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Shear rate effect on the residual strength characteristics of saturated loess

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Abstract

Residual shear strength of soils is an important soil parameter for assessing the stability of landslides. To investigate the effect of the shear rate on the residual shear strength of loessic soils, a series of ring shear tests were carried out on loess from three landslides at two shear rates (0.1 mm/min and 1 mm/min). Naturally drained ring shear tests results showed that the shear displacement to achieve the residual stage for specimens with higher shear rate was greater than that of the lower rate; both the peak and residual friction coefficient became smaller with increase of shear rate for each sample; at two shear rates, the residual friction coefficients for all specimens under the lower normal stress were greater than that under the higher normal stress. The tests results revealed that the difference in the residual friction angle ϕ_r at the two shear rates, ϕ_r (1)- ϕ_r (0.1), under each normal stress level were either positive or negative values. However, the difference ϕ_r (1) - ϕ_r (0.1) under all normal stresses was negative, which indicates that the residual shear parameters reduced with the increasing of the shear rate in loess area. Such negative shear rate effect on loess could be attributed to a greater ability of clay particles in specimen to restore broken bonds at low shear rates.

Keywords: Loess; Residual shear strength; Ring shear test; Shear rate; Residual shear parameter

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1. Introduction

Residual shear strength of soil is of great significance for evaluating the stability for the slip surface of first-time landslides as well as reactivated landslides (Bishop et al., 1971; Mesri and Shahien, 2003). The residual strength of soils is defined as the minimum constant value of strength along the slip plane, in which the soil particles are reoriented and subjected to sufficiently large displacements in relatively low shear rate (Skempton, 1985).

Numerical studies have been done to assess the residual strength through the laboratory tests using ring shear tests and reversal direct shear tests (Moeyersons et al., 2008; Summa et al., 2010; Vithana et al., 2012; Chen and Liu, 2013; Summa et al., 2018). It is a generally accepted fact that the measurement of the residual strength is most preferred done with a ring shear test since it allows the soil specimen be sheared at unlimited displacement which can simulate the field conditions more accurately (Lupini et al., 1981; Sassa et al., 2004; Tiwari and Marui, 2005; Bhat, 2013). Until now, great efforts have been paid to the study of the shear rate effect on the minimum value of clay or sand strength at residual states (Morgenstern and Hungr, 1984; Lemos, 1985; Tika, 1999; Tika and Hutchinson, 1999; Suzuki et al., 2007; Grelle and Guadagno, 2010; Bhat, 2013). As a result, the residual strength of clay or sand under the effect of shear rate has been made relatively clear. However, compared with the results of tests on clay or sand, understanding of the shear characteristics of silty soil, such as loess, is not yet complete. As pointed out by Ding (2016), some drained ring shear tests have concluded that the increase in shear rate causes the residual strength

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of loess to increase. On the contrary, Kimura et al. (2014) reported that the residual strength of Malan loess decreases with the increase of shear rate. Furthermore, Wang et al. (2015) found that the effect of shear rate on residual strength of loess is closely associated with the normal stress levels, and the change in residual strength of loess samples under high normal stress levels is small in ring shear tests.

Therefore, some inconsistent or even opposite results have been reported in the ring shear tests on loess above, which implied that there is still a lack of experimental data on this topic. From the above investigations, it can be concluded that the effect of the shear rate on the residual strength of the loess is not fully understood and needs further scrutiny. Meanwhile, almost all of these investigations (Kimura et al., 2014; Wang et al., 2015; Ding, 2016) focused on the residual shear characteristics of loess obtained from the same location, while studies of loess collected from different locations have only been rarely performed. Moreover, it should be noted that the residual strength parameters (friction angle) obtained from using different shear rates may be adopted to provide a guide for designing some precision engineering which require high accuracy of the design parameters, thus, the effect of the shear rate on the residual strength of soils should be fully investigated to determine the parameters with high reliability. In addition, residual strength parameters of soil play a key role in assessing the stability analysis of landslides. Therefore, accurate determination of the residual strength parameters and their dependence on the shear rate may affect the stability evaluation of landslides. Thus, it is necessary to study the change of residual strength of loess with shear rate in order to have a good understanding of the suitable

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approach for the residual strength parameters measurement.

In this backdrop, to clarify the residual shear characteristics of loess under the effect of the shear rate, a series of naturally drained ring shear tests were conducted on loess obtained from three landslides at two shear rates (0.1 mm/min and 1 mm/min). The residual shear characteristics of loess at the residual state was examined. Considering that shear strength of loess reduces with moisture content (Dijkstra et al., 1994; Zhang et al., 2009; Picarelli, 2010), ring shear tests were conducted on saturated loess samples corresponding to the worst condition in field engineering. Furthermore, this study investigated the change in the residual strength parameters of loess at different shear rates and their relationships with the normal stress in naturally drained ring shear tests as well.

2. Geological setting of landslide sites

Soil samples from three landslides in the northwest of China were selected in this study. Soil samples used for the ring shear tests and index measuring tests predominantly consist of loess deposits and were collected in a disturbed condition. For convenience, the names of landslide sites were abbreviated into Djg, Ydg, and Dbz. Fig. 1 shows the study sites and some views of the landslides.

Dingjiagou landslide (Djg)

The Djg landslide, located at the mouth of Dingjia Gully in Yan'an of China, is geologically composed of upper loess and lower sand shale in the Yan-chang formation. The dustpan-shaped landslide is inclined to the east, with its inclination 75.85°. The landslide is 350 m in width, 180 m in length, 70 m in elevation. The average thickness of slip mass is around 20 m, and the volume of landslide totaled approximately 105 x 10^4 m^3. The slip mass is mainly constituted by loess, whereas the sliding bed consists of sand shale in Yan-chang formation. The thickness of the sliding zone varied from 30 to 50 cm. The front lateral region of the main slide section of the Djg landslide, where the sampling was performed, was found to be silty clay.

Yandonggou landslide (Ydg)

The Ydg landslide, located in the Qiaogou town of Yan'an in Shaan xi province of China. The top and the toe altitude of the landslide are about 1165 m and 1110 m above the sea level, with the height difference between the toe and the top of landslide about 55 m. The slides have well-developed boundaries with the main sliding direction of 240° and slope angle of 30°. From the landslides profile, the sliding masses from top to bottom were classified by late Pleistocene (Q_3) loess, Lishi (Q_2) loess and clay soil, respectively. Multiple landslides had occurred in this site, and the soil samples used in this study were collected from Q_2 loess stratum within the slide ranged from 4.5 m to 18 m in height.

Dabuzi landslide (Dbz)

The Dbz landslide located in the middle part of Shaanxi province (about E 108°51'36" and N 34°28'48"), China, which is a semi-arid zone dominated by loessic geology. In this region, the investigated site is classified as a typical loess tableland with quaternary stratum. The sedimentary losses in this area are grey yellow, and the exposure stratum in this area has been divided into two stratigraphic units, namely, the upper Malan (Q_3) loess and the lower Lishi (Q_2) loess, of which the Q_3 loess is

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younger. The Q_3 loess is closest to the surface and is up to approximately 12 m thick, while the thickness of Q_2 loess may reach an upper limit of about 50 m (Leng et al., 2018). The loess in this area have well-developed vertical joints (Sun et al., 2009). The travel distance and the maximum width of the slip mass are roughly estimated to be 122 m and 133 m, respectively. The armchair-shaped landslide shows an apparent sliding plane, with an area of approximately 15,660 m^2 and about 66.25 m maximum difference in elevation. The main direction of this landslide is approximately 355°. The exposed side scarp of the landslide, where the sampling was done, was found to be entirely in the Q_2 loess stratum.

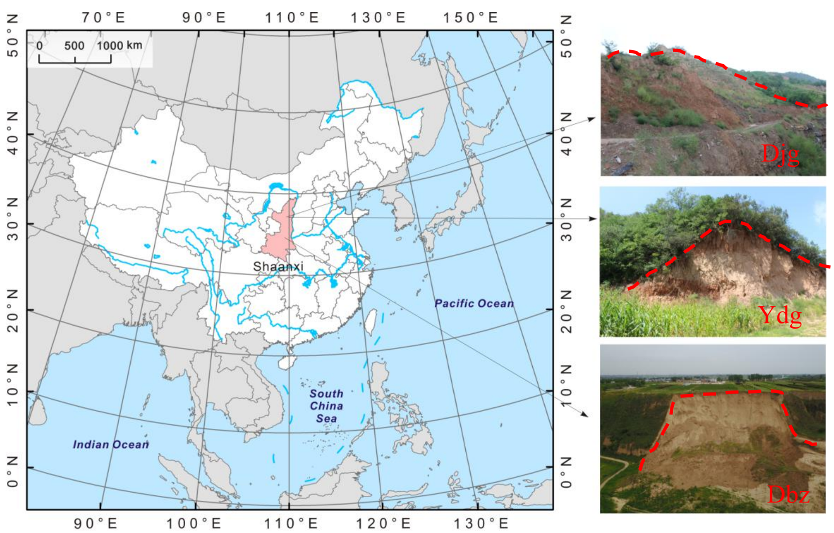

Figure 1. Location of study sites and some views of landslides

Notes: Red dashed lines in the Figure 1 represent landslide boundary.

3. Experimental scheme

3.1. Testing sample

The fact that the residual shear strength is independent of the stress history has been reported by many researchers (Bishop et al., 1971; Stark Timothy et al., 2005;

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Vithana et al., 2012). Thus, disturbed loess samples from each landslide weighing about 25 kg were collected to investigate the residual shear strength.

The soil samples were air-dried, and then crushed with a mortar and pestle. It was found that small lumps may exist in air-dried samples, which may be too big for the cell, so lumps were crushed in order to make sample uniform. This should be done with care so as not to destroy silty-dominated loess. After that, soil samples were processed through 0.5 mm sieve. Distilled water was then added to the soil samples until saturated water content were obtained. The physical parameters such as natural moisture content (*in-situ* moisture content), specific gravity, bulk density, plastic limit, and liquid limit were determined in accordance with the Chinese National Standards (CNS) GB/T 50123-1999 (standards for soil test methods) (SAC, 1999), but clay size was defined to be less than 2 *u*m followed ASTM, D 422 (ASTM, 2007). Each soil sample was separated into clay (sub 0.002 mm), silt (0.002-0.075 mm), and sand (0.075-0.5 mm) fractions. The physical indexes of the soil are listed in Table 1.

The grain size distribution of soil was measured using a laser particle size analyzer Bettersize 2000 (Dandong Bettersize Instruments Corporation, Dandong, China). The sieved soil samples were used to determine particle size distribution this study, soil samples were treated with sodium hexaphosphate, serving as a dispersant, to disaggregate the bond between the particles. The results show that the clay fraction in Djg landslide soil (24%) is more than two times than that from Ydg (9%) and Dbz (9.1%). Furthermore, the particle size analysis illustrated that the percentage of silt-sized soil in three landslides ranged from 75.66% to 87.4%. In

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addition, Ydg landslide soil consists of the greatest percentage of the sand fraction which reaches up to 10.55%.

Table 1 Physical parameters of slip-zone loess

sites	ρ_d	W	ρ	G_S	W_L	W_p	Grain size fractions (%)			
							<0.002mm	0.002-0.005mm	0.005-0.075	0.075-0.5mm
Djg	1.74	19.5	2.08	2.65	36	20	24	11.48	64.18	0.34
Ydg	1.47	18	1.74	2.71	33	19	9	5.28	75.17	10.55
Dbz	1.48	16	1.72	2.70	32	21	9.1	6.4	81	3.5

Notes: ρ_d= dry density (g/cm^3); w=moisture water content (%); ρ= bulk density (g/cm^3); G_S = specific gravity; W_L=liquid limit; W_p= plastic limit

3.2. Testing apparatus

An advanced ring shearing apparatus (SRS-150) manufactured by GCTS (Arizona, USA) was adopted in ring shear tests and the photos of apparatus were shown in Fig. 2, which consists mainly of a shear box with an outer diameter of 150 mm, an inter diameter of 100 mm and the maximal sample height of 250 mm. The shearing box consists of the upper shear box and the lower shear box. In the shearing process, the upper shear box keeps still while the lower one rotates. The apparatus which provides effective specimen area of 98 cm^2, is capable of shearing the specimen for large displacements. The annular specimen is confined by inside and outside metal rings. Moreover, the specimen is confined by bottom annular porous plates and top annular porous plates in which have sharp-edged radial metal fins which protrude vertically into the top and bottom of the specimen at the shearing process. Two annual porous plates were used to provide drainage condition in the test following previous research (Stark and Vettel, 1992). The normal stress, shear strength and shear displacement can

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be monitored by computer in shearing process. The measurement features of the ring shear apparatus employed in this study are described as follows: shear rate range from 0.001 degrees to 360 degrees per minute, 10 kN axial load capacity, 300 N continuous torque capacity, maximum normal stress of 1000 kN/m^2.

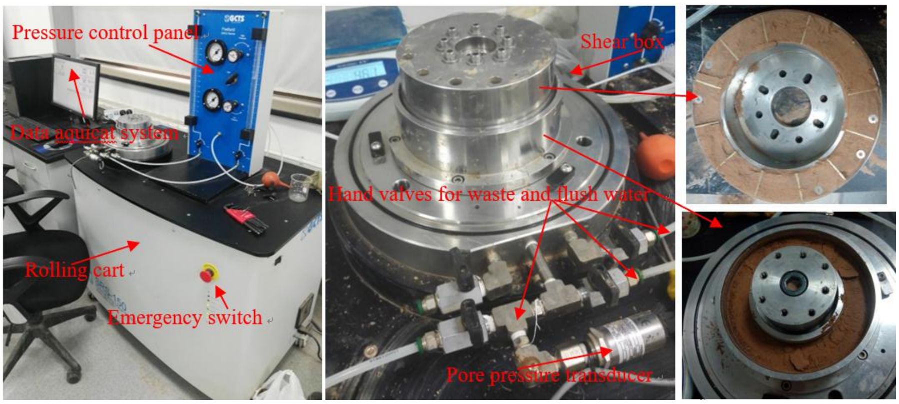

Figure 2. Ring shear apparatus (SRS-150)

3.3. Testing procedure

In present study, reconstituted samples of the sub 0.5 mm soil fractions were used in the testing as it was reported that the residual strength of the soil was unaffected by its initial structure (Bishop et al., 1971; Vithana et al., 2012). Specimens were first prepared by adding distilled water to the air-dried soil until the saturated moisture contents were obtained. Then, specimens were kept in a sealed container for at least one week to fully hydrate. Afterwards, specimens are reconstituted in the ring-shaped chamber of the apparatus by compaction. The specimen was then consolidated under a specific effective normal stress in a range of 100 kN/m^2 to 400 kN/m^2 until consolidation was achieved. In this study, consolidation was completed when the consolidation deformation was smaller than 0.01 mm within 24 hr (Kramer et al., 1999; Shinohara and Golman, 2002). Then, the consolidated specimen is subjected to

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shearing under constant normal stress by rotating the lower half of the shear box attached to a gear, while the upper half remains still. In ring shear tests, the normal stress at the shearing was the same as at consolidation stage. Shear strength of loess specimen was recorded at intervals of 1s before the peak shear strength, after the peak, the sampling rate was increased to 1 min.

In this study, ring shear tests were performed in a single stage under naturally drained condition and the samples were subjected to shear until the residual state was achieved. Drained condition of the shearing process is provided by two porous stones attached on the top and the bottom platen of the specimen container. As for soil specimens with low permeability, the rate of excess pore pressure generation in the shear box may exceeded that of pore-pressure dissipation, this type of condition is identified as naturally drained condition in previous studies([illegible]da et al., 2004). Furthermore, Tiwari (2000) asserted that it was acceptable to use a shear rate below 1.1 mm/min to simulate the field naturally drained condition. Thus, shear rates of 0.1 mm/min and 1 mm/min were used in this study to simulate the naturally drained condition of the slip zone soils.

4. Results

Twenty -four specimens were tested to investigate the residual shear characteristics of the saturated loess in the ring shear apparatus. Residual shear strength of loess was determined following the research conducted by Bromhead (1992) who pointed out that the residual stage is attained if a constant shear stress is measured for more than half an hour. Tests results are shown in this section.

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4.1. Shear behavior

Figs. 3(a)- 5(a) show the typical shear characteristics of the loess (shear rate of 0.1 mm/min and 1 mm/min) obtained from three different locations, where, the shear stress is plotted against the shear displacement. It is a widely accepted fact that normal stress has effect on the shear behavior of the soil (Stark Timothy et al., 2005; Eid, 2014; Kimura et al., 2015; Wang et al., 2019), thus, the shear behavior of samples at the peak and residual stages, where, the determined peak friction coefficient as well as residual friction coefficient are plotted in Figs. 3(b)-5(b) against the corresponding effective normal stresses as well. The friction coefficient is defined as the shear stress divided by the effective normal stress.

Figs. 3(a)-5(a) demonstrate that shear stress increases dramatically within small shear displacement and then reduces with shear displacement, until residual conditions were achieved at large displacements. Furthermore, it is obvious that the peak strength and the residual strength of samples with high shear rate are almost smaller than that of the samples with low shear rate. It can be found that shear displacement to achieve the residual stage for specimens with high shear rate is greater than that of the low rate. For example, the minimum shear displacements for attaining residual condition for Djg specimens with low and high shear rate were about 360 mm and 650 mm, respectively. Under the shear rate of 0.1 mm/min and 1 mm/min, Ydg specimens need approximately 80 mm and 1,400 mm displacement to achieve residual stage. However, Dbz specimens require about 40 mm and 60 mm displacement to reach residual condition for low and high shear rate, respectively.

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In Figs. 3(a)- 5(a), a clear drop can be seen, at any normal stress, for specimens obtained from all sites. It is obvious that Djg specimens showed greater peak-post drop than that of Ydg and Dbz specimens. For example, at the normal stress of 100 kN/m^2, Djg samples show approximately 47.3% and 36.8% decrease from the peak friction coefficient to the residual friction coefficient at low and high shear rates (Fig. 3(b)), respectively, which is greater than in the Ydg samples (about 9.8% and 10.3% in Fig. 4(b)) and Dbz samples (about 2.4% and 3.2% in Fig. 5(b)). In Djg samples, an obvious slickenside was observed on the shear surface (Fig. 6). This phenomenon indicates a high degree of reorientation of platy clay minerals parallel to the direction of shearing. In Figs. 3(b)- 5(b), on average, it was found that the decrease in the friction coefficient from the peak strength in the Djg sample is almost 18.1% and 21.3% for the sample consolidated at normal stress of 400 kN/m^2 under the low and high shear rate (Fig. 3(b)), while such reduction in friction coefficient in Ydg sample are only about 4.1% and 4.8% (Fig. 4(b)). Furthermore, under the low and high shear rate, the friction coefficient reduction in Dbz samples are only approximately 5.6% and 6.0% (Fig. 5(b)). Skempton (1985) reported that the strength of soils falls to the residual value in ring shear tests, owing to reorientation of platy clay minerals parallel to the direction of shearing. Based on the conclusion that the post-peak drop in strength of normally consolidated soil is only due to particle reorientation after the peak strength (Skepmton, 1964; Mesri and Shahien, 2003), the results demonstrated that the Djg landslide soil existed the greater particle reorientation compared with that of other two landslide soils.

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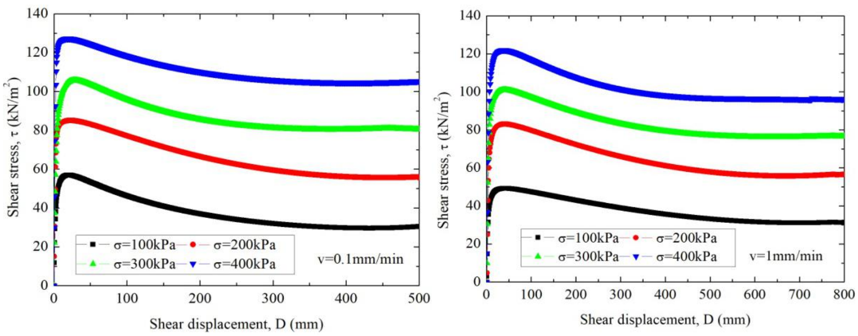
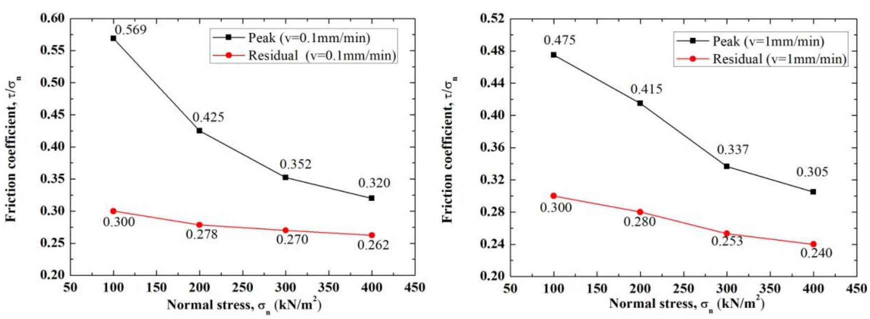
4.2. Effect of normal stress on the friction coefficients

It can be seen from the Figs. 3(b)-5(b) that the friction coefficients (peak and residual) are higher at low effective normal stress levels compared with that at high normal stress. For example, with normal stress increasing from 100 kN/m^2 to 400 kN/m^2, the peak and residual friction coefficient of Djg landslide soils at the shear rate of 0.1 mm/min reduce from 0.569 to 0.32 and from 0.3 to 0.262 (Fig. 3(b)), respectively. Similarly, results obtained from other two landslides loess also show that the friction coefficients decrease nonlinearly with normal stresses (Figs. 4(b) and 5(b)). Furthermore, specimens with shear rate of 0.1 mm/min attained greater friction coefficients than that with shear rate of 1 mm/min (Figs. 3(b)-5(b)).



(a)Relationship between shear stress and shear displacement



(b)Relationship between friction coefficient and normal stress

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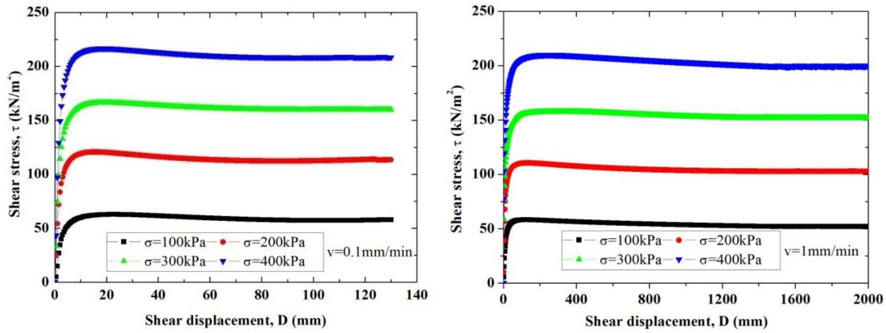
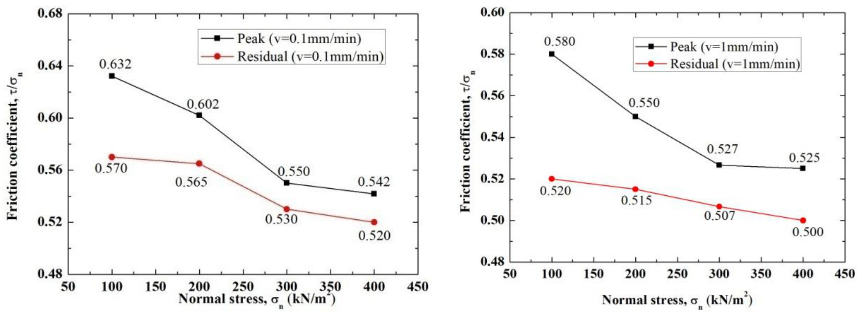
Figure 3. Shear behavior characteristics of Djg soil samples

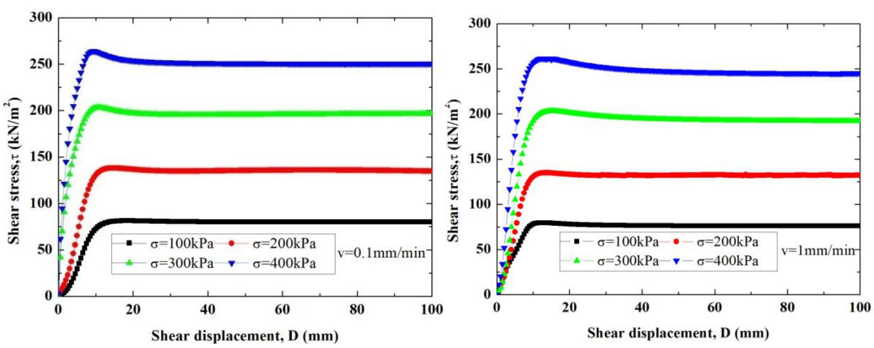


(a)Relationship between shear stress and shear displacement



(b)Relationship between friction coefficient and normal stress

Figure 4. Shear behavior characteristics of Ydg soil samples



(a) Relationship between shear stress and shear displacement

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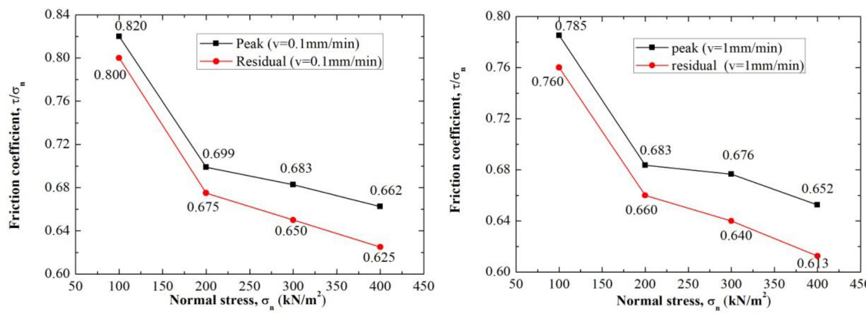

(b) Relationship between friction coefficient and normal stress

Figure 5. Shear behavior characteristics of the Dbz soil samples

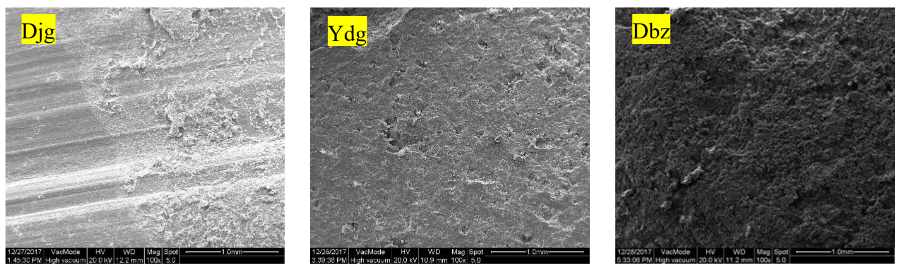

Figure 6. SEM photographs of the shear surface of loess samples (100 magnification)

4.3. Effects of shear rate on residual strength parameter

For the samples described above, Figs. 7-9 show the relationships between the residual friction coefficient and the normal stress, and the residual strength parameters. The residual friction coefficient is plotted against the normal stress. The residual friction coefficient is defined as the residual shear strength divided by normal stress. It has been recognized that the shear strength parameters including cohesion and friction angle (Terzaghi, 1951; Stark Timothy et al., 2005). However, according to the previous studies, the residual angle of soils varies depended on the soil properties as well as the magnitude of normal stress provided the residual cohesion of soil is zero (Skempton, 1964; Bishop; Kimura et al., 2014). Thus, in this study, the residual frictions are calculated by Coulomb’s law assumed the residual cohesion is zero

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following the previous studies (Skempton, 1985). The residual strength parameters were defined as ϕ_r (0.1) and ϕ_r (1) at the low shear rate and high shear rate, respectively. And the difference between the residual friction angles at two shear rates was defined as ϕ_r (1) - ϕ_r (0.1). Comparatively, the residual friction coefficient was defined as τ_r/σ_n (0.1) at the low shear rate and τ_r/σ_n (1) at the high shear rate, respectively. Furthermore, the difference between the residual friction coefficients was defined as τ_r/σ_n (1) - τ_r/σ_n (0.1). Table 2 summarized the residual shear parameters of the landslide soils.

Fig. 7 shows that the residual friction coefficients are relatively low in Djg samples. The coefficients τ_r/σ_n (0.1) and τ_r/σ_n (1) at the normal stress of 100 kN/m^2 to 400 kN/m^2 ranged from 0.3 to 0.262 and from 0.3 to 0.24, respectively. The difference between the friction coefficients, τ_r/σ_n (1)- τ_r/σ_n (0.1), at each normal stress level are varied in a range of -0.022 to +0.002. For the difference between the residual friction angles, ϕ_r(1)- ϕ_r(0.1), ranged from -1.212° to +0.079° (Table 2). For normal stress above 200 kN/m^2, the residual friction coefficient τ_r/σ_n (0.1) was found to be greater than the residual friction coefficient τ_r/σ_n (1). For this sample, residual friction coefficients show a slight decrease with the shear rate for normal stress above 200 kN/m^2.

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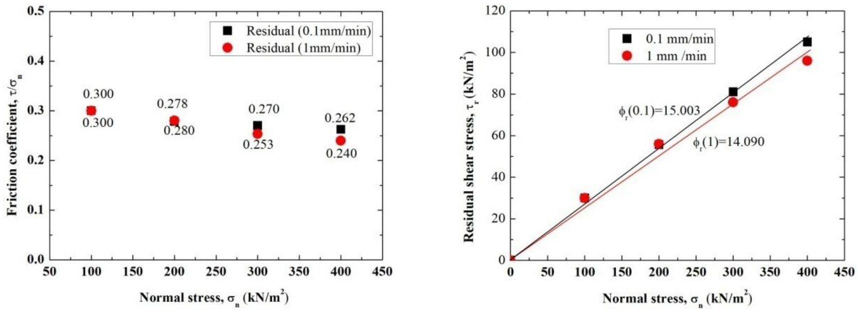

Figure 7. Relationships between residual shear stress and normal stress, and residual strength parameter for Djg soil sample

Fig. 8 gives the results of the Ydg samples. The coefficients τ_r/σ_n (0.1) and τ_r/σ_n (1) under the normal stress of 100 kN/m^2 to 400 kN/m^2 ranged from 0.57 to 0.52 and from 0.52 to 0.50, respectively. Furthermore, the difference τ_r/σ_n (1)- τ_r/σ_n (0.1) at each normal stress was from -0.05 to -0.02. As for the difference between the residual friction angles, ϕ_r (1) - ϕ_r (0.1), was in a range of -2.218° to -0.909°. In case of Ydg soil sample, the residual friction coefficients decreased with increase of shear rate for all normal stress levels.

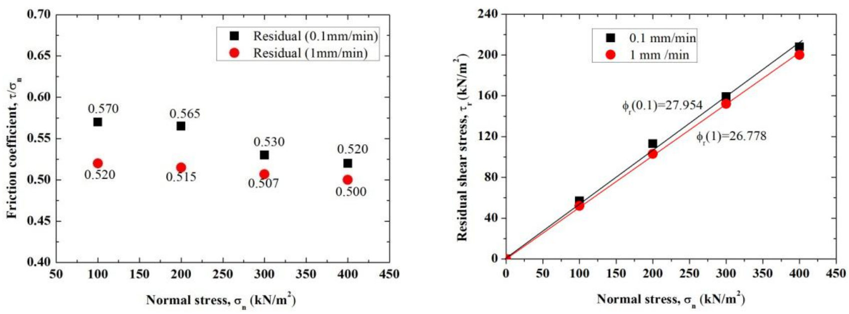

Figure 8. Relationships between residual shear stress and normal stress, and residual strength parameter for Ydg soil samples

Fig. 9 presents the results of the Dbz samples. The coefficients τ_r/σ_n (0.1) and τ_r/σ_n (1) at the normal stress of 100 kN/m^2 to 400 kN/m^2 ranged from 0.8 to 0.625 and

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from 0.76 to 0.613, respectively. The difference τ_r/σ_n (1)- τ_r/σ_n (0.1) at each normal stress was from -0.04 to -0.01. The difference $\phi_r(1)$- $\phi_r(0.1)$ was from -1.425° to -0.405°. For Dbz samples, there was somewhat decrease tendency of the residual friction coefficients with the increasing of the shear rate for all normal stress levels. It is noted that the maximum difference was found at the lowest normal stress of 100 kN/m^2.

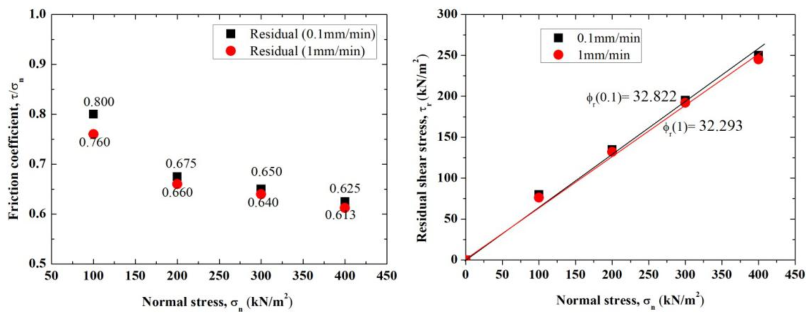

Figure 9. Relationships between residual shear stress and normal stress, and residual strength parameter for Dbz soil sample

Table 2 summarizes residual strength parameters including ϕ_r (0.1) and ϕ_r (1) of all specimens obtained from the ring shear tests in this study. As for the Djg samples, the residual strength parameter $\phi_r(0.1)$ and $\phi_r(1)$ for all normal stress were found to be 15.003° and 14.09° (Fig. 7), respectively. However, the residual friction angles ϕ_r (0.1) and ϕ_r (1) of the Ydg samples were obtained to be 27.954 ° and 26.778° (Fig. 8), respectively. In the case of Dbz sample, the friction angles ϕ_r (0.1) and ϕ_r (1) were high, 32.822° and 32.293° (Fig. 9), respectively. The residual friction angles ϕ_r (0.1) and ϕ_r (1) under all normal stresses were from 15.003° to 32.822° and from 14.09° to 32.293°, respectively.

Due to the influence of the shear rate, the difference ϕ_r (1) - ϕ_r (0.1) in the Djg,

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Ydg and Dbz samples, were -0.913°, -1.176° and -0.529° , respectively. Wang (2014) and Fan et al. (2017) asserted that the residual shear strength of remolded loess hardly affected by shear rate below 5 mm/min. However, the results in this study shown that ϕ_r (1) - ϕ_r (0.1) under all normal stress levels were negative for loess. Moreover, the absolute value of ϕ_r (1)- ϕ_r (0.1) in Ydg samples even reached up to 1.176°.

Table 2 Residual shear strength parameter of landslide soils

No	Sample	Normal stress(kN/m²)	Residual strength parameter				Difference in parameter	
			0.1 mm/min $\phi_{r(0.1)}$ ($c_{r(0.1)}$=0) (Degrees)		1 mm/min $\phi_{r(1)}$ ($c_{r(1)}$=0) (Degrees)		$\phi_{r(1)}$- $\phi_{r(0.1)}$ (Degrees)	
			Under each σ_n	Under all σ_n	Under each σ_n	Under all σ_n	Under each σ_n	Under all σ_n
1	Djg	100	16.699	15.003	16.699	14.090	0	-0.913
		200	15.563		15.642		0.079	
		300	15.110		14.216		-0.894	
		400	14.708		13.496		-1.212	
2	Ydg	100	29.683	27.954	27.474	26.778	-2.209	-1.176
		200	29.466		27.248		-2.218	
		300	27.923		26.870		-1.053	
		400	27.474		26.565		-0.909	
3	Dbz	100	38.660	32.822	37.235	32.293	-1.425	-0.529
		200	34.019		33.425		-0.594	
		300	33.024		32.619		-0.405	
		400	32.005		31.487		-0.518	

4.4. Influence of the shear rate on the residual friction angles according to soil properties

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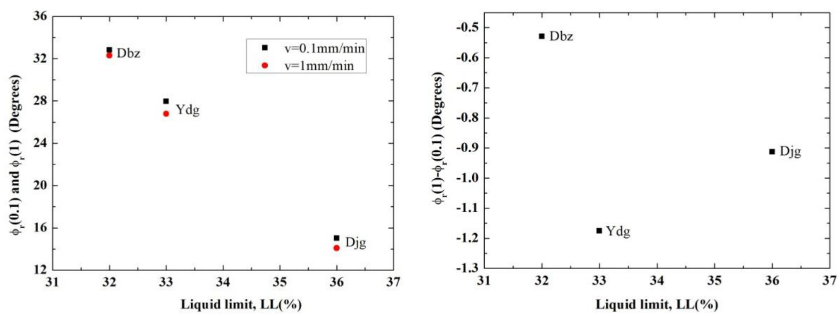
It has been recognized that residual shear strength of soils is closely related with soil properties, such as particle size distribution (PSD), liquid limit (LL), plasticity index (Ip)and clay fraction (CF) (Terzaghi et al., 1996). Fig. 10 depicts the relationships between residual friction angles as well as the difference in the residual friction angles and soil properties including liquid limit (LL), plasticity index (Ip) and clay fraction (CF) at two shear rates. The residual friction angles at two shear rates decreased nonlinearly with the increasing of the LL. As for the relationship between the ϕ_r and Ip, the ϕ_r under the low and high shear rates decreases from about 32° to 15° with increasing the Ip from 11 to 16. These findings agree well with the early studies (Wesley, 2003; Tiwari et al., 2005). With increasing of CF from 9% to 24%, the residual friction angles under low and high shear rates were found to decrease (Fig. 10). These observations are consistent with previous studies (Lupini et al., 1981; Gibo et al., 1987). Interestingly, for Dbz and Ydg soils of which have similar percentage of clay fraction, the residual friction angles at both shear rates varied. However, in the relationships between the difference in the residual friction angles and the soil properties, no clear correlations were found.



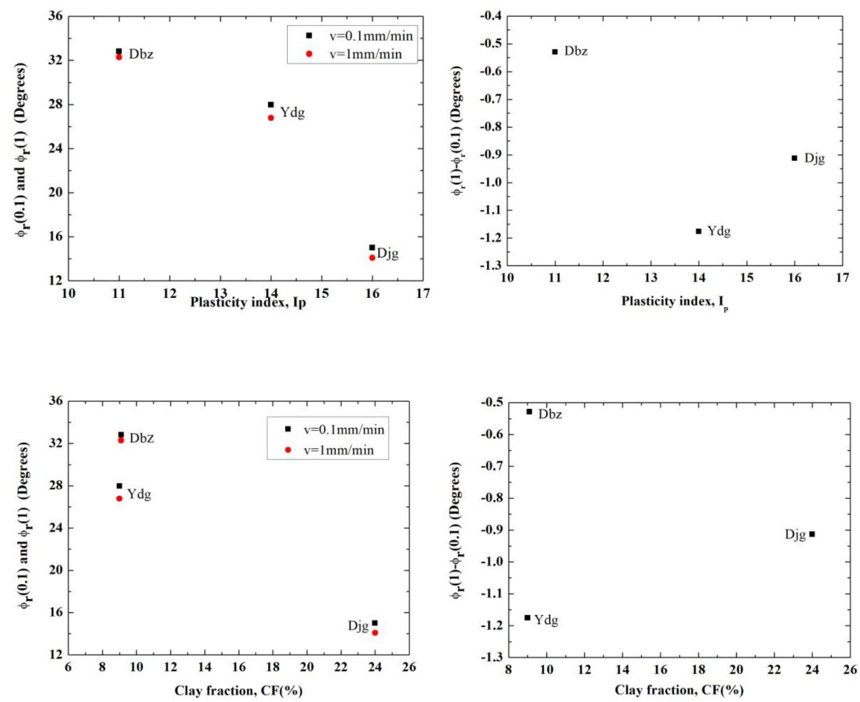


Figure 10. Relationships between residual shear parameter, the difference in residual shear parameter and the soil properties at two shear rates

5. Discussion

Examination of the ring shear test results provides a basis for some general comments on the use of tests results with different shear rates, partially deepening some aspects deriving from previous studies.

From the experimental results on the three selected landslides, it was found that there is a negative relationship between residual friction coefficients and shear rates for all samples (Figs. 7, 8 and 9). Such a negative effect of shear rate (higher residual friction coefficients at lower rates) has been reported in the literature for fine-grained soils (Tika et al., 1996; Gratchev Ivan and Sassa, 2015). This effect may be closely associated with ability of clay particles in specimen to restore broken bonds at

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different shear rates. Previous studies (Osipov et al., 1984; Perret et al., 1996). concluded that with higher shear rates, the breakdown of the bonds between clay particles or flocs exceeds the restoration bond, leading to reduction in residual friction coefficients. In contrast, the bonds between particles are rebuilt quickly and the recovery rate can catch up the breakdown rate at lower shear rates. Therefore, the weaker bonding between particles could explain the strength drop with the increasing of the shear rate in this study.

The difference between the friction coefficients, $\tau_r/\sigma_n(1)$- $\tau_r/\sigma_n(0.1)$, at each normal stress level varies in different locations. $\tau_r/\sigma_n(1)$- $\tau_r/\sigma_n(0.1)$ in Ydg specimen are greater compared with that in Djg and in Dbz specimen (Table 2). As for Ydg and Dbz specimen, it is found that the shear rate effect on the friction coefficient can be seen to decrease with normal stress (Figs. 8 and 9). By contrast, there is an increasing tendency in the influence of shear rate on the friction coefficient with normal stress in Djg specimen (Fig. 7). Gibo et al. (1987) reported that the residual friction angle of soils was controlled by the effective normal stress as well as by the CF. Interestingly, Ydg (with CF 9%) and Dbz (with CF 9.1%) specimens with almost the same fraction of clay showed similar shear rate effect on the residual friction coefficient with normal stress increasing, however, Djg (with 24% CF) showed the contrast tendency of shear rate effect on residual friction coefficient with normal stress, indicating that such effect is closely associated with CF. Therefore, as for Ydg and Dbz with relatively low fraction of CF, there is an increase effect of shear rate on residual friction coefficient with decreasing of normal stress. Thus, for the application of

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measured residual friction coefficient for stability analysis of shallow landslides with lower overburden pressure, it is significant for us to use a low shear rate in ring shear tests to measure residual shear strength parameters. On other hand, for Djg with high CF, it is more reliable to use a low shear rate in ring shear tests to determine residual friction coefficient for stability analysis of deep landslides with high overburden pressure.

6. Conclusion

A series of ring shear tests were conducted on loess obtained from three landslides to study the residual shear characteristics of saturated loess. Based on the test results, the effect of the shear rate on the residual shear characteristics of loess in naturally drained condition was examined. The following conclusions can be drawn:

1. Ring shear test revealed that (i) shear displacement to achieve the residual stage with high shear rate is greater than that of the low shear rate; (ii) Both the peak and residual friction coefficient became smaller with increase of shear rate for each sample;(iii) The greater difference between the peak and the residual friction coefficient in loess samples could be attributed to relatively well-developed slickenside on the shear surface.
2. At the two shear rates, there was a nonlinearly decrease trend of the residual friction coefficient with the normal stress in all loess samples. The difference between the friction coefficients, $\tau_r/\sigma_n(1)$- $\tau_r/\sigma_n(0.1)$ was found to decrease with normal stress in Ydg and Dbz specimens while increase with normal stress in

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Djg specimens, indicating that CF may be closely associated with shear rate effect on residual friction coefficient with normal stress.

3. The difference at the two shear rates, $\phi_r(1)$ - $\phi_r(0.1)$, under each normal stress level were either negative or positive. However, under all normal stress, the difference at the two shear rates $\phi_r(1)$ - $\phi_r(0.1)$ was found to be negative. Such negative shear rate effect on loess could be attributed to greater ability of clay particles in specimen to restore broken bonds at low shear rates.
4. The relationships between the ϕ_r under two shear rates and soil properties (LL, Ip), demonstrated that the ϕ_r at both shear rates decreased gradually with the increasing of LL and Ip. However, no clear correlations between the difference in the ϕ_r at low and high shear rates and the soil properties were found.

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Code availability: Code can be made available by the authors upon request.

Data availability: Data can be made available by the authors upon request.

Author contributions: BL,JP and QH conceived and designed the method; BL produced the results, and wrote the original manuscript under the supervision of JP. JP and QH writing-review and editing.

Competing interest: The authors declare that they have no conflicts of interest.

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