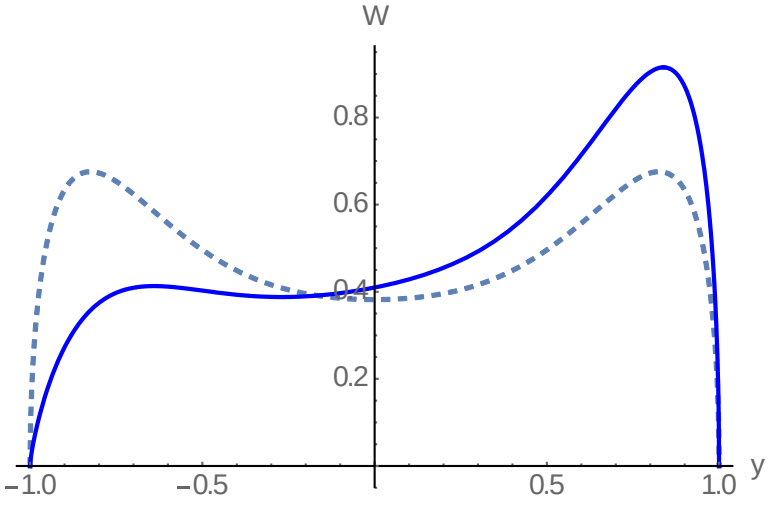

Fig. 7. Probabilistic density function of the shoreline vertical displacement in the linear theory (dashed line) and non-linear theory (solid line)

6. The wave breaking effect on probabilistic run-up characteristics

The theory described above is valid for non-breaking waves. The mentioned wave ensemble, strictly speaking, cannot be the Gaussian one, as it always has unlimited tails in the probability density function. Let us briefly discuss what the formulas obtained for non-breaking waves lead to in the presence of broken waves. Fig. 8 shows the parametric curve (3.11) - (3.12) when Br = 2. Formally, the curve became multi-valued in the range of negative values corresponding to the maximum water outflow from the coast. We have already indicated that the probability density function of the moving shoreline vertical displacement $W(\xi)$ coincides with the relative residence time $\xi(t)$ of the function in the interval (ξ, $\xi + d\xi$), which is calculated by formula

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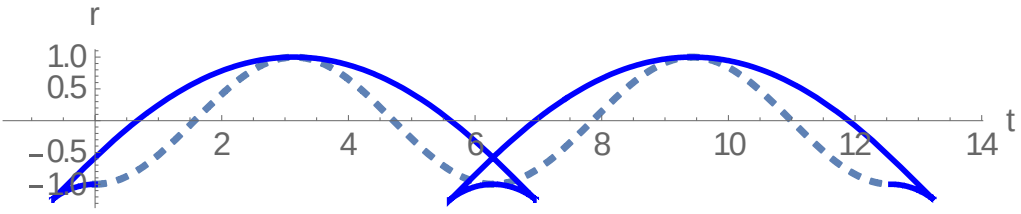
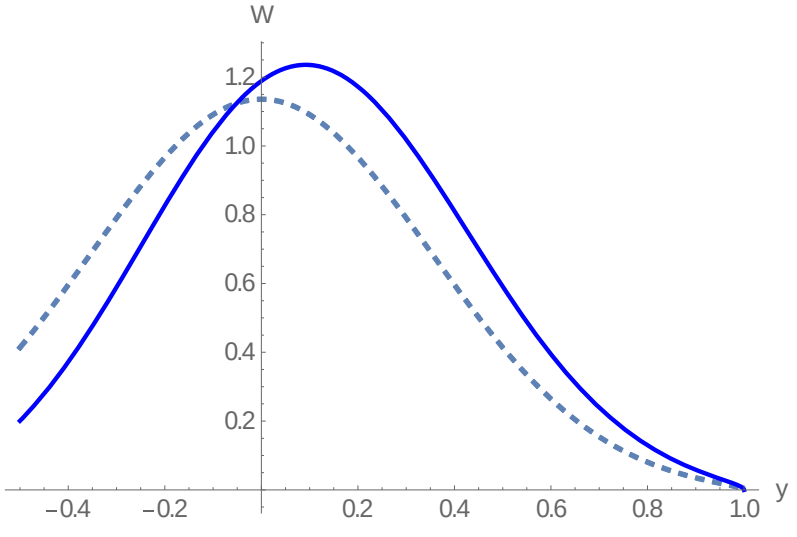
409 (3.1). In contrast to negative cut-off bias values, in the area of positive values there is no
410 ambiguity, and, therefore, all the calculations can be carried out by using the formulas described
411 above. An example of such calculation with *Br* = 2 and *r*> -0.5 (in the zone of one-value
412 solution) is shown in Fig. 9.



413
414

415 Fig. 8. The parametric curve (3.11) - (3.12) with *Br* = 2 (the solid curve) in comparison with the
416 linear problem with *Br* = 0 (the dashed line)



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418 Fig. 9. The probability density function at *Br* = 2, constructed by formulas (5.3), (5.4) and (5.5)
419 (the solid line) in comparison with the linear distribution (5.6) is the dotted line. A_s/A_{max} = 0.7.

420

421 However, these results should be treated with caution, since after the wave breaking at the run-
422 down stage; it is not obvious that the next wave climbing on the coast will not break. This
423 important issue requires going beyond the theory discussed in this article.

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7. Discussion and conclusion

In this paper, we study the run-up of irregular narrow-band waves with a random envelope (swell, storm surges, and tsunami) on a beach of a constant slope. The work was carried out in the framework of the nonlinear wave theory with one important assumption: there should be no breaking waves in the wave ensemble. This restriction is quite strict for field and laboratory conditions, but nevertheless, there are cases when it is performed. For instance, 75% of historical tsunami waves climbed on the coast with no breaking (Mazova et al, 1983). In the experiments performed in the Warwick University tank and in the Large Tank in Hannover (Denissenko et al, 2011, 2013), this condition was fulfilled.

The wave nonlinearity at the run-up stage leads to increased deviations from Gaussianity, as might be expected from general considerations. Nevertheless, it is shown that the probability distribution of the moving shoreline velocity does not depend on the wave nonlinearity and can be calculated within the linear theory framework. The same conclusion can be drawn about the distribution of the extreme run-up characteristics (the moving shoreline displacement and speed), which, in fact, has already been discussed earlier (Didenkulova et al, 2008). However, the probabilistic density function of the moving shoreline displacement differs from that predicted one in the linear theory framework. It is described by formula (5.4) by using either the theoretical or the measured distribution of the incident wave amplitudes. The paper gives the calculation results of the probable run-up characteristics with a modified Rayleigh distribution for wave amplitudes.

The wave breaking leads to the inapplicability of the wave run-up theory based on the Carrier-Greenspan transformation. If, nevertheless, the share of large amplitude waves is small, the breaking occurs mainly at the run-down stage, having little effect on the long-wave coast flooding characteristics (see Section 6). This question, however, requires a special study based on direct numerical solutions of the shallow-water equations or their nonlinear-dispersive generalizations.

Finally, it is worth noting that we considered the narrow-band wave run-up with a random amplitude and phase; as for the random waves with a wide spectrum – it is the problem of further consideration.

Obtained probability density functions of the vertical displacement of the moving shoreline are useful to compute statistical characteristics of flooding time and force on coasts and constructions, which are necessity for mitigation of natural marine hazards.

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