

## 1 **Supplementary Information: Hazard area performance with optimised, global and hold-back** 2 **parameters**

3 At each of the six study sites we optimise the two parameters in the SHALRUN-EQ model required  
4 to predict hazard area, initiation angle ( $\theta_m$ ) and stopping angle ( $\theta_s$ ), by sampling values for each  
5 parameter uniformly in 1 degree increments over the range [20,70] for initiation angle and [0,50] for  
6 stopping angle, and imposing the requirement:  $\theta_m > \theta_s$ . For our objective function we use the area  
7 under the receiver operating characteristic (ROC) curve, comparing landslide hazard derived from  
8 hazard area to the inventory of observed landslides at each site. The optimisation surfaces are  
9 shown in Figure S1. To generalise our results, we then take arithmetic means of the optimum  
10 initiation and stopping angles, to generate hazard area predictions using a single 'global' rule  
11 averaged over all six inventories (Table S1). To remove the influence of test data on the test itself,  
12 we re-run the hazard area prediction for each inventory as a hold back-test, in which we re-calculate  
13 the initiation and stopping parameters excluding the optimised values from that inventory and using  
14 only the remaining five inventories.

15 We find that the differences in ROC curves (Figure S2) and area under the curve values (Table S1)  
16 are fairly subtle. Hazard area with global averaged parameters performs well overall, with AUC  
17 values that range from 0.78 to 0.86. Hazard area with parameters that are optimised for each  
18 inventory offers only a slight further improvement, with AUC increased by <3% in each case (Table  
19 S1). Optimised initiation and stopping angles can differ quite radically between sites, ranging from  
20 31-45° for initiation angle and from 3-19° for stopping angle. This might signal cause for concern  
21 about how feasible it is to find a single general rule given such variability in optimum parameters  
22 between sites. However, hazard area skill is relatively insensitive to parameter variation close to the  
23 optimum parameters, as indicated by the relatively smooth and gentle peaks of the optimisation  
24 surfaces in Figure S1. Thus, the (sometimes large) differences between global and optimised  
25 parameter values do not translate into large performance differences between hazard area  
26 predictions using global or optimised parameters. The use of hold-back rather than global  
27 parameters results in an even smaller difference in performance; AUC values are reduced by <1%  
28 for every inventory and hazard area is still the best metric at all sites. For this reason, we include  
29 hold-back tests here but report results from global average parameters rather than hold-back

30 parameters in the paper for simplicity. It is these global average parameters (initiation angle of 39°  
 31 and stopping angle of 10°) that form the basis of our simple rule, and that we would recommend  
 32 when applying the SHALRUN-EQ approach to a new location (in the absence of a landslide inventory  
 33 with which to test and calibrate the parameters).

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35 Table S1: Parameter values and areas under the ROC curve for the six inventories

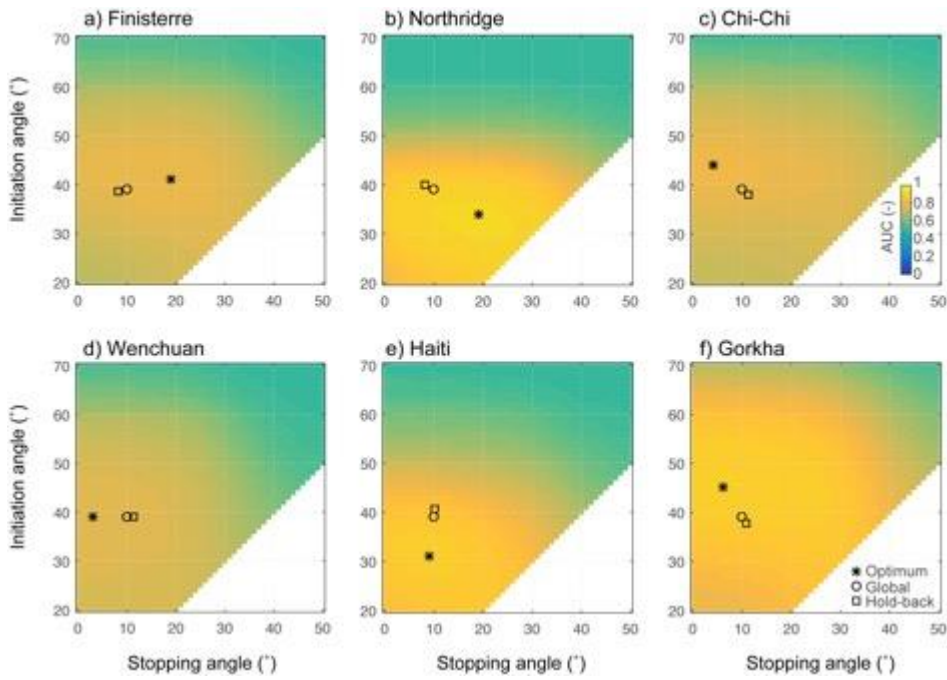
	Parameters		Area Under ROC Curve		
	Initiation slope $\theta_i$ (°)	Stopping slope $\theta_s$ (°)	Hazard area optimised	Hazard area global	Hazard area holdback
Finisterre	34	19	0.91	0.89	0.88
Northridge	41	19	0.80	0.79	0.78
Chichi	44	4	0.80	0.80	0.79
Wenchuan	39	3	0.78	0.78	0.78
Haiti	31	9	0.88	0.86	0.85
Gorkha	45	6	0.89	0.88	0.88
Average	<b>39</b>	<b>10</b>	<b>0.84</b>	<b>0.83</b>	<b>0.83</b>
1 $\sigma$	<b>6</b>	<b>7</b>	<b>0.1</b>	<b>0.1</b>	<b>0.1</b>

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39 Figure S1: Model predictive skill for SHALRUN-EQ for each of the six landslide inventories across  
40 reasonable ranges for the two parameters, initiation angle ( $\theta_m$ ) and stopping angle ( $\theta_s$ ). Predictive  
41 skill is quantified using area under the receiver operating characteristic curve. The six inventories  
42 are: a) Finisterre, b) Northridge, c) Chi-Chi, d) Wenchuan, e) Haiti, f) Gorkha. Symbols show the  
43 parameter combinations from site specific optimisation, global average and hold-back average.



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46 Figure S2: Receiver operating characteristic (ROC) curves for the six landslide inventories and five  
 47 metrics examined here, as shown in Figure 6 of the paper, but with the addition of ROC curves for  
 48 SHALRUN-EQ with site-specific optimised parameters and hold-back parameters (i.e., global  
 49 averages from five sites excluding the test site). The six inventories are: a) Finisterre, b)  
 50 Northridge, c) Chi-Chi, d) Wenchuan, e) Haiti, f) Gorkha. False positive rate is given by the number  
 51 of false positives divided by the sum of false positives and true negatives. True positive rate is  
 52 given by the number of true positives divided by the sum of true positives and false negatives. The  
 53 1:1 line represents the naïve (random) case. Curves plotting closer to the top left corner of each  
 54 panel represent better model performance.

