



1      **Study on the combined threshold for gully-type debris flow early warning**

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9      **Abstract**

10     Gully-type debris flow induced by high-intensity and short-duration rainfall, frequently cause a great  
11    loss of properties and causalities in mountainous regions of Southwest China. In order to reduce the  
12    risk by geohazards, early warning systems have been provided. A triggering index can be detected in  
13    an early stage by the monitoring of rainfall and the changes in physical properties of the deposited  
14    materials along debris flow channel. Based on the method of critical pore pressure for slope stability  
15    analysis, this study presents critical pore pressure thresholds in combination with rainfall factors for  
16    gully-type debris flow early warning. The Wenjia gully, which contains an enormous amount of loose  
17    materials, was selected as a case study to reveal the relationship between the rainfalls and pore  
18    pressure, which can be used as a combined warning threshold. A three-level early warning system  
19    (Zero, Attention, and Warning) is adopted and the corresponding judgement conditions are defined in  
20    real-time. Based on this threshold, several rainfall events in recent years have been validated to prove  
21    that such a comprehensive threshold may be a reliable approach for the early warning of debris flows  
22    to safeguard the population in the mountainous areas.

23    **Keywords:** gully-type debris flow, pore pressure, rainfall threshold, early warning

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29 **1. Introduction**

30 Debris flows occur in mountainous area in Southwest China every year during the rainy season.

31 Gully-type debris flows are mainly triggered by high-intensity short-duration rainfall causing a

32 runoff-induced effect. They are partly initiated by shallow landslides distributed along the gullies

33 (Kean et al., 2013). The fast growth of the population and economic development in these areas

34 increase the frequency of catastrophic accidents and consequent socio-economic losses. The

35 Wenchuan earthquake on May12, 2008, Yushu earthquake on April 14, 2010, Lushan earthquake on

36 April 20, 2013, Ludian earthquake on August, 3 2014 and the Nepal earthquake on April, 25 2015

37 triggered thousands of landslides and cracked mountains which made these areas prone for debris flow

38 development under rainstorm conditions (Shieh et al., 2009). In the Chi-Chi earthquake area Taiwan,

39 numerous co-seismic landslides were triggered as well, causing the continuous triggering of

40 debris-flows during 10 years after the earthquake (Yu et al., 2013b). These catastrophic events have

41 greatly shocked the local people and government, because of the human vulnerability to natural

42 hazards as well as the lack of knowledge on natural disaster prevention and mitigation. For the

43 descendant, there is an urgent demand for an effective method to reduce the hazard and risk. Therefore,

44 researchers have been working on the forecast of debris flow occurrence and setting up of early

45 warning systems for several decades. At the regional scale, the methods for shallow landslides early

46 warning are mostly based on statistical models which have already been proved their importance in

47 landslide prevention and mitigation (Keefer et al., 1987;Guzzetti et al., 2007a;Baum and Godt,

48 2009;Segoni et al., 2014;Shuin et al., 2012;Tropeano and Turconi, 2004). Generally, one or two

49 parameters were selected for the assessment of rainfall thresholds, e.g. rainfall intensity and duration

50 (Keefer et al., 1987;Guzzetti et al., 2007a;Guzzetti et al., 2007b;Cannon et al., 2008), antecedent

51 precipitation (Glade et al., 2000), and cumulative rainfall(Guo et al., 2013). Besides, Baum and Godt

52 (2009) presented a combination threshold, including cumulative rainfall threshold, rainfall



53 intensity-duration threshold and antecedent water index or soil wetness for the shallow landslide  
54 forecasting. At the local scale, physical methods (e.g. numerical simulation) were used to find  
55 relationships among rainfall, soil properties, and pore pressure and their contributions to slope stability  
56 (Iverson, 1997; Peng et al., 2014; van Asch et al., 2013; Thiebes, 2012; Chae and Kim, 2011). However,  
57 detailed information related to landslide triggering are required to establish the site-specific thresholds,  
58 which are very difficult to extrapolate to other places due to the large variation in soil properties  
59 between different regions. In the Chenyulan River Watershed of Taiwan, debris flows were frequently  
60 triggered by Typhoons. Yu et al. (2013a) selected several decade identified factors related to  
61 topography, geology, and hydrology, to develop a normalized critical rainfall factor combined with an  
62 effective cumulative precipitation and maximum hourly rainfall intensity index for the forecast of  
63 gully-type debris flows. The model which is partly based on a runoff-induced mechanism has been  
64 successfully applied to the Wangmo River catchment, Guizhou Province, Southwest China (Yu et al.,  
65 2014).

66 In Southwest China, the strong earthquake shocks caused a significant rise in the frequency of  
67 debris flow. Researchers have already paid great attention to the mechanism, movement characteristics,  
68 and thresholds of debris flow in these shocked areas (Yu et al.; Yin et al., 2010; Zhou and Tang,  
69 2013; Guo et al., 2013; Huang et al., 2015a). The long-term effect by earthquakes cause the region  
70 become a high risk area, and particularly the gullies in mountain with no debris flows before become  
71 the debris flow gullies at present. Unfortunately, there is a significant lack of available data in these  
72 areas, e.g. the rainfall events which are very important to understand the debris flow triggering  
73 threshold. But in the earthquake shocked regions, numbers of unstable slope or loose deposited  
74 material distributed along the catchments. Therefore, rainfall is not the only triggering factor for debris  
75 flow occurrence. Xue and Huang (2016) discussed a possibility of establishing a comprehensive  
76 threshold for debris flow early warning by combination of rainfall and pore water pressure threshold.



77 Thus, during this study, pore pressure in slope stability analysis have been considered for gully-type  
78 debris flow forecasting. The goal of the here presented study is to propose a comprehensive method  
79 for such kind of debris flow early warning by real-time monitoring of rainfall and changes in pore  
80 pressure in the deposited material along channel in Southwest China. The infinite slope stability  
81 analysis was applied to identify the critical stability conditions of the deposited material. Then, a  
82 comprehensive warning threshold for rainfall and critical pore pressure will be presented, which  
83 includes both rainfall conditions and soil properties. Finally, verification and revision has been  
84 discussed to search a practical and useful method for reducing the risks of debris flows in Southwest  
85 China.

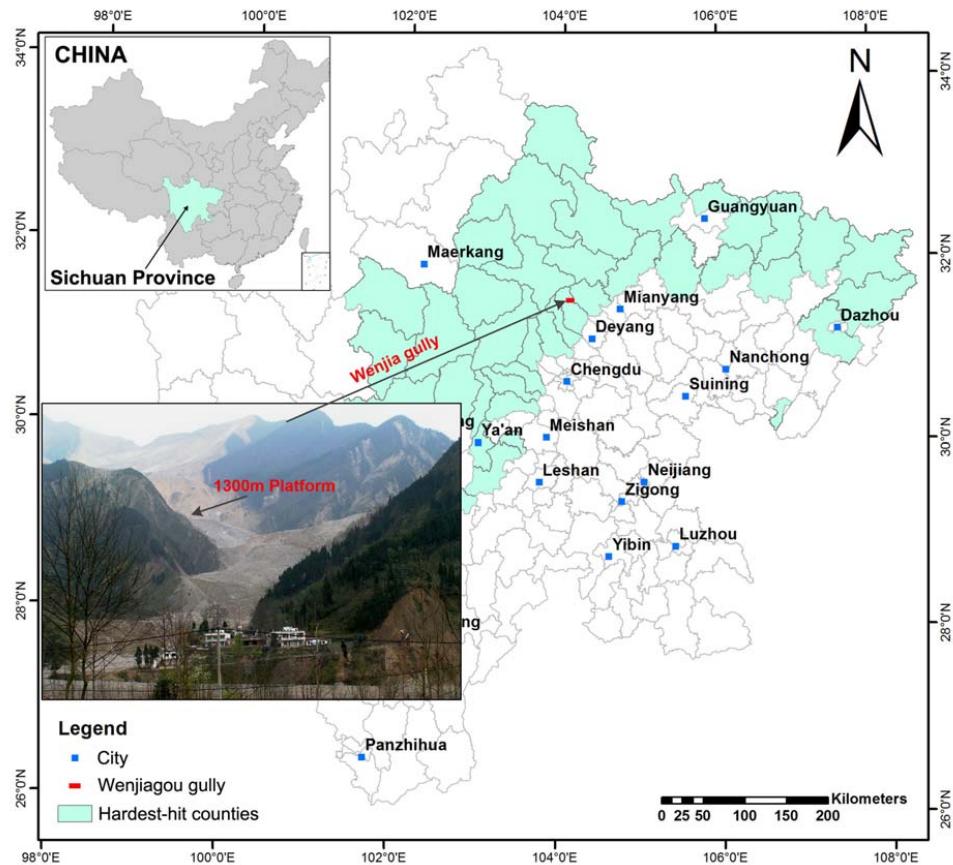
86 **2. Study area**

87 The Wenjia gully is located at the north of Qingping town, Mianzhu city, Sichuan province,  
88 Southwest China, and has a catchment area of 7.8 km<sup>2</sup> and a 5.2 km long main channel, as shown in  
89 Fig. 1. The elevation of this study area ranges from 300 m to 1,600 m above sea level, and the main  
90 valley with slope inclinations between 30° and 70° has been deeply incised by the Mianyuan river.  
91 The average yearly temperature is about 16 °C, and the climate is mild semi-tropical and moist with  
92 abundant rainfall and four distinguishable seasons. Eighty percent of the rainfall is concentrated in  
93 three months from July to September.

94 Before the Wenchuan earthquake on May12, 2008, the Wenjia catchment was covered by rich  
95 vegetation, and the channel was smooth and stable, as shown in Fig.2 (a). At that time, few geological  
96 disasters occurred in this region. Therefore, many farmers settled down at the foothills along the  
97 Mianyuan River. Qingping town downstream of the Wenjia channel's outlet (Fig 2 a & b). During the  
98 earthquake, a giant landslide occurred upstream in the catchment at the top of the watershed, which  
99 generated abundant co-seismic rock fall material and finer landslide deposits on a platform with an  
100 elevation of 1,300 m above sea level (Fig. 1, the photograph at left bottom of the main map). These



101 loose solid erodible materials could easily transform into debris flows during a rain storm. Shortly  
102 after the earthquake on Sep. 24, 2008, one rainfall event caused the first debris flow in this gully. The  
103 catastrophic debris flow triggered by a heavy rainfall on August 13, 2010, with a peak discharge of  
104  $1,530 \text{ m}^3/\text{s}$  and a total volume of  $4.5 \times 10^6 \text{ m}^3$ , caused many victims and the burying of reconstructed  
105 houses, most of the downstream check dams along the channel (Yu et al., 2012).



106  
107 Fig. 1. Location of Wenjia gully modified from Huang et al. (2013). The inset photograph of Wenjia gully at the  
108 left bottom was taken from the other side of Mianyuan River on August 10, 2008.

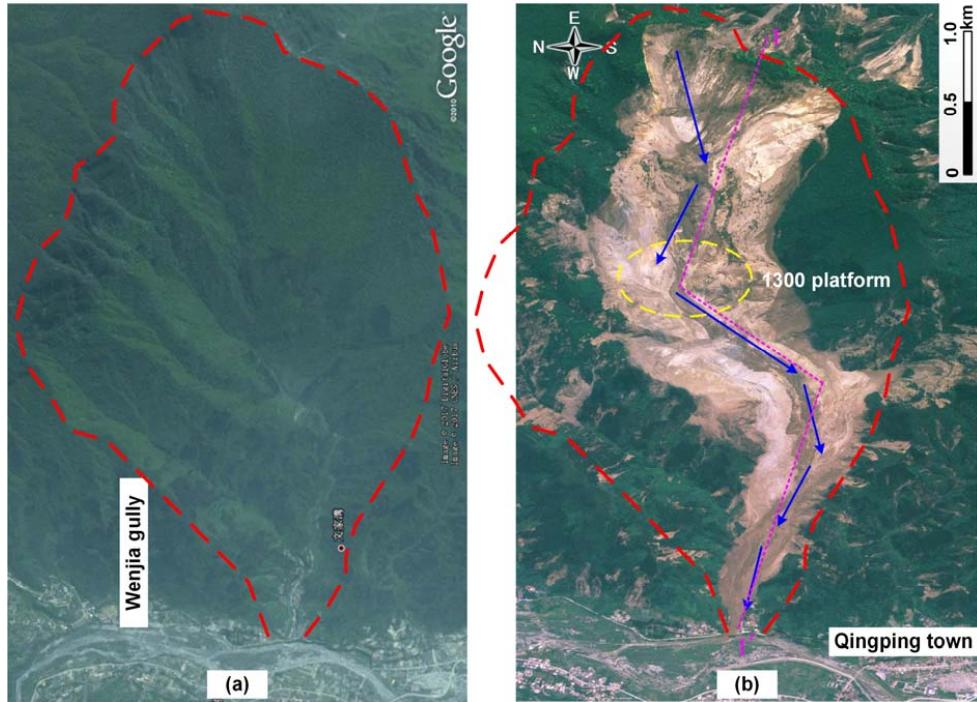
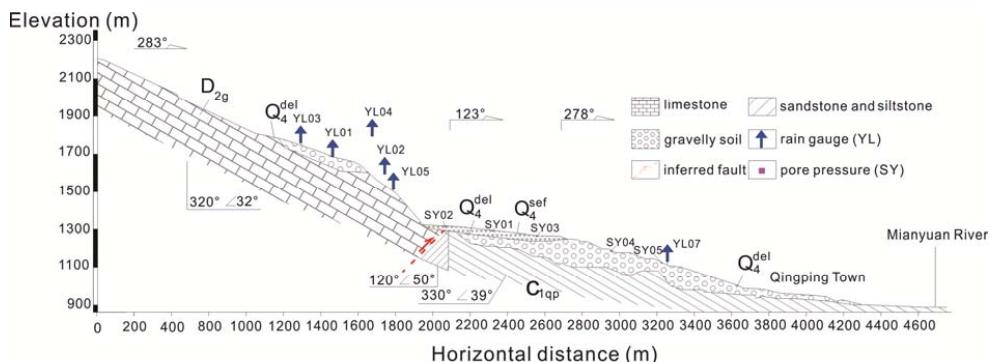


Fig. 2. Aerial image of Wenjia gully (a. image from Google Earth on Dec. 31, 2007; b. aerial photograph taken on May 18, 2008)



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110

Fig. 3. Geological profile of the main channel of Wenjia gully

111

Fig. 3 is the geological profile of cross section I - I' in Wenjia gully (Fig. 2b). The exposure  
 112 strata is Guanwushan Group (upper devonian period) with limestone, and Qingping Group (cambrian  
 113 period) with sandstone and siltstone. Field investigation also shows that the main loose deposits are  
 114 located at the 1300 platform (Fig 1 & 2). During heavy rains, the intense surface run-off may cause the



115 unstable slope collapse into the channel, maybe bed failure or run-off scouring of the loose deposited  
116 material. This explains why there would be giant debris flow occurrence in this gully, e.g. the debris  
117 flow event on August 13, 2010 above-mentioned.

118 **3. Methodology**

119 According to Terzaghi theory in soil mechanics, the shear strength of material at a point within a  
120 slope can be expressed as Eq. (1).

121 
$$\tau = c + (\sigma - u) \tan \phi \quad (1)$$

122 where  $\tau$  is the shear strength of the slope material,  $c$  is the effective cohesion of the material,  
123  $\phi$  is the effective friction angle of the material,  $\sigma$  is the total stress normal to a potential slip  
124 surface, and  $u$  is the pore pressure. Generally, the strength parameters ( $c, \phi$ ) of the slope material  
125 mainly determined the stability of the slope and the potential position of the slip surface.

126 Rainfall infiltrates into a hillslope, always accumulating in a saturated zone above a permeability  
127 barrier, and increases the pore pressures within the slope material. Based on the Terzaghi's work, the  
128 increase in  $u$  would cause the effective overburden stress ( $\sigma - u$ ) to decrease, and therefore the  
129 decrease of the shear strength until the slope fails. A formula to calculate the critical level of the pore  
130 pressure, for a highly idealized model of an infinite slope composed of cohesionless materials ( $c = 0$ )  
131 has been presented by Keefer et al. (1987), assuming both slip surface and piezometric surface are  
132 parallel to the ground surface. For all these assumptions, the critical pore pressure can be calculated by  
133 Eq. (2).

134 
$$u_c = Z \times \gamma_t \times \left(1 - \frac{\tan \theta}{\tan \phi}\right) \quad (2)$$

135 where  $Z$  is the depth of slip surface,  $\gamma_t$  is the total unit weight of the slope material, and  $\theta$  is  
136 the slope inclination, the other parameters are the same to those mentioned-above.

137 Since the deposited material along the channel usually is loose and has a grain shape, it can be



138 regarded as an infinite slope composed of cohesionless materials. Therefore, the critical pore pressure  
139 (Eq. 2) can be used to calculate the stability of the source area. Then pore pressure and rainfall  
140 monitoring sensors were installed in the Wenjia gully to capture the real-time data and put forward a  
141 comprehensive warning threshold for forecasting debris flow occurrence. The history events about  
142 rainfall with debris flow occurrences and non-occurrences have been collected for this study from  
143 2008 to 2018. Fortunately, three debris flow events with detailed rainfall and pore pressure monitoring  
144 data have been recorded, which could be an important evidence to prove the presented methodology.

145 **3.1 Data analysis**

146 Data were collected from the literature about the occurrence of debris flows in the Wenjia gully  
147 and from technical reports and documents presented by government agency. Since there is a large  
148 difference in debris flow frequency before and after the Wenchuan earthquake, only the data after  
149 quake were used for the analyses and set-up of an early warning system (Table 1). There was no debris  
150 flow events after 2014, so the rainfall data are omitted in the table.

151 Table 1. Primary rainfall events in the catchment of Wenjia gully (2008-2018), added from Xu (2010)

152 & Yu et al. (2012)

Time	Maximum hourly rainfall intensity (I <sub>h</sub> : mm/h)	Accumulated precipitation (R <sub>dt</sub> : mm)	Debris flow occurrence or not	Volume of debris flow (m <sup>3</sup> )
Sep. 24, 2008	30.5	88.0	Yes	5.0×10 <sup>5</sup>
Jul. 18, 2009	20.5	70.5	No	-
Aug. 25, 2009	28.9	86.7	No	-
Sep. 13, 2009	15.4	84.6	No	-
May 27, 2010	10.5	34.9	No	-
Jun. 13, 2010	5.5	95.1	No	-
Jul. 25, 2010	11.6	89.6	No	-
Jul. 31, 2010	51.7	60.2	Yes	1.0~2.0×10 <sup>5</sup>
<b>Aug. 13, 2010</b>	<b>70.6</b>	<b>185.0</b>	<b>Yes</b>	<b>4.5×10<sup>6</sup></b>
Aug. 19, 2010	31.9	72.6	Yes	3.0×10 <sup>5</sup>
Sep. 18, 2010	29.0	52.0	Yes	1.7×10 <sup>5</sup>
Sep. 22, 2010	24.5	81.2	No	-
May 2, 2011	5.6	35.8	No	-



Jul. 5, 2011	12.5	61.3	No	-
Jul. 21, 2011	23.5	63.2	No	-
Jul. 30, 2011	18.2	78.3	No	-
Aug. 16, 2011	10.5	44.3	No	-
Aug. 21, 2011	13.6	76.6	No	-
Sep. 7, 2011	15.2	51.3	No	-
Oct. 27, 2011	8.5	36.9	No	-
Jul. 21, 2012	30.5	76	No	-
Aug. 14, 2012	68	109	Yes	$3.2 \times 10^4$
Aug. 17, 2012	41	89.5	Yes	$7.8 \times 10^4$
Aug. 18, 2012	69	104.5	No	-
Sep. 16, 2012	12	44	No	-
Sep. 25, 2012	4.5	52	No	-
Jun. 19, 2013	33.5	62	No	-
Jun. 29, 2013	16.5	41.5	No	-
Jun. 30, 2013	40.5	94	No	-
Jul. 4, 2013	32	98	No	-
Jul. 8, 2013	53	195	Yes	$34.4 \times 10^4$
Jul. 10, 2014	51.5	67	No	-
Aug. 8, 2014	50.5	68.5	No	-
.....	.....	.....	.....	.....

153 Table 1 shows that the number of debris flows decreases with time, from 2008 to 2014. Several  
154 years after the earthquake, however, giant debris flows still caused catastrophic losses, which alarmed  
155 the public and government because of its huge destructive power and long-term impact. Particularly  
156 on Aug. 13, 2010, a great rainstorm lasting for 2 hours during midnight, triggered a giant debris flow,  
157 which buried the Qingping town in the Miayuan River floodplain. According to the inventory report,  
158 the maximum deposition height was up to 6 m. Most of the check dams located in the downstream part  
159 of the Wenjia gully collapsed and lost their effectiveness after passing of the debris flow. Meanwhile,  
160 it eroded the channel bottom over a depth of about 13 m (Yu et al. 2012).

161 Pore pressure and rainfall monitoring sensors have been installed for understanding their  
162 relationship, and the link with debris flow occurrence. The real-time monitoring system in the Wenjia  
163 gully includes 7 automatic rain gauges and 5 pore pressure monitoring instruments. The installation  
164 was finished by April 1, 2012 (see Table 2, Figure 3 and Figure 4). It can be seen that all rain gauges  
165 are arranged in the upstream part of the Wenjia gully catchment, while pore pressure monitoring

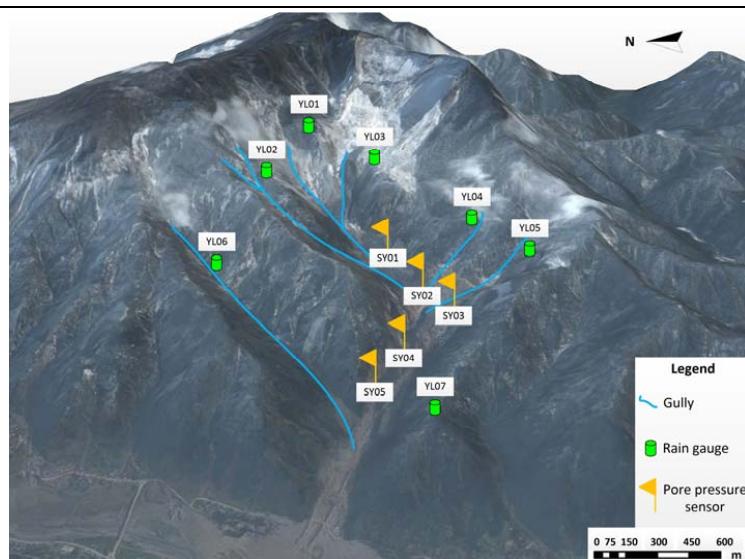


166 sensors are distributed along the mainstream of the Wenjia gully, with a depth of 1 m below the  
 167 ground surface.

168 Table 2. List of monitoring devices in the Wenjia gully

No.	Longitude	Latitude	Elevation(m)	Photo
YL01	E104°8'21"	N31°33'32"	1652	
YL02	E104°7'55"	N31°33'11"	1390	
YL03	E104°8'39"	N31°33'14"	1671	
YL04	E104°8'16"	N31°32'47"	1490	
YL05	E104°7'47"	N31°32'39"	1433	
YL06	E104°7'46"	N31°33'29"	1166	
YL07	E104°7'9"	N31°32'59"	1025	

SY01	E104°8'12"	N31°33'9"	1210	
SY02	E104°8'11"	N31°33'9"	1212	
SY03	E104°8'11"	N31°33'8"	1208	
SY04	E104°7'49"	N31°32'55"	1092	
SY05	E104°7'48"	N31°32'56"	1081	

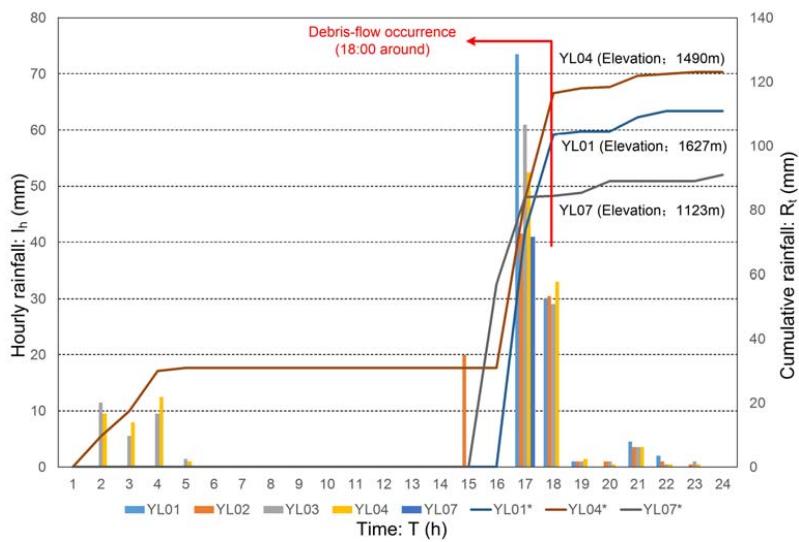


169  
 170 Fig. 4. Layout map of the monitoring devices installed in the Wenjia gully ( The base map is from Google Earth,  
 171 the date of background image is Dec. 18, 2010).

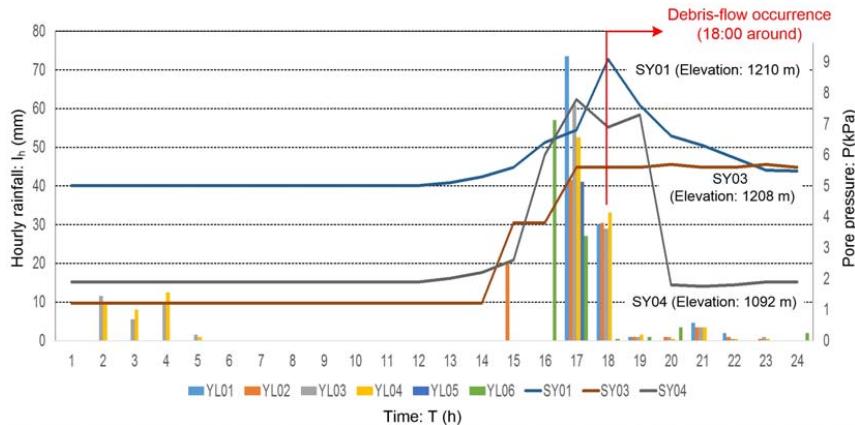
172 The 2012, heavy rainfall event on August 14, which triggered a debris flow has been caught totally



173 by the real-time monitoring system. During the rainstorm, monitoring sensors YL05, YL06 and SY02,  
174 SY05 lost the connection with the monitoring center. The other monitoring sensors worked well, as  
175 shown in Figure 5 and Figure 6. The figures show that the rainfall was almost concentrated in two  
176 hours from 17:00 until 19:00. The amount of precipitation was highly variable along the channel of the  
177 Wengjia gully. The maximum hourly rainfall intensity is 73.5 mm (YL01, 17:00), and the cumulative  
178 maximum rainfall is 118 mm (YL04). The receive frequency is every 5 minutes during the rainfall  
179 event, which is defined as the moment that hourly rainfall amount is more than 5 mm/h, and the end is  
180 when the hourly rainfall amount is less than 5 mm/h, and this should last for at least 6 h.



181  
182 Fig. 5. The rainfall in Wenjia gully on Aug. 14, 2012 (the column graphs are hourly rainfall and the single line  
183 curves are cumulative rainfall)  
184



185

186 Fig. 6. The rainfall and pore pressure in Wenjia gully on Aug. 14, 2012 (the column graphs are hourly rainfall  
187 and the single line curves are pore pressure)

188 The maximum hourly rainfall and cumulative rainfall are not found in the highest part of the  
189 catchment. The variety in cumulative maximum rainfall is larger than the variety in maximum hourly  
190 rainfall intensity. The Figure 6 shows the relation between hourly rainfall and pore pressure: the small  
191 amount of rain from 2:00 to 5:00 with a maximum hourly rainfall of 12.5 mm did not trigger any  
192 change in pore pressure. However, during the concentrated rain period between 15:00 and 18:00 there  
193 was a sudden rise of the pore pressure. The debris flow was triggered adjacently when it reached the  
194 maximum rise of the pore pressure. The highest value of the pore pressure are 9.01 kPa (SY01) at  
195 18:00, 5.7 kPa (SY03) at 20:00 and 7.8 kPa (SY04) at 17:00. The sudden rise of pore pressure,  
196 therefore may be a good indicator for contributing to the gully-type debris flows occurrence.

197 **3.2 Warning threshold for the Wenjia gully**

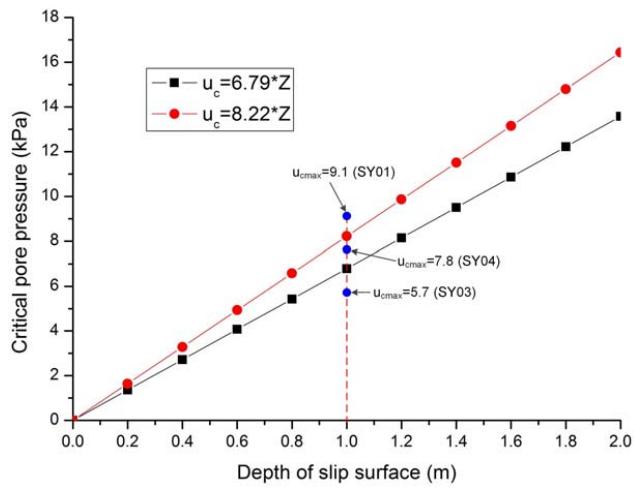
198 In order to improve the warning thresholds for forecasting the debris flow occurrence, which do  
199 not just represent a simple relationship between rainfall and debris flow occurrence, the pore pressure  
200 of landslide deposits was incorporated into the assessment of a threshold. Critical pore pressure for  
201 bed failure generating debris flows can be estimated with Eq.(2). The total unit weight of deposit  
202 material at 1300 platform in the Wenjia gully is around  $21 \pm 2 \text{ kN/m}^3$ , average slope inclination of  
203  $18.5^\circ$ , and average effective friction angle is  $27.5^\circ$  by consolidated undrained indoor test. Thus, the



204 critical pore pressure of the deposited material can be calculated by Eq. (3).

205 
$$u_c = (6.79 - 8.22) \times Z \quad (3)$$

206 Obviously, it's a linear function, as shown in Figure 7. According to the real-time monitoring  
 207 system, therefore, the critical pore pressure should be 6.79~8.22 kPa at the depth of 1 m below the  
 208 ground surface. According to Table 1, on Aug. 14, 2012, there was a debris flow with run-off volume  
 209 of  $3.2 \times 10^4 \text{ m}^3$ , and before the debris flow event pore pressure monitoring data show its maximum  
 210 value was up to 9.1 kPa (SY01), 7.8 kPa (SY04) and 5.7 kPa (SY03). Obviously, SY01 has already  
 211 exceeded the upper threshold of critical pore pressure (8.22 kPa), which means that the critical pore  
 212 pressure might be an important factor in debris flow occurrence.



213  
 214 Fig. 7. The critical pore pressure with probable depth of slip surface in the Wenjia gully

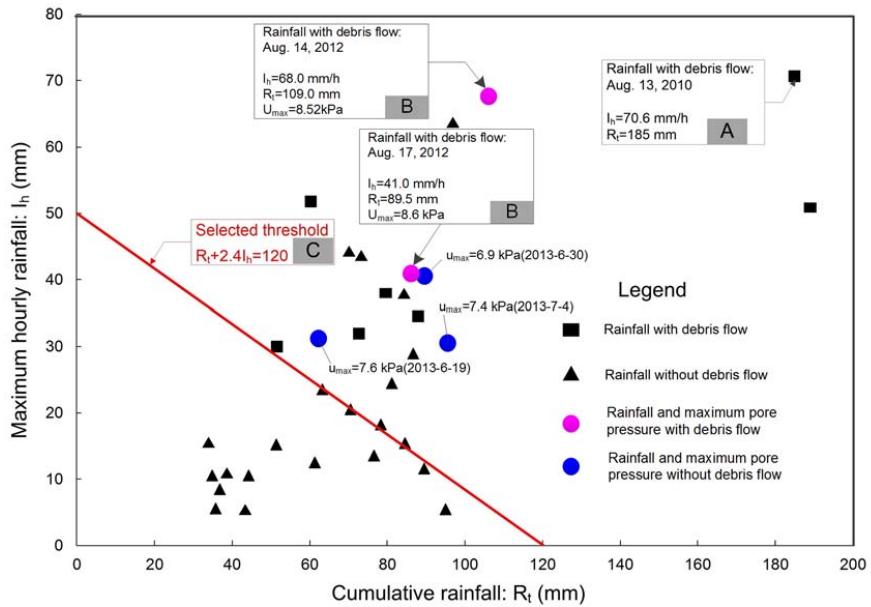
215 Considering the acquired available data, the maximum hourly rainfall ( $I_h$ : mm) and cumulative  
 216 rainfall ( $R_t$ : mm) are selected as the basic triggering rainfall parameters for the rainfall threshold, and  
 217 the critical pore pressure ( $u_c$ ) has been defined as an supporting factor in forecasting debris flow  
 218 occurrence. For each rainfall event with or without debris flow occurrence,  $R_t$  (Cumulative rainfall)  
 219 and  $I_h$  (Hourly intensity), can be plotted in a X-Y field, like the debris flow event on Aug. 13, 2010  
 220 (Figure 8 Tag A). The red line drawn under the lowest rectangle points which represent debris flow



221 occurrences under such rainfall conditions. The area between the line and the x and y axes defines  
 222 combinations of  $R_t$  and  $I_h$  with a zero probability of debris flow occurrence. The gradient is an  
 223 uncertain parameter which can be determined by experts' experiences and historical data sets (Huang  
 224 et al., 2015b). Then, the rainfall threshold can be defined by Eq. (4) in Figure 8 (Tag C).

225 
$$R_t + 2.4I_h = 120 \quad (4)$$

226 where  $R_t$  is the cumulative rainfall (mm),  $I_h$  is the maximum hourly rainfall (mm).



227  
 228 Fig. 8. Warning threshold combined with rainfall and pore pressure

229 While above the red line, the probability of debris flow occurrence is higher. But among these  
 230 points, there are 8 rectangular points with debris flow. The possibility of debris flow occurrence can be  
 231 predicted correctly up to 62% by rainfall threshold, which seems to be fine as a preliminary  
 232 assessment. If the pore pressure monitoring data has been considered, in Figure 8, there are three blue  
 233 circular points without debris flow, but two magenta points show debris flow happened. The different  
 234 between them is that maximum pore pressure has exceeded the critical pore pressure line (8.22 kPa).  
 235 Therefore, the rainfall threshold and pore pressure threshold need to be combined during forecasting



236 debris flow occurrence, then there must be a much higher possibility of successful prediction. For a  
237 given rainfall event, the starting point and its trend can be calculated and plotted in Figure 8. In order  
238 to verify in real time whether the trend line exceed the warning threshold. More detail information will  
239 be discussed with an example as follow.

240 **4. Example of application**

241 In order to make a better use for the presented method, early warning criteria have to be  
242 simplified to make a clear understanding for the study area. Therefore, a three-level early warning  
243 system has been proposed for the Wenjia gully, as shown in Table 3. At level one there is low  
244 possibility of debris flow occurrence. At level two there is a chance of debris flow occurrence in the  
245 near future, and warning messages need to be sent to local authority and countermeasures need to be  
246 discussed. At level three there is very likely to occur right now, therefore, local residents need to be  
247 alerted and forbidden going to the threatened places.

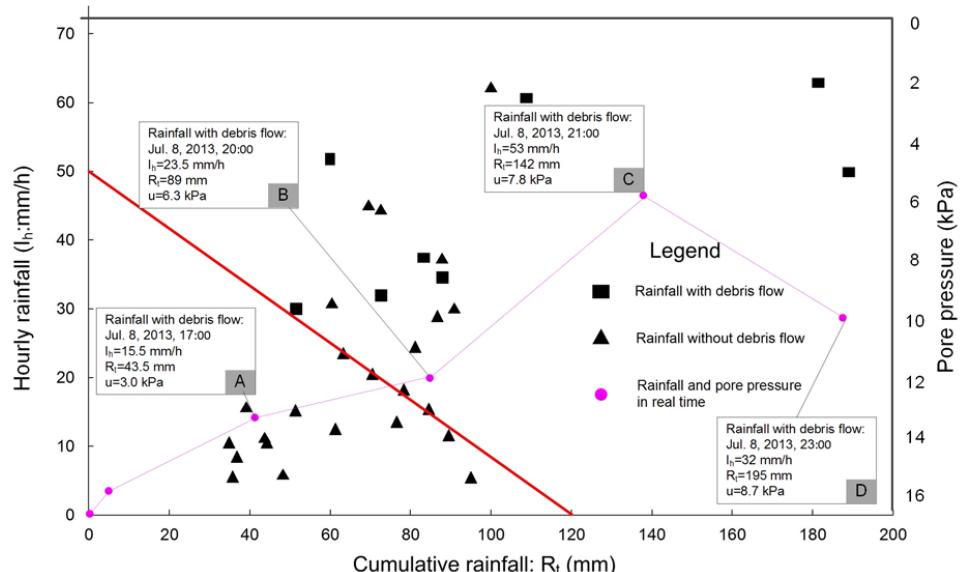
248 Table 3. Recommended warning levels for Wenjia gully

Warning level	Trigger	Response
I	Default level. Not exceeding rainfall threshold and critical pore pressure.	<b>Null:</b> but data are checked daily. Weekly monitoring bulletin.
II	Attention level. Exceeding rainfall threshold but critical pore pressure not.	<b>Watch:</b> data are checked more frequently. Daily monitoring bulletin. Authority and expert are alerted. Preparing for alarm.
III	Alert level. Exceeding both of rainfall threshold and critical pore pressure.	<b>Warning:</b> data are checked even more frequently. Two monitoring bulletins per day. Local people are alerted.

249 In order to explain how the presented method can be used in a real-time debris flow early warning  
250 case, the rainfall on Jul. 8, 2013 has been selected as an application (Figure 9). The small circular  
251 magenta solid points connected by a magenta line shows the course of the real-time monitored data  
252 during this rain storm, with the cumulative rainfall on the X axis and hourly rainfall intensity on the Y  
253 axis. The Tag A in Figure 9 shows the rainfall data at 17:00 on Jul. 8, 2013, with a pore pressure of  
254 3.00 kPa at that time. Three hours later at 20:00 (Tag B), the real-time rainfall has exceeded the



255 rainfall threshold, but the pore pressure didn't exceed the critical pore pressure ( $6.3 \text{ kPa} < 6.79 \text{ or}$   
 256  $8.22 \text{ kPa}$ ) indicating that the warning information stayed in level II. One hour later at 21:00 (Tag C),  
 257 the pore pressure did exceed the lower critical pore pressure ( $7.8 \text{ kPa} > 6.79 \text{ kPa}$ ) indicating that debris  
 258 flow had a much higher possibility to occur. Further, the pore pressure went up to  $8.7 \text{ kPa}$  over the  
 259 upper critical pore pressure ( $8.22 \text{ kPa}$ ), and triggered a debris flow occurrence finally (Tag D).



260

261

Fig. 9. Case application of the presented method in Wenjia gully (Jul. 8, 2013)

262

The case study shows that how to use this presented combined warning threshold in a real-time  
 263 way during a rain storm. In 2014, two heavy rainstorms (Table 1) both have exceeded the rainfall  
 264 threshold, but pore pressure did not cross the critical pore pressure during the whole course of the  
 265 rainfall. Therefore, a warning message has been sent to the local government with a median possibility  
 266 of debris flow occurrence. At last, fortunately no debris flow occurred during these rain storms.  
 267 Therefore, the presented comprehensive warning threshold can be used as a helpful tool for debris  
 268 flow prediction in mountainous area, especially in this earthquake area of Southwest China where a lot  
 269 of loose material is available.

## 270 5. Discussion and conclusion



271        Gully-type debris flow, usually triggered by high-intensity and short-duration rainstorms cause  
272        serious harm to human lives and properties every year in the mountainous region of Southwest China.  
273        Therefore, in order to prevent such natural disasters, there is an urgent requirement for an effective  
274        method to predict debris flow occurrence. The combined warning threshold proposed and discussed in  
275        this paper, not only use the common rainfall threshold, but also include the critical pore pressure  
276        determined by a hydro mechanical stability model.

277        Two rainfall triggering factors: maximum hourly rainfall and cumulative rainfall, have been  
278        selected to establish a simple rainfall threshold as a baseline for debris flow early warning. Critical  
279        pore pressure can be used as a combined threshold to make the warning threshold better in practical  
280        usage. The Wenjia gully was selected as a case study for a detailed explanation of the presented  
281        method, for the great volume of deposited materials triggered by Wenchuan earthquake along the  
282        channel. The results show that the combined threshold can play a great role in debris flow predicting,  
283        at least reduce the mistaken alerts for debris flow occurrence compared to use of only a rainfall  
284        threshold. However, such a combined warning threshold still has some restrictions. First, the critical  
285        pore pressure is a linear function with the depth of a potential slip surface, which is difficult to  
286        determine in an actual gully by the real time monitoring system. In this study, one meter depth of the  
287        slip surface was selected as a possible condition for this preliminary study. Second, the study area still  
288        focused on the Wenjia gully, therefore the presented method can't be used in another gullies directly.  
289        But in the near future, different gully-type debris flows will be researched, and more subsequent work  
290        need to be carried on for a better understanding of debris flow prediction. Finally, the most complex  
291        problem is the final determination whether to alert the local population, and whether some reactions  
292        need to be done immediately, or later. Debris flow early warning is not an imminent hazard but is just  
293        regarded as a potential danger. In spite of these limitations, the methodology presented in this paper  
294        has reached the goal to establish a preliminary combined warning threshold for gully-type debris flow



295 prediction. In the future studies, the critical pore pressure threshold which are dependent on  
296 topography, geology, and soil properties, can be determined by long-term field monitoring, and more  
297 important by debris flow tests in laboratory with different slope angles, and depths of slip surface to  
298 reduce the loss of properties and lives.

299

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