Assessment of geodetic velocities using GPS campaign measurements over long baseline lengths

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Abstract. GPS campaign measurements are frequently used in order to determine geophysical phenomena such as tectonic motion, fault zones, landslides, and volcanoes. When observation duration is shorter, the accuracy of coordinates are degraded and also the accuracy of point velocities are affected. The accuracies of the geodetic site velocities from a global network of the International GNSS Service (IGS) stations were previously investigated using only PPP. In this study, we extend that study in which site velocities will also be assessed including fundamental relative positioning. PPP derived results will also be evaluated to see the effect of JPL reprocessed products, single receiver ambiguity resolution, repeating survey campaigns minimum 3 days

at the site, and eliminating noisier solution prior to the year 2000. Globally distributed 18 continuously operating IGS stations were chosen to create synthetic GPS campaigns. GPS data were processed comparatively using GAMIT/GLOBK v10.6 and GIPSY/OASIS II v6.3. The data of synthetic campaign GPS time series were processed using a regression model accounting

10 for the linear and seasonal variation of the ground motion. Once accepting the velocities derived from 24 hour sessions as the truth, the results from sub-sessions were compared with the results of 24 hours and hypothesis testing was applied for the significance of the differences. The major outcome of this study is that at global scales (i.e. over long distances) with short observation sessions, the fundamental relative positioning produces results similar to PPP. The reliability of the velocity estimation for GPS horizontal baseline components has now been improved to about 85% on the average for observation

15 durations of 12 h.

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1 Introduction

GPS measurements were gathered from campaign surveys from the end of 80s through mid 90s. As of the emerge of continuous GPS in the early 90s and after the release of IGS official orbit in 1994 campaign GPS measurements were combined with continuous GPS. By doing this, researchers wanted to take the advantage of episodic GPS measurements accumulated over the

20 past 10 years. Campaign GPS measurements were mainly referred to monitor the global sea level in an attempt to decouple crustal motion from the actual sea level rise (Bingley et. al., 2001) and to monitor tectonic motion (Zhang et. al., 1997; Dixon et. al., 2000; Reilinger et.al., 1997).

Zhang et. al. (1997) studied stochastic properties of continuous GPS (19-month long) data from permanent stations. They then extended their time series by extrapolation to 5 years and generated campaign GPS measurements. Velocities were estimated from those synthetically generated campaign measurements. Velocity estimation (i.e. standard) errors of campaign

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measurements were assessed employing white noise and colored noise models. The stochastic model derived from continuous measurements was recommended for finding the standard errors of deformation rates obtained from campaign measurements.

Dixon et. al. (2000) used both campaign and continuous GPS to interpret the motion of Sierra Nevada Block. They followed a similar procedure as given in Zhang et. al. (1997) and determined the stochastic model of their continuous measurements to

5 later calibrate the velocity error of their combined time series. Bingley et. al. (2001) followed a similar procedure in finding crustal motion in monitoring of the sea level, and velocities of campaign GPS measurements were computed in the combination model using the suggestions from Zhang et. al. (1997) and Mao et. al. (1999).

In the new milenium, many studies (Vernant et. al., 2004; Serpelloni et. al., 2007; Hollenstein et. al., 2008; Chousianitis et. al., 2015; Bitharis et. al., 2016) in which GPS velocity fields have been used to facilitate tectonic and geodynamic research were

- 10 performed applying the procedure detailed in Zhang et. al. (1997), Mao et. al. (1999), and Dixon et. al. (2000). However, many others that employ campaign measurements were performed with the procedure; 1-day per year, collecting GPS measurements with only 8-10 hour observation session during the measurement day (Miranda et. al., 2012; Elliott et. al., 2010; Rontogianni, 2010; Ashurkov et. al., 2011; Ozener et. al., 2013; Tran et. al., 2013; Catalão et. al., 2011). Unluckily, the velocities from such campaigns vere estimated from only a couple of years (i.e. using only 2-3 estimates). Ambiguity resolution from the
- 15 GPS baseline processing and hence the positioning accuracy as well as velocity estimation from the above campaigns were deteriorated due to the fact that GPS baseline solutions were produced for long baselines up to 2000 km with only 8-10 h of the data.

To critisize the above studies Akarsu et. al. (2015) designed a global IGS study in which station velocities from 8-12 h GPS campaigns were assessed against those of the 24 h GPS campaigns. Differing from the studies which aim to assess the "standard error level of estimated velocities" from campaign measurements (i.e. Zhang et. al. (1997); Dixon et. al. (2000); Mao et. al. (1999)),Akarsu et. al. (2015) emphasized the term "accuracy of velocities" by which the accuracy of velocities estimated from 8-12 h observation time series is assessed against those of 24 h observations which are taken as the truth. They used the PPP online module of GIPSY/OASIS II (APPS) to analyze the GPS data. The results revealed that only 30-40% of the horizontal and none of the vertical velocities were comparable to the accuracy derived from 24 h campaigns.

- On the other hand, the analysis of Akarsu et. al. (2015) at the time did not include some of the improvements due to recent developments in regard to the GIPSY/OASIS II processing, such as new JPL reprocessed products (i.e. orbits and clocks) and single receiver ambiguity solution. Considering those developments and adding some extra measures to the surveying procedure, we believe the success rate of estimated velocities will be improved. The extra measures mentioned above consider carrying out campaign GPS measurements in 3 consecutive days with overlapping sessions and including GPS days with iono-
- 30 spheric kappa index less than 4. Furthermore, the PPP results produced will be assessed with fundamental relative positioning using GAMIT/GLOBK analysis with the hypothesis "GPS relative positioning over long baseline lengths with short occupation durations should produce positioning information equivalent to PPP campaign results". To handle this experiment a global network of 18 IGS stations were selected and the GPS data were analyzed using GAMIT and GIPSY. Synthetic GPS campaigns were created from the continuous observations with 8, 12 and 24 h sessions. GPS data were processed for all sessions to form
- 35 north, east and up campaign time series. Velocities derived from all three GPS components calculated from both 8 and 12 h

sub-sessions were compared with the velocities from 24 h which were accepted as the truth. The differences from the truth were statistically tested and the result were interpreted.

2 Methodology

2.1 GPS Data Analysis

- 5 GPS data were downloaded in Receiver Independent Exchange (RINEX) format with 30 sec. intervals from the Scripps Orbit and Permanent Array Center (SOPAC) which is one of the data archives of the International GNSS Service (IGS) at http://sopac.ucsd.edu/. The IGS stations used in the study are demonstrated in Figure 1. First of all, to determine the horizontal velocities for each of the stations we selected three successive days in October each year for the years 2000 through 2015. Akarsu et. al. (2015) did the similar sampling using only 1 day in a year. This is the procedure followed by many of the GPS
- 10 experiments using repeated surveys (Aktuğ et. al., 2009, 2013; Dogan et. al., 2014; Koulali et. al., 2015; McClusky et. al., 2000; Ozener et. al., 2010; Tatar et. al., 2012). Using 3 consecutive days here we believe we increased the reliability of the solutions. A treatment in regard to the solar activity, which was missing in Akarsu et. al. (2015), was also taken into consideration (i.e. days with kappa index \leq 4) here. In addition, three successive days in every month were included for the processing of the vertical component. In order to model the significant annual signal on GPS heights, here we did the sampling monthly. The
- 15 GPS data were segmented into sub-sessions as listed in Table 1 in order to generate the repeated GPS measurements.

2.1.1 GAMIT/GLOBK Processing

The GPS data were processed with GAMIT/GLOBK v10.6 software for relative point positioning (Herring et. al., 2006a, b) and with GIPSY/OASIS II v6.3 for PPP (Zumberge et. al., 1997). The elevation cut-off angle was set to 7 degrees on both software.

- The processing of the GPS data using GAMIT/GLOBK was conducted in three steps (Feigl et. al., 1993; McClusky et. al., 2000; Reilinger et. al., 2006; Tatar et. al., 2012; Dong et. al., 1998; Cetin et. al., 2018). We selected 18 globally scattered IGS stations. At first, the loosely constrained station coordinates, atmospheric zenith delays of each points, and Earth Orientation Parameters (EOP) were estimated using doubly differenced GPS phase measurements and IGS final products. Global Pressure and Temperature 2 (GPT2) mapping function developed by Lagler et. al. (2013) was used to model the delay in the atmosphere.
- The ocean tide loading correction was applied using FES2004 model of Lyard et. al. (2006). Ambiguities were on the average resolved with 90% success for the wide-lane and 80% success for the narrow-lane (Figure 2).

Secondly, GLOBK was used to estimate the point coordinates and velocities from a combined solution comprising the daily loosely constrained estimates, EOP values, orbit data, and their covariance through Kalman Filtering. We used the IERS (International Earth Rotation and Reference Systems Service) Bulletin B values for Earth rotation parameters. Since our study

30 was initially designed to be a global experiment, in this step we did not extra enlarge our network with more globally scattered and loosely constrained IGS stations. In the last step, the reference frame was realized on each day through "generalized constraints". Iterations were applied on the initially chosen 18 IGS stations, and about 5 bad sites were eliminated after 4 iterations. The reference frame was realized on each day employing a reliable set of round 13 IGS stations in the ITRF2008 no-net-rotation (NNR) frame (Altamimi et. al., 2012). The reliability of the IGS stations was characterized with GPS days which do not contain the effect of bad ionospheric

conditions with kappa index values smaller than 4, having at least 95% data coverage, being available on the common days,

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The processing strategies described above were applied to each subset of sessions listed in Table 1. The coordinate values for all sub-sessions were transformed to the topocentric system consisting of East, North, and Up. The time series of the site ZIMM from relative positioning and PPP solutions for all sub-sessions were illustrated in Figure 3.

10 2.1.2 GIPSY-OASIS II Processing

and repeating in 3 consecutive days with overlapping sessions.

We used JPL final precise (flinnR) orbits and clocks in the analysis. The (precise point positioning) PPP module of GIPSY/OASIS II v6.3 was developed by Zumberge et. al. (1997). In GIPSY analysis, final orbits and clocks are determined from a global network solution. The results were represented using the International Earth Rotation Service's reference system ITRS (Petit and Luzum, 2010), as realized through the reference frame ITRF2008 (Altamimi et. al., 2012). Tropospheric Zenith Wet Delay was

modelled as a random-walk parameter with a variance rate of 5 mm² per hour and wet delay gradient with a variance rate of 0.5 mm² per hour. The dry troposphere was modelled using GPT2 mapping function a priori zenith conditions (Lagler et. al., 2013). Pseudo-range and carrier phase observations were employed to eliminate the ionospheric delay using L1 and L2 data combination. Kedar et. al. (2003) model was used to eliminate the effect of second order ionosphere. Satellite and receiver antenna phase centre variation (APV) maps were automatically applied following the IGS standards (Haines et. al., 2010).
Desai (2002) model was used to eliminate the effect of ocean tide loading.

2.2 Velocity Estimation and Statistical Tests

In this section, with the motivation from Akarsu et. al. (2015), the estimation of an IGS site velocity and the related statistical tests will be explained. In Figure 3, the comparison of all sub-session coordinate time series for all three GPS baseline components from both software results have been shown. Once looking at the time series, all sub-sessions get along well with each other. For the horizontal components that are East and North, the variations are almost perfectly linear, and this shows us the tectonic motion clearly. To estimate the linear variation (i.e. the velocity) the model of

$$x_i = a.t_i + b + o_i.x_{off} + v_i \tag{1}$$

was used. There x_i represents any coordinate value, a site velocity, t_i the time, b the intercept, and v_i the residuals. In a GPS solution time series there are additional terms such as to clarify the sudden displacements due to earthquakes. Then, Eq. (1) is expanded to include an offset value x_{off} and the corresponding coefficient o_i (Montillet et. al., 2015). For instance in

our analysis, the stations AREO and USUD include offset values in their time series due to earthquakes. For all stations, the velocity estimations were calculated using Eq. (1) by means of the least square estimation.

The vertical component additionally includes significant seasonal variation. The coordinate time series for vertical components contain repeating annual cycle stemming from hydrological and atmospheric loading (Blewitt and Lavallée, 2002).

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Santamaría-Gómez et. al. (2011) noticed seasonal motions in smaller periods like 3 and 4 months and diminishing amplitudes in GPS time series from continuously operating stations. Given these circumstances, it is not sufficient to determine vertical velocities with a linear model. The seasonal model we use here take into account the annual and semi-annual periodicities;

$$x_{i} = a.t_{i} + b + o_{i}.x_{off} + \sum_{n=1}^{q} [c_{n}.cos\frac{2\pi.t_{i}}{T_{n}} + d_{n}.sin\frac{2\pi.t_{i}}{T_{n}}] + v_{i}$$
⁽²⁾

where q = 2, $T_1 = 1$ year and $T_2 = 0.5$ year. The use of the offset parameter is the same as in the horizontal assessment. Furthermore, R^2 value known as "coefficient of determination" was computed in regression analysis as a statistical tool, which 10 shows how well the data fit to the model estimated. For any coordinate component from a regression analysis, computation of R^2 is given with;

$$R^{2} = 1 - \frac{\sum_{i=1}^{n} \hat{v}_{i}^{2}}{\sum_{i=1}^{n} (x_{i} - \overline{x})^{2}} = 1 - \frac{\sum_{i=1}^{n} (x_{i} - \hat{x}_{i})^{2}}{\sum_{i=1}^{n} (x_{i} - \overline{x})^{2}}$$
(3)

where $\hat{v}_i = x_i - \hat{x}_i$ refers to the regression values $\hat{x}_i = \hat{a}t_i + \hat{b}$ based on the least square estimation $(\sum_{i=1}^n v_i^2 = min)$, and \overline{x} is the arithmetic average of n number of measurements used in the estimation. The velocity estimation results and R^2 values 15 from both processing strategies for the station of ZIMM have been listed in Table 2. Almost all R^2 values of the horizontal components in Table 2 for both software are at the level of 0.99 whereas those of the vertical ones range from 0.27 to 0.49. It is because the up component sampled using monthly data is not obviously linear. Parallel to the low R^2 values, the estimated velocities also fluctuate larger for the vertical component.

- 20 For all the stations in the IGS network, the solutions from sub-sessions were compared with the solutions (i.e. velocities) of 24 hours accepted as the truth. The statistical assessments of hypotheses were carried out in three steps. Then, the equivalancy between the unit variance derived from LSE of the sub-session given in Table 1 and with that of the 24h session was tested. The relevant hypothesis testing was set to be $H_0: \sigma_{24}^2 = \sigma_s^2$ and $H_A: \sigma_{24}^2 \neq \sigma_s^2$ where σ^2 represents the unit variance and subscripts represent the observation session. A hypothesis testing based on F-distribution was applied to check the equivalancy
- of the variances. In the case unit variances were found to be equivalent, Student's t test was applied whether or not the velocity 25 estimated from the campaign GPS significantly differs from the velocity derived from continuous GPS. The null hypothesis was set to be $(H_0: a_{24} = a_s)$ against the alternative hypothesis $(H_0: a_{24} \neq a_s)$ where a_i denotes the velocity values in Eq. (1) and (2). Briefly, it was tested whether or not there is a significant difference between the results of 24 hour solutions and those of the sub-sessions. In these statistical tests, the degree of freedom values for the horizontal components where approximately
- 42 whereas the degree of freedom for the vertical component was about 345. The degree of freedom varied with respect to the 30 number of insignificant parameters from the LSE.

3 Results and Discussion

As described in the previous section, the time series generated from all sessions of each continuous GPS site were analyzed. The coefficient of determination (i.e. R^2), which shows how well the data fits to the model, is computed according to Eq. (3). Tables 3, 4 and 5 compare the results of sub-sessions with those of the 24-hour statistically. Tables generally consist of two

5 columns, which includes the relative evaluation results from GAMIT / GLOBK v10.60 and the PPP results from GIPSY-OASIS II v6.3 software. In each column, R^2 values and hypothesis test results are given.

Hypothesis test results are based on a 95% confidence level. If the hypothesis H_0 is accepted, it is shown that there is no statistically significant difference from the geodetic site velocities from sub-sessions to those from 24h session results. If the hypothesis H_0 is rejected (only expressed in **bold**), a posteriori unit variance obtained from the least square estimation is

10 statistically different from the 24 h one based on the F-test, that is, the models used for the geodetic velocity estimation are not equivalent. Furthermore, both the results expressed in **bold and underlined** indicate that the model is equivalent, but the deformation rate from 24-hour session is statistically different from the velocities from the sub-sessions based on the Student's t test.

In Fig. 3, the subplots of the horizontal component clearly show the character of the tectonic motion linearly. In this context, once Table 4 and 5 are examined, it is obviously seen that R^2 values estimated from all sessions are so close to 1 except for GUAM, KERG, USUD (in Table 4) and DAV1 (in Table 5). For instance, the motion in USUD is thought to be due to the postseismic relaxation.

Success rates of velocity estimation from PPP and relative positioning are illustrated in Fig. 4. There blue bars are for 8h- and orange bars are for 12h-sessions. With the success rate here, we mean the success of velocity estimation from short sessions

- 20 when velocity estimation from 24h- is taken as the truth. Dashed pattern shows PPP results, whereas no pattern is for relative positioning. First of all, success rates for the horizontal components vary from 40 to 90%. Furthermore, the rates from 12 h sessions are higher than those of the 8 h sessions as expected. Note that the horizontal success rates from PPP are higher than those of the relative positioning, formed over long baselines to use in tectonic studies.
- The fact that the accuracy of the vertical component is worse than that of the horizontal component is often expressed in the literature and in practice by many researchers. Therefore, the repeatabilities for this component are larger, and the seasonal effects are much more apparent than the horizontal ones. For this reason, the values of R^2 in Table 5 are much lower than those calculated from the horizontal component (around 0.40). Likewise, the results of the hypothesis test were rejected at a higher rate. Both for PPP and relative positioning, success rates for the vertical component are so low varying from about 5 to 15%. These rates are almost same for both methods.
- 30 Overall, the success rates of 12h- solutions are higher than those of 8h- solutions, the systematic effect acting on shorter sessions is varried and greater. For both positioning methods, the east component has greater success than the north one with regard to the truth. The success rates in Fig. 4 are higher for PPP than relative positioning because in the GAMIT/GLOBK processing are formed long baseline lengths. Over long baseline lengths, troposphere and ionosphere modelling become difficult, orbit errors accumulate, and hence ambiguity resolution becomes worse.

The reliability of velocity estimation from short GPS campaigns using PPP has been improved here when comparing results with those of Akarsu et. al. (2015). By the improvement we mean that the statistical agreement between the velocity estimated from short GPS observation and those of 24h sessions is higher here. The improvement in the horizontal component is 35% and 40% for 8h and 12h respectively. The vertical component was improved 4% and 17% for 8h and 12h respectively. This

- 5 improvement might be ascribed to a few developments in the analysis procedures. First of all, here we used GPS time series spread over the years 2000 onwards. In other words, the noisier part 1990-2000 which might have affected the quality of estimated velocities in Akarsu et. al. (2015) is eliminated. Second, the analysis was performed with reprocessed orbits and clocks. JPL changed its orbit and clock estimation strategy as of the year 2007 (Hayal and Sanli, 2016). Third, GIPSY single receiver ambiguity resolution was further improved the accuracy of PPP (Bertiger et. al., 2010). Bertiger et. al. (2010) and Hayal
- 10 and Sanli (2016) showed how positioning accuracy was improved with reprocessed JPL products and single receiver ambiguity resolution. Reprocessing especially improved the east component and this is correlated with the findings in this paper. Fourth, campaign measurements were performed in three consecutive days (i.e. the sampling was made such that IGS data were processed sellecting 3-consecutive days from the archive). Therefore, it was possible to eliminate the outlier solution from the processing. Finally, GPS campaigns were selected from the days in which the effect of geomagnetic storms is eliminated.
- Eckl et. al. (2001) showed that using proper ambiguity resolution, troposphere modelling, and IGS precise orbits relative positioning performs uniformly, i.e. is not dependent on baseline length, for baseline lengths shorter than 300 km. In this experiment, GAMIT/GLOBK relative positioning used baseline lengths longer than 300 km. This degraded the accuracy of positioning and hence the velocity estimation of relative positioning. This was even achieved with slightly coarser accuracy than the PPP positioning. Based on relative positioning, BERNESE processing also gave similar results in Duman and Sanli (2016). Many studies in the literature monitoring tectonics with long baselines to stable plates need to take this into account

(Ayhan et. al., 2002; Aktuğ et. al., 2015; Reilinger et. al., 2006; Ozener et. al., 2010).

4 Conclusions

We incorporated relative positioning in the determination of the accuracy of GPS site velocities from GPS campaigns (i.e. Observation sessions shorter than 24 h). Relative positioning results were produced from GAMIT/GLOBK. The results were
also compared with PPP solutions derived from GIPSY/OASIS II. A global experiment for proper sampling was adopted using the IGS network.

The results indicate that relative positioning using long baseline lengths and short observation sessions produces similar results as with PPP. The accuracy is slightly coarser for horizontal positioning and slightly better for vertical positioning. Previously it has been noted that the accuracy of relative positioning does not depend on baseline length if baselines are shorter than 300 km. In the GAMIT/GLOBK processing here, reference points were chosen longer than 300 km.

It has also been noted that the accuracy of GPS site velocities derived from short observation sessions using PPP was improved here compared to previous studies. This is ascribed to the fact that the new GIPSY PPP runs with a new ambiguity resolution algorithm called single receiver ambiguity resolution. This especially improved the east component and the east

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results in this study show better accuracy. Furthermore, the analysis was performed using reprocessed JPL orbits and clocks. The contribution of JPL reprocessed products to positioning was previously discussed among researchers. Differing from the previous studies, our sampling here also comprises GPS days freed from the effect of geomagnetic storms. In addition, repeating campaign GPS measurements in three consecutive days helps removal of a bad solution from the analysis. The noisier IGS

5 time series between 1990 and 2000 was not used. If the user takes into account the above listed factors in the planning of their field works they should expect similar types of accuracy levels.

In this study, the horizontal velocity accuracy of GPS campaigns with 12 h observation sessions from PPP seems to reach the confidence level of about 85%. However, the reliability of vertical velocities is very poor and about at 20% level. This means that tectonic studies trying to use the daylight as the observation duration would still produce poorer accuracy than the

10 expected 95%. Of course this result is based on GPS solutions only, one should expect 95% levels once solutions are compiled from multi-GNSS experiments. Although the accuracy of velocity estimation was improved about 40% for horizontal and 20% for vertical positioning, it is still not at the desired confidence level.

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Figure 1. IGS continuous GPS sites used in the study.



Figure 2. Daily fixed phase ambiguity resolution in percentage. WL: Wide-Lane and NL: Narrow-Lane ambiguity resolutions.



Figure 3. Time series of all sub-sessions for the site ZIMM from (a) relative positioning and (b) PPP solutions.



Figure 4. Success rates of 8h- and 12h-sessions. The velocity estimation from short sessions is compared with 24h results for each GPS component. Blue bars are for the 8h- and orange bars are for the 12h-sessions. Dashed patterns illustrate PPP estimates whereas no patterns are for the relative positioning.

Table 1. Segmented sub-sessions

Session Length	Session Duration Times									
[hours]	a	b	c							
8	00:00 - 08:00	08:00 - 16:00	16:00 - 24:00							
12	00:00 - 12:00	12:00 - 24:00								

GPS Baselines		R^2 / Velocities [mm/yr]								
Observation Ses	08a	08b	08c	12a	12b	24				
	Б (0.9998	0.9994	0.9998	0.9999	0.9995	0.9998			
	East	19.58	19.73	19.85	19.65	19.82	19.76			
CAMIT/CLOBY	North	0.9997	0.9991	0.9994	0.9997	0.9995	0.9997			
GAMIII/GLUDK	North	16.25	16.21	16.29	16.34	16.21	16.28			
	Up	0.4338	0.3095	0.2704	0.4099	0.3615	0.4714			
		1.06	1.06	0.67	0.96	0.76	0.91			
	East	0.9997	0.9991	0.9996	0.9997	0.9994	0.9997			
	Last	19.69	19.77	19.78	19.73	19.77	19.75			
CIDEV/OACIC II	Manth	0.9996	0.9992	0.9989	0.9996	0.9991	0.9996			
GIPS 1/UASIS II	North	16.16	16.10	16.11	16.17	16.04	16.11			
	Un	0.4233	0.3174	0.3433	0.4324	0.4005	0.4900			
	Up	1.08	0.97	0.92	1.00	0.99	0.99			

Table 2. Site velocities and R^2 values from both solutions for the site ZIMM

Table 3. For the north component, R^2 values and hypothesis test results for relative positioning and PPP

	GAMIT/GLOBK v10.60						GIPSY/OASIS II v6.3				
Stations	8 h		12 h		24 h	8 h		12 h		24 h	
	\mathbb{R}^2	Test Results	\mathbb{R}^2	Test Results	\mathbb{R}^2	\mathbb{R}^2	Test Results	\mathbb{R}^2	Test Results	\mathbb{R}^2	
	0.9816	H0 accepted	0.9810	H0 accepted	0.9811	0.9853	H0 accepted	0.9850	H0 accepted	0.9840	
AREQ	0.9823	H0 accepted	0.9782	H0 accepted		0.9839	H0 accepted	0.9833	H0 accepted		
	0.9792	H0 accepted				0.9828	H0 accepted				
	0.9953	H0 rejected	0.9967	H0 accepted	0.9974	0.9980	H0 accepted	0.9980	H0 accepted	0.9984	
CRO1	0.9926	H0 rejected	0.9966	H0 accepted		0.9970	H0 rejected	0.9968	H0 rejected		
	0.9960	H0 accepted				0.9975	H0 accepted				
	0.9883	H0 rejected	0.9915	H0 rejected	0.9803	0.9817	H0 accepted	0.9847	H0 accepted	0.9825	
DAV1	0.9825	H0 rejected	0.9756	H0 accepted		0.9804	H0 accepted	0.9744	H0 accepted		
	0.9720	H0 accepted				0.9718	H0 accepted				
	0.7315	H0 accepted	0.7835	H0 accepted	0.7817	0.8922	H0 accepted	0.9037	H0 accepted	0.9020	
GUAM	0.8178	H0 accepted	0.7880	H0 rejected		0.9168	H0 accepted	0.8759	H0 accepted		
	0.7830	H0 accepted				0.8702	H0 accepted				
	0.9998	H0 rejected	0.9999	H0 accepted	0.9999	0.9999	H0 rejected	0.9999	H0 rejected	0.9999	
HOB2	0.9998	H0 rejected	0.9998	H0 rejected		0.9999	H0 accepted	0.9999	H0 accepted		
	0.9998	H0 rejected				0.9999	H0 rejected				
	0.7352	H0 rejected	0.7891	H0 rejected	0.8809	0.8324	H0 accepted	0.8298	H0 accepted	0.8766	
KERG	0.8470	H0 accepted	0.8152	H0 accepted		0.8457	H0 accepted	0.8423	H0 rejected		
	0.8121	H0 rejected				0.7685	H0 rejected				
	0.9992	H0 rejected	0.9994	H0 rejected	0.9993	0.9991	H0 accepted	0.9991	H0 accepted	0.9991	
KIRU	0.9989	H0 rejected	0.9992	H0 accepted		0.9985	H0 rejected	0.9987	H0 accepted		
	0.9992	H0 rejected				0.9990	H0 rejected				
	0.9995	H0 rejected	0.9996	H0 rejected	0.9998	0.9994	H0 rejected	0.9995	H0 accepted	0.9997	
MATE	0.9996	H0 rejected	0.9995	H0 rejected		0.9992	H0 rejected	0.9994	H0 rejected		
	0.9993	H0 rejected				0.9991	H0 rejected				
	0.9981	H0 rejected	0.9981	H0 rejected	0.9989	0.9992	H0 accepted	0.9992	H0 accepted	0.9993	
NYAL	0.9979	H0 rejected	0.9988	H0 accepted		0.9990	H0 accepted	0.9988	H0 rejected		
	0.9980	H0 rejected				0.9988	H0 rejected				
	0.9797	H0 rejected	0.9755	H0 rejected	0.9841	0.9885	H0 rejected	0.9902	H0 accepted	0.9900	
POL2	0.9851	H0 accepted	0.9855	H0 rejected		0.9855	H0 accepted	0.9879	H0 accepted		
	0.9832	H0 rejected				0.9834	H0 rejected				
	0.9993	H0 accepted	0.9994	H0 rejected	0.9994	0.9992	H0 rejected	0.9994	H0 accepted	0.9996	
REYK	0.9991	H0 accepted	0.9992	H0 accepted		0.9995	H0 accepted	0.9995	H0 accepted		
	0.9991	H0 accepted				0.9993	H0 accepted				
	0.9992	H0 rejected	0.9996	H0 accepted	0.9996	0.9998	H0 rejected	0.9998	H0 rejected	0.9999	
TOW2	0.9995	H0 rejected	0.9996	H0 rejected		0.9999	H0 accepted	0.9999	H0 accepted		
	0.9996	H0 accepted				0.9999	H0 rejected				
	0.9970	H0 accepted	0.9976	H0 accepted	0.9969	0.9982	H0 rejected	0.9961	H0 rejected	0.9993	
TRAK	0.9931	H0 rejected	0.9926	H0 rejected		0.9972	H0 rejected	0.9993	H0 accepted		
	0.9920	H0 rejected				0.9986	H0 rejected				
	0.8624	H0 accepted	0.9008	H0 accepted	0.9162	0.9436	H0 accepted	0.9470	H0 accepted	0.9456	
USUD	0.9182	H0 accepted	0.8921	H0 rejected		0.9365	H0 accepted	0.9400	H0 accepted		
	0.8852	H0 accepted				0.9402	H0 accepted				
	0.9990	H0 rejected	0.9992	H0 rejected	0.9995	0.9983	H0 accepted	0.9987	H0 accepted	0.9989	
VILL	0.9992	H0 rejected	0.9997	H0 accepted		0.9987	H0 accepted	0.9988	H0 accepted		
	0.9993	H0 accepted				0.9983	H0 accepted				
	0.9995	H0 rejected	0.9996	H0 rejected	0.9998	0.9994	H0 accepted	0.9995	H0 accepted	0.9996	
WTZR	0.9994	H0 rejected	0.9997	H0 rejected		0.9985	H0 rejected	0.9995	H0 accepted		
	0.9997	H0 accepted				0.9995	H0 accepted				
	0.9940	H0 rejected	0.9958	H0 accepted	0.9953	0.9970	H0 accepted	0.9973	H0 accepted	0.9970	
YELL	0.9923	H0 rejected	0.9912	H0 rejected		0.9961	H0 accepted	0.9937	H0 rejected		
	0.9879	H0 rejected				0.9921	H0 rejected				
	0.9997	H0 accepted	0.9997	H0 accepted	0.9997	0.9996	H0 accepted	0.9996	H0 accepted	0.9996	
ZIMM	0.9991	H0 rejected	0.9995	H0 rejected		0.9992	H0 rejected	0.9991	H0 rejected		
	0.9994	H0 rejected				0.9989	H0 rejected				

Table 4. For the east component, R^2 values and hypothesis test results for relative positioning and PPP.

	GAMIT/GLOBK v10.60						GIPSY/OASIS II v6.3					
Stations	8 h	h 12 h 24 l					12 h			24 h		
	R^2	Test Results	R^2	Test Results	R^2	\mathbb{R}^2	Test Results	R^2	Test Results	R^2		
	0.9825	H0 accepted	0.9815	H0 accepted	0.9817	0.9870	H0 accepted	0.9875	H0 accepted	0.9882		
AREQ	0.9835	H0 accepted	0.9808	H0 accepted		0.9883	H0 accepted	0.9888	H0 accepted			
	0.9816	H0 accepted				0.9888	H0 accepted					
	0.9935	H0 accepted	0.9945	H0 accepted	0.9944	0.9897	H0 accepted	0.9920	H0 accepted	0.9944		
CRO1	0.9892	H0 rejected	0.9925	H0 accepted		0.9940	H0 accepted	0.9808	H0 rejected			
	0.9930	H0 accepted				0.9909	H0 accepted					
	0.8492	H0 accepted	0.9085	H0 accepted	0.9065	0.9745	H0 accepted	0.9776	H0 accepted	0.9801		
DAV1	0.9139	H0 rejected	0.9241	H0 accepted		0.9746	H0 accepted	0.9619	H0 rejected			
	0.8434	H0 rejected				0.9521	H0 rejected					
	0.9902	H0 rejected	0.9892	H0 accepted	0.9916	0.9916	H0 accepted	0.9912	H0 accepted	0.9941		
GUAM	0.9872	H0 accepted	0.9885	H0 accepted		0.9906	H0 accepted	0.9942	H0 accepted			
	0.9877	H0 rejected				0.9931	H0 rejected					
	0.9985	H0 rejected	0.9989	H0 rejected	0.9995	0.9971	H0 rejected	0.9983	H0 accepted	0.9988		
HOB2	0.9984	H0 rejected	0.9992	H0 accepted		0.9985	H0 accepted	0.9985	H0 accepted			
	0.9967	H0 rejected				0.9978	H0 rejected					
	0.9161	H0 rejected	0.9546	H0 accepted	0.9521	0.9695	H0 accepted	0.9684	H0 accepted	0.9702		
KERG	0.9618	H0 rejected	0.9464	H0 accepted		0.9669	H0 accepted	0.9683	H0 accepted			
	0.9381	H0 accepted				0.9607	H0 rejected					
	0.9994	H0 rejected	0.9995	H0 rejected	0.9995	0.9987	H0 accepted	0.9989	H0 accepted	0.9990		
KIRU	0.9994	H0 rejected	0.9994	H0 accepted		0.9989	H0 accepted	0.9989	H0 accepted			
inite	0.9987	H0 rejected				0.9988	H0 accepted					
MATE	0.9997	H0 rejected	0.9998	H0 accepted	0.9999	0.9997	H0 accepted	0.9997	H0 accepted	0.9998		
	0.9995	H0 rejected	0.9997	H0 rejected		0.9997	H0 accepted	0.9997	H0 accepted			
	0.9998	H0 rejected				0.9995	H0 rejected					
NYAL	0.9989	H0 rejected	0.9993	H0 accepted	0.9993	0.9988	H0 accepted	0.9989	H0 accepted	0.9990		
	0.9987	H0 rejected	0.9996	H0 accepted		0.9982	H0 rejected	0.9988	H0 accepted			
	0.9988	H0 accepted				0.9976	H0 rejected		r			
	0.9987	H0 rejected	0.9986	H0 rejected	0.9993	0.9991	H0 accepted	0.9993	H0 accepted	0.9993		
POL2	0.9993	H0 accepted	0.9992	H0 accepted		0.9994	H0 accepted	0.9993	H0 accepted			
	0.9993	H0 accepted				0.9990	H0 accepted		r			
	0.9965	H0 rejected	0 9977	H0 accented	0 9974	0.9960	H0 accepted	0 9974	H0 accented	0 9974		
REYK	0.9962	H0 accented	0.9964	H0 accepted	0.7771	0.9976	H0 accepted	0.9964	H0 accepted	0.7771		
iii iii	0.9946	H0 rejected	0.7701	no accepted		0.9962	H0 accepted	0.7701	no accepted			
	0 9994	H0 accented	0 9995	H0 rejected	0 9996	0.9996	H0 accepted	0 9996	H0 accented	0 9997		
TOW2	0.9994	H0 accepted	0.9997	H0 accepted		0.9996	H0 accepted	0.9997	H0 accepted			
	0 9989	H0 rejected				0.9996	H0 accepted		r			
	0.9996	H0 accented	0.9996	H0 accented	0 9995	0.9993	H0 rejected	0 9995	H0 accented	0 9997		
TRAK	0 9994	H0 accepted	0 9995	H0 accented		0 9993	H0 rejected	0 9997	H0 accented			
	0.9992	H0 accepted	0.7770	no accepted		0.9978	H0 rejected	0.,,,,,	no accepted			
	0.9811	H0 accented	0.9810	H0 accented	0.9814	0.9790	H0 accented	0.9824	H0 accented	0.9826		
USUD	0.9836	H0 accented	0.9826	H0 accented	0.7014	0.9826	H0 accented	0.9824	H0 accented	0.7620		
0000	0.9827	H0 accepted	0.9620	110 accepted		0.9796	H0 accepted	0.9620	110 accepted			
	0.9027	H0 accepted	0 9997	H() accented	0.0007	0.9995	H0 accepted	0.0006	H0 accented	0.0006		
VILI	0.9994	H0 rejected	0.9996	H0 rejected	0.7771	0.9993	H0 rejected	0.9996	H0 accented	0.2220		
TILL	0.9996	H0 accented	0.7770	<u>10 rejetitu</u>		0.9995	H0 accented	0.2220	10 accepted			
	0.9990	H0 rejected	0 9006	H0 rejected	0 0000	0.0002	H0 rejected	0.0005	H0 accented	0 9997		
WT7P	0.9993	H0 rejected	0.9990	H0 accented	0.2220	0.9993	H0 accented	0.2222	H0 accepted	0.2777		
W IZK	0.9997	H0 accented	0.9998	no accepted		0.9990	H0 accepted	0.9998	no accepted			
	0.9998	Ho accepted	0.0005	TIO material	0.0075	0.9997	TIO accepted	0.0002	110	0.0007		
VEL	0.9970	HU rejected	0.9985	HU rejected	0.9965	0.9979	HU accepted	0.9983	HU accepted	0.9986		
TELL	0.9975	HU accepted	0.9933	nu rejected		0.998/	HU accepted	0.9966	riu rejected			
	0.9891	H0 rejected	0.0000	TIO material	0.0000	0.989/	IIO rejected	0.0007	110	0.0007		
70.04	0.9998	HU rejected	0.9999	HU rejected	0.9998	0.9999/	HU accepted	0.9999/	HU accepted	0.9997		
ZIMM	0.9994	HU rejected	0.9995	HU rejected		0.9991	HU rejected	0.9994	H0 rejected			
	0.9998	HU accepted				0.9996	HU accepted					

Table 5. For the up component, R^2 values and hypothesis test results for relative positioning and PPP.

	GAMIT/GLOBK v10.60						GIPSY/OASIS II v6.3					
Stations	8 h	12 h				8 h	12 h			24 h		
	R^2	Test Results	\mathbb{R}^2	Test Results	\mathbb{R}^2	\mathbb{R}^2	Test Results	\mathbb{R}^2	Test Results	\mathbb{R}^2		
	0.2631	H0 rejected	0.2216	H0 rejected	0.3542	0.4916	H0 rejected	0.5595	H0 accepted	0.5372		
AREQ	0.2445	H0 rejected	0.1730	H0 rejected		0.4303	H0 rejected	0.4172	H0 rejected			
	0.1148	H0 rejected				0.3689	H0 rejected					
	0.3195	H0 rejected	0.3316	H0 rejected	0.4295	0.2017	H0 rejected	0.2893	H0 rejected	0.4269		
CRO1	0.3564	H0 rejected	0.2437	H0 rejected		0.2525	H0 rejected	0.2026	H0 rejected			
	0.2114	H0 rejected				0.2185	H0 rejected					
	0.2535	H0 rejected	0.2231	H0 rejected	0.2382	0.2246	H0 rejected	0.3060	H0 rejected	0.2259		
DAV1	0.1533	H0 rejected	0.1747	H0 rejected		0.2042	H0 rejected	0.0599	H0 rejected			
	0.1072	H0 rejected				0.0528	H0 rejected					
	0.1177	H0 rejected	0.1343	H0 rejected	0.1125	0.0513	H0 rejected	0.0490	H0 rejected	0.0571		
GUAM	0.0462	H0 rejected	0.0999	H0 rejected		0.0184	H0 rejected	0.0469	H0 rejected			
	0.1015	H0 rejected				0.0427	H0 rejected					
	0.0387	H0 rejected	0.0282	H0 rejected	0.0546	0.1889	H0 rejected	0.2199	H0 rejected	0.2894		
HOB2	0.0615	H0 rejected	0.0620	H0 rejected		0.1836	H0 rejected	0.1611	H0 rejected			
	0.0567	H0 rejected				0.0958	H0 rejected					
	0.2870	H0 rejected	0.3320	H0 rejected	0.4723	0.0932	H0 rejected	0.1247	H0 rejected	0.1993		
KERG	0.3759	H0 rejected	0.4180	H0 rejected		0.0992	H0 rejected	0.1478	H0 rejected			
	0.3579	H0 rejected				0.1337	H0 rejected					
	0.8169	H0 accepted	0.8241	H0 accepted	0.8174	0.8280	H0 accepted	0.8331	H0 accepted	0.8425		
KIRU	0.7776	H0 accepted	0.7961	H0 accepted		0.8169	H0 rejected	0.8185	H0 accepted			
	0.7893	H0 accepted				0.8184	H0 accepted					
	0.2250	H0 rejected	0.1726	H0 rejected	0.2347	0.0930	H0 rejected	0.1125	H0 rejected	0.2044		
MATE	0.1861	H0 rejected	0.2603	H0 rejected		0.1218	H0 rejected	0.1824	H0 rejected			
	0.1653	H0 rejected				0.1254	H0 rejected					
	0.9689	H0 rejected	0.9691	H0 rejected	0.9783	0.9628	H0 rejected	0.9646	H0 rejected	0.9733		
NYAL	0.9547	H0 rejected	0.9673	H0 rejected		0.9518	H0 rejected	0.9635	H0 rejected			
	0.9612	H0 rejected				0.9584	H0 rejected					
	0.3080	H0 rejected	0.2624	H0 rejected	0.3324	0.2000	H0 rejected	0.1977	H0 rejected	0.2095		
POL2	0.1290	H0 rejected	0.3037	H0 rejected		0.1167	H0 rejected	0.1575	H0 rejected			
	0.2513	H0 rejected				0.1790	H0 rejected					
	0.2590	H0 rejected	0.2774	H0 accepted	0.2492	0.2705	H0 rejected	0.3187	H0 accepted	0.3112		
REYK	0.2942	H0 rejected	0.2525	H0 rejected		0.3359	H0 rejected	0.2428	H0 rejected			
	0.2324	H0 rejected				0.1716	H0 rejected					
	0.3345	H0 rejected	0.2440	H0 rejected	0.3889	0.5033	H0 rejected	0.5034	H0 rejected	0.5657		
TOW2	0.1781	H0 rejected	0.3598	H0 rejected		0.3938	H0 rejected	0.4722	H0 rejected			
	0.3405	H0 rejected				0.4446	H0 rejected					
	0.2662	H0 rejected	0.2262	H0 rejected	0.2887	0.2370	H0 rejected	0.3055	H0 rejected	0.3646		
TRAK	0.0784	H0 rejected	0.2334	H0 rejected		0.3616	H0 rejected	0.2880	H0 rejected			
	0.3202	H0 rejected				0.2040	H0 rejected					
	0.3990	H0 rejected	0.4883	H0 rejected	0.5123	0.4952	H0 rejected	0.5507	H0 rejected	0.5685		
USUD	0.4516	H0 rejected	0.5359	H0 accepted		0.5178	H0 rejected	0.4920	H0 accepted			
	0.5662	H0 accepted				0.4842	H0 rejected					
	0.1156	H0 rejected	0.1620	H0 rejected	0.2615	0.3436	H0 rejected	0.4192	H0 rejected	0.4938		
VILL	0.1169	H0 rejected	0.2393	H0 rejected		0.3105	H0 rejected	0.3591	H0 rejected			
	0.2488	H0 rejected				0.2690	H0 rejected					
	0.3145	H0 rejected	0.4220	H0 rejected	0.4262	0.2357	H0 rejected	0.3047	H0 rejected	0.3060		
WTZR	0.3689	H0 rejected	0.3815	H0 rejected		0.2412	H0 rejected	0.2306	H0 rejected			
	0.3281	H0 rejected				0.2087	H0 rejected					
	0.9095	H0 rejected	0.9272	H0 accepted	0.9362	0.9287	H0 rejected	0.9394	H0 rejected	0.9494		
YELL	0.9106	H0 rejected	0.9274	H0 accepted		0.9340	H0 rejected	0.9449	H0 accepted			
	0.9090	H0 rejected				0.9369	H0 rejected					
	0.4338	H0 rejected	0.4099	H0 rejected	0.4714	0.4233	H0 rejected	0.4324	H0 rejected	0.4900		
ZIMM	0.3095	H0 rejected	0.3615	H0 rejected		0.3174	H0 rejected	0.4005	H0 rejected			
	0.2704	H0 rejected				0.3433	H0 rejected					