# **Detailed Response Letter for NHESS-2018-328 Review Comments**

Probabilistic seismic hazard analysis using logic tree approach- Patna District (India)

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# **Response to All the Reviewers Comments**

We thank all reviews and editor for their valuable to time to review manuscript and give valuable suggestions to improve the same. Most of the comments are suggestions to improve the current version of manuscript, which will incorporate in the revised manuscript. Few clarifications are requested, we have given our response for the same below and also highlighted that respective points will be added in the revised manuscript. As editor informed only prepare response to reviewers comments, we are not submitting revised manuscript now, But we have given revised text will be modified in the revised version.

# **Response to Reviewer 1**

General Comment: - Abstract In the article of "Probabilistic seismic hazard analysis using logic approach-Patna District (India)" (Nat. Hazards Earth Sci. Discuss., tree Syst. https://doi.org/10.5194/nhess 2018-328) studied by Anbazhagan et al., a popular tool called the logic tree approach is employed for seismic hazard analysis of Patna District, India. Despite being an extensive study, it is observed that the logic tree application needs to be more informative about the weighting factors of terminal branches and selection of attenuation equations. This discussion mainly aims to present some comments and criticisms for some clarifications of the logic tree application.

Key words: Logic tree, weighting factors, seismic hazard analysis, attenuation equation.

Due to its capability of combination of multiple models alternatively, the logic tree approach employed in the article is of scientifically significance that practically offers a solution for the issues of the seismicity of the region (Patna District, India). However, the following technical points are the comments that could be queried for the application of logic tree approach in the study.

**Response:** - The authors would like to thank the reviewer for his/her valuable time for reviewing the manuscript. The following are the detailed response to the comments.

Comment 1: - In the logic tree approach, the seismic hazard analysis is carried out by the combination of models and/or parameters constructed with each terminal branch regarding with weighting factors. However, for construction of logic tree branches with the weightings of models, it appears that the criteria are lack and/or not clear in the article. They are the questions that what are the experimenter's (authors') concerns (issues) in practice and what are the expert's recommendations about the seismicity of the region. As a consequence, without accounting the weighting factors realistically, it is not possible to obtain a realistic result of seismic hazard analysis using the logic tree (Gullu and Iyisan, 2016).

**Response:** - The questions that what are the experimenter's concerns in practice and what are the expert's recommendations about the seismicity of the region is also explained in the revised article. In the revised manuscript, the construction of logic tree and the weighting of the different branches of the logic tree has been explained at different places. **Please see the line number 31-32 on Page number 3, and line number 1-4 on Page number 4.** 

Change in the manuscript: Patna district lies near to the seismically active Himalayan belt and on the deep deposits of the Indo-Gangetic basin (IGB). It is also surrounded by various active ridges as Monghyr-Saharsa Ridge Fault many active tectonic features such as Munger-Saharsa-Ridge Fault, and active faults such as East Patna Fault or West Patna Fault. These faults are acknowledged as transverse faults, and the occurrence of seismic events is due to stimulus of fluvial dynamics in the North Patna plains transverse faults (Valdiya1976; Dasguptaet al.1987). According to Banghar (1991) the East Patna Fault is one of the active faults in the study area and its interaction with Himalayan Frontal Thrust is characterized by a cluster of earthquakes. Dasgupta et al. (1993) accounted that all other faults between Motihari and Kishanganj city have the same possibility of seismic hazard as they form a part of related fault system.

Comment 2: - One of the power utilities of the logic tree comes from its relatively less effort compared to the conventional seismic hazard methodologies. It is important to note that using the logic tree with the judged weighting factor requires a calculation effort that dramatically increases with increased branches (Bommer et al., 2005; Sabetta et al., 2005). Thus, in order for preventing the troubles from the increased branches during estimations, the branches with slight differences are strongly recommended to be avoided (Bommer et al., 2005). Hence, readers of the article should be informed whether the authors avoided from similar nodes in the logic tree branches. Again, this specifically requires presentation of selection criteria of weighting factors in detail.

**Response:** - In the present study, the weight factor for different GMPEs has been calculated using the log likelihood values, which is explained in the manuscript. No such branch having with slight differences in weights have been observed in the present study. **Please see the line number 7-12 on Page number 13.** 

Change in the manuscript: It is necessary here to note that the experimenters performing for the seismic hazard assessment using weighting factor may lead to complication in the calculations

with the inclusion of different branches. To prevent this trouble, Bommer et al. (2005) suggested avoiding using the branches having slightly differences between the options that it carries, in cases when those options result in very similar nodes. Therefore, when selecting the weighting factors in the logic tree in this study, the cases contrasting (or different) with each other as much as possible have been taken into consideration.

Comment 3: - Past works (Sabetta et al. 2005; Scherbaum and Kühn, 2011) indicate that selection of attenuation models (i.e., ground motion prediction equations) is much important for seismic hazard analysis using the logic tree approach. Moreover, their selection for the seismic hazard assessment has a greater impact than expert's judgments for the weightings of the logic tree branches. In order to provide a consistency within a probabilistic framework, it is proposed (Scherbaum and Kühn, 2011) that the weight factors in attenuation equations are assigned in a sequential manner (such that if the first equation of three selected gains a weight of 0.6, then the remaining equations as sum must be 0.4). Consequently, the study in the article requires being more informative about how the authors assigned the weights of their selected attenuation equations into account of logic tree frame.

**Response:** - We agreed with the reviewer, in the present study the weights have been assigned in the sequential manner. This has been already explained in the revised manuscript with proper references. Please see the line number 14-18 on Page number 7.

Change in the manuscript: Scherbaum and Kühn (2011) showed the importance of weight treatments through the logic tree approach as probabilities instead of simply as generic quality measures of attenuation equations, which are subsequently normalized. They also indicated the risk of independently assigning of grades by different quality criteria, which could result in an apparent insensitivity to the weights. In order to provide the consistency with a probabilistic framework, they proposed assigning the weight factors in a sequential manner, which is used in the present study.

Comment 4: - In the article, the authors perform seismic hazard estimations by Frankel approach as well as the logic tree. The logic tree estimations should principally show the whole terminal branches (i.e., combinations of all possible models), not sub-branches. However, the study is not convincing that how the authors can compare the logic tree's responses with the ones of its sub-branch of Frankel approach. This makes confusing about the estimation by Frankel approach whether it is estimated using sub-branches of logic tress or using its relevant formula.

**Response:** - In the present study, the hazards values are calculated using the Frankel approach considering the four models proposed by Frankel (1995). Further the final map developed using Frankel (1995) has been weighted and combined with the areal seismic sources to calculate the hazard values using the zoneless approach.

# Response to Reviewer 2

General Comment: - The Manuscript entitled "Probabilistic seismic hazard analysis using logic tree approach- Patna District (India)" presents a comprehensive PSHA study for one specific region in north India. Authors employ different alternatives for main PSHA-analyses components including, e.g., Mc, maximum magnitude, GMPE-set, zonation model, etc. to populate the epistemic logic tree. The study is confident, uses extensive local sources dataset and employs upto-date PSHA analytical tools incorporated into the logic tree approach to treat the epistemic uncertainty. In general, I would recommend publishing present study in NHESS. Nevertheless, I would recommend "major revision" because of the two issues. Both issues deal with the art of presentation, so, I think, Authors could easily accommodate them. First- the manuscript has too many figures in the results section, namely23! Some of them could be combined into one plot. For example, figures presenting PGA maps for the three approaches: 'classical', 'areal seismic zone' and 'Frankel' (Fig. 8a, 11a, 16a). Same for the deaggregation diagrams, and so on. Such a combination, if possible, would make presentation more structured and comparison between methods more evident. Alternatively, Authors may think of moving some figures into the supplementary material. The second issue is writing style. English is generally OK, but the writing style is somewhat sloppy. Especially in the beginning of the manuscript. Please read thoroughly statement-by-statement and put attention at clarity and correctness of the text. To avoid dubious statements like that on Page 2, Lines 10-11.

**Response:** - The authors would like to thank the reviewer for his valuable comments which helped us in reviewing the manuscript. As per the suggestion figures have been combined and few has been used as supplementary material. The writing style has been also improved and the manuscript has been checked thoroughly statement-by-statement.

Page 2 and line 10-11 has been revised. Please see the line number 7-12 on Page number 13.

**Change in the manuscript:** In the absence of appropriate region-specific models of wave propagation, ground motion prediction models are generally used to determine the hazard value.

**Comment 1: -** 1-17: tsunami

**Response:** - It has been changed in the revised manuscript. Please see the line number 17 on Page number 1.

**Comment 2: -** 1-18: Triggering tsunamis is nothing to do with ground shaking because tsunamis respond to residual, static deformation of the seabed, not to PGV or PGA.

**Response:** - Tsunami has been removed in the revised manuscript. **Please see the line number 17** on **Page number 1.** 

Comment 3: - 1-20: "subduction"

**Response:** - It has been changed in the revised manuscript. Please see the line number 20-21 on Page number 1.

**Comment 4: -** 1-20: I am not sure if you can call the India-Eurasia collision as "subduction zone" because the latter term commonly implies subduction of the oceanic lithosphere whereas in this case, we actually have continent-to-continent collision.

**Response:** - The word "subduction zone" has been replaced by "continent-to-continent collision". **Please see the line number 20-21 on Page number 1.** 

Change in the manuscript: Besides, many great events (2015, Nepal earthquake) have originated from continental-to-continental collision.

**Comment 5: -** 2-6: Does aleatoric uncertainty include "randomness of ground motion prediction"? GMPE's are derived by people, not by nature. Maybe, better to say that it includes randomness of wave propagation and site amplification?

**Response:** - It has been changed as per the suggestion. The statement has been changed. **Please** see the line number 7 on Page number 2.

**Change in the manuscript:** One is due to randomness of the nature of earthquake, wave propagation, and site amplification named as aleatory uncertainty while other is due to incomplete knowledge of earthquake process named as epistemic uncertainty.

**Comment 6: -** 2-11: I do not see the logical connection between the sentence starting with "Generally, ground motion: : ::" and the next one. Logic tree is used to quantify all kinds of epistemic uncertainty, not only that related to GMPE's. Please consider re-formulating these paragraphs.

**Response:** - As per the suggestion this paragraph has been revised. It has been revised. **Please see** the line number 12-17 on Page number 2.

Change in the manuscript: Epistemic uncertainty is due to improper knowledge about the process involve in earthquake events and algorithms used to model them. Hence, in this study, logic tree framework has been used to reduce the epistemic uncertainty in the final hazard value calculation. In the absence of appropriate region-specific models of wave propagation, ground motion prediction models are generally used to determine the hazard value. The uncertainty in GMPEs can be reduced by incorporating logic tree in the hazard analysis study.

**Comment 7: -** 2-15: if weight is assigned, we cannot speak about "qualitative" assessment any more

**Response:** - This word has been removed in the revised manuscript. **Please see the line number 20 on Page number 2.** 

Comment 8: - 2-21: "As per Bilham" – what is "per"?

**Response:** - "As per" has been replaced with "similar to". **Please see the line number 26 on Page number 2.** 

**Comment 9: -** 2-28: "determined weighted mean"?

**Response:** - Apology for the typo. This statement has been revised. **Please see the line number 32-33 on Page number 2.** 

Change in the manuscript: Maximum magnitude has been determined using weighted mean considering three methods as increment factor on maximum observed magnitude, Kijko and Sellevoll (1989) and regional rupture characteristics (Anbazhagan et al. 2015b).

**Comment 10: -** 2-31: "viz."?

Response: - "viz." has been replaced by "namely". Please see the line number 2 on Page number 3.

**Comment 11: -** 3-7: what is "SSA". Define explicitly before using abbreviation for the first time.

**Response:** - "SSA" is seismic study area and it has been mentioned in the revised manuscript. **Please see the line number 12 on Page number 3.** 

**Comment 12: -** 3-8: an area cannot have only one single value of lon and lat. A point can, area – not.

**Response:** - The statement has been changed as follow. Please see the line number 13-14 on Page number 3.

**Change in the manuscript:** The present study area has covered the longitude 84.6-85.65°E and latitude 25.2-25.8°N

**Comment 13: -** 3-10: give reference to Figure 1 in the beginning of Patna region description Figure 1: source labels not readable I suggest adding a supplementary table describing individual faults. Or, alternatively, to extend Table S1 with additional parameters like position, rupture length.

**Response:** - As per the suggestion, the refence of Figure 1 has been given in the beginning and Table S1 has been extended by providing the position (latitude and longitude of the end points), total fault length and rupture length.

**Comment 14: -** 3-16/17: redundancy

**Response:** - As per the suggestion the sentences are moved blow at relevant position. Please see the line number 31-32 on Page number 3 and line number 1-4 on Page 4.

**Comment 15: -** 3-28: this sentence looks redundant. The whole paragraph is better to move to the beginning of the current chapter.

**Response:** - As per the suggestion the whole paragraph is moved in the beginning of the paragraph. **Please see the line number 17-27 on Page number 3.** 

Change in the manuscript: Based on damage distribution map i.e. isoseismal map (1833 Nepal earthquake and 1934 Bihar-Nepal earthquake) and location of Main Boundary Trust, Main Central Trust and Himalayan Frontal Thrust (HFT), a radius of 500 km has been selected for present SSA. The detail study about selecting SA of 500 km is given in Anbazhagan et al. (2015a). Geographical information of India demonstrates that approximately 60% of the land is highly susceptible to earthquakes (NDMA, 2010). The tectonic feature of SA has been compiled from the Seismotectonic Atlas (SEISAT, 2010) published by the Geological Survey of India (GSI, 2000). The seismotectonic map was developed by considering 500 km radius from Patna district boundary by considering linear sources (faults and lineaments) from SEISAT and published literatures (e.g. NDMA, 2010; Nath and Thingbaijam, 2012; Kumar et al., 2013). Separation of MBT and MCT has been done and all the faults along with MBT and MCT have also been numbered. Seismotectonic map for Patna District is shown in Figure 1. A brief description of seismicity and seismotectonics of SSA is given below.

**Comment 16:** - 4-21: it is still worth to provide GR-expression with 'a' and 'b' parameters Seismicity parameters 'a' and 'b' are discussed in both Sections 3.1 and 3.2. That is why present Section titles look somewhat misleading. Consider renaming these sections, for example, according to the derivation approach: period of completeness (3.1) vs magnitude of completeness (3.2).

**Response:** - Both the sections have been renamed as per the suggestion. **Please see the line** number 4 on Page number 5.

**Comment 17:** - 5-13: why M4.5 was finally accepted as Mc? This statement comes into contradiction with following statements where Authors accept M6-model to be their reference model. M6 has different Mc values for the two regions.

**Response:** - Apology for the same. This statement has been removed as it's a typo error.

**Comment 18:** - General Remark to Section 3.2: Authors employ 9 different methods to estimate 'a', 'b', and Mc. But finally accept only one model, M6, giving the corresponding logic tree node weight = 0.5. That means all other models were given zero weights despite some of them (M1,3,5) show results similar to M6. Authors should clearer justify why they do neglect all other 8 models.

**Response:** - Nine methods have been used to check the variability in 'a', 'b', and Mc for the same study area. However as per Boomer et al. (2005) calculation effort increases dramatically with the inclusion of more branches in the logic tree. Therefore, Bommer et al. (2005) suggested avoiding using branches with slight differences between the options, in cases when those options result in very similar nodes. Hence only M6 has been used as M6 method is capable for  $M_c$  calculation as it synthetically maximises the available data and stabilises the  $M_c$  value. Please see the line number 7-11 on Page number 6.

Change in the manuscript: According to Boomer et al. (2005) calculation effort increases dramatically with the inclusion of more branches in the logic tree. Therefore, Bommer et al. (2005) suggested avoiding using branches with slight differences between the options, in cases when those options result in very similar nodes. Hence only M6 has been used as M6 method is capable for  $M_c$  calculation as it synthetically maximises the available data and stabilises the  $M_c$  value.

Comment 19: - 9-29: vulnerable?

**Response:** - Apology for the typo. This word has been replaced.

# Response to Reviewer 3

General Comment: - Journal: NHESS Title: Probabilistic seismic hazard analysis using logic tree approach — Patna District (India) Author(s): Panjamani Anbazhagan et al. MS No.: nhess-2018-328 The article titled "Probabilistic seismic hazard analysis using logic tree approach Patna District (India)" utilize logic tree technique to conduct PSHA study for Patna District, India. Authors

employ different branches in the logic tree for PSHA calculations to handle the epistemic uncertainties. Although the work is extensive, and the exerted efforts are great, this paper still needs many clarifications, so it can be accepted for publication. It is not well organized, and, in many parts, it is non-properly sequenced with non-threaded paragraphs, leaving the reader confused and suffering to catch the idea. The English language of the paper is poor and negatively affects the understanding of many paragraphs. English needs to be revised critically. Abbreviations should be mentioned at its first appearance. Avoid using the same abbreviation for two different terms (e.g. SA is used for spectral acceleration and for study area). What are SSA, MBT, MCT, S60,: :.etc. All abbreviations should be defined at their first appearance in the text. All localities, faults and geological structures mentioned in the manuscript should be shown on maps. I could not appropriately follow the seismotectonic part of the area due to lack of such illustrations.

**Response:** - The authors would like to thank the reviewer for his valuable comments which helped us in reviewing the manuscript. The manuscript has been revised thoroughly for English and flow has been maintained to make it easy for the readers. Abbreviations have been provided at the first place. SA is only used for the spectral acceleration in the revised manuscript. The faults mentioned in the manuscript has been shown properly and quality of the seismotectonic map has been improve.

## Introduction

**Comment 1: -** Page 1, lines 20-21: Which gap? Please provide more explanation.

**Response:** - It is the Himalayan seismic gap and detail explanation is given in Bilham and Wallace (2005); which is also mentioned in the manuscript.

Change in the manuscript: The Himalayan seismic gap (Bilham and Wallace, 2005) and thick soft soil sediments makes the scenario more dangerous for cities close to Himalayan region.

**Comment 2: -** Page 2, lines 3-5: Very accurate sentence, but nothing is carried out in the end. Why this sentence is written here?

**Response:** - This sentence is mentioned to justify the need of the hazard analysis for the Patna city and in the present study an updated map, and methodology used to determine the hazard value at bedrock for Patna city.

**Comment 3: -** Page 2, line 27: I could not understand "Maximum magnitude has been determined weighted mean using increment : : :: ::"

Response: - This statement has been revised and given below. Please see the line number 32-33 on Page number 2.

Change in the manuscript: Maximum magnitude has been determined using weighted mean considering three methods as increment factor on maximum observed magnitude, Kijko and Sellevoll (1989) and regional rupture characteristics (Anbazhagan et al. 2015b).

Geology, Seismotectonics and seismicity of the study area (SA)

**Comment 4: -** Page 3, line 8: coordinates here are for a point, it is not for an area.

Response: - The statement has been changed as follow. Please see the line number 13-14 on Page number 3.

**Change in the manuscript:** The present study area has covered the longitude 84.6-85.65°E and latitude 25.2-25.8°N

**Comment 5: -** Page 3, line 29: "and published literatures" give references.

**Response:** - It has been mentioned in the revised manuscript. **Please see the line number 24-25** on **Page number 3.** 

Change in the manuscript: The seismotectonic map was developed by considering 500 km radius from Patna district boundary by considering linear sources (faults and lineaments) from SEISAT and published literatures (e.g. NDMA, 2010; Nath and Thingbaijam, 2012; Kumar et al., 2013).

**Comment 6:** - Page 4, lines 1-3: Authors should show the priority scheme in selecting the earthquake from each data base. I mean if the same earthquake is available in more than one database, which one will be selected? Which magnitude scale from which database has the first priority and which has the second and so on? Is the same magnitude scale for the same earthquake at different database yield the same value? All the above queries should be clarified in detail. Please show the start and end time of the catalogue to be able to assess its reliability.

**Response:** - The events have been selected from all the mentioned agencies. The duplicate events have been deleted and further the magnitude has been homogenized to moment magnitude scale. This is mentioned in the revised manuscript. Further the start and end time of the catalogue is also given in the revised manuscript. **Please see the line number 21-23 on Page number 4.** 

**Change in the manuscript:** The events have been selected from all the mentioned agencies. The duplicate events have been deleted and further the magnitude has been homogenized to moment magnitude scale.

**Comment 7: -**Page 4, lines 15-18: Please revise the earthquake numbers in each magnitude range as their sum should be 818 as mentioned in Page 4 line 9.

**Response:** - Apology for the same. The correct number has been mentioned in the revised manuscript. **Please see the line number 28 on Page number 4.** 

# a and b parameters

**Comment 8:** -This is the most confusing part of the manuscript. In this section the a and b values are calculated for two regions (I and II). What is the role of these two areas and their seismicity parameters in the hazard calculations? The classical method used 178 seismic sources and the zoneless method used 7 area seismic zones. Why this is interfered in the current study. Secondly, the magnitude of completeness should be calculated before evaluating the seismicity parameters as GR parameters should use complete data only.

**Response:** - The seismic study area has been divided into two regions based on the seismicity. That is why a and b values are calculated for two regions (I and II). The hazard values are calculated using classical approach in which 178 seismic sources have been used as input parameter, whereas, in the zoneless approach, 7 areal sources have been used which are delineate based on the seismicity parameters.

a and b values have been calculated considering two ways one considering magnitude of completeness and other period of completeness.

**Comment 9:** - Magnitude of completeness Page 5, line 12: This great difference in the Mc values casts doubt on the calculated values. Please explain why different methods have such different outputs. Also justify the great difference in a and b values in lines 17-19. B values of 0.149 and 0.176 are not physically accepted. Again, it is not clear how the authors used the a and b values shown in this section in the hazard calculations?

**Response:** -We agreed with the reviewer, the difference in Mc values is due to the different algorithms used, which is also explained in the revised manuscript. However, we used these nine different methods to estimate the uncertainty in the seismicity parameters. The lower b-value is observed as it is calculated based on the magnitude of completeness, but it is not used for the analysis and is also explained in the revised manuscript. **Please see the line number 4-6 on Page number 6.** 

**Change in the manuscript:** The lower b-value is observed as it is calculated based on the magnitude of completeness which may be due to the change in the algorithm as it selected the completed magnitude as minimum observed magnitude. This is not used further in the hazard calculation.

# **Maximum magnitude estimation (Mmax)**

**Comment 10:** - Page 5, line 32: "based on b values" to add 0.5 based on b value, b value should range between 0.9 and -1.0, which is not the case here.

**Response:** -The calculated and adopted "b-values" is in the range of 0.8 to 1.0, hence as per the suggestion adding 0.5 to maximum magnitude observed is justifiable.

Comment 11: - The authors used the region-specific rupture technique to calculate Mmax and provide it the maximum weight. The technique depends on the ratio between the rupture length and the total fault length. My questions are: 1- Is the seismic record enough to be sure about the above ratio? The answer is NO as the authors themselves clarified when they justify the use of zoneless method, stating that "many sources given in Figure 1 are not well studied to prove its seismic activity". This raises great uncertainty on the maximum magnitude calculated for these seismic sources. 2- Is there any possibility to rupture the entire fault length in one earthquake? Recent studies suppose that the entire fault length will be ruptured in one earthquake when calculating the maximum earthquake.

Response: -We agreed with the reviewer but seismic sources we used are 178 in number which is enough as per our knowledge to justify the ratio and which can also be observed from the trend shown in Anbazhagan et al. (2015 a). However, in addition to that we also used other methods which is based on the seismicity of the region i.e. Kijko method and incremental method. All the sources used in the present study are from published literature and mentioned in the manuscript. There may be a possibility of total rupture of total fault length, however, as far as Himalayan seismotectonic is concerned, no study exists on this context as per knowledge. We may consider the total rupture in our future study.

## 8.1 Classical approach

Comment 12: - Page 9, line 27: Authors used 178 seismic sources. The seismicity of many of these faults are not well studied. It is not clear how the seismicity parameters are calculated for each single source. It is well known that GR model cannot be used to calculate a and b values for single faults. Slip rate could be used but with many not well studied sources, the results should be at least uncertain. Using logic tree does not mean ignoring use the right input parameters for each method.

**Response:** -We agreed with the reviewer that seismicity of the sources may not be properly studied, hence, due to that we used a well-defined approach explained by Anbazhagan et al. (2009). As far as this study is concerned, we did not calculate GR "a" and "b" parameter for single fault. Slip rate can be used but for determining the hazard value, we used well-defined algorithm defined by Cornell (1968), which does not require the same.

# **Zoneless approach**

**Comment 13:** -Page 10, line27: use return period instead of "frequency of exceedance" Four models (figure 4) using zoneless approach (Frankel, 1995)

**Response:** -It has been replaced, as per the suggestion. Please see the line number 27 on Page number 11.

Comment 14: -Page 11, line 15: the return period 85 years (of what? This is most probably PGA)

**Response:** -Yes, it is the defined for PGA.

Comment 15: -Page 11, line 19: From which model the deaggregation plot is calculated? Or the authors used weighted deaggregation values based upon the weighs given for each of the four models. This should be very clear. Authors should explain why the results of the two methods are completely different in terms of hazard values and terms of the change in the spatial distribution (many low hazard areas in one method show very high hazard in the other method). This should be justified, as it is not enough to say for this the logic tree is created. A mistake could be done in the calculation or a method is not adequate for the region. Therefore, it is better to justify the use of zoneless methods.

**Response:** -The deaggregation has been calculated by considering the weighted mean from all the four models. This is mentioned in the revised manuscript. As these two methods have different input values, hence the results are different that is why logic tree approach has been used to reduce the uncertainty. The difference in results in explained in more details in the revised manuscript. The used of zoneless approach is due to spatial variability of the seismicity of the region and to estimate the hazard value where seismic source is not well studied. This is also explained in the revised manuscript.

**Change in the manuscript:** The deaggregation has been calculated by considering the weighted mean from all the four models.

**Comment 16: -**Page 12, line 5: Please add for 10% probability before "The PGA values" Final hazard map using logic tree

**Response:** -As per the suggestion, it has been added.

Comment 17: -Page 12, lines 26-27: As the high hazard values are related to the East and West Patna Fault, then, why the classical hazard values which are more related to the faults show very much less values?? Authors compared their results with previous studies. I recommend comparing the results of each method with the recent observations and with the previous studies to show a reason why the results are very inconsistent. If the current results are accurate, authors should recommend to change IS 1893 (2002) in Patna as the current hazard values highly exceed its summit.

Figure 1 is very unclear and need to be provided in a higher resolution way.

**Response:** -As per the results and calculations, PGA is higher near to the East and West Patna Fault (See Figure 8). As per the suggestions, the values form all the methods are also compared in

the revised manuscript. Also detailed comparison with previous studies are revised in the revised manuscript. Please see the line number 3-14 on Page number 14.

Figure 1 has been revised as per the suggestion and detailed source are given.

Change in the manuscript: It has seen from the mean deaggregation plot that the motion for 6.0  $M_w$  at 40 km hypocentral distance, 6.0  $M_w$  at 15 km hypocentral distance and 6.0  $M_w$  at 25.25 km hypocentral distance is predominant in case of Cornel's, Areal and Frankel's approach respectively considering 2 % probability in 50 years. However, the motion for 5.5  $M_w$  at 50 km hypocentral distance, 5.75  $M_w$  at 20 km hypocentral distance and 5.75  $M_w$  at 30.3 km hypocentral distance respectively predominant in case of Cornel's, Areal and Frankel's approach. The PGA values varies from 0.08 to 0.43 g, 0.29 to 0.41 g and 0.26 to 0.36 g in case of Cornel's, Areal and Frankel's approach respectively considering 2 % probability in 50 years. Whereas it from 0.04 g to 0.18 g, 0.09 g to 0.16 g and 0.09 g to 0.16 g respectively considering 10 % probability of exceedence in 50 years in case of Cornel's, Areal and Frankel's approach.

# Probabilistic seismic hazard analysis using logic tree approach-Patna District (India)

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**Abstract.** PGA and SA distribution for Patna district is presented considering both classical and zoneless approach through logic tree frame work to capture the epistemic uncertainty. Seismicity parameters are calculated by considering completed and mixed earthquake data. Maximum magnitude <a href="was-is-calculated">was-is-calculated</a> using three methods namely incremental method, Kijko method and regional rupture characteristics approach. Best suitable GMPEs <a href="was-are-selected">was-are-selected</a> by carrying out "efficacy test" using log likelihood. Uniform hazard response spectra have been compared with Indian standard BIS 1893. PGA varies from 0.38 g to 0.30 g from southern to northern periphery considering 2 % probability of exceedence in 50 years.

#### 1 Introduction

Seismic hazard analysis is effective in presenting the potentially damaging phenomenon associated with earthquake. Earthquake disaster is not only associated with collapsing of structures due to ground shaking but also triggers fire, liquefaction, and landslide, and Tsunami. So, it is indispensable to forecast the ground shaking level to serve the engineering needs in mitigating the risk associated with earthquakes. In India, moderate earthquakes ( $M_w < 7$ ) including Anjar 1956, Koyna 1967, Udaypur 1988, Uttarkashi 1991, Chamoli 1999 have caused significant damage in last 10 decades (Nath and Thingbaijam 2012). Besides, many great events (2015, Nepal earthquake) have originated from continental-to-continental collision Subduction zone. The Himalayan seismic gap (Bilham and Wallace, 2005) -and thick soft soil sediments makes the scenario more dangerous for cities close to Himalayan region. Apart from this, improper planning, increase in population density, poor land use and substandard construction practices in these cities magnify the prevailing seismic risk. Most of the existing seismic hazard maps are mainly on macro level for different parts of Indian subcontinent and are not up to state of art knowledge in engineering seismology. For example, Khattri et al. (1984) developed a hazard map representing peak ground acceleration (PGA) of for entire India with 10% probability of exceedence in 50 years. Under the Global Seismic Hazard Assessment Program (GSHAP), Bhatia et al. (1999) presented a probabilistic seismic hazard analysis (PSHA) of India. framework. Mahajan et al. (2010) delivered PSHA for the northwestern Himalayas. Recently, National Disaster Management Authority (NDMA 2010) and Nath and Thingbaijam (2012) have given-presented the PSHA map for entire India. In addition, Kumar et al. (2013) has developed thea deterministic seismic hazard analysis (DSHA) and PSHA map for Lucknow region considering local and active seismic gap. Additionally, the current Indian Standard (IS 1893 2016) code consists of many constraints such as poor delamination

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of active seismic sources, lack of vulnerable sources study, improper seismic hazard parameters which are not region-specific, and limited soil amplification consideration (Anbazhagan et al. 2014). Subsequently an updated seismic hazard map at micro level is essential for <a href="the-cities">the-cities</a> near to the Himalayan region, by considering new data, updated knowledge and improvement in previous methodologies.

There are two types of uncertainties associated with hazard analysis. One is due to randomness of the nature of earthquake, wave propagation, and ground motion predictionsite amplification named as aleatory uncertainty while other is due to incomplete knowledge of earthquake process named as epistemic uncertainty. Former can be easily reduced by integrating the distribution of ground motion about the median (Bommer and Abrahamson 2006) and latter can be assessed using logic tree approach. As Gullu and lyisan (2016) selected the GMPEs for the logic tree based on the the weighting factors were incorporated with a Venn diagram of attenuation models regarding experimenter's concern and expert's knowledge. Epistemic uncertainty is due to improper knowledge about the process involve in earthquake events and algorithms used to model them. Hence, In this study, logic tree framework has been made used to reduce the epistemic uncertainty in the final hazard value calculation. Epistemic uncertainty is due to improper knowledge about the process involve in earthquake events and algorithms used to model them. Generally, In the absence of the appropriate region-specific models of wave propagation, ground motion prediction models are more representative when the appropriate region-specific models of wave propagation are not available are generally used to determine the hazard value. This can be examined The uncertainty in GMPEs can be reduced by incorporating on of logic tree in the hazard analysis study. Logic tree represents the various nodes that defines the alternative input choices and each branch is assigned a-with a weight factor that signifies the quantitatively or qualitatively degree of plausibilitylikelihood assigned. To quantify the epistemic uncertainty, different branches of logic tree need to be considered which is based on source models, regionalization of bvalue, determination of magnitude of completeness and maximum magnitude and epistemic uncertainty in GMPE using the representative suitable approach.

In the present study, PSHA of Patna district (India) at micro level has been prepared along with the response spectrum by reducing the epistemic uncertainty. Patna lies at 250 km from the Central Seismic Gap (Khattri 1987) in the Himalayan region where the huge devastation and destruction due to 1803, 1934 Bihar-Nepal and 2015 Nepal earthquakes were reported. As perSimilar to Bilham (2015), a large earthquake appears to be imminent in future due to failure of rupturing of the main fault beneath the Himalaya because of Nepal 2015 earthquake. Hence such studies need to be done for the cities that lie within the vicinity of the Himalayan region and on Indo Gangetic Basin. Seismic sources and seismic events have been taken for 500 km radius around the district centre as per Anbazhagan et al. (2015a). The 'a' and 'b' parameters have been arrived by taking into consideration the completed earthquake data using Gutenberg-Richter (G-R) relationship and mixed data using methods proposed by Woessner and Wiemer (2005). The magnitude of completeness ( $M_c$ ) is also calculated by nine methods proposed by Woessner and Wiemer (2005). Maximum magnitude has been determined using weighted mean using considering three methods as increment factor on maximum observed magnitude, Kijko and Sellevoll (1989) and regional rupture characteristics (Anbazhagan et al. 2015b). Ground motion

prediction equations (GMPEs) has been selected from the twenty-seven numbers of applicable GMPEs for the region. The seismic hazard map for Patna district has been developed using PSHA applying probabilistic methods viz.namely classical method proposed by Cornell (1968) which was later upgraded by Algermissen et al. (1982) and smoothed-gridded seismicity models using areal source and four models proposed by Frankel (1995). For the development of hazard map using areal approach, delineation of seismic zones has been done based on the seismicity parameters i.e. 'a', 'b' and  $M_c$ . The hazard curves between mean annual rate of exceedence versus PGA and spectral acceleration ( $S_a$ ) are developed at the rock levels by both models. The final hazard map in terms of the rock level peak ground acceleration values are mapped for 2% and 10% probability of exceedence in 50 years i.e. return period of 2475 and 475 years based on logic tree. Additionally, hazard map for  $S_a$  at 0.2 and 1 s for return period of 2475 and 475 years is also given. Furthermore, uniform hazard spectrum for Patna district at rock level for return period of 2475 and 475 years based on logic tree has been estimated and compared with Indian standard IS 1893.

## 2 Geology, Seismotectonics and seismicity of study area (SA)

Regional seismicity, geological, seismological and seismotectonics information of seismic study area (SSA) have been assembled and evaluated for a desirable radius for seismic hazard analysis. The present study area has covered the longitude 8584.1446-85.65°E and latitude 25.6112-25.8°N and is near to various rivers such as Gandak in west, Ganga in southern side, Kosi and Bhagmati rivers in north side (see Figure 1). Patna lies in the Seismic zone IV with zone factor of 0.24 as per IS: 1893 (2016). To carry out a seismic hazard analysis, details and documentation about seismic features such as faults, shear zones and lineaments along with all earthquake events ( $M_w > 4$ ) that have occurred in the SSA are mandatory. Based on damage distribution map i.e. isoseismal map (1833 Nepal earthquake and 1934 Bihar-Nepal earthquake) and location of Main Boundary Trust, Main Central Trust and Himalayan Frontal Thrust (HFT), a radius of 500 km has been selected for present SSA. The detail study about selecting SA of 500 km is given in Anbazhagan et al. (2015a). Geographical information of India demonstrates that approximately 60 % of the land is highly susceptible to earthquakes (NDMA, 2010). The tectonic feature of SA has been compiled from the Seismotectonic Atlas (SEISAT, 2010) published by the Geological Survey of India (GSI, 2000). The seismotectonic map was developed by considering 500 km radius from Patna district boundary by considering linear sources (faults and lineaments) from SEISAT and published literatures (e.g. NDMA, 2010; Nath and Thingbaijam, 2012; Kumar et al., 2013). Separation of MBT and MCT has been done and all the faults along with MBT and MCT have also been numbered. Seismotectonic map for Patna District is shown in Figure 1. A brief description of seismicity and seismotectonics of SSA is given below.

Patna district lies near to the seismically active Himalayan belt and on the deep deposits of the Indo-Gangetic basin (IGB). Present study arealt is also surrounded by various active ridges as Monghyr-Saharsa Ridge Fault many active tectonic features such as Munger-Saharsa-Ridge Fault, and active faults such as East Patna Fault or West Patna Fault. These faults are acknowledged as transverse faults, and

transverse faults (Valdiya1976; Dasguptaet al.1987). According to Banghar (1991) the East Patna Fault is one of the active faults in the study area and its interaction with Himalayan Frontal Thrust is characterized by a cluster of earthquakes. Dasgupta et al. (1993) accounted that all other faults between Motihari and Kishanganj city have the same possibility of seismic hazard as they form a part of related fault system. Historic earthquakes such has 1833 Bihar, 1934 Bihar-Nepal, 1988 Bihar-Nepal has affected Patna city as far as economic loss and loss of lives is concerned. Many other earthquakes that have occurred near Bihar-Nepal border also prove to be devastating for Patna district. In addition to that, north side Patna is near East and West Patna fault. The frequency of seismic events on these faults are high (Valdiya 1976; Dasgupta et al. 1987). Besides SSA is also at 250 km from the Himalayan plate boundary. These plate boundaries were the source of major historic earthquakes. Considering the above seismic aspects, Patna district, can be acknowledged under a high seismic risk. Thus, in the present work, PSHA of Patna district has been carried out by considering all seismic sources and earthquake events by reducing epistemic uncertainty using logic tree approach.

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The earthquake data is collected from various agencies such as National Earthquake Information Centre (NEIC), International Seismological Centre, Indian Meteorological Department (IMD), United State Geological Survey (USGS), Northern California Earthquake Data Centre (NCEDC), and GSI. The events have been selected from all the mentioned agencies. The duplicate events have been deleted and further the magnitude has been homogenized to moment magnitude scale. A total of 2325 events have been compiled which are in different magnitude scale such as local magnitude, surface wave magnitude and body wave magnitudes. To attain uniformity, all the reported events are converted to moment magnitude  $(M_W)$  using relations given by Scordilis (2006) considering worldwide data. Furthermore, declustering algorithm proposed by Gardner and Knopoff (1974), modified by Uhrhammer (1986) was used for the separation of main event from dependent events. Out of 2325 events, 54% were noticed as dependent events i.e. 1272 events were documented as main shock for Patna region. The complete catalogue contains 454 events having moment magnitude less than 4 and  $\frac{818-1127}{127}$  events with  $M_w \ge 1$ 4. To develop the seismotectonic map, the linear source map was superimposed with the declustered earthquake events with and given as Figure 1. Near to MBT and MCT, earthquake events are densely located (See Figure 1) as compared to other part of seismotectonic map. As per Cornell (1968) and Frankel (1995) seismic study area need to be divided based on the seismicity or tectonic provision for calculating the significant hazard value from any potential source. Based on the event distribution SSA is divided into Region I (which belongs to MBT and MCT) and Region II. These regions were separated

using a polygon, as shown in Figure 1; Region I fit in to events inside and Region II belongs to events outside the polygon. Region I contained 280 events with  $M_w4$  to 5, 197 events with  $M_w5.1$  to 6, 26 events with  $M_w_6.1$  to 7 and 4 events with  $M_w$  greater than 7, whereas region II contained a total of 310 significant events viz. 168 events with  $M_w4$  to 5, 121 events with  $M_w5.1$  to 6 and 21 events with  $M_w6.1$  to 7. Both the regions were separately analysed for the seismic hazard estimation.

#### **3 Seismicity Parameters**

#### 3.1 'a' and 'b' parameters considering period of completeness

The most widely known Guttenberg-Richter (G-R) relationship (Gutenberg and Richter 1956) are usually used for the determination of 'a' and 'b' parameters for any SSA. The seismic recurrence rate can be precisely calculated only for the complete seismic event data. Stepp (1972) is used for examining the completeness of both the regions. Based on the analysis, it has been observed that for  $M_w > 5$ , catalogue is completed for 110 years for both the regions. However, for  $M_w < 5$ , catalogue is completed for last 80 years and 70 years respectively for region I and region II. After determining the completeness of catalogue, G-R recurrence law for both the region has been estimated. The 'b' value for the region I and region II respectively were found as 0.87 and 0.97. Whereas the 'a' value for region I and region II respectively for present study was determined as 5.32 and 4.98. More details about period of completeness and G-R recurrence law were described in Anbazhagan et al. (2015a).

#### 3.2 Magnitude of completeness $(M_c)$

Magnitude of completeness is defined as the lowest magnitude at which 100% of the events in a spacetime volume is detected (Rydelek and Sacks 1989; Taylor et al. 1990; Wiemer and Wyss 2000).  $M_c$  is also important for mapping out seismicity parameters such as b-value of Gutenberg-Richter relationship. The magnitude of completeness was calculated using nine different methods defined by Woessner and Wiemer (2005). Addition to magnitude of completeness, these methods also estimate G-R 'a', and 'b' parameters. These methods are Maximum Curvature Method (M1), Fixed Minimum Magnitude observed ( $M_{min}$ ) (M2), goodness of fit  $M_{min}90$  (M3) and  $M_{min}95$  (M4), Best combination of  $M_{min}90$ and  $M_{min}$  90 and maximum curvature (M5), entire magnitude range (M6), Shi and Bolt (1982) method (M7), Bootstrap method (M8), Cao and Gao (2002) method (M9). Magnitude of completeness for Patna site for Region I and Region II (shown in Figure 1) was estimated using software package ZMAP (Wiemer, 2001), a MATLAB based programme. The 'a', 'b' and  $M_c$  from each method is represented as Figure 2 for method M1, M2, M3, M4, M5, M6, M7, M8 and M9 for both the regions. It has been observed that  $M_c$  varies from 1.7 to 5.0  $M_w$  for region I and 1.9 to 4.9  $M_w$  for region II. So, for the further analysis, magnitude moment of 4.5 would be considered as magnitude of completeness. It is also observed that at R-value of 95% fit for the observed magnitude-frequency distribution cannot be modeled by a straight line for the region II due to lack of large amount of data. The Guttenberg-Richter ' $\alpha$ ' and 'b' parameter calculated using these 9 methods is different from calculated using completed data with G-R relationship values for both the region. Calculated values of G-R 'a' and 'b' parameter for both the regions is given in Table 1. The value of 'a' parameter calculated from the above methods vary from 3.11 to 6.57 for region I and 3.07 to 6.4 for region II. However, 'b' parameter calculated from the above

methods varies from 0.149 to 0.843 for region I and 0.176 to 0.848 for region II. The lower b-value is observed as it is calculated based on the magnitude of completeness which may be due to the change in the algorithm as it selected the completed magnitude as minimum observed magnitude. This is not used further in the hazard calculation. The difference in 'a' and 'b' parameters determined using the above methods, as it is calculated based on magnitude of completeness using mixed data- (Woessner and Wiemer 2005) instead of period of completeness for completed data of earthquake events. It has been seen from Table 1 that average value of 'a'-parameter is 4.95 for region I which is low as compared with the number of earthquakes in the region. Similarly, average b'-value of 0.522 and 0.661 for region I and region II isare also low when compared to the number of earthquake events having larger magnitude. According to Boomer et al. (2005) calculation effort increases dramatically with the inclusion of more branches in the logic tree. Therefore, Bommer et al. (2005) suggested avoiding using branches with slight differences between the options, in cases when those options result in very similar nodes. Hence only M6 has been used as M6 method is capable for  $M_c$  calculation as it synthetically maximises the available data and stabilises the M<sub>c</sub> value. So, as per-Woessner and Wiemer (2005) suggested that, M6 method is capable for  $M_c$  calculation as it synthetically maximises the available data and stabilises the  $M_c$  value. Therefore, for further analysis, 'a' and 'b' value of 6.57 and 0.843 and 6.22 and 0.815 respectively had considered for region I and II. For further study, weight factor of 0.5 was given to each of the method (i.e. period of completeness and magnitude of completeness viz. M6) used to determine the 'a' and 'b' value for both the regions. The final value of 5.0  $M_{\rm w}$  and 4.8  $M_{\rm w}$  is adopted as magnitude of completeness for region I and II respectively for further study.

#### 3.3 Maximum Magnitude estimation (M<sub>max</sub>)

The maximum probable earthquake magnitude has been calculated using both deterministic and probabilistic approach. Three methods viz. conventional methods of increment of 0.5 in maximum observed magnitude ( $M_{obs}^{max}$ ) based on 'b' values, Kijko Method (Kijko and Sellevoll 1989) and regional rupture characteristics (Anbazhagan et al. 2015b) have been used in  $M_{max}$  calculation. For the estimation of  $M_{max}$  using Kijko and Sellevoll (1989), calculation of  $M_c$  is already discussed above. Secondly,  $M_{max}$  magnitude has been calculated by adding a constant value of 0.5 to  $M_{max}^{obs}$  value at each fault (see Figure 1) like NDMA (2010) report.  $M_{max}$  is also estimated using regional rupture characteristics by considering the  $M_{max}^{obs}$  and possible seismic source. The whole procedure to calculate region-specific rupture characteristic was presented in Anbazhagan et al. (2015a). As per Risk Engineering Inc (1988) and others, increment varies from source zone to source zone and as per Wheeler (2009) short historical records produce samples of seismicity that are too small to constrain  $M_{max}$ . As per Anbazhagan et al. (2015b),  $M_{max}$  estimated from probabilistic method i.e. Kijko and Sellevoll (1989) is sensitive to SSA and seismicity parameters of a region. However,  $M_{max}$  determined using regional rupture characteristic is more reliable as it depends upon the seismic source and rupture length. Taking these points into consideration a qualitative weight factor of 0.3, 0.3 and 0.4 has been assigned to incremental method, Kijko method and regional rupture method respectively. More weight is given to regional rupture approach as it accounts for rupture of seismic source which in turn depends upon the energy released for an event. Maximum magnitude calculating corresponding to each fault is submitted as an electronic material (Table S1) and available Anbazhagan et al. (2015a).

#### **4 Selection of Ground Motion Prediction Equation (GMPE)**

GMPEs has been selected based on the efficacy test recommended by Scherbaum et al. (2009) and Delavaud et al. (2009). There are various GMPEs are available for the active crustal region and basin. Out of various GMPEs, 27 GMPEs are applicable for the present SA. The details of the efficacy test have been given in Anbazhagan et al. (2015c). Detail of these GMPEs are given in Anbazhagan et al. (2015a). Similar to Anbazhagan et al. (2015 a), the hypocentral distance is divided into three length bins viz. 0-100 km, 100-300 km and 300-500 km. The determined PGA values are used to estimate the loglikelihood (LLH) values, further Data Support Index (DSI) given by Delavaud et al. (2012) is used to rank the best suitable GMPEs. Positive DSI values have been identified for each segment and ranked based on maximum to minimum values. Positive DSI values for Patna earthquake is marked as bold in Table 3. It has been seen from Table 3 that three GMPE such as ANBU-13, NDMA-10 and KANO-06 can be used up to 100 km of hypocentral distance. For 100-300 km distance, ANBU-13, NDMA-10, KANO-06 and BOAT-10 and for hypocentral distance greater than 300 km, NDMA-10 will be used for further hazard analysis. Seismic hazard values in terms of PGA and SA can be calculated considering these equations for each seismic source. In addition to that, LLH based weight as per Delayaud et al. (2012) for selected GMPEs were also calculated. Scherbaum and Kühn (2011) showed the importance of weight treatments through the logic tree approach as probabilities instead of simply as generic quality measures of attenuation equations, which are subsequently normalized. They also indicated the risk of independently assigning of grades by different quality criteria, which could result in an apparent insensitivity to the weights. In order to provide the consistency with a probabilistic framework, they proposed assigning the weight factors in a sequential manner, which is used in the present study. The weight factors of 0.72, 0.17 and 0.11 are assigned calculated with ANBU-13, NDMA-10 and KANO-06 up to 100 km of hypocentral distance according to Delavaud et al. (2012). For 100-300 km distance, KANO-06, ANBU-13, NDMA-10 and BOAT-10 with weight factor of 0.32, 0.28, 0.26 and 0.14 are used-calculated and hypocentral distance greater than 300 km weight factor of 1 has been associated with NDMA-10. It can be noted here that only one GMPE is surfaced with positive DSI for distance segment of 300 km to 500 km and required additional GMPEs in this range, which is important for the far filed damage scenario in the region. These GMPEs with associated weight factor were further used in probabilistic seismic hazard analysis of Patna SSA. These weight factors would further useful in forming the logic tree to reduce the epistemic uncertainty in final hazard value. Detailed analysis of determination of LLH and weight factor corresponding to each GMPE is given in Anbazhagan et al. (2015a).

# 5 Delineation and spatial smoothening of seismic source model

Various researchers have delineated the seismic source for various parts of India. Considering the tectonic features and the past earthquake events, Gupta (2006) delineated the seismic sources for India. Kiran et al. (2008) and NDMA (2010) have done the same on the basis on the seismicity parameters. Furthermore, Nath and Thingbaijam (2011) have delineated based on focal mechanism data from the Global Centroid Moment Tensor database. Vipin and Sitharam (2013) determined the seismic sources in peninsular considering the seismicity parameters. In the present study, delineation of the seismic sources has been done based on the seismicity parameters viz. 'a', 'b' and magnitude of completeness

 $(M_c)$ . For delineation of different zones, Patna SSA has been divided into a grid size of  $0.02^{\circ} \times 0.02^{\circ}$  and from the centre of each grid a radius of 500 km is considered. The number of earthquakes events within 500 km of each radius were considered to determine the seismicity parameters. The reason for selection of 500 km radius was discussed above and given in detail in Anbazhagan et al. (2015a, 2013a). Considering the seismicity parameters (a-value, b-value and  $M_c$ ), the whole study area has been divided into 7 areal seismic zones and shown in Figure 3 (variation of only b-value is shown in background). These seven zones are considered as areal seismic sources as these are spread over a large area. The seismicity parameter has been calculated for each of these zones considering the frequency magnitude distribution (FMD) at 90% confidence level.  $M_{max}$  for each seismic zone has been calculated as per method discussed earlier. The average values of 'a', 'b',  $M_c$  and  $M_{max}$  have been given in Table 4.

For spatially smoothening of seismic source model, a grid size of  $0.02^{\circ}\times0.02^{\circ}$  along the longitude and latitude respectively was selected for representing different kinds of seismic source and to count number of earthquakes with magnitude less than or equal to  $M_c$  for each grid. To account the seismicity of the Patna SSA, the maximum likelihood estimates of  $10^a$  for that grid cell has been determined which correspond to the number of earthquakes per year. Using maximum likelihood estimate of  $10^a$ , the recurrence rate for different magnitude intervals has been estimated using algorithm recommended by McGuire and Arabasz (1990). The value  $10^a$  for each grid has been smoothed by applying a Gaussian function, given as equation (1), to find the final modified values corresponding to each grid. This smoothing is made to account for the uncertainty related to the location of earthquake events.

$$\tilde{\mathbf{n}}_{i} = \frac{\sum_{j} n_{j} e^{-\Delta_{ij}^{2}/c^{2}}}{\sum_{j} e^{-\Delta_{ij}^{2}/c^{2}}}$$
(1)

where,  $n_j$  is the number of earthquake in the  $j^{th}$  grid,  $\tilde{\mathbf{n}}_i$  is the smoothed number of earthquake in  $i^{th}$  cell, c is the correlation distance to account for the location uncertainties and  $\Delta ij$  is the distance between the  $i^{th}$  and the  $j^{th}$  cell. The sum is taken over the  $j^{th}$  cell should be within the distance of 3c of the  $i^{th}$  cell.

### 6 Computation Models for determining hazard value

Probability of exceedance of a ground motion for a spectral period can be determined once the probability of its size, locations and level of ground shaking is identified cumulatively. Seismic hazard map for Patna district has been developed by applying probabilistic method namely classical method proposed by Cornell (1968) which was later improved by Algermissen et al. (1982) and smoothed-gridded seismicity models (Frankel, 1995).

178 seismic sources (shown in Figure 1 and given as Table ET1) have been used for determining the probability of occurrence of a specific magnitude, probability of hypocentral distance and probability of ground motion exceeding a specific value have been estimated per Cornell (1968). Probability of rupture to occur at different hypocentral distances has been determined as per Kiureghian and Ang

(1977). The condition probability of exceedence for GMPEs was determined using a lognormal distribution as given by EM-1110 (1999). The ground motion at a site for a known probability of exceedence in a desired period has been calculated by amalgamating all the above probabilities. As a result of PSHA, hazard curve showing PGA or SA versus the frequency of exceedence of the level of ground motion. Detailed explanation is given in Anbazhagan et al. (2015 a). The deaggregation based on the principle of superposition has been proposed by lyenger and Ghosh (2004) has been used. The probability of exceedence of ground motion for each seismic source has been computed by merging these uncertainties. Detailed discussion on the methodology of PSHA can be found in Anbazhagan et al. (2009).

It can be noted that in the SSA, North-west and central part of Patna is not fully covered by well identified seismic sources and many sources given in the Figure 1 are not well studied to prove its seismic activity. Moreover, there are many places where linear source has not been identified. So, to overcome the limitation, zoneless approach proposed by Frankel (1995) has been used for developing the PSHA map for Patna SSA. This method accounts the spatial smoothing of historic seismicity to directly calculate the probabilistic hazard. The annual rate of exceedence for a given ground acceleration level is given by equation 2

$$\lambda(Z > z) = \sum_{d} \sum_{i} 10^{[\log_{10}(N_d/T) - b(m_i - m_{cut})]} P(Z > z/D_d M_i)$$
(2)

where, d and i are indices for distance and magnitude bins.  $N_d$  is the total of  $\tilde{\mathbf{n}}_i$  values over a given hypocentral distance increment (calculated using equation 1),  $P(Z > z/D_d M_i)$  will give the probability that a PGA of Z of will exceed z, when an earthquake of magnitude  $M_i$  occur at a distance of  $D_d$ , T is the time in years of earthquake catalogue used to determine  $N_d$ . The probability that a PGA of Z of will exceed z can be determined using by EM-1110, 1999. The hazard map has been determined by the four models proposed by Frankel, 1995. Model 1, Model 2 and Model 3 used for magnitude less than 7, however model 4 can be used for magnitude greater than 7. In model 1, the earthquake events having  $M_{\rm w}$  between 3 and 5 are assumed to illuminate areas of faulting which can produce destructive events. Model 2 also ensures that the hazard map reflects the local, historic rate of magnitude moment of 5 and larger events. As this model cannot explain the cause of major earthquake in the Active region with certainty, it is prudent to address the possibility of near-repeats i.e. within about 100 km of an historic moderate earthquake. Model 3 is based on a uniform source zone encompassing the Active seismicity zone, which is opposite to model 2. Model 4 associated with hazard from the larger events that is  $M_w >$ 7. As these events are less in the active seismic region and limited to a few areas only, therefore sources associated with them has been considered for determining hazard. These models are shown in Figure 4 which is used for the development of PSHA map using method proposed by Frankel (1995).

# 7 Modelling of Logic tree for hazard analysis

Seismic hazard can be assessed more practically using logic tree (Kulkarni et al., 1984) as it includes the accounted epistemic errors, components of seismic models and ground motion predictions (Figure 5). For determining the consistent model with different degrees of confidence each branch of logic tree is

to be investigated for implementing the uncertainties in probability models. The important consideration has been given to each branch of logic tree by incorporating the respected weights for assessing the final hazard of Patna district. After declustering the catalogue and developing the seismotectonic map, two models have been used with an equal weight of 50% for both classical and zone less approach. Zone less approach has been further divided as areal approach and Frankel approach of equal weight of 50% each. For Frankel approach, SSA has been considered for four models (discussed above) with weight factor of 30%, 30%, 20% and 20% for model 1, model 2, model 3 and model 4 respectively. These weights have been adopted based on the reliability of the source model. Larger weights are assigned to model 1 and model 2 because they are based on more reliable data and assumedly better representation of seismicity of SSA. Model 3 deals with the weak assumption that earthquakes with magnitude 3.0-7.0 are equally probable everywhere in Patna SSA whereas there is a great uncertainty in the data used for model 4. In addition, b-value were calculated for each of the model using Gutenberg and Richter (1956) and Woessner and Wiemer, (2005) (using entire magnitude range method) by assigning equal weight factor of 0.5. Furthermore  $M_{max}$  has been calculated using three methods namely increment to  $M_{max}^{obs}$ , Kijko and Sellevoll (1989) and regional rupture characteristic with weight factor of 30%, 30% and 40% respectively for each model as shown in Figure 5. Segmented based analysis of GMPE was done and weight was assigned to each GMPE based on the efficacy test. Based on the above discussion final hazard map for Patna SSA has been produced for 2% and 10% probability of exceedance in 50 years.

#### 8 Mapping of probability of exceedence using different approach considering epistemic uncertainty

### 8.1 Classical Approach (Cornell, 1968)

For determining the hazard value, different weight has been considered with respect to b-value, maximum magnitude and GMPE (see Figure 5). The seismic hazard using classical approach (Cornell, 1968) has been estimated using 178 seismic sources. SSA is divided into1725 grids of size 0.02°×0.02°. The whole procedure can be referred from Anbazhagan et al. (2015 a). Hazard curve from 10 most venerable sources are given as Figure 6 (a) and S60 is determined as most venerable vulnerable for Patna district (7.5  $M_w$  and hypocentral distance 55.11 km). Figure 6b showed a cumulative hazard curve obtained at the Patna district centre for zero s, 0.05 s, 0.1 s, 0.2 s, 0.3 s, 0.4 s, 0.6 s, 0.8 s, 1.0 s, 1.6 s and 2 s. It can be observed from the Figure 6b, that the frequency of exceedance for 0.075 g at zero second is 0.001 which will give the return period 834 years. This indicates that PGA of 0.075 g has 5.03% probability of exceedence in 50 years at the Patna. Further explanation can be referred from Anbazhagan et al. (2015 a). The mean deaggregation plot for Patna for return period of 2475 and 475 years is given as Figure 7a and 7b. PGA for 6.0  $M_w$  at 40 km hypocentral distance is notable for 2% probability of exceedence at 50 years. Likewise, for 10% probability of exceedence at 50 years the motion for 5.5  $M_{\rm w}$  at 50 km hypocentral distance is most contributing. Hazard curve has been generated at each grid for Patna, and the level of ground motion for frequency of exceedence  $\nu(z)$  can be estimated from it. Figure 8a and 8b shows the PSHA maps for Patna district for return period of 2475 and 475 years respectively. PGA varies from 0.35g in the north western and 0.43 north eastern peripheries to 0.08g towards the central part (See Figure 8a). Similarly, PGA vale at north eastern

periphery is 5.3 times more than central part of Patna considering 10% probability in 50 years (see Figure 8b). These results are similar to the previous study done by Anbazhagan et al. (2015 a).

# 8.2 Zoneless Approach

Likewise, classical approaches, epistemic uncertainty has been considered and weight factor are considered as shown in Figure 5. The PGA map of Patna has been developed using zoneless approach by dividing it into seven areal zones based on seismicity-parameters (Figure 3). For the development of PSHA map using simplified areal zonal modal, the seven zones along with the seismic parameters (Figure 3 and Table 4) are used. These seven areal seismic sources are smoothed using smoothed historic seismicity approach recommended by Frankel (1995). For development of the seismic hazard map, grid size of 0.02°×0.02° was selected for each of these seven areal sources. The activity rate was calculated in every grid cell and it was obtained by counting the earthquake having magnitude greater than or equal to  $M_c$  (Table 4) for the whole earthquake catalogue using MATLAB. The calculated activity rate was then spatially smoothed according to Equation 1, and the chosen correlation distance  $c=50\,\mathrm{km}$ . The annual rate of exceedence at the centre of each grid for the seven zones has been calculated using equation 2. The cumulative hazard curves for different period at the Patna district centre is given as Figure 9EF1. At zero period, frequency of exceedence for 0.075 g is 0.012 and estimated return period is 84 years, which means 0.075 g has 44.96 % probability of exceedence in 50 years. Similarly, for 0.5 g, return period is 24.4 thousand years and probability of exceedance of  $2.05 \times 10^{-1}$  % in 50 years at Patna district centre. As the period on interest rises from zero second to 0.8 seconds, a huge change in return period has been noticed (see Figure EF1, submitted as electronic supplement). Primarily the frequency of exceedence return period decreases from 84 years at zero periods to 13 years at 1.0 second which has further increased to 28 years at 0.2 second and again till 1.97E+05 years for 2 second. The mean deaggregation plot for Patna SSA for return period of 2745 and 475 years is given as Figures 10a-E2a and  $\frac{10bE2b}{1}$ . Figure  $\frac{10a-E2a}{1}$  shows that the motion for 6.0  $M_w$  at 15 km hypocentral distance is dominant for 2% probability of exceedence at 50 years. It changed to 5.75  $M_{\rm w}$  at 20 km hypocentral distance for 10% probability of exceedence at 50 years. Figures 11a 9a and 11b 9b are the PSHA maps for Patna urban centre for 2-% and 10-% probabilities of exceedence in 50 years respectively considering zoneless approach. PGA varies from 0.41 g in the south-eastern periphery to 0.34 g towards the central part (See Figure 11a9a). However, southwest part of the district encounters PGA of 1.4 times that of northwest part of the district. Similar PGA at southwest part increases to 1.57 folds as compared to north western part while considering 10% probability of exceedence in 50 years (Figure 1119b).

# 8.3 Four models (Figure 4) using Zoneless Approach (Frankel, 1995)

The hazard value for Patna district has also been determined by the four-model proposed by Frankel (1995). Each of these four models (Figure 4) has different spatial distribution of seismic activity. However present SSA have 5 characteristic earthquakes ( $M_w \geq 7$ ) so model 1, 2 and 3 have been analysed separately by considering earthquake events and PGA map using model 4 have been developed based on seismic sources associated with characteristic earthquake. The seismic hazard map is generated considering grid size of  $0.02^{\circ} \times 0.02^{\circ}$ . The activity rate was calculated in every grid cell and it has been obtained by counting the earthquake having magnitude greater than or equal to  $M_C =$ 

3.0 & 5.0 for Model 1 and Model 2 & 3 for different period of earthquake catalogue (Figure 4) using MATLAB. The calculated activity rate was then spatially smoothed according to Equation 1, and the chosen correlation distance c = 50, 75 km for model 1 and model 2 & 3. The annual rate of exceedence at the centre of each grid for the seven zones has been calculated using equation 2. The cumulative hazard curve has been obtained from model 1, 2, 3 and 4 at the Patna district centre for zero s, 0.05 s, 0.1 s, 0.2 s, 0.3 s, 0.4 s, 0.6 s, 0.8 s, 1.0 s, 1.6 s and 2 s and shown in Figure 12E3. At zero period, return period is 85 years and 0.075 g have 43.96 % probability of exceedence in 50 years at the Patna district centre and 0.5 g, return period increased 24.4 thousand years, in case of PGA. Primarily the frequency of exceedence declines from 85 years at zero periods to 14 years at 1.0 seconds which has further increased to 29 years at 0.2 seconds and again till 2.0E+05 years for 2 second. Figures 13a-E4a and 13b E4b shows the mean deaggregation plot for Patna for 2% and 10% probability of exceedence at 50 years. The deaggregation has been calculated by considering the weighted mean from all the four models. PGA for 6.0  $M_w$  at 25.25 km hypocentral distance and 5.75  $M_w$  at 30.3 km hypocentral distance is predominant for 2 and 10% probability of exceedence at 50 years. With the four models described in Figure 4, PGA map has been developed for Patna SSA and given in Figure 14aE5a, E514b, E514c& E514d considering 2% probability of exceedence in 50 years and Figure E615a, E615b, E615c & E615d considering 10% probability of exceedence in 50 years. It can be noted from model 1 that south-western part of Patna has high hazard value similar trend has been seen from model 2. The model 3 is a map of uniform hazard whereas as far as model 4 is concerned, north-eastern part and central part have high hazard because that portion of SSA is associated with characteristic earthquakes. The weighted mean PGA map for Patna has been developed by assigning different weight to these 4 models as 0.3, 0.3, 0.2 and 0.2 for model 1, 2, 3 and 4 respectively. A larger weight is given to model 1 and 2 as they represent real seismic activity because they are based on more reliable data. However, model 3 deals with weak conjecture that earthquake events between 3 to 7 are equally likely everywhere in Patna and Model 4 has great uncertainty in occurrence of characteristic earthquake. Figures 16a 10a and 16b 10b are the PSHA maps for Patna district for return period of 2475 and 475 years respectively. PGA varies from 0.34g in the eastern periphery to 0.26 g towards the north-western periphery, while increases to 1.38-fold for southwest part of the district (see Figure 16a10a). Similarly, considering 10% probability of exceedence in 50 years, PGA value in south western part of Patna is 1.5 times the south-western part (see Figure <del>16b</del>10b).

It has seen from the mean deaggregation plot that the motion for  $6.0\,M_W$  at  $40\,\mathrm{km}$  hypocentral distance,  $6.0\,M_W$  at  $15\,\mathrm{km}$  hypocentral distance and  $6.0\,M_W$  at  $25.25\,\mathrm{km}$  hypocentral distance is predominant in case of Cornel's, Areal and Frankel's approach respectively considering  $2\,\%$  probability in  $50\,\mathrm{years}$ . However, the motion for  $5.5\,M_W$  at  $50\,\mathrm{km}$  hypocentral distance,  $5.75\,M_W$  at  $20\,\mathrm{km}$  hypocentral distance and  $5.75\,M_W$  at  $30.3\,\mathrm{km}$  hypocentral distance respectively predominant in case of Cornel's, Areal and Frankel's approach. The PGA values varies from  $0.08\,\mathrm{to}\,0.43\,\mathrm{g}$ ,  $0.29\,\mathrm{to}\,0.41\,\mathrm{g}$  and  $0.26\,\mathrm{to}\,0.36\,\mathrm{g}$  in case of Cornel's, Areal and Frankel's approach respectively considering  $2\,\%$  probability in  $50\,\mathrm{years}$ . Whereas it from  $0.04\,\mathrm{g}$  to  $0.18\,\mathrm{g}$ ,  $0.09\,\mathrm{g}$  to  $0.16\,\mathrm{g}$  and  $0.09\,\mathrm{g}$  to  $0.16\,\mathrm{g}$  respectively considering  $10\,\%$  probability of exceedence in  $50\,\mathrm{years}$  in case of Cornel's, Areal and Frankel's approach. On comparing hazard map developed using classical approach and zoneless approach, it has been seen that northeastern part of Patna SSA has experienced maximum PGA value. As per classical approach (Cornell,

1968), predicted PGA value for central part of Patna district is 0.08 g whereas per Frankel's approach (Frankel, 1995) approach it is 0.32 g, however as per areal approach it is 0.31 g. Similarly, PGA value of 0.15g, 0.39 g and 0.39 g has been observed in case of Cornel's, Frankel's and Areal approach approximately in south western part of Patna SSA. It is because of absence of well-defined seismic source in that area whereas earthquake events of moment magnitude of 6 and above have occurred. However, in north western part PGA value is almost equal calculating using these approaches. This is the reason both zoneless and classical approach has been considered in this study to counter the epistemic uncertainty. So, that both the seismic sources and earthquake events can be accounted properly.

## 9 Final hazard map using Logic tree approach

The final hazard value has been developed by assigning the weight factor or 0.5 to both PGA value calculated corresponding to classical and zoneless approach. It is necessary here to note that the experimenters performing for the seismic hazard assessment using weighting factor may lead to complication in the calculations with the inclusion of different branches. To prevent this trouble, Bommer et al. (2005) suggested avoiding using the branches having slightly differences between the options that it carries, in cases when those options result in very similar nodes. Therefore, when selecting the weighting factors in the logic tree in this study, the cases contrasting (or different) with each other as much as possible have been taken into consideration. In zoneless approach, 0.5 weight factor were given to both PGA map developed using areal and Frankel's (1995) approach as explained earlier. So, both the hazard maps were compiled and finally 0.5 weight factor is given to zoneless approach. The final PGA variation corresponds to 2% and 10% probability of exceedance in 50 years were shown as Figures 117-a and 117-b. In addition to that SA at respectively 0.2 and 1 s considering epistemic uncertainty has been given as Figure 128a, 128b, 128c, and 128d for 2% and 10% probability of exceedence in 50 years respectively. PGA varies from 0.37 g in the south-eastern periphery to 0.30 g towards the northwest periphery, whereas southwest part of the district encounters PGA of 0.31 g (See Figure 117 a). Similarly, PGA corresponding to 475 years return period is about 0.12 g in the northwestern periphery and 0.15 g in the south-eastern periphery (Figure 1711 b). The reason for having maximum PGA value in the south-eastern periphery is due to the location of East Patna and West Patna Fault and PGA value of 0.35 g in south western part is due to the presence of earthquake events of magnitude moment more than 6. It has seen from the mean deaggregation plot that the motion for 6.0  $M_w$  at 40 km hypocentral distance, 6.0  $M_w$  at 15 km hypocentral distance and 6.0  $M_w$  at 25.25 km hypocentral distance is predominant in case of Cornel's, Areal and Frankel's approach respectively considering 2 % probability in 50 years. However, the motion for 5.5  $M_w$  at 50 km hypocentral distance,  $5.75 M_w$  at 20 km hypocentral distance and  $5.75 M_w$  at 30.3 km hypocentral distance respectively predominant in case of Cornel's, Areal and Frankel's approach. The PGA values varies from 0.08 to 0.43 g, 0.29 to 0.41 g and 0.26 to 0.36 g in case of Cornel's, Areal and Frankel's approach respectively considering 2 % probability in 50 years. Whereas it from 0.04 g to 0.18 g, 0.09 g to 0.16 g and 0.09 g to 0.16 g respectively considering 10 % probability of exceedence in 50 years in case of Cornel's, Areal and Frankel's approach. PGA value varies from 0.12 to 0.15 g for a return period of 2475 year which is comparable with PSHA map of India developed by Nath and Thingbaijam (2012). Recently, a major thrust faulting earthquake of magnitude 7.8 on 25 April 2015 occurred in Nepal which affected various

place in India including Patna district is one of them. We have completed our mapping before this earthquake and compared our results with shake map published by USGS (2015). It is noticed that PGA values for 10% probability of exceedence in 50 years is matches with USGS (2015) shake map on recent Nepal Earthquake.

In addition to that, uniform hazard response spectrum (UHRS) has been developed considering all the three approaches and compared with IS 1893 (2002). For developing UHRS, seismic hazard curves of spectral accelerations at different spectral period for the same probability of exceedence has been developed. The UHRS at 2 and 10 % probability of exceedence for 50 years at the centre of the district using classical and zoneless approach viz. Frankel's and areal approach has been drawn and given as Ffigure 139 a (marked as star in figure 117 a). Similarly, UHRS has been developed at the North-eastern part of Patna considering 2 and 10 % probability of exceedance, shown as Ffigure 139 b (marked as plus in figure 117 a). It has been seen from Figure 139 that the hazard value at 2 % probability is more for the same return period when compared to 10% probability of exceedence in 50 years. It has been also observed that spectral acceleration at zero period i.e. PGA is less in case of Cornell's approach when compared to Frankel's and Areal approach at the centre of the district where as it is more when compared to the North-eastern part of SSA. The developed UHRS has been compared with IS 1893 (2002) and it has been observed that the SA predicted is lower at the centre of the district at 2 and 10 % probability of exceedence in 50 years except for Frankel's approach. However, in case of North eastern parts of SSA, the predicted SA values are more as compared to IS 1893 (2002) (Figure 139 b). Hence, UHRS should be developed based on the regional characteristics so that it could be effectively used in infrastructural development of a district.

#### 10 Conclusion

A new seismic hazard map for Patna district was developed considering the earthquake events and seismic sources through logic tree approach. Based on past earthquake damage distribution, seismic study area of 500 km was arrived and the seismotectonic map was generated. The maximum magnitude has been estimated by considering weighted mean three methods, i.e. incremental method, Kijko method and regional rupture-based characteristic. From 27 applicable GMPEs, GMPEs ANBU-13, NDMA-10 and KANO-06 were selected upto 100 km epicentral distance, however ANBU-13, NDMA-10, BOAT-10 and KANO-06 up to 300 km and NDMA-10 for more than 300 km. These GMPEs were ranked and weights were found based on the Log-Likelihood method. A new hazard map for Patna district has been developed using both classical and zoneless approach considering different weight factor corresponds to b-value, maximum magnitude and GMPE to reduce the uncertainty values. The logic tree has been accounted to capture this epistemic uncertainty in the seismicity models. The final seismic hazard map corresponding to 2% and 10% probability of exceedence in 50 years has been developed by giving weight factor to the seismicity models, maximum magnitude and GMPEs. The PGA values varies from 0.08 to 0.43 g, 0.29 to 0.41 g and 0.26 to 0.36 g in case of Cornel's, Areal and Frankel's approach respectively considering 2 % probability in 50 years. Whereas it from 0.04 g to 0.18 g, 0.09 g to 0.16 g and 0.09 g to 0.16 g respectively considering 10 % probability of exceedence in 50 years in case of Cornel's, Areal and Frankel's approach. However, hazard values in terms of PGA at bed rock level after

considering logic tree varies from 0.30 to 0.37 g and 0.11 to 0.15 g respectively considering 2 and 10 % probability of exceedence in 50 years. In addition to that spectral acceleration hazard map has been developed at a period of 0.2 and 1 s corresponds to 2% and 10 % probability of exceedence in 50 years. Hence the logic tree should be used to reduce the epistemic uncertainty in determining the hazard value for any seismic study area. It has been also concluded that uniform hazard response spectra should be developed considering regional specific parameters.

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