RESPONSES TO COMMENTS

The authors thank the referees for their constructive and valuable comments. Point-by-point responses to the referee comments are as follows. Referee comments are in black, and the authors' responses are in blue. Note that line numbers in the authors' replies are associated with line numbers in the revised manuscript.

Referee 1.

1. In Abstract, there are no general findings from this study.

Response: As the referee's recommendation, we added the following sentences to the abstract (Page 1, Line 23~25):

"The results of this study show that loss amounts due to potential earthquakes are significantly less than those of the previous studies. The challenge of this study is to implement earthquake response spectrum and to reflect actual asset values of buildings of the metropolitan city of Seoul in Korea."

2. In Introduction, challenge of this study should be added. In Introduction, addition of literature review is required to emphasize the challenge of this study. Numerate past research outcomes and their limitations.

Response: As the referee's recommendation, we added the following sentences to the introduction (Page 2, Line 14~15):

"This study differs from the previous studies in that it implements the actual building and insurance data and the observed seismic characteristics of Korea."

3. The results from this study are much different from those from the previous reports written in the introduction. Please compare their results and explain the reasons of the difference.

Response: As the referee's recommendation, we added the following sentences to the result part (Page 10, Line 5~12):

"Nonetheless, the loss from the M_w 7.0 scale earthquake is only 4% compared to loss resulted from MPSS (2015). The main reasons of the difference in loss are as follows: (1) The duration of strong motion is applied as 0.6 seconds in the standard response spectrum in the previous studies; however, in this study, the duration of 0.2 seconds is implemented to reflect the characteristics of the recent earthquake occurred in the Korean peninsula; (2) The replacement costs of buildings are reflected in the analysis using statistics of the actual insured data, but the previous studies were used the replacement costs published in Square Foot Costs (RSMeans, 2002) in USA; and (3) This study did not consider indirect loss such as relocation expenses, income loss, and rental income loss."

4. (Page 2 Line 2 and thereafter) Indicate specific magnitude scale in the manuscript with brief explanation of physics. (example: Richter local magnitude...)

Response: As the referee's recommendation, we added the following sentences in Page 5, Line $9 \sim 12$:

"The Richter magnitude scale (M_L) is a unit based on logarithms calculated from the largest amplitude observed in the seismometer but it is difficult to measure the amplitude accurately. In this study, the moment magnitude scale (M_w) is used, which was suggested by the United States Geological Survey (USGS) to calculate and report magnitudes for large earthquakes."

5. (Page 2 Line 30) Do not use ambiguous expression in referencing figures and tables (replace "As shown in the above figure" with "As shown in Fig. 2")

Response: Modification are made as the referee's recommendation. (Page 2, Line 30)

6. (Page3 Line 6) Replace "36 the structure types" with "36 structure types"; Classification of structure types, occupancies, and seismic codes are not clearly explained.

Response: As the referee's comment, we added the following sentences in Page 3, Line 6~9:

"The extracted data are classified into 36 structure types and 33 occupancies as same as the building type of HAZUS-MH, and divided into 3 seismic codes estimated based on comprehensive consideration of the construction year, total building area and occupancy. The details of classifications of 36 structure types and 33 occupancies are showed in Tables 1 and 2, respectively."

7. (Table 3) In addition to Distribution, add frequencies corresponding to each distribution.

Response: As the referee's recommendation, we revised Table 3. And in the text (Page 2 Line 16 and Page 4 Line 7), there exists a typo; therefore, the number of buildings is revised to 6.3 million from 630,000 (the number in the previous manuscript).

8. (Table 2) There are three formulas in Table 2. It is necessary to either provide the other two formulas or erase contents of formulas I and II.

Response: Regarding the reviewer's comment, the following are added for more clear understanding (in Page 5, Line 21~25) and the Table 2 was removed.

"The attenuation equation (or formula) of Eq. (1) proposed by MPSS (2012) is used in this study. The attenuation formula of MPSS requires four coefficients (or fitting parameters). In this study, the four coefficients in Eq. (1) of $C_0 = 5.0244$, $C_1 = 0.5442$, $C_2 = -1.0020$, and $C_3 = 0$ are assumed in the analysis as the combination of the coefficients resulted in least error in prediction of maximum ground acceleration."

9. (Page 4 Line 7) Indicate the reference time of building statistics of 630,000

Response: As the referee's recommendation, we added the following sentences in Page 4, Line 7: "Seoul city as of 2016 database of building registration records"

10. (Page 4 Line 16) Replace "each building" with "each building damaged by earthquake." Reference is required for information provided by Korea Appraisal Board.

Response: As the referee's recommendation, we revised the sentences in Page 4 Line 16, and added a reference in Page 4 Line 17. (Korea Appraisal Board (KAB): Construction Cost Table, 2016. (in Korean))

11. (Page 4 Line 27) "Korea has been" should be "Korea has been considered as." Replace "neighboring countries" with "neighboring countries, such as Japan, China, and Taiwan." **Response:** As the referee's recommendation, we revised the sentences in Page 4 Line 27~28.

12. Abbreviation should be spelled out at its first appearance. "PGA" should be "Peak Ground Acceleration (PGA).

Response: As the referee's recommendation, we revised the sentences in Page 5 Line 15.

13. [Eq. (1)] To use minimum number of symbols, replace symbol S with PGA in Eq. (1). **Response:** As the referee's recommendation, we revised the sentences in Page 5 Line 23.

14. (Page 6 Line 23) "as shown table 3" should be "as shown in Table 3"**Response:** As the referee's recommendation, we revised the sentences in Page 6 Line 23.

15. (Page 7 Line 7) "zones: Zone I which includes Seoul area and Zone II" **Response:** As the referee's recommendation, we revised the sentences in Page 7 Line 7.

16. (Page 7 Line 33) "four 5 states;" should be "four 5 states:"**Response:** As the referee's recommendation, we revised the sentences in Page 7 Line 33.

17. (Page 8 Line 3) Subscription is required for "Sd" and symbols in Eq. (3)**Response:** As the referee's recommendation, we revised the sentences in Page 8 Line 3.

18. (Page 8 Line 8) "is median value" should be "is the median value"**Response:** As the referee's recommendation, we revised the sentences in Page 8 Line 8.

19. (Page 8 Line 26) "Table 5 and 6" should be "Tables 5 and 6"**Response:** As the referee's recommendation, we revised the sentences in Page 8 Line 26.

20. (Page 8 Line 30) "isn't" should be "is not" **Response:** As the referee's recommendation, we revised the sentences in Page 8 Line 30.

21. (Page 9 Line 1) "higher" should be "larger"**Response:** As the referee's recommendation, we revised the sentences in Page 9 Line 1.

22. (Page 9 Line 2) "like" should be "such as"

Response: As the referee's recommendation, we revised the sentences in Page 9 Line 2.

23. (Page 9 Line 1) Unified expression of dash use: "low-rise" and "low rise" are mixed. **Response:** As the referee's recommendation, we revised the sentences in Page 9 Line 1.

24. [Eq. (4)] There are mis fonts in subscription in Symbols in Eq. (4). **Response:** As the referee's recommendation, we revised the Eq. (4) in Page 9 Line 27.

25. (Page 10 Line 4) "% 15" should be "15%"**Response:** As the referee's recommendation, we revised the sentences in Page 10 Line 4.

26. (Tables 6, 7, and 8) "Km" should be "km"

Response: As the referee's recommendation, we revised the sentences in Tables 6, 7 and 8.

Referee 2.

1. The amount of damage predicted in the first and second revised manuscript is very different. Authors have to explain why the loss amount predicted in original manuscript was revised. **Response:** In this study, we estimated loss amounts based on the KRW. An error occurred converting the estimated loss amount to USD. That is why the loss amount has been revised.

2. The description of the methodology used isn't clear enough. It needs to be explained more clearly.

Response: As the referee's recommendation, we revised the sentences to understand clearly in Page 2 Line 30~31, Page 3 Line 16, Line 25~26, Line 31~32.

"(STEP 1) Information database of property which may be exposed to disaster should be constructed.

(STEP 2) Hazard module for generation of a physical hazard map from a simulated event of disaster should be developed.

(STEP 3) Vulnerability module to assess damage state of individual properties should be prepared by combining the information of exposed property and hazard intensity.

(STEP 4) The financial module is implemented to quantify the damage of individual buildings into a monetary loss to predict a total loss amount."

3. A few words used in this paper seem to be misleading in the interpretation, so it is necessary to replace them with words that cannot be interpreted in error. **Response:** As the referee's recommendation, we revised some misleading words

(Page 4, Line 6) Replace "etc. affecting" with "and other minor considerations. Influencing"

(Page 4 Line 18) Replace "900 billion dollars" with "900 billion US dollars"

(Page 4 Line 19) Replace "between USD 100,000 to 1,000,000" with "0.1~1 million US dollars."

Thank you for your valuable and constructive comments. The authors appreciate it.

Loss assessment of building and content damages from potential 2 earthquake risk in Seoul, Korea

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12 Abstract. After the 2016 Gyeongju earthquake and the 2017 Pohang earthquake struck the Korean peninsula, securing 13 financial stability for earthquake risk has become an important issue in Korea. Many domestic researchers are currently studying potential earthquake risk. However, empirical analysis and statistical approach are ambiguous in the case of Korea 14 15 because no major earthquake has ever occurred on the Korean peninsula since Korean Meteorological Agency started 16 monitoring earthquakes in 1978. This study focuses on evaluating possible losses due to earthquake risk in Seoul, the capital 17 of Korea, by using catastrophe model methodology integrated with GIS (Geographic Information System). The building 18 information such as structure and location is taken from the building registration database and the replacement cost for building 19 is obtained from insurance information. As the seismic design code in KBC (Korea Building Code) is similar to the seismic 20 design code of UBC (Uniform Building Code), the damage functions provided by HAZUS-MH are used to assess the damage 21 state of each building in event of an earthquake. 12 earthquake scenarios are evaluated considering the distribution and 22 characteristics of active fault zones in the Korean peninsula, and damages with loss amounts are calculated for each of the 23 scenarios. The results of this study show that loss amounts due to potential earthquakes are significantly less than those of the previous studies. Thise challenge of this study is to implement is why the earthquake response spectrum and to reflect actual 24 asset value of each-buildings of the metropolitan city of Seoul are reflected as actual data fromin Korea. 25

26 1 Introduction

On November 15, 2017, an earthquake of M 5.4 on Richter scale hit the northern region near Pohang city located in southeastern part of the Korean peninsula. After 5.8 Gyeongju earthquake in 2016, it was the second strongest recorded earthquake in Korea since the monitoring began in 1978 (Fig. 1).

30

31 (Figure 1 is about here)

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- 2 The earthquakes occurred in Gyeongju and Pohang are expected to be caused by Yangsan fault zone which is classified as 3 active fault on the Korean Peninsula, which has the ability to generate a maximum of 7.0 M earthquake according to Kyung (2010) and MPSS (2012). If earthquake of M 6.0, close to the Gyeongju and Pohang earthquakes, occurs in or near Seoul, 4 5 where major industrial and commercial facilities are concentrated, huge loss that has never been experienced in the past might 6 occur. Especially, disaster risk financing industry such as the insurance can subject to catastrophic damage. According to the 7 Natural Disaster Reduction Project report prepared at the request of the MPSS (2015), 2.76 million people may lose their life 8 and 2,848 billion US dollars of economic loss including indirect loss such as business interruption may occur if an earthquake 9 of M 7.0 strikes Seoul (Note that the losses in US dollars in this study is converted from the original Korean currency based on the exchange rate of $1 \text{ USD} \approx 1,200 \text{ KRW}$, as of January 1, 2016). -However, as this report relies on the HAZUS-MH for 10
- 11 most of the analysis data such as replacement cost of property and seismic characteristics of earthquake, the estimated result
- 12 may differ from actual damage loss amount in Korea.
- 13 This study uses catastrophe model methodology to predict loss and damage of buildings and contents from the potential
- 14 earthquake that can occur in Seoul. This study differs from the previous studies in that it implements the applies the actual
- 15 <u>building and insurance data and the observed seismic characteristics inof Korea.</u> The detailed information of approximate
- 16 <u>630,000</u>6.3 million buildings across Seoul is acquired through the building registration database. The replacement cost of each
- 17 building and contents are statistically estimated by using insurance database which is classified by occupancy to meet the
- 18 reality of Korea.

19 2 Methodology

- 20 Predicting loss amount of potential disaster using catastrophe model differs from the actuarial approach model. While the
- 21 actuarial technique estimates the loss based on empirical data, the catastrophe model generates disaster scenarios based on
 22 scientific understanding of disasters and assesses the loss amount from event scenario. For possible quakes in Korea, it is
- 23 appropriate to use the catastrophe model for predicting losses because empirical data from earthquakes on the Korean peninsula
- 24 is too scarce to enable actuarial processing.
- 25 The definition and procedure of catastrophe model can marginally differ between researchers or suppliers but the conventional
- 26 procedure can be illustrated as Fig. 2.
- 27
- 28 (Figure 2 is about here)
- 29
- 30 As shown in Fig. 2, As shown in the above figure, the catastrophe model has a four step process. (STEP 1) Information
- 31 database of property which may be exposed to disaster should be constructed. The first step is to build information database of
- 32 property which may be exposed to disaster. However the exposure data sets in previous studies is typically available at

relatively coarse resolutions because it is accompanied by difficulties related to limited resources or privacy issues, among 1 2 others (Dell'Acqua et al., 2012, Figueiredo and Martina, 2016). In order to overcome these limitations, this study used the 3 building registration database of Korea to build exposure data set. The detail information of the building must be recorded, 4 which is registered in the building registration database whenever the building is constructed or reconstructed according to the 5 Building Act in Korea. In this study, the detail information needed to evaluate the vulnerability of all buildings in Seoul was 6 extracted from the building registration database. The extracted data are classified into 36 structure types and 33 occupancies 7 as same as the building type of HAZUS-MH, and divided into 3 seismic codes estimated based on comprehensive consideration of the construction year, total building area and occupancy. The details of classifications of 36 structure types and 33 8 9 occupancies are showed in Table 1 and 2, respectively The extracted data are classified into 36 the structure types, 33 10 occupancies and divided into 3 seismic codes estimated based on comprehensive consideration of the construction year, total 11 building area and occupancy. 12

- 13 (Table 1 is about here)
- 14 (Table 2 is about here)
- 15

16 (STEP 2) Hazard module for generation of a physical hazard map from a simulated event of disaster should be developed. The second step, called hazard module, generates a physical hazard map from a simulated event of disaster. For example, the peak 17 18 ground acceleration can be represented as hazard intensity in an earthquake hazard map. The seismic events are usually 19 generated by stochastic methodologies such as Monte Carlo simulation. However, it has not been less than 40 years since the 20 earthquake began to be monitored on the Korean Peninsula, and there was no large-scale earthquake in Seoul during the 21 monitoring period. In this study, synthetic earthquakes were generated considering the activity of the active faults passing 22 through Seoul, the seismic hazard map was prepared by selecting the attenuation relation that most closely resembles the 23 Gyeongju earthquake and the Pohang earthquake among a lot of attenuation relations proposed by many domestic and abroad 24 researchers.

25 (STEP 3) Vulnerability module to assess damage state of individual properties should be prepared by combining the 26 information of exposed property and hazard intensity. The third step is to prepare vulnerability module to assess damage state 27 of individual properties by combining the information of exposed property and hazard intensity. The probabilities of each 28 damage states of the building should be estimated from spectral displacement of building due to seismic impact in the 29 vulnerability module. The spectral displacement is determined by performance point, which is the intersection of the demand 30 curve and the capacity spectrum.

- 31 (STEP 4) The financial module is implemented to quantify the damage of individual buildings into a monetary loss to predict
- 32 <u>a total loss amount. The final step, the financial module, is to quantify the damage of individual buildings into a monetary loss</u>
- 33 to predict a total loss amount. In order to estimate the repair cost of a building due to a seismic impact, it is necessary to
- 34 ascertain the replacement value or the current asset of the building calculated in cost mode. In this study, the values of building,

1 contents and inventories of representative building in each categories were estimated by statistical processing of appraisal data

- 2 for insuring property.
- 3

4 3 Construction of exposure information

The detailed information of each building such as location, structure, size, floor area, construction year, occupancy and other 5 6 minor considerations influencing, etc. affecting the seismic response is obtained from computerized database of building 7 registration records. There are presently about 630,000 buildings within Seoul city as of 2016 database of building registration 8 records. There are presently 6.3 million buildings within Seoul city. These buildings are classified as residential (76% of the 9 total number of buildings), commercial (20.3%), industrial (0.5%) and others (3.2%) that includes government and education 10 institute buildings. Residential are predominantly dominated by masonry structure of less than five stories, and concrete structures are dominant in commercial. 82% of the buildings in Seoul were built before 1988 when seismic code of building 11 12 began to be considered. Table 13 summarizes the statistical characteristics of buildings in Seoul.

13

14 (Table $\frac{13}{2}$ is about here)

15

The replacement costs for each building <u>damaged by earthquake</u> and content are estimated based on statistical processing of 17 1,500 records of asset evaluation data for property insurances and e<u>C</u>onstruction e<u>C</u>ost <u>t</u><u>T</u>able (KAB, 2016). issued by Korea 18 Appraisal Board. On processing, the total replacement cost of buildings and contents is estimated to be about 900 billion <u>US</u> 19 dollars in Seoul and approximately 72% of buildings in Seoul were estimated to have replacement cost <u>0.1~1 million US</u> 20 <u>dollars</u><u>between USD 100,000 to 1,000,000</u>. The indirect costs and losses attributed to land and intangible assets and business 21 interruption are not considered in this study.

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25 4 Hazard Assessment

26 4.1 Scenario selection

In the Circum-Pacific seismic zone, Korea has been <u>considered as</u> safer and less prone to quakes as compared with its neighboring countries <u>such as Japan, China, and Taiwan.</u> However, many domestic researchers insist that there are two

- 29 representative active faults in Korea. One of these, the Yangsan Fault, caused the Gyeongju earthquake. The second fault,
 - 4

1 Chugaryeong Fault is centrally located on the Korean peninsula (Choi et al., 2012; MPSS, 2012; Chung et al., 2014).

- 2 Chugaryeong Fault crosses the eastern side of Seoul and is believed to have caused 2010 earthquake, of M 3.0, in Seoul.
- 3
- 4 (Figure 3 is about here)
- 5
- The Chugaryeong Fault has similar activity to Yangsan Fault which has the capacity to cause an earthquake of M 7.0, also
 most earthquakes in Korea occur or are likely to occur at focal depth of about 10 km (Lee, 2010; MPSS, 2012). Based on this,
- 8 earthquakes of M 4.0 to 7.0 occurring at focal depths of 10 to 20 km at the southeast of Seoul due to activity of the Chugaryeong
- 9 Fault are selected as event scenarios of this study. The Richter magnitude scale (M_L) is a unit based on logarithms calculated
- 10 from the largest amplitude observed in the seismometer but it is difficult to measure the amplitude accurately. In this study,
- 11 the moment magnitude scale (M_w) is used, which itwas <u>used</u> suggested by the United States Geological Survey (USGS) to
- 12 calculate and report magnitudes for all modern large earthquakes is used.

13 4.2 Construction of hazard map and response spectrum

- 14 To construct each hazard map from each earthquake event scenario, it is important to understand the attenuation relationship
- 15 of ground motions from epi-central distance. The ground motion can be characterized by peak ground acceleration (PGA) and
- 16 spectral response based on a response spectrum shape.
- 17 A lot of experimental attenuation formulas for estimating PGA have been developed by means of regression analysis (Atkinson and Boore, 1997; Toro et al., 1997; Atkinson and Silva, 2000; Lee and Kim, 2002; MPSS; 2012). However, in choosing the 18 19 attenuation formula, a careful approach is needed since the effect of the formula is very large on estimating amount of 20 earthquake loss. MPSS (2012) proposed three attenuation formulas for Korean Peninsula, which are expressed with the equation as following Eq. (1)_{5.} and the values of the coefficients of C_{0_2} C_{1_2} C_{2_2} and C_{2_2} are shown in table 2. The attenuation 21 equation (or formula) of Eq. (1) proposed by MPSS (2012) is used in this study. The attenuation formula of MPSS requires 22 23 four coefficients (or fitting parameters). In this study, the four coefficients in Eq. (1) of $C_0 = 5.0244$, $C_1 = 0.5442$, $C_2 = -1.0020$, 24 and $C_3 = 0$ are assumed in the analysis as the combination of the coefficients resulted in least error in prediction of maximum 25 ground acceleration.
- 26
- 27 In $S = C_0 + C_1 M + C_2 ln R + C_3 R$,
- 28

(1)

- 31 (Table 2 is about here)
- 32

Where, *S* is Peak Ground Acceleration (PGA), M_w is moment magnitude magnitude of earthquake and R is epi-central distance.

The influence of the seismic attenuation equation on the seismic hazard map is very large, but the reliability of the attenuation equations presented so far remains controversial. In this study, we tried to utilize the results of domestic studies reflecting the seismic characteristics in Korea, and the <u>attenuation equation of Formula IIIEq. (1)</u>, which is considered to be the most conservative formula because the attenuation of seismic wave is the least of the formulas proposed by MPSS (2012), is chosen for building the earthquake hazard map from the event scenario. The hazard maps according to the each scenario are shown in Fig. 4. PGA in Seoul ranges from 0.06g to 0.7g in these scenarios which earthquakes of M_w 4.0 to 7.0 occurred at focal depths of 10 to 20 km.

9 (Fig. 4 is about here)

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8

The severity of vibratory response of building to earthquake impact depends on relationship between the characteristics of 11 12 ground motion described as response spectrum (which has a different shape according to ground conditions) and structural 13 characteristics of building. But since the design response spectrum currently used in Korea is based on the high seismicity 14 region like California, a lot of domestic researchers insist that the spectrum is different from characteristics of the earthquake 15 on the Korean peninsula (Kim et al., 1998; Han, 2003; Hwang et al., 2015; Lee and Ju, 2017). In general, the ground condition of Korea including Seoul is characterized by shallow bedrock, and the earthquakes occurred in Korea have a characteristic that 16 17 the duration of strong motion is shorter than one in high seismicity region. In the case of the Gyeongju earthquake, the strong 18 motion with short duration of 0.1~0.2 second was also observed. As shown in Fig. 5, shape of the standard response spectrum 19 is described by four transition points. S is Peak Ground Acceleration (PGA) and aA is the amplification factor at the short-20 period. Heo et al.(2018) calculated the shapes and transition periods of the response spectrums through regression analysis of 21 the accelerations and spectral displacements of the Gyeongju and the Pohang earthquakes and found that the standard response 22 spectrum which had been used previously for seismic design in Korea was overly conservative in long period part. The factor 23 adapted the spectrum in this study are set as shown in t_a below after comparing the spectra of earthquakes in Gyeongju 24 and the Pohang.

25

26 (Fig. 5 is about here)

- 27 (Table 34 is about here)
- 28

29 5 Assessment of building vulnerability

30 5.1 The status of seismic design code in Korea

31 In 1988 when an earthquake occurred in Mexico, seismic design code in Korea were first mandated for building with six and

32 more stories or floor area of 100,000 m² or more, and then it was gradually expanded to be adapted seismic design code for all

- 1 buildings with three and more stories or floor area of more than 500 m² through the revision of KBC in 2015. Nevertheless,
- 2 93.2% of all buildings in Korea did not apply seismic code and have more vulnerable characteristics to earthquakes (SMG,
- 3 2012; Choi, 2016).

4 The seismic design codes in KBC were established based on the Uniform Building Code (UBC), the Applied Technology

- 5 Council (ATC) and the International Building Code (IBC) (SMG, 2012; Lee, 2015). While the seismic zone in UBC is divided
- 6 into six zones which have each regional factor defined as design peak ground acceleration (PGA), the zone in KBC is divided
- 7 into two zones;: zZone I which includes Seoul area and zZone II. The regional factor of zone I was 0.11 before 2009 but
- 8 strengthened to 0.22 after that, and the seismic design code of buildings built in Seoul before 2009 is similar to zone 2A of
- 9 UBC and the code of buildings built after 2009 is similar to zone 2B of UBC.
- 10
- 11 (Table 45 is about here)
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13 5.2. Application of damage function

As mentioned above, since seismic design code of Korea is similar to the UBC and the ATC code, the damage functions 14 proposed by HAZUS-MH can be applied to estimate building damage due to seismic impact. The damage function for each 15 building type in HAZUS-MH includes two types of damage curves; capacity curve and fragility curve. The capacity curve is 16 used to determine peak building response from the capacity spectrum method. This method is a schematic procedure for 17 18 comparing the capacity curve obtained by push-over analysis with the demand spectrum of ground motion on the Acceleration 19 Displacement Response Spectrum (ADRS). Thus response spectrum has to be converted to demand spectrum for representing 20 the relationship between spectral displacement and spectral acceleration. Eq. (2) proposed by HAZUS-MH can relate spectral acceleration with spectral displacement for given period value (FEMA, 2013). 21

22

24

25 Where, S_d is spectral displacement (inches), S_a is spectral acceleration (g) at a period (T, second)

26

The intersection of the capacity curve and the demand spectrum is a performance point which can evaluate the associated damage state for the structure and compare that damage state for different earthquakes (Fig. 6).

(2)

- 29
- 30 (Fig. 6 is about here)
- 31

32 The fragility curves estimate the probability of exceeding different damage states given peak building response represented as

- 33 spectral displacement or spectral acceleration at performance point. The damage state is divided into four states; Slight,
 - 7

1 Moderate, Extensive, and Complete. Each fragility curve is expressed as lognormal function defined by a median value of 2 peak building response, corresponding to the mean threshold of associated damage state by a logarithmic standard deviation 3 (β). The fragility curve for structural component of building uses spectral displacement (S_dd) as peak building response and 4 define the function of Eq. (3) and Fig. 7.

7

$$P[ds|S_d] = \Phi[\frac{1}{\beta_{ds}}\ln(\frac{S_d}{\bar{S}_{d,ds}})],\tag{3}$$

8 Where, $\Phi(\cdot)$ is the standard normal distribution function and $\bar{S}_{d,ds}$ is <u>the</u> median value of spectral displacement at which the 9 building reaches the threshold of damage state.

10

11 (Fig. 7 is about here)

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The non-structural components of the building are divided into drift-sensitive components and acceleration-sensitive components. In general, while architectural components such as interior or exterior wall are more drift-sensitive, the mechanical and electrical components of building are acceleration-sensitive. Therefore the functions of inter-story drift is used to estimate damage state of drift-sensitive components and function of floor acceleration is used to estimate the damage state of acceleration sensitive components or contents in the building.

The capacity curve and the fragility curve in the HAZUS-MH are classified into high-code, moderate-code, low-code and precode buildings as per seismic design codes (FEMA, 2013). When all buildings in Seoul are classified comparing seismic design code of the HAZUS-MH, it is estimated to approximately 91.7% pre-code, 5.4% low-code and 2.9% moderate-code

21 buildings.

22

23 5.3. Calculation of loss ratio

Using estimates, which include the structural and nonstructural repair costs caused by building damage and the associated loss 24 25 of building contents and business inventory, provided by HAZUS-MH, the probability of exceeding different damage state for the each component can convert to loss ratio of replacement cost for evaluation of direct economic loss. Tables 56 and 67 26 27 summarize the estimated mean loss ratio of building which includes structural and non-structural components, and contents 28 depending on occupancy and structure type. It is a common pattern that the majority of damage occur to low-rise residential 29 building made of masonry in the Korean Peninsula where the earthquake characterized by strong short-period component is 30 dominant. However this common pattern is notn't clearly shown in the result of this study, and there are two main reasons for 31 this.

The first reason can be found that although the number of low_-rise residential building made of masonry is much <u>largerhigher</u>, the total asset value is much lower than the high rise residential building made of reinforced concrete <u>such aslike</u> apartment, which is generally classified as luxury residence, while low_--rise masonry house is classified as low priced residence in Seoul. The second reason is that the non-structural elements such as mechanical and electrical components, which are more vulnerable to ground shaking than structural components, in the buildings made of concrete and steel structure have higher proportion than in masonry.

- 7 8
- (Table $\frac{56}{50}$ is about here)
- 9 (Table $\underline{67}$ is about here)
- 10

Fig. 8 is a map that shows the loss ratio of each building in the Gangnam district, located 3km away from epi-center with M_w 4.0~7.0 and focal depth 10km. According to the results, if an earthquake of M_w 4.0 strikes southeast part of Seoul, damage to the residential buildings of pre-code start to occur and an earthquake of M_w 5.0 can damage almost all buildings due to ground shaking. And if an earthquake of M_w 6.0 occurs, office buildings of low-code begin to be damaged by seismic impact, and an earthquake of M_w 7.0 is estimated to cause an average 14.8% and 14.9% of total replacement cost of all buildings and contents respectively in Seoul.

- 17
- 18 (Fig. 8 is about here)
- 19

20 6. Estimation of loss amount

The total loss amount for each scenario can be simulated by replacement cost, seismic intensity, damage function and other factors mentioned above. But since systematic data issues or biases across a portfolio can result in losses being consistently under- or over-simulated (LMA, 2017), the results need to be corrected by comparing empirical data. Linear Scaling Method (LSM), which is one of the common method to correct systematic errors, can be used to calibrate pre-simulated loss amount. LSM reflects the difference between pre-simulated results and observed results in the simulated results as shown by Eq. (4).

26

27
$$L_{cor,i,j} = L_{sim,i,j} + \left(\sum_{i=1}^{n} L_{obs,i,j} - \sum_{i=1}^{n} L_{obs,i,j} - \sum_{i=1}^{n} L_{sim,i,j} \right),$$
(4)

28

Where *i* is $M_{\underline{w}}$ of earthquake, *j* is focal depth. *Lcor, i, j* is the corrected loss, *Lobs, i, j* is the observed loss, and *Lsim, i, j* is the presimulated loss. There has never been an earthquake of $M_{\underline{w}}$ 4.0 or more in or near Seoul since earthquake monitoring began in

1978. Therefore, all pre-simulated results were inevitably corrected using empirical data of the earthquake of M_{w} 3.0 that 1 2 occurred near Seoul in 2010. The calibrated loss amounts for each scenario are summarized in Table 78. The total loss in the 3 case of an earthquake of $M_{\underline{w}}$ 4.0 is estimated at 2.2 billion <u>US</u> dollars. However, if the $M_{\underline{w}}$ of the earthquake increase to 7, the 4 total loss is estimated to increase 58 times of M_w 4.0, reaching 126.6 billion US dollars which is close to $\frac{9-15\%}{2}$ of total replacement cost for all buildings in Seoul. Nonetheless, the loss from the Mw 7.0 earthquake is only 4% compared to loss 5 6 resulted from MPSS (2015). The main reasons of the difference in loss are as follows: (1) The duration of strong motion is 7 applied as 0.6 secondsecond in the standard response spectrum in previous study; however, in this study, the duration of 0.2seconds is implemented to reflect econd reflected the characteristics of the recent earthquake occurred ieharacteristics in the 8 9 Korean peninsula; is applied in this study. (2) The replacement costs of each-buildings are is-reflected in the analysis using applied statisticsally of to the actual insured data, but the previous studies were used the applied the replacement cost published 10 in Square Foot Costs (RSMeans, 2002) in USA; -(3) This study did noton't consider indirect loss such as relocation expenses, 11 income loss, and rental income loss et al. 12

13

14 (Table $78 \div$ is about here)

15 7. Conclusion

16 The existence of active fault zones on the Korean peninsula and recent quakes that affected Gyeongju and Pohang cities have 17 made experts question whether current overall practices would still be adequate if a similar quake occurs in Seoul. And the 18 concentration of major industrial and commercial facilities carries a significant inherent risk to cause catastrophic loss of life 19 and economy and significant administrative challenge for disaster management in Korea. The disaster management is divided 20 into four phases; 1) mitigation, 2) preparedness, 3) response and 4) recovery. At each phase which has particular needs and 21 problems, different strategy and support are required to force social resilience against each natural disaster. And it is also 22 important that the activities at each phase generate virtuous cycle and assist in making each other to be stronger. 23 The development of insurance industry can be a good example to explain virtuous cycle in disaster management. The insurance 24 industry as disaster risk financing commonly plays a major role to secure financial stability for smooth recovery from natural

- disaster. However, it also helps these activities to perform more effective during the other phases such as mitigation, preparedness and response. The Sichuan earthquake of 2008 is in stark contrast with New Zealand earthquake of 2010 in terms of disaster management efficiency due to limited insurance penetration. The Sichuan earthquake of M 8.0 that occurred in China, where insurance penetration is relatively low, caused approximately 70,000 deaths, more than 370,000 injuries, and 127 billion <u>US</u> dollars of economic loss. However, the insured loss was under 3% of the economic loss. On the other hand, the
- 30 earthquake of M 7.1 that occurred in New Zealand, where insurance penetration is very high, caused only 2 injuries and 2.7
- 31 billion <u>US</u> dollars of economic loss, which is more than 50% of economic loss that was covered from various insurance
- 32 programs such as direct insurance, reinsurance and international financing market (WEF, 2011).

Most domestic insurers believe that it is impossible to predict loss amount from potential earthquake and it is difficult to 1 2 quantify the earthquake risk in Korea. This belief of insurers is a major obstacle to development of the earthquake insurance 3 programs. However, as mentioned above, various studies required for the catastrophe model methodology have been either 4 completed or in progress by various domestic researchers and a lot of database related to potential earthquake risk in Korea is 5 being accumulated. Compared to other studies, this study is differ in that real insurance information and building registration 6 database are used to predict loss amount from potential earthquake. It not only helps advance the prediction process but also 7 serves insurer to better understand and estimate the earthquake risk. This study shows that risk due to potential quakes in Korea 8 is significant and insurance industry can support more detailed studies for better understanding of insurance risk and expanding 9 scope of current insurance practices for earthquake risks. Because of this, Insurance companies have an opportunity to further 10 explore currently under tapped areas of business in property insurance.

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- 8

9

2 TABLE

1

3 4 <u>Table 1: Model building types</u>

			Height				
<u>No.</u>	Label	Description	Range		<u>Typical</u>		
		-	Name	Stories	Stories	Feet	
<u>1</u>	<u>W1</u>	<u>Wood, Light Frame (≤5,000 sq. ft.)</u>		<u>1 - 2</u>	<u>1</u>	<u>14</u>	
<u>2</u>	<u>W2</u>	Wood, Commercial and Industrial (> 5,000 sq. ft.)		All	<u>2</u>	<u>24</u>	
3	S1L	Steel Moment Frame	Low-Rise	<u>1 - 3</u>	<u>2</u>	24	
4	S1M		Mid-Rise	<u>4 - 7</u>	<u>5</u>	60	
5	S1H		High-Rise	<u>8+</u>	<u>13</u>	156	
6	S2L	Steel Braced Frame	Low-Rise	<u>1 - 3</u>	<u>2</u>	24	
7	S2M		Mid-Rise	<u>4 - 7</u>	<u>5</u>	60	
<u>8</u>	<u>S2H</u>		High-Rise	<u>8+</u>	<u>13</u>	156	
9	<u>S3</u>	Steel Light Frame		<u>A11</u>	<u>1</u>	15	
10	S4L	Steel Frame with Cast-in Place Concrete Shear Walls	Low-Rise	1 - 3	2	24	
11	S4M		Mid-Rise	4 - 7	<u>5</u>	60	
12	S4H		High-Rise	<u>8+</u>	<u>13</u>	156	
13	S5L	Steel Frame with Unreinforced Masonry Infill Walls	Low-Rise	<u>1 - 3</u>	<u>2</u>	24	
14	S5M		Mid-Rise	<u>4 - 7</u>	<u>5</u>	60	
15	S5H		High-Rise	<u>8+</u>	<u>13</u>	156	
16	C1L	Concrete Moment Frame	Low-Rise	<u>1 - 3</u>	2	20	
17	C1M		Mid-Rise	<u>4 - 7</u>	<u>5</u>	50	
18	C1H		High-Rise	<u>8+</u>	<u>12</u>	120	
19	C2L	Concrete Shear Walls	Low-Rise	<u>1 - 3</u>	<u>2</u>	20	
20	C2M		Mid-Rise	<u>4 - 7</u>	<u>5</u>	50	
21	C2H		High-Rise	<u>8+</u>	<u>12</u>	120	
22	C3L	Concrete Frame with Unreinforced Masonry Infill	Low-Rise	<u>1 - 3</u>	<u>2</u>	20	
23	C3M	Walls	Mid-Rise	<u>4 - 7</u>	<u>5</u>	50	
24	СЗН		High-Rise	<u>8+</u>	<u>12</u>	120	
25	PC1	Precast Concrete Tilt-Up Walls		<u>A11</u>	<u>1</u>	15	
26	PC2L	Precast Concrete Frames with Concrete Shear Walls	Low-Rise	<u>1 - 3</u>	<u>2</u>	20	
27	PC2M		Mid-Rise	<u>4 - 7</u>	<u>5</u>	50	
28	PC2H		High-Rise	<u>8+</u>	<u>12</u>	120	
29	RM1L	Reinforced Masonry Bearing Walls with Wood or	Low-Rise	<u>1 - 3</u>	<u>2</u>	20	
30	RM1M	Metal Deck Diaphragms	Mid-Rise	4+	<u>5</u>	50	
31	RM2L	Reinforced Masonry Bearing Walls with Precast	Low-Rise	<u>1 - 3</u>	<u>2</u>	20	
32	RM2M	Concrete Diaphragms	Mid-Rise	<u>4 - 7</u>	<u>5</u>	50	
33	RM2H		High-Rise	<u>8+</u>	<u>12</u>	120	
34	URML	Unreinforced Masonry Bearing Walls	Low-Rise	<u>1 - 2</u>	<u>1</u>	15	
35	URMM		Mid-Rise	<u>3+</u>	<u>3</u>	35	
36	MH	Mobile Homes		<u>A11</u>	<u>1</u>	10	
		2012					

5 Source: FEMA (2013)

No.	Label	Occupancy Class	Description
		Residential	
1	RES1	Single Family Dwelling	Detached House
2	RES2	Mobile Home	Mobile Home
3-8	RES3a-f	Multi Family Dwelling	Apartment/Condominium
94	RES4	Temporary Lodging	Hotel/Motel
105	RES5	Institutional Dormitory	Group Housing(military, college), Jails
<u>116</u>	RES6	Nursing Home	
7		Commercial	
<u>812</u>	<u>COM1</u>	Retail Trade	Store
<u>139</u>	COM2	Wholesale Trade	Warehouse
<u>140</u>	<u>COM3</u>	Personal and Repair Services	Service Station/Shop
<u>15</u>	<u>COM4</u>	Professional/Technical/Business Services	Offices
<u>16</u> 2	<u>COM5</u>	Banks/Financial Institutions	
<u>173</u>	<u>COM6</u>	<u>Hospital</u>	
<u>18</u> 4	<u>COM7</u>	Medical Office/Clinic	Offices
<u>195</u>	<u>COM8</u>	Entertainment & Recreation	Restaurants/Bars
<u>2016</u>	<u>COM9</u>	Theaters	Theaters
<u>2117</u>	<u>COM10</u>	Parking	Garages
<u>18</u>		<u>Industrial</u>	
<u>22</u>	<u>IND1</u>	Heavy	<u>Factory</u>
<u>23</u>	IND2	<u>Light</u>	<u>Factory</u>
<u>24</u>	IND3	Food/Drugs/Chemicals	Factory
<u>25</u>	IND4	Metals/Minerals Processing	Factory
<u>26</u>	IND5	High Technology	Factory
<u>27</u>	IND6	Construction	Office
25		<u>Agriculture</u>	
26 28	AGR1	Agriculture	
27		Religion/Non-Profit	
<u>289</u>	<u>REL1</u>	Church/Membership Organization	
		<u>Government</u>	
<u>30</u>	GOV1	General Services	Office
<u>31</u>	GOV2	Emergency Response	Police/Fire Station
		Education	
<u>32</u>	EDU1	Schools/Libraries	
<u>33</u>	EDU2	Colleges/Universities	Does not include group housing
35			
36			
Sources	EENA (201	(2)	

<u>Source: FEMA (2013)</u>

2 3

Table 13: A summary of the statistical characteristics of buildings in Seoul.

Classification	Frequencies	Distribution (%)
Occupancy		
Residential	478,000	76.0
Commercial	127,676	20.3
Industrial	<u>3,145</u>	0.5
Others	<u>20,126</u>	3.2
Structure		
Masonry	<u>310,071</u>	49.3
Reinforced Concrete	273,592	43.5
Steel	<u>1,258</u>	0.2
Wood	<u>33,334</u>	5.3
Others	10,692	1.7
Floor area (100m ²)		
~ 1	<u>129,563</u>	20.6
1~2	<u>144,658</u>	23.0
2~3	<u>102,518</u>	16.3
3 ~ 5	100,003	15.9
5~10	<u>86,795</u>	13.9
10 ~ 30	35,850	5.7
30 ~	<u>29,561</u>	4.7
Number of Floors		
1	<u>127,676</u>	20.3
2~5	<u>456,616</u>	72.1
6 ~ 10	<u>26,416</u>	4.2
11~20	<u>14,466</u>	2.3
21 ~ 30	<u>3,145</u>	0.5
31 ~	<u>629</u>	0.1

1 Table 2: Coefficient Value of Each Formula.

Formula		Coeff		Standard	
i ormuta	C_{θ}	C_{4}	C_2	C ₃	Deviation
Formula I	0.4853	1.2	-0.8416	-0.0061	0.8036
Formula II	0.5577	1.2	- 0.8587	- 0.0062	0.7629
Formula III	5.02 44	0.5442	-1.0020	0.0	0.1000

2 Source: MPSS (2012)

Table 34: Factors of standard response spectrum in this study.

	Amplification factor	Tra	Transition Period (sec)		
	at short periods (α_A)	T ₀	Ts	T_L	
Gyeongju Earthquake	2.85	0.054	0.22	1.5	
Pohang Earthquake	3.15	0.07	0.195	4.475	
This study	2.8	0.06	0.2	3	

1 Table 4<u>5</u>: Alteration of seismic design code in Korea.

Classification		Seismic design code								
		1988 ~ 2000	2005 ~ 2009	2009 ~						
Deference basis		UBC85	UBC85	IBC2000	IBC2000					
Referen		ATC3-06	ATC3-06	IDC2000	IDC2000					
		Gwangju-si / Gangwon-do / Jeollabuk-	-							
	Zone I	do / Gochang-gun / Jeollanam-do /	All area except zone II							
Regional		Uljin-gun / Jeju-do								
factor		0.12	0.11	0.11	0.22					
	Zone II	All area except zone I	North Gangwon-do /	/ Jellanam-do/ So	uthwest/Jeju-do					
		0.08	0.07	0.07	0.14					
Seismic design object		Building (>6 stories), Total floo								
			Building (2	>3 stories)						
		Floor area (>10,000m ² sales facility), Asser	Total floor	(>1,000m²)						
		General hospital (>1,000m ²), Power plant	, Public service facility							

1 Table 56: Estimated mean loss ratio of building based on occupancy type.

	Focal	Resid	lential	Comn	nercial	Indu	strial	Oth	iers
М	Depth (<u>km</u> Km)	Building	Contents	Building	Contents	Building	Contents	Building	Contents
	10	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
4	15	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	20	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	10	1.7%	1.0%	1.9%	1.0%	1.0%	1.0%	1.0%	1.0%
5	15	0.7%	0.0%	0.9%	0.0%	0.0%	0.0%	0.0%	0.0%
	20	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	10	6.2%	4.0%	6.7%	4.9%	4.0%	4.0%	5.0%	3.9%
6	15	3.5%	2.0%	3.8%	2.1%	3.0%	2.0%	2.9%	1.9%
	20	1.7%	1.0%	1.9%	1.0%	1.0%	1.0%	1.9%	1.0%
	10	17.0%	13.7%	18.4%	14.4%	13.0%	12.0%	17.0%	13.6%
7	15	11.2%	8.7%	12.1%	9.0%	9.0%	8.0%	10.6%	8.7%
	20	7.5%	5.7%	7.7%	5.9%	6.0%	5.0%	6.8%	5.8%

1 Table 67: Estimated mean loss ratio of building based on structure type.

	Focal	Mas	onry	Con	crete	St	eel	Wo	ood	Oth	iers
М	Depth (<u>km</u> K m)	Building	Contents								
	10	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
4	15	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
-	20	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	10	2.0%	1.0%	1.0%	1.0%	1.0%	1.0%	1.0%	1.0%	1.0%	0.0%
5	15	1.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
-	20	0.1%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	10	7.0%	4.0%	6.0%	5.0%	5.0%	5.2%	4.0%	4.0%	5.0%	2.0%
6	15	4.0%	2.0%	3.0%	2.0%	2.1%	2.2%	3.0%	2.0%	3.0%	1.0%
-	20	3.0%	1.0%	1.0%	1.0%	1.0%	1.0%	2.0%	1.0%	2.0%	0.0%
	10	18.0%	13.0%	19.0%	15.0%	16.9%	14.8%	13.0%	14.0%	16.0%	8.0%
7	15	12.0%	8.0%	12.0%	10.0%	10.1%	9.2%	9.0%	9.0%	10.0%	5.0%
	20	8.1%	5.0%	7.0%	6.0%	6.1%	6.0%	6.0%	6.0%	7.0%	3.0%

1 Table 78: Aggregated loss amount due to each scenario.

M	Focal Depth	Aggr	USD)	
IVI	(<u>km</u> Km)	Building	Contents	Total
	10	1,789	384	2,173
4	15	583	110	694
-	20	58	0	58
	10	8,879	2,430	11,309
5	15	4,330	1,089	5,419
-	20	2,243	500	2,744
	10	32,955	9,558	42,512
6	15	17,974	5,234	23,208
-	20	10,749	3,091	13,840
	10	98,927	27,668	126,594
7	15	61,120	17,861	78,980
-	20	39,416	11,773	51,189



3 Figure 1: MMI map due to Pohang earthquake (left) and Gyeongju earthquake (right). Source: KMA (2018).





2 Figure 3: Chugaryeong fault zone in the middle of the Korean peninsula. Source: Modified from Chung et al. (2014)



- 2 Figure 4: PGA hazard map of Seoul according to each scenario event.



2 Figure 5: Shape of standard response spectrum.



2 Figure 6: Performance point according to intersection of capacity curve and demand spectrum.



2 Figure 7: Example of fragility curve for structural component.





- 2 Figure 8: Loss ratio map for each building by the scenario.

- U