Response to review comments (Round #2)

Manuscript title: Flood risk assessment due to cyclone induced dike breaching on coastal areas of Bangladesh Manuscript Id: NHESS-2018-169 Authors: Md Feroz Islam, Biswa Bhattacharya, Ioana Popescu Submitted to NHESS Response Round#2 (December 2018)

RESPONSE TO EDITOR'S COMMENTS

Comment: Both reviewers have looked at the revised manuscript and find that it has considerably improved. However, they also provide a number of comments where they think that improvements are still necessary. I have looked as well at the manuscript and think that clarity and conciseness should further be improved. Moreover, I miss clarification about my earlier remark on the first version: "... It also needs to be very clear what the scientific contribution and innovation of the work is. Case studies can be published in nhess, however, it does not suffice to only apply established methods, so you should be very careful in pointing out what could be transferred, whether there are generic findings etc...." Please think about what this work could offer to the international audience of nhess that is not interested in your case study area, but could be interested in whether/how your insights and methods could be transferred to other area. It would be good to have a few thoughts/sentences in the introduction, discussion and/or conclusions chapters on the issues of scientific contribution and transferability.

Reply:

The authors appreciate your comments. We have updated the manuscript to reflect the applicability at other location so that the manuscript does not read like as a case study report.

Specific changes made to the manuscript are:

In Abstract (P 1, Line 25 to 30):

"The frequency and intensity of the cyclone around the world are likely to increase due to climate change which will require resource intensive improvement of existing or new protection works for the deltas. Identification and prioritising maintenance of critical location of dike breaching can potentially prevent a disaster. Non-structural tools such as land use zoning with the help of flood risk maps and probabilistic flood maps has the potential to reduce risk and damage. The method presented in this research can potentially be utilized for the deltas around the world to reduce vulnerability and flood risk due to dike breach cause by cyclone induced storm surge."

In Introduction (P3, Line 15 to 20):

"With the effect of climate change, the frequency and intensity of the cyclone around the world will increase. The protective structures for the deltas around the world will require adjustments which will be resource intensive. Non-structural tools such as land use zoning with the help of flood risk maps and

probabilistic flood maps has the potential to reduce risk and damage. Identification of critical location of breaching and intensifying the maintained effort for these locations can potentially prevent a disaster. Although coastal region of Bangladesh was selected as the case study area, the method presented in this research can be utilized for the vulnerable deltas around the world."

In Conclusion (P 24, Line 1 to 6):

"Climate change will likely cause increase in the frequency and intensity of the cyclone around the world. This will call for large investments for the improvement of existing or new protection works for the deltas. Identification and prioritising maintenance of critical locations of dike breaching can potentially prevent a disaster. Non-structural tools such as land use zoning with the help of flood risk maps and probabilistic flood maps have the potential to reduce the risk and the damage due to dike breaching. The method presented in this research can potentially be utilized for the deltas around the world to reduce vulnerability and flood risk due to dike breach caused by cyclone induced storm surges."

The authors are very thankful to the Editor for the valuable comments. Addressing the comments has helped us in improving the manuscript.

RESPONSE TO COMMENTS OF REVIEWER #1

Comment: Overview:

The paper has improved significantly in all of the three main points mentioned previously (message, methodology and English). This, along with the improved figures, gives the reader a much better understanding of the nature of the research. However, the problems with these areas have not been fully resolved. Despite the much improved manuscript, in my opinion these issues still require major revisions to the methodology and the message. However, methodological changes or extra data analyses are not necessarily needed to achieve a publishable article.

Reply: We are thankful to the reviewer for the appreciation and in the following we provide answers to the specific review comments.

Comment: General Comments:

The improvements from the previous manuscript, as well as the continued (or new) problems I observe in the 3 areas mentioned above are described below;

Methodology:

The methodology is much clearer in the second manuscript, and helped by the flowchart. However, there are 3 aspects that need to be addressed.

Reply: Specific replies are provided below against specific comments

Comment [Methodology, part 1]: The first is the differentiation between the 3 extreme scenarios the 72 scenarios. I previously suggested that a different name be given for these sets of scenarios, but this was not done, and it requires careful analysis for the reader to dissect this for themselves. The flowchart helps a little but it also causes more questions, which are listed in the specific comments below.

Reply: The authors apologise for not incorporating this suggestion in the previously revised manuscript. Figure 2 (shown below as well) has been updated now to incorporate this suggestion.

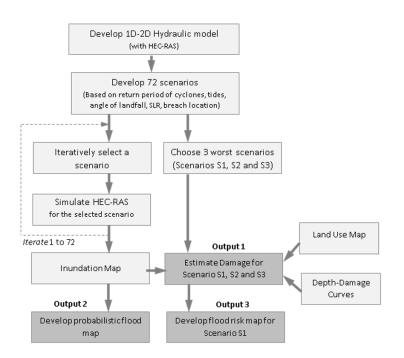


Figure 1: Methodological approach followed in this study.

It may be noted that the scenarios have been named as S1, S2 and S3. Subsequent discussion in the manuscript (for example, P 11, L9) have been modified to include the names of these three scenarios.

Comment [Methodology, part 2]: The second aspect is the fact that all the outputs relate to a 1:25yr event. Highlighting this more clearly would help the reader to understand the context of the research in terms of a wider flood risk analysis for the region, (see comments on message, below). A serious problem not addressed with the results of this calculation event is that the authors do not define for which temporal period risks are applicable. For example, if the results represent the current risk, then of the 72 simulations, those simulations with future SLR should not be included. For the risk in 2100 (the date at which the SLR value is predicted to happen), the simulations with current sea level should not be used. Furthermore, subsidence over time was accounted for to estimate the current topography, but not future topography. This is briefly mentioned in the conclusions, but not the significance for the results are not.

Reply:

[Part a, 1:25-year event] Authors appreciate the suggestions and we have updated the manuscript to reflect this aspect. As shown below we have included this explanation in the introduction, discussion and conclusions sections.

<u>*P 1, Line 15:*</u> "Storm surge for a cyclone event of 1 in 25 return period was considered for all the scenarios."

<u>*P 2, Line 17 and 18:*</u> "A storm surge event of 25 year return period was considered in this study for the generation of different scenarios."

P 3, Line 14 and 15: "A cyclone event of 25 year return period was considered in this research."

Furthermore, the following explanation on the results of scenarios with and without the climate change (sea level rise) impact have been added.

<u>*P* 11, Line 12 to 13:</u> "As the storm surge height suggested by Islam et al. (2013) corresponds to an event of 25 year return period, the PFM generated in this study corresponds to 1 in 25 year return period."

[Part b, temporal period]

This is indeed an important point and we have added the following explanation in the discussion chapter:

<u>*P 2, Line 22 to 27:*</u> "The scenarios with the effect of climate change (sea level rise) had more damage compared to the scenarios without climate change. Scenarios S1, S2 and S3 were associated with the highest storm surge height. With the same set of conditions without climate change (sea level rise) the storm surge height was 6.52 m PWD (Table 2). The damage corresponding to breaching of eastern, central and western locations of the dike due to the storm surge without climate change impact were 23.3%, 20.5% and 21.7% respectively lower than the damages with the climate change. The corresponding values for the flood extent were 30.1%, 21.67% and 27.21% respectively lower than the flood extent areas with the climate change impact."

<u>P 22, Line 29 and 30:</u>

"The scenarios considering the effect of climate change (sea level rise) indicated that the flood extent and damage due to flood will increase with sea level rise."

[Part c, subsidence]

This indeed is an important point and it has been explained with the following text (P5, Line 13 to L 17):

"The same DEM was used for the simulations of the year 2100 without any corrections for further subsidence. Subsidence of the coast in the past has been reported by Brown and Nicholls (2015) and was verified with the survey data from IWM and FINMAP. Subsidence in the future may continue but in the absence of scientific studies it was not considered for the future scenarios in this research. It is noteworthy that if subsidence continues then the effect of the SLR may be increased and the results reported in this research should be treated as to some extent under-estimated values."

Comment [Methodology, part 3]: Finally the 1D modelling explanation needs to be improved, especially in terms of boundary conditions. Please see the specific comments below.

"The primary objective of the research was to present a methodology for generating FRM and PFM for the breaching of dike during a cyclone". This line from the conclusion should have similar versions in the abstract and introduction, and in the opinion of this reviewer, should

shape the overall message of the paper. It is also closer to the title of the paper. Instead the abstract and introduction sections describe the paper as "an investigation of the inundation pattern in a protected area", which is an interesting case-study, but not innovative or of interest to a general audience. For example, a line of logic for the introduction could be;

- Bangladesh is susceptible to cyclones;
- Damage estimates and flood maps, as well the identification of critical breaching locations, are useful for mitigating risk
- Quantifying this data requires taking account of SLR, cyclone frequency etc. and potential for breaching.
- A method to do so for the 1:25yr event (design criteria), for a particular polder, is given below.

Then, as well as the specific results, the applicability of the method to other areas and return period events could be estimated.

Reply: We appreciate this excellent suggestion and we have updated the manuscript to incorporate the suggestions. The specific changes in the manuscript are described below:

Abstract, <u>P 1, Line 16 and 17:</u> "The primary objective of this research was to present a methodology for identifying the critical location of dike breach, generating flood risk map (FRM) and probabilistic flood map (PFM) for the breaching of dike during a cyclone."

Introduction, <u>*P* 2, *Line* 22 *to* 27: "The coast of Bangladesh is frequently hit by severe cyclones (5 cyclones between 1995 and 2010, Dasgupta et al., 2014). Bangladesh Water Development Board (BWDB) is responsible for the operation and maintenance of these dikes and lacks fund to conduct proper repairing of damaged dikes subsequent to any severe cyclone. As a result the dykes remain vulnerable to breaching. Identifying the critical location(s) of dike breach and prioritising the repairing of the critical location is likely to reduce the breaching possibility."</u>

<u>*P 3, Line 10 to 12:*</u> "This paper presents a methodology to identify the critical location of dike breach due to cyclones, generate flood risk map (FRM) and probabilistic flood map (PFM) due to breaching of the dike by cyclone induced storm surges."

<u>*P 3, Line 13 and 14:*</u> "A cyclone event of 25 year return period was considered in this research. A coastal polder (Polder 48) of southern Bangladesh was selected as the study area."

Comment: English:

This has improved significantly, but again, continued errors distract the reader, especially in the conclusion. The paper cannot be accepted with so many mistakes, and it is strongly suggested to ensure they are removed before resubmission.

Reply: We have worked on improving the English of the manuscript, especially of the conclusions section. To the best of our understanding the language is now consistent across the manuscript.

Specific Comments:

Comment: Abstract

P1, Line 14: "Scenarios were developed by considering... geometrical properties of the breach, breach propagation time...". This line directly conflicts with P8, Line12: "As the geometry of the breach is not independent, it was not considered as a parameter for scenario development". This was highlighted previously and needs to be resolved.

Reply: Thank you for pointing it out and we have updated manuscript as follows: P 1, Line 13 to 15):

"Scenarios were developed by considering tidal variations, angle of cyclone at landfall, possible dike breach locations, geometrical properties of the breach, breach propagation time and the sea level rise due to climate change according to the fifth assessment report (AR5) of Intergovernmental Panel on Climate Change (IPCC)."

Comment: Introduction

P2, Line 26: "Furthermore, by the year 2100 the annual estimated damage due to tropical cyclones may increase by US\$53 billion" This is surely due to the reasons the authors mention previously, and therefore not 'furthermore'.

Reply: Authors acknowledge the suggestion and the manuscript is adjusted accordingly.

<u>*P 3, Line 5 and 6:*</u> "By the year 2100 the annual estimated damage due to tropical cyclones may increase by US\$53 billion"

Comment: P2, Line 26: "study area is not benefitted with..." This sounds strange.

Reply: Authors acknowledge the suggestion and the manuscript is adjusted accordingly (P 3, Line 7):

"At present, flood forecasting system is not available for the coastal region of Bangladesh."

Comment: Study Area

P3: Lines 9-13: This part seems just like a list of data, and doesn't connect well, consider revising.

Reply: We have updated the manuscript based on this suggestion (P 3, Line 29 to P 4 Line 2):

"Climate and agricultural practices of Kuakata is similar to the climate and agricultural practices of the country (Bangladesh). The average yearly rainfall in Kuakata is 2590mm (Climate-Data, 2016) and the annual average temperature is 25.9°C (Climate-Data, 2016). Rabi (November to February), Kharif-I (March to May) and Kharif-II (June to October) are the three seasons for growing crops (DAE, 2009). The elevation

of 80% of the area is 1.55m PWD, the vertical datum established by Public Works Department of Bangladesh, which is 0.46m below the MSL."

Comment: P4, figure 1: Please plot the extent of the dike on this map or on figure 3, as you mention it is only on the seaward side. Including the chainage points given in Figure 6 would also be useful.

Reply: Thank you for the suggestion. As stated earlier in the section, study area (polder 48) is surrounded by dikes, the line denoting the study area also denotes the alignment of the dikes. This information is added to the manuscript to increase clarity. Chainage points and the extent of the dike for the area are added in the figure 3 (shown below as well).

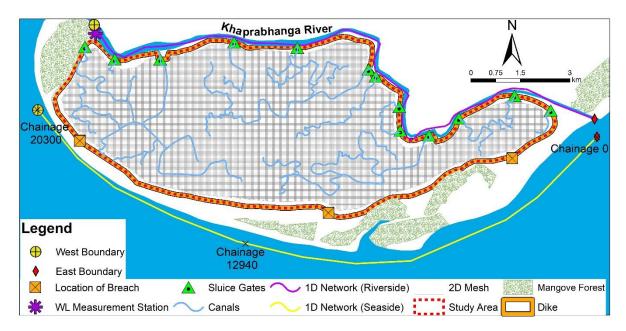


Figure 2: Schematic diagram of the study area with location of control structures and gauges and the considered breach locations.

Comment: Methodology

Comment: P5, figure 2: The arrow from HEC-RAS to 'Estimate damage' during a loop is confusing. The output of 72 simulations from the loop should be used.

Reply: Authors thank the reviewer for the suggestion. The flow chart has been adjusted (Figure 2, page 5).

Comment: P5, figure 2: Perhaps the damage and maps sections could be highlighted as outputs.

Reply: The flow chart has been adjusted following the suggestion indicating the estimated damage, probabilistic flood map and flood risk map as Output 1, 2 and 3 (Figure 2, page 5) respectively.

Comment: P6, line 5: I don't think the HEC-Ras description here needs to be so detailed. In fact this whole paragraph should be reviewed for structure and cohesion.

Reply: The description of HEC-RAS was adjusted following the suggestion of the reviewer (P 6, Line 9 to 13):

"The river analysis tool HEC-RAS (version 5.0) from the US Army Corps of Engineers was used to develop the 1D-2D coupled inundation model. The flow in the river was modelled in 1D whereas the flow over the floodplain was modelled in 2D. HEC-RAS 5.0 is a free tool which can simulate 1D, 2D and 1D-2D coupled models for steady and unsteady flow. The 2D module of HEC-RAS provides option to simulate flow of water either with the diffusion wave equation or with the full shallow water equation (St. Venant equation). The availability of irregular flexible mesh in HEC-RAS and the option for faster simulations led to the selection of HEC-RAS 5.0 as the modelling tool."

Comment: P7, line 3-5: The English is poor here, and it is unclear. Are all cells rectangular? How can they have a single resolution or area? This is made more confusing by the grid representation in the figure.

Reply: Thank you for pointing this out. Authors acknowledge the suggestion and the manuscript was adjusted accordingly.

<u>*P* 7, Line 6 to 7:</u> "The rectangular cells of the developed 2D mesh had a resolution of 25 m and the non-rectangular cells had areas ranging from 625 square meters to 1282 square meters."

Comment: P7: Figure 3: Presumably Khaprabhanga is more of a channel than a river, as it seems to connect two parts of the Bay of Bengal. If this is the case it should be mentioned.

Reply: Khaprabhanga River is connected to Galachipa River on the east and Andharmanik River on the west. This is shown in Fig. 1.

Comment: P7: Figure 3: How are the upstream and downstream locations selected? Presumably it is because it is assumed a cyclone always come from the west and therefore imposes a water level downstream, but this is never stated.

If I am correct in this assumption of a water level timeseries as the main driver in the model, why wasn't a QH relationship used at the other end? This raises a number of questions about the water level profile along the seafront.

Why was the Khaprabhanga included at all? No breaches occurred at that end, and it is not connected to the other 1D part.

Reply:

We have updated Fig 3 to show western and eastern boundary instead of upstream and downstream boundary.

It was considered that the water level will be similar at all boundary locations. The upstream and downstream terminology was used to denote different boundary locations only. Authors agree that a simple terminology as boundary locations would have been enough.

Khapravabhga River was added to the model to make sure the results are similar to what happened during the cyclone Sidr when the dikes on the river side did not overtop or breached. The 1D network representing Khaprabhanga River was connected to the 2D model through lateral structures representing the dikes on the river side. The simulation of the storm surges during cyclone Sidr indicated that the dikes on the river side did not overtop indeed.

Comment: P7, line 16: Mangrove ForestS.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

<u>P 7, Line 18:</u>

"The western and eastern side of the embankment have Mangrove Forests between the rivers and the embankment"

Comment: P7: Line 17: "The storm surges..." English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

Comment: P8: Line 8: "...therefore, the wider and larger canals were included in the DEM". This sounds like the canals were 'burnt' into the DEM, which I understand was not the case.

Reply: Indeed, the canals were not burned in the DEM. The DEM was generated from the land level survey points provided by IWM. These points included the points on the canals with bed level.

Comment: P8: Line 8: "As the geometry of the breach is not independent, it was not considered as a parameter for scenario development". As mentioned above this is contradicts another statement. Also, the geometry is independent of the water levels, the failure is not.

Reply: Authors thanks the reviewer for pointing this out. Authors acknowledge the suggestion and the manuscript was adjusted accordingly.

<u>P 1, Line 13 to 15:</u>

"Scenarios were developed by considering tidal variations, angle of cyclone at landfall, possible dike breach locations, geometrical properties of the breach, breach propagation time and the sea level rise due to climate change according to the fifth assessment report (AR5) of Intergovernmental Panel on Climate Change (IPCC)."

Comment: P9, figure 6: Why is the middle chainage higher than the others during the rising limb? This raises more questions about the boundary conditions.

Reply: Thank you for the query. But the authors failed to identify significant difference in water levels at the three chainage presented in figure 6.

Comment: P10, Line 13: The 1:25yr design criteria should be mentioned in the abstract and introduction, as it dictates the method and outputs.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

<u>P 1, Line 15:</u>

"Storm surge for a cyclone event of 1 in 25 return period was considered for all the scenarios."

<u>P 2, Line 17 and 18:</u>

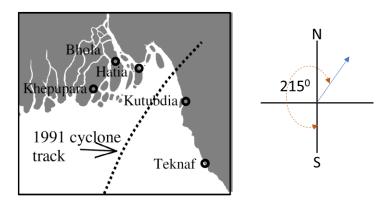
"A storm surge event of 25 year return period was considered in this study for the generation of different scenarios."

<u>P 3, Line 14 and 15:</u>

"A cyclone event of 25 year return period was considered for this research."

Comment: P10, line 18: from which direction is the angle measured, i.e. does angle of landfall of 230 degress indicate a cyclone moving from South to North? Apologies if this is an obvious question, but I am not hugely familiar cyclones.

Reply: It is measured from the south. The effect of the angle of landfall of the cyclone was studied by Azam et al., 2004. To illustrate how they defined the angle of landfall an example is provided below. In their article they defined the angle for the cyclone of 1991 shown in figure below as "During landfall, the cyclone made an angle of 215°".



Azam, M.H., Samad, M.A. and Mahboob-Ul-Kabir, 2004. Effect of cyclone track and landfall angle on the magnitude of storm surges along the coast of Bangladesh in the northern Bay of Bengal. *Coastal engineering journal*, 46(03), pp.269-290.

Comment: P10, Line 34: "Single breach was considered for each scenario". English.

Also, perhaps the authors can suggest the consequences of the assumption of 1 breach for a 1/25yr storm. Is 1 an over or under estimate? How many breaches have been recorded before?

Reply: There are reports of dike breaching during a cyclone but no database is available for the location and number of the breach. Therefore, it is difficult to state if 1 breach is an underestimation or over estimation.

Comment: P11, line 8; English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

Comment: P11, line 10; It is important to clearly identify what the maps and outputs represent. For example the PFMS are probabilistic inundations maps for a single event (1/25yr) in which a breach occurs.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

<u>P 11, Line 12 to 13:</u>

"As the storm surge height suggested by Islam et al. (2013) corresponds to an event of 25 year return period, the PFM generated in this study corresponds to 1 in 25 year return period."

Comment: P12, line 23; The fact that you do not account for duration or velocity of inundation should be mentioned, especially if highlighting their importance.

Reply: The manuscript is adjusted following your suggestion.

<u>P 12, Line 29 and 30:</u>

"The simplified (with regards to flow velocity and flood duration) depth-damage curve for rice fields suggested by Chau et al. (2014)"

Comment: P14, line 2. English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

Comment: P14, line 7; "Pfj is the probability of reaching a certain storm surge level in simulation number j". Is each Pfj will be equal to 1/25 here? As mentioned I think it is important to specify these results relate to the 1/25yr level.

Reply: Authors thank the reviewer for the suggestion. Following the suggestion made by the reviewer in the previous comment the manuscript was adjusted accordingly.

<u>P 11, Line 12 to 13:</u>

"As the storm surge height suggested by Islam et al. (2013) corresponds to an event of 25 year return period, the PFM generated in this study corresponds to 1 in 25 year return period."

Comment: Results and Discussion

P15, line 6: "...for identifying the critical location of breaching". This could be confused as a process to identify locations for the modelling process. Consider revising, and/or changing to 'regions'.

Reply: Authors' intention was to represent a method for comparing the results due to breaching and identify the most critical location of the dike for breaching. If these are identified and strengthened, then damage due to storm surges can be reduced significantly.

Comment: P16, figure 9: Presumably these figures are averages of subsets of the 72 simulations, This should be indicated in the text.

Reply: figure 9 represented the flood extents of different scenarios considering the breaching at central part of the sea facing dike. The title of the figure was adjusted as "Comparison of flooded areas corresponding to different Scenarios considering the breaching at central part of the sea facing dike." to provide more clarity.

Comment: P16, line 3: Now the authors move back to the subset of 3 scenarios. I find this hard to follow, especially since the names 'scenarios 1,2, and 3' do not relate to any cardinal numbers, but to breach locations on the west, centre and east.

Reply: Details about scenarios are presented in section "Cyclonic scenarios considered". Table 3 (Page 16) and Table 4 (Page 17) were adjusted for more clarity by adding western, central and eastern part to indicate which part of the dike was considered for breaching.

Comment: P18, figure 11: This figure and figure 10 need clarification. Can I infer from them that the area in which the maximum flood depth was less than 0.1m in scenario 1 (western breach) had an inundation of just above 2km2, which causes about 400,000 euros of damage? I see this is later explained in the discussion, but the authors might consider a clearer explanation at this point too.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

<u>P 18, Line 2 and 3:</u>

"Figure 10 and Figure 11 corresponds to the flooded area and damage due to different range of inundation depth respectively. The flood area and damage was highest for the inundation depth of 0.5 m to 1.0 m."

Comment: P18, line 3: Section 4.5 describes how the western breach was selected as the critical location, but you should mention that result here, as the flood map is clearly dependent on that. Perhaps it should also be plotted in figure 12 as well.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

<u>P 18, Line 5 and 6:</u>

"Comparison of flooded area and damage due to flood for the three worst case scenarios lead to the identification of Scenario S1 as the critical location of breaching."

Comment: P19, line 8; "This arbitrary threshold...". It has just been explained that the threshold is not arbitrary.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

<u>P 19, Line 8:</u>

"This threshold was used in developing the PMFs."

Comment: P19, line 8; "...and the estimation of damage due to flood was not affected". I don't understand this sentence at all.

Reply: Authors thanks the reviewer for pointing this out. The sentence indeed required more clarification and it was adjusted to provide clearer message.

<u>*P* 19, Line 8 and 9:</u> "This threshold was not considered while the estimation of damage due to flood was conducted."

Comment: P20, figure 13: Again I think it should be mentioned that this is the 1/25yr PFM.

Reply: Following the previous suggestion, the manuscript was adjusted.

<u>P 11, Line 12 to 13:</u>

"As the storm surge height suggested by Islam et al. (2013) corresponds to an event of 25 year return period, the PFM generated in this study corresponds to 1 in 25 year return period."

Comment: P20, line2: "Three worst case scenarios (Scenario 1, 2 and 3)..." Again there is confusion about these scenarios. They are not the 3 worst case scenarios, they are the worst case scenarios in terms of boundary conditions for each of the 3 potential breach locations.

Reply: Thank you for the suggestion and the manuscript is adjusted accordingly.

<u>P 11, Line 2 to 4:</u>

"The highest storm surge height as the boundary condition with breaching at the western, central and eastern parts of the dike were considered as the worst case scenarios and were denoted as Scenario S1, S2 and S3 respectively."

Comment: P20, line 3: "demonstrate that large area is flooded...". English

Reply: Authors thanks the reviewer, acknowledge the suggestion and manuscript adjusted accordingly

Comment: P20, line 4: The text references figure 9, which relates to all 72 simulations, as I understand. This is in the middle of text about the 3 extreme scenarios, and further highlights the issue already mentioned.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

<u>P 20, Line 2 to 4:</u>

"The flood extent for the simulated result of 72 scenarios were compared. Flood extent varies for different scenarios with different conditions such as the daily (high and low tide) and biweekly (spring and neap tide) tidal variation, sea level rise and angle of landfall."

Comment: P20, line 5: "More than 25% of the total area of Polder 48 was inundated for the three scenarios...". Please make this sentence clearer, I understand it to mean 'At least 25% of the total area of Poder 48 was inundated in all 3 extreme scenarios"

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

<u>P 20, Line 7:</u>

"At least 25% of the total area of Polder 48 was inundated for the three scenarios"

Comment: P20, line 10. It is not quite correct to say the risk is X million euro. Firstly it needs to be defined as a value per year or per event. Secondly these values are only the extreme versions of the 1/25yr event defined.

Reply: Authors agree with the reviewer that the risk should not be defined in "X million euros". However, the line states the damage due to flood, not the flood risk.

Comment: P21, line 8: English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

Comment: P21, line 10: "due to breaching of unprotected location of the dike". English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

Comment: P21, line12: "Scenario 1 had higher risk of flooding as the damage due to flooding was maximum for Scenario 1". This sounds strange, consider revising.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

<u>P 21, Line 15 and 16:</u>

"The damage due to flooding was maximum for Scenario S1 which results in higher risk of flooding for scenario S1."

Comment: Conclusion

P22, line 1: "investigate inundation pattern in a polder". English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

Comment: P22, line 2: "were compared using total flooded area and estimated damage". For which scenario set? 72 or 3?

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

<u>P 22, Line 14 to 16:</u>

"Different scenarios were formulated and simulated using a 1D-2D coupled model. The results of these simulations were used to calculate the total flooded area and damage due to flooding. Simulated results of three worst case scenarios S1, S2 and S3 were compared based on the total flooded area and estimated damage."

Comment: P22, line 5: "Flood risk map and probabilistic flood map...". English. These mistakes are very distracting.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly

Comment: P22, line 8: "during the breaching of central part of the sea facing dike". It doesn't happen during the breaching.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

<u>P 22, Line 20 and 21:</u>

"Flood inundation for the three worst case scenarios S1, S2 and S3 indicated that the maximum flooded area was obtained corresponding to the breaching of the central part of the sea facing dike."

Comment: P23, line 8: "Most flooded area had flood depth of 0.1 to 0.5 m...". English.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

Comment: P22, line 20: "...are least and most probable land use respectively". This sounds strange.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

<u>P 23, Line 5 and 6:</u>

"Inundation maps of all 72 scenarios were compared to generate the probabilistic flood map, which indicated that the areas with rice fields are the least and the settlements are the most probable areas to be flooded."

Comment: P22, line 24: This is the first mention of 'synthetic water level time series'. It is clear from the bottom of figure 6 that they are present, but not how they were generated.

Reply: The water levels presented in Figure 6 are result of having synthetic water level time series at the boundaries of the model. Unfortunately, measured water level during a cyclone was not available. The time series boundary file with the storm surge height considered for the 72 scenarios were generated following the measured tidal water level pattern. The following was added to clarify:

<u>P 8, Line 3 and 4:</u>

"The synthetic water level data for boundaries of the model were generated by following the tidal water level pattern and the storm surge height considered for the all scenarios."

Comment: P22, line 27:" This stresses the importance of field observation pre, post and during event". I don' see what actually stresses this importance.

Reply: Authors intended to state that due to lack of field observation, calibration and validation was difficult. Field observation will assist in future studies.

Comment: P22, line 30: "Comprehensive survey should be conducted...". English.

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

Comment: P22, line 33 "...a join probability" English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

Comment: P23, line 1: "Single breach was considered for all the developed Scenarios". English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

Comment: P23, line 2: "...should be studies as well". English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

Comment: P23, line 7: "Conducting field survey to generate these curves..." English

Reply: Authors acknowledge the suggestion and manuscript adjusted accordingly.

The authors are very thankful to the reviewer for the valuable comments. Addressing the comments has tremendously helped us in improving the manuscript.

REVIEW COMMENTS OF REVIEWER #2

Second review of manuscript: "Flood risk assessment due to cyclone induced dike breaching on coastal areas of Bangladesh".

Comment: Overview and general remarks

The second version of the manuscript is better than the first one. The authors put obvious effort in editing the text after the referee's comments and suggestions. There are significant improvements in the Methods and Discussion/Conclusions section in terms of the content required for the study and readability. The Figures and Tables are clear. Most of language mistakes are corrected. Nevertheless, there are some improvements should be done, mostly related to refining some description in the Methods and Conclusion sections, missing/wrong reference and language. Therefore, I suggest to return the manuscript for minor revisions.

Reply: We are thankful to the reviewer for the appreciation and in the following we provide answers to the specific review comments.

Comment: Specific remarks

Figure 12 and 13 miss a scale bar.

Reply: Authors acknowledge the suggestion and the figures were adjusted accordingly. The adjusted figures are presented below:

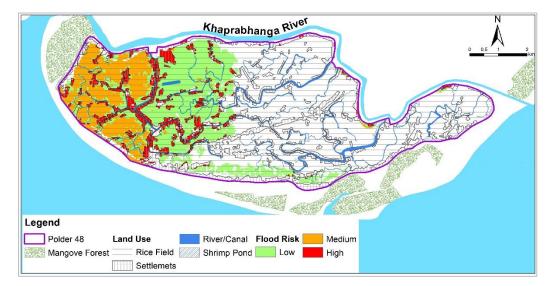


Figure 12: Flood risk map corresponding to the dike breach at the critical location of the dike. The following three classes of risk are shown: high, medium and low. The considered four landuses are shown as well.

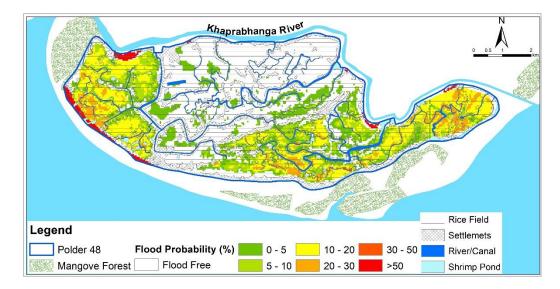


Figure 13: Probabilistic flood map of the study area. Varying colours indicate probabilities of obtaining flood depths more than 0.5m.

Comment: p.2 line 10. Were *recently* designed.

Reply: Thank you for pointing it out. The manuscript was adjusted accordingly.

<u>P 2, Line 16:</u>

"Crest levels of the coastal dikes were recently designed for an event of 25 year return period"

Comment: p.2 line 20. The intensity of tropical cyclones is *likely* to increase.

Reply: The line was adjusted as "Furthermore, the intensity and frequency of these tropical cyclones are likely to increase in the future due to climate change." (Page 2, Line 32)

Comment: p.3 line 7. The land use is mainly this sentence needs to be rephrased.

Reply: The line was adjusted as "The land use is classified by the Ministry of Land, Bangladesh into the following four classes: rice fields, settlements, shrimp ponds and water bodies (river/canal)". (Page 3, Line 28 and 29)

Comment: p.5 line 8. ...(a company from Finland). In my opinion this information is unnecessary.

Reply: Thank you for the suggestion and adjusted accordingly by removing the redundant information. (Page 5, Line 8)

Comment: p.6 line 1. As was pointed out in the previous round of reviews, "model development" brings ambiguity to what is described. In the majority of cases "model development" means you worked and modified the source code of HEC-Ras in a certain way, if this was not the case I would recommend to change it to "set-up" or "build".

Reply: Authors' acknowledge the suggestion for clarity and manuscript is adjusted accordingly by stating as "Setting up of 1D-2D coupled model".

Comment: p.6 line 7. "Computationally efficient" needs references on other studies which prove the point.

Reply: Authors' thanks the reviewer for the suggestion and line has been removed.

Comment: p.12 line 18. Information missing on satellite image source and the way it was processed.

Reply: Authors' acknowledge the suggestion for clarity and manuscript is adjusted accordingly.

Page 12, Line 22 to 24:

"Satellite image from google earth was used for analysis. The satellite image of the area was downloaded and georeferenced. Then, the areas for buildings and open areas for households were manually calculated using ARCGIS."

Comment: p.12 line 25. "However, when the flood level ..."

Reply: Thank you for the suggestion and the line was adjusted accordingly following reviewer's suggestion. (Page 12, Line 32)

Comment: p.12 line 30. "Further research ..." such statements should be moved to the Conclusion section.

Reply: Authors' acknowledge the suggestion for clarity and manuscript is adjusted accordingly by removing the statement.

Comment: p.13 line 8. The reference (Helm, 1996) doesn't belong to the statement. The study of Helm gives the definition of the risk used in this manuscript at line 11. Klijn (2009) and Van

Manen and Brinkhuis (2005) used already existing definitions for their research. This has to be corrected.

Reply: Authors' acknowledge the suggestion and manuscript is adjusted accordingly by adjusting the references following the reviewer's suggestion (Page 13, Line 11 and Line 15)

Comment: p.14 line 27. The indicator of error has to be specified.

Reply: The line was adjusted as "The difference between the reported and the simulated flood depth was 4.5%" (Page 14, Line 29).

Comment: p.20 line 17. "poor" is a rather vague definition, some numbers or indicators would bring more clarity.

Reply: Authors' acknowledge the suggestion and manuscript is adjusted accordingly with numbers and references. (Page 21, Line 1 and 2).

Comment: p. 21 line 2. "risky" is recommended to be removed.

Reply: Authors' acknowledge the suggestion and manuscript is adjusted accordingly by adjusting the sentence as "Fishing in the coastal region of Bangladesh as it yields lower economic returns leading to enhanced poverty". (Page 21, Line 5 and 6).

Comment: p.22 line 20. "Probabilistic flood maps..." is not clear, recommended to be rephrased.

Reply: The line was adjusted as "Inundation maps of all 72 scenarios were compared to generate the probabilistic flood map, which indicated that the areas with rice fields are the least and the settlements are the most probable areas to be flooded." (Page 23, Line 5 and 6)

Comment: p.23 line 5 "..., the data provided..." this part of sentence should be rephrased.

Reply: Authors' acknowledge the suggestion and manuscript is adjusted accordingly as "Bathymetric data with coarse grid resolution from GEBCO was used as the measured bathymetric data for the sea was not available." (Page 23, Line 23 and 24).

The authors are very thankful to the reviewer for the valuable comments. Addressing the comments has tremendously helped us in improving the manuscript.

Flood risk assessment due to cyclone induced dike breaching on coastal areas of Bangladesh

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Abstract. Bangladesh, one of the most disaster-prone countries in the world, has a dynamic delta with 123 polders protected by earthen dikes. Cyclone induced storm surges cause severe damages to these polders by overtopping and breaching of dikes. Nineteen major tropical storms hit the coast in last 50 years and the storm frequency is likely to increase due to climate change.

- 10 The present paper presents an investigation of the inundation pattern in a protected area behind dikes due to floods caused by storm surges and identifies possible critical locations of dike breaches. Polder 48 in the coastal region, also known as Kuakata, was selected as the study area. A HEC-RAS 1D-2D hydrodynamic model was developed to simulate inundation in the polder under different scenarios. Scenarios were developed by considering tidal variations, angle of cyclone at landfall, possible dike breach locations, geometrical properties of the breach, breach propagation time and the sea level rise due to climate change
- 15 according to the fifth assessment report (AR5) of Intergovernmental Panel on Climate Change (IPCC). Storm surge for a cyclone event of 1 in 25 year return period was considered for all the scenarios. The primary objective of thise research was to present a methodology for identifying the critical location of dike breach, generating flood risk map (FRM) and probabilistic flood map (PFM) for the breaching of dike during a cyclone. The critical location of the dike breach among the chosen possible locations was identified by comparing the inundation extent and damage due to flood corresponding to the developed scenarios.
- A flood risk map (FRM) corresponding to the breaching at the critical location was developed, which indicated that settlements 20 adjacent to the canals in the polders were exposed to higher risk. A- probabilistic flood map (PFM) was developed using the simulation results corresponding to- the developed scenarios, which was used to recommend the need of appropriate land use zoning to minimize the vulnerability to flooding. The developed hydrodynamic model can be used to forecast-inundation, to identify critical locations of the dike requiring maintenance and to study the effect of climate change on flood inundation in
- 25 the study area-.

The frequency and intensity of the cyclone around the world are likely to increase due to climate change which will require resource intensive improvement of existing or new protection works for the deltas. Identification and prioritising maintenance of critical location of dike breaching can potentially prevent a disaster. Non-structural tools such as land use zoning with the help of flood risk maps and probabilistic flood maps has the potential to reduce risk and damage. The method presented in this

30 research can potentially be utilized for the deltas around the world to reduce vulnerability and flood risk due to dike breach cause by cyclone induced storm surge.

1. Introduction

Bangladesh is the low lying delta of three major rivers: Ganges, Brahmaputra and Meghna. Eighty percent of the country's land is located below 10m AMSL (above mean sea level) (Heitzman and Worden, 1989) and it is formed of sediments carried

- 5 by the above mentioned rivers. The population of Bangladesh was about 131.5 million by the year 2000 (World Bank, 2018) of which about 49% were living in the coastal zones (Neumann *et al.*, 2015). The coastal areas of Bangladesh are flooded frequently due to cyclone induced storm surges and occasionally due to high water levels in the rivers caused by heavy rainfall in the upstream catchments of Ganges, Brahmaputra and Meghna. The coast was hit by 5 severe cyclones between 1995 and 2010 causing flooding, huge damages and loss of life (Dasgupta *et al.*, 2014).
- 10 Bangladesh has 123 polders in the coastal area, each surrounded by earthen dikes, which are designed to protect the inland from flooding due to- high tides. The existing crest level of these dikes are only adequate enough to protect the coastal area from cyclones with 5 to 12 year return periods (Islam *et al.*, 2013). These dikes usually get damaged <u>and sometimes breached</u> by tropical cyclones of high intensity-<u>due to overtopping</u>, which causes flooding inside the protected areas, damages to properties and loss of life. For example, cyclone Sidr hit the coast of Bangladesh in 2007 affecting 8.9 million people, causing
- 15 US\$1.-7 billion of damage (GOB, 2008;) (Dasgupta *et al.*, 2014). In 2009. Cyclone Aila affected 3.9 million people with an estimated damage of US\$270 million (EMDAT, 2009).

Crest levels of the coastal dikes were rerecently designed recently for an event of 25 year return period under the Coastal Embankment Improvement Project (CEIP) (BWDB, 2013). <u>A storm surge event of 25 year return period was considered in</u> this study for the generation of different scenarios. Under the project CEIP the Crest levels of the dikes were designed

- 20 considering wave actions, astronomical tides and the required free-board. Raising the crest level was considered as the only mitigating measure. Various studies on the coastal areas of Bangladesh (e.g. Karim and Mimura, 2008; IWM, 2005; Azam *et al.*, 2004; Madsen and Jakobsen, 2004; CSPS, 1998; Flather, 1994) considered flooding only due to overtopping of the dikes during storm surges. Effect of breaching of the dikes due to piping and scouring on the landside during cyclones have not been studied. As tThe coast of Bangladesh is frequently hit by severe cyclones frequently (5 cyclones between 1995 andto 2010, 1995).
- 25 Dasgupta *et al.*, 2014). and t Bangladesh Water Development Board (BWDB) is responsiblehe authority designated for the operation and maintenance of these dikes (Bangladesh Water Development Board, BWDB) and lacks fundbudget to conduct proper repairing of all the damaged dikes subsequent to anybetween the landfall of two severe cyclones. As a result the dykes remain vulnerable to breaching. Identifying the critical location(s) of dike breach and prioritising the repairingprotection of the critical location isean likelypotentially to reduce the breaching possibilitydamage due to flood and risk of flooding.

30 substantially.

Moreover, non-structural measures for flood risk management such as land use zoning using the flood risk map (FRM) and probabilistic flood maps (PFM) to locate the vulnerable areas are currently unavailable for the coastal areas of Bangladesh.

Flood zoning can be a useful risk mitigation measure as land use governs the exposure and may aggravate the hazard (Barredo and Engelen, 2010).

MoreoverFurthermore, the intensity and frequency of these tropical cyclones is are likely to increase in the future due to climate change. It is projected that by the year 2100, the frequency of the most intense cyclones will increase substantially and the

- 5 intensity of tropical cyclones will increase by 2 to 11% due to global warming (Knutson *et al.*, 2010). Flooding by tropical cyclones will also increase in the future as a result of sea level rise (SLR) (Woodruff *et al.*, 2013). SLR and sea surface temperature (SST) will affect the cyclone induced storm surge height in the Bay of Bengal (Karim and Mimura, 2008). With increasing SST, the storm surge height may increase from 21% to 49% and with SLR, the flood depth due to storm surges may increase by 30-40% (Karim and Mimura, 2008). The land subsidence in the delta will exacerbate the effect of SLR.
- 10 Furthermore, by By the year 2100 the annual estimated damage due to tropical cyclones may increase by US\$53 billion (Mendelsohn *et al.*, 2012).

<u>At present, flood forecasting system is not available for the The study areacoastal region of Bangladesh.</u> is not benefitted with an enabled flood forecasting system. Bangladesh Water Development Board (BWDB), which is mandated to protect the area, does not have a clear picture about the inundation patterns corresponding to various climatic conditions. Moreover, identifying

- 15 zones in the embankment critical to flooding in the polder will help BWDB in prioritising their maintenance. This paper presents an investigation of the inundation pattern behind dikes due to flooding caused by storm surgesa methodology to identify the critical location of dike breach due to cyclones, generate flood risk map (FRM) and probabilistic flood map (PFM) due to breaching of the dike by cyclone induced storm surges. Different scenarios of storm surges were formulated utilised by considering storms of different frequencies with varying tidal conditions, angle of cyclone at landfall and SLR. The simulated
- 20 flood inundations were used in creating a probabilistic flood map of the area. A cyclone event of 25 year return period was considered infor this research. A coastal polder (Polder 48) of southern Bangladesh was selected as the study area. With the effect of climate change, the frequency and intensity of the cyclone around the world will increase. The protective structures for the deltas around the world will require adjustments which will be resource intensive. Non-structural tools such as land use zoning with the help of flood risk maps and probabilistic flood maps has the potential to reduce risk and damage.
- 25 <u>Identification of critical location of breaching and intensifying the maintained effort for these locations can potentially prevent</u> <u>a disaster. Although coastal region of Bangladesh was selected as the case study area, the method presented in this research</u> can be utilized for the vulnerable deltas around the world.

2. Study area

Polder 48, which was considered as the study area for this research, is surrounded by dikes and has a sea facing dike of about
 20 km length on the southern side of the polder. The polder is located in the south western coast of Bangladesh Delta (Figure 1Figure 1) stretching from 21°50'28" N 90°05'17" E to 21°50'06" N 90°14'14" E. The outline of the study area in Figure 1 Figure 1 (alsond in Figure 3) depicts the dike alignment of the study area as well. The area is also known as Kuakata

and it is in the administrative zone of Kalapara sub-district (Upazilla) of Patuakhali District. It has an area of 50.75 km² with 24,240 inhabitants according to the census of 2011 (BBS, 2012). Most of the inhabitants are farmers and fishermen (Nasreen *et al.*, 2013). Shrimp culture and tourism are also part of the economic activities. The land use is mainly-classified by the Ministry of Land, Bangladesh into the following four classes: rice fields, settlements, shrimp ponds and water bodies

- 5 (river/canal) by the Ministry of Land, Bangladesh. Climate and agricultural practices of Kuakata is similar to the climate and agricultural practices of the country (Bangladesh). The average yearly rainfall in Kuakata is 2590mm (Climate-Data, 2016) and t. The month with the highest rainfall is July with an average of 611mm. The withhe annual average temperature isof Kuakata is 25.9°C with minimum and maximum temperature as 13°C and 34°C respectively (Climate-Data, 2016). and . There are three seasons for growing crops (DAE, 2009). They are, Rabi (November to February), Kharif-I (March to May) and
- 10 Kharif-II (June to October) are the three seasons for growing crops (DAE, 2009). The area is relatively flat and low lying, with The elevation of 80% of the area is of its elevation below 1.55m PWD, the vertical datum established by Public Works Department of Bangladesh, which is 0.46m below the MSL. The land level surveys at different times have indicated that this polder is facing land subsidence issues. Brown and Nicholls (2015) reported the estimated mean subsidence rate of Ganges-Bhrahmaputra-Meghna (GBM) delta as 5.6 mm per year with an overall median of 2.9 mm per year.
- 15 The area was severely affected by recent storms Sidr, Aila and Mohasen in 2007, 2009 and 2013 respectively. For example, during cyclone Sidr, 94 people died and 45% of the crops were lost (Ahamed, 2012).



Figure 1: Location map of the study area Polder 48 (Kuakata).

Andharmanik, Galachipa and Khaprabhanga rivers are on the east, west and north of the study area respectively, whereas the Bay of Bengal is on the southern side of the study area (Figure 1Figure 1). Galachipa River is the widest among the rivers surrounding the area. On the southern side, the study area has sea shore of 20 km width, which is partly protected by the mangrove forest at several locations. There is a narrow sea beach in the south-western side of the area. The western part of the

sea facing dike was overtopped during cyclone Sidr causing flood inside the polder (Hasegawa, 2008). The loss of livestock and food grains were such that it created partial deficiency of food in Kuakata (TANGO International, 2010). The average crest level of Polder 48 in the northern side is 4.5m PWD and in the southern side (sea facing side) is 6m PWD (Islam *et al.*, 2013). The existing embankments of 17 polders of the region, including Polder 48, were redesigned and rehabilitated during

5 the first phase of CEIP (Islam *et al.*, 2013). CEIP proposed a crest level of 7.36 m PWD for the dike of Polder 48 (Islam *et al.*, 2013).

3. Methodology

The methodology followed is presented in Figure 2 and described in the following sub-sections.

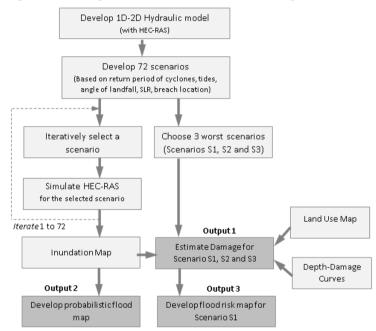


Figure 2: Methodological approach followed in this study.

3.1 <u>Setting up of</u> 1D-2D coupled model developmentset-up

In order to build a 1D-2D inundation model field measurements (land level surveys, observed water levels, canal alignments and cross sections of the river and canals) and information from remote sensing (satellite imagery) were gathered (Figure 3). Institute of Water Modelling (IWM) of Bangladesh collected hydraulic, hydrologic and land level data of the study area (along with other polders) in the framework of the feasibility study of Coastal Embankment Improvement Project (CEIP). IWM has kindly provided the measured data for the study area.

The Digital Elevation Model (DEM) was generated by combining the land level surveys conducted by IWM and FINMAP (a <u>company from Finland</u>). The land level survey of IWM (conducted in 2012) did not cover the whole study area. FINMAP conducted the topographic survey of the study area in 1988 (MIWF, 1993). The differences in elevation between land surveys of IWM and FINMAP indicated the land subsidence. An average subsidence was computed, which was

- 5 used to update the elevations of the FINMAP survey for the areas within Polder 48 for which survey data from IWM was not available. The combined DEM has a resolution of 50 m. The same DEM was used for the simulations of the years 2050 and 2100 without any corrections for further subsidence. Subsidence of the coast in the past has been reported by Brown and Nicholls (2015) and was verified with the survey data from IWM and FINMAP. Subsidence in the future may continue but in the absence of scientific studies it was not considered for the future scenarios in this research. It is noteworthy that if subsidence
- 10 continues then the effect of the SLR may be increased and the results reported in this research should be treated as to some extent under-estimated values.

The bathymetry of the sea near the coast was collected from global bathymetric chart of ocean (GEBCO) (Smith and Sandwell, 1997). The land use data was collected from the Ministry of Land of Bangladesh. MODIS reflectance data was used for the analysis of previous flood events. The methodology and equations suggested by Hoque *et al.* (2007) were used to analyse the

15 MODIS reflectance data to determine flood extents during previous flood events. The intention was to utilise the flood extent generated from MODIS reflectance for calibration of the hydraulic model. However, no flood image from MODIS was available during the simulation period.

The river analysis tool HEC-RAS (version 5.0) from the US Army Corps of Engineers was used to develop the 1D-2D coupled
inundation model. The flow in the river was modelled in 1D whereas the flow over the floodplain was modelled in 2D. HEC-RAS 5.0 is a free tool which can simulate 1D, 2D and 1D-2D coupled models for steady and unsteady flow. The 2D module of HEC-RAS provides option to simulate flow of water either with the diffusion wave equation or with the full shallow water equation (St. Venant equation). The flow equations are solved using Skyline/Gaussian reduction matrix solution technique by HEC-RAS. HEC RAS also provides the Pardiso solver for complex systems. The two dimensional module in HEC-RAS is computationally efficient. Moreover, HEC RAS generates irregular flexible mesh to represent a complex shape of the 2D flow area. As HEC RAS is a free tool, a model developed by it can be utilized by anyone. The availability of irregular flexible mesh

<u>in HEC-RAS</u> and <u>the option</u> for faster simulations -led to the selection of HEC-RAS 5.0 as the mathematical-modelling tool for this research. Data utilized for developing the model and their sources are presented in Table 1.

30

 Table 1: The data used in developing the mathematical model and their sources.

IWM, GEBCO and JSCE stand for Institute for Water Modelling, General Bathymetric Chart of the Oceans and Japan Society of Civil Engineers respectively.

| Component of the Model | Data collected and used | Source | | |
|------------------------|-------------------------|---------------------|--|--|
| 1D networks | Alignment | River network: IWM; | | |

| Component of the Model | Data collected and used | Source | | | |
|------------------------|---|---|--|--|--|
| | | The network on the sea side: Satellite image (Google Earth) | | | |
| | Cross section | River: IWM; Bathymetry of the sea side: GEBCO | | | |
| | Water Level | IWM | | | |
| | Discharge | IWM | | | |
| | DEM | IWM and FINMAP | | | |
| 2D Mesh | Land Use | Ministry of Land | | | |
| | Dike Alignment | IWM | | | |
| | Crest Level of the existing dike | IWM | | | |
| | Geometric properties of the dike | IWM | | | |
| 1D-2D coupled model | Design crest level of the dike for future development | Islam et al., 2013 | | | |
| | Storm surge height | Azam et al., 2004, Islam et al., 2013 and Dasgupt et al., 2014 | | | |
| | Flood depths of previous events | JSCE | | | |

The 1D section of the model was developed and calibrated using the information shared by IWM. The 1D part of the developed model was calibrated for non-flood conditions as measured discharge/ water level data during a cyclone event was unavailable. The model was simulated using discharge as the <u>upstream-west</u> boundary and water level as the <u>downstream-east</u> boundary

5 conditions (Figure 3). The calibrated 1D model was then coupled with the 2D model of flow over the floodplain using the DEM of the study area.

For the 1D-2D inundation model, a computational mesh with flexible shape was developed in HEC-RAS (Figure 3). HEC-RAS generates mesh with irregular shapes. The rectangular cells of the developed 2D mesh had a resolution of 25 m and the non-rectangular cells rest of the cells had an areas of ranging from 625 square meters to 1282 square meters. The roughness

10 coefficient (Manning's *n* varying from 0.025 to 0.05) was provided according to the landuse of each cell. A sensitivity analysis as suggested by Hall *et al.* (2005) was carried out by varying Manning's roughness coefficient *n* before the calibration of the 2D inundation model.

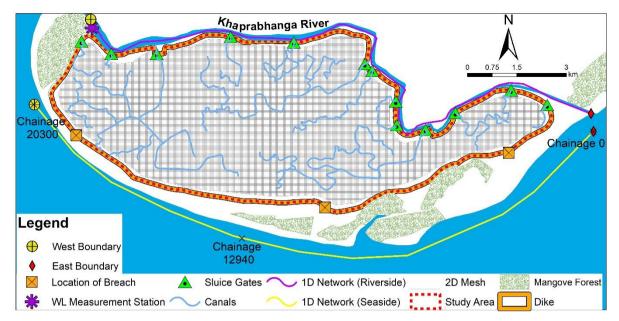
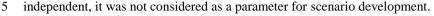


Figure 3: Schematic diagram of the study area with location of control structures and gauges and the considered breach locations.

Building and calibrating the 1D model was the preliminary step for developing the 1D-2D coupled model. The water bodies surrounding the study area were included in the 1D model. The study area has Khaprabhanga River on the northern side and

- 5 sea on the southern side (Figure 3). The connection of Khaprabhanga River with other rivers was not considered in the model. This was due to the fact that storm surges are observed during the pre_ or post_-monsoon periods whereas fluvial floods are observed during the monsoon. Flow through rivers did not play a major role during the previous cyclones. The western and eastern side of the embankment have <u>mMangrove <u>F</u>forests between the rivers and the embankment (Figure 3).</u>
- For the river, the surveyed cross sections were used in the 1D model (Figure 4). The storm surges on the sea was conceptualised as a water surface profile in a- 1D channel on the southern side of the study area (Figure 3). The GEBCO bathymetry (Figure 5) was used for the channel. An alternative was to develop- a 2D model for the coastal hydrodynamics. However, as the coast of Bangladesh is flat and shallow a large area of the sea would have been included in the model. As the focus was on studying the inundation in Polder 48 and not the coastal sea we followed a simpler representation of the storm surges using a 1D model. The synthetic water level data for boundaries of the model were generated by following the tidal water level pattern and the
- 15 storm surge height considered for the all scenarios (Table 2). The water surface profile corresponding to each scenario (Table 2, discussed in Section 3.2) was considered as the profile in the 1D model of the sea side (Figure 6). The dense canal network of 122 km, inside the study area, is connected with the Khaprabhanga River, which regulates the inand out flow into the river network through a system of 13 control structures. The regulators remain closed during cyclones making the canal network isolated. Therefore, the canal network inside the polder was not included in the 1D model. However,
- 20 the simulation of the overland flow consequent to breaching of the dike will be affected by the canal geometry and therefore, the wider and larger canals were included in the DEM.

The geometry and propagation of the breach of the dike depends primarily on the storm surge height, angle of landfall, soil properties and wave action. The coastal embankments of Bangladesh are usually earthen. The geometrical properties of the breaching of the dike and the time required for breaching were calculated following the instructions of US Bureau of Reclamation. An *S*-curve was used for breach propagation with time (Oumeraci, 2006). As the geometry of the breach is not



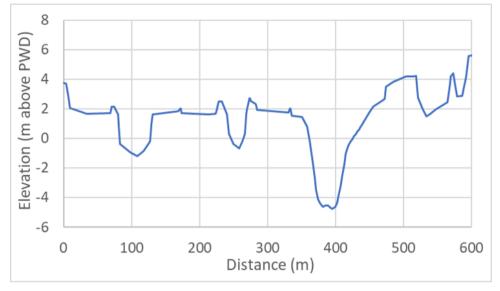


Figure 4: A typical cross section of the Khaprabhanga River

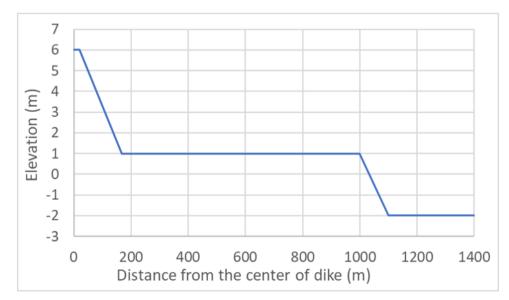


Figure 5: Cross section for the 1D network on the sea side

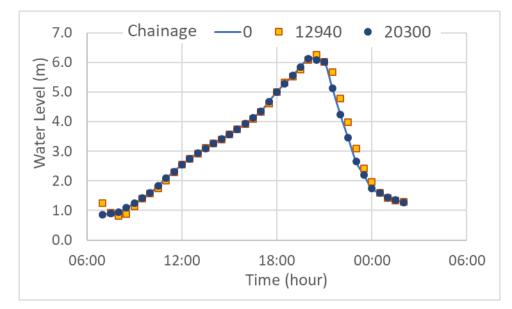


Figure 6: Variation of water level at three locations (chainage 0, 12940 and 20300)- along the 1D channel on the sea side according to a specific Scenario (out of 72 Scenario).

In order to ensure model stability a maximum spacing between the computational points was imposed and computed using Samuels' formula (1989) presented in Eq. (1):

(1)

(2)

$$\Delta x \leq 0.15 * D/So$$

5

where, Δx is the spacing between the computational points, *D* is the average bank full depth of the channel and *S*₀ is the average slope of the channel. The maximum spacing between cross sections was calculated as 300 m. The river had steeper bed slope than the long shore slope of the sea bathymetry requiring smaller Δx to ensure stability and same Δx will reduce instability of the foreshore as well.

As suggested by Fromm (1961) the Courant number was kept less than or equal to 1.0 to maintain the stability of the numerical

10 model by controlling the time step. The Courant number was calculated using the following Eq. (2):

$$Cr = V * \Delta t / \Delta x$$

where Cr is Courant number, V is velocity, Δt is the time step and Δx is the spacing between the cross sections.

3.2 Cyclonic scenarios considered

Different scenarios were developed considering the probability of occurrence of cyclones, the angle of landfall, SLR due to

15 climate change, diurnal, semi-diurnal and seasonal variation of tides, locations of breaching of the dike and geometrical properties of the breach.

Frequency of cyclone: A cyclone of 1 in 25 year return period was considered for all the scenarios as this is used as the design criteria for the dikes (BWDB, 2013). Nineteen previous cyclones for different tidal conditions were simulated by IWM using

a 2D model for the Bay of Bengal. A statistical analysis was conducted using these model results to generate the storm surge height corresponding to a cyclone of 25 year return period (Islam *et al.*, 2013). Due to lack of data, change in the probability of occurrence of the cyclone in the future was not considered.

Angle of landfall: The angle of landfall affects the height of storm surges. The storm surge height increases with angle of the

5 storm to the coastline (Azam *et al.*, 2004). Angle of attack governs the wind speed which is one of the parameters for the height of cyclone induced storm surges (Azam *et al.*, 2013).

Tides: The difference between the storm surge at high tide and low tide is 1.2m for the study area (Azam *et al.*, 2004). The average seasonal variation of the tidal range is 1.3m.

- Sea level rise: The coast of Bangladesh may be severely affected by SLR and one fourth of the land may be lost due to SLR
 by 2100, which will directly affect 3 million people (Ericson et al., 2005). IPCC published their 5th assessment report (AR5) in 2013. Among the scenarios considered in AR5, RCP (representative concentration pathways) 2.6 is the most optimistic one and RCP 8.5 is the worst considering the carbon emission, rise in temperature and SLR. The mean SLR at the end of 21st century is estimated to be 0.4m, 0.47m, 0.48m and 0.63m for RCP 2.6, RC 4.5, RCP 6.0 and RCO 8.5 respectively (Stocker *et al.*, 2013). For this study, RCP 8.5 with SLR of 0.63 m was considered for developing the scenarios.
- 15 *Location of breach*: The sections of the sea facing dike of the study area protected by mangrove forest, sand dunes and wide beach are least likely to be breached due to storm surges. The study considered breach locations with least protection. The considered locations for dike breach as well as the mangrove forest around the study area are shown in Figure 3.
- A scenario matrix consisting of 72 scenarios were generated by combining different phases of tides, angle of landfall, SLR and breach locations (Table 2). Single breach was considered for each all the scenario. The highest storm surge height among
- all the developed scenarios was 7.2 m_PWD considering the angle of landfall as 230° , high tidal phase during spring tides, SLR and dike breaching at any of chosen locations. Th<u>eis highest</u> storm surge height <u>as the boundary condition</u> with breaching at the western, central and eastern parts of the dike -were considered as the worst case scenarios and were denoted as Scenario <u>S</u>1, <u>S</u>2 and <u>S</u>3 respectively (Figure 2). Flooding due to overtopping of the dikes was not considered as the crest level (7.36 m PWD) was higher than the highest storm surge height (7.2 m_PWD).
- 25

Table 2: Storm surge heights corresponding to different Scenarios considered

| | Tidal Variation | | Breach Locations | | | | | |
|----------|-----------------|-------------|------------------------|------|-------------|---------------|-------------|--------------|
| Angle of | | | East | | West | | Central | |
| Landfall | | | With SLR Without SLR | With | Without SLR | With | Without SLR | |
| | | | Whiti SER White de SER | | SLR | | SLR | While of the |
| | | | | | Storm S | Surge Heights | | |
| | High Tide | Spring tide | 4.06 | 3.38 | 4.06 | 3.38 | 4.06 | 3.38 |
| 200 | ingii ilue | Neap tide | 2.77 | 2.09 | 2.77 | 2.09 | 2.77 | 2.09 |
| | Low Tide | Spring tide | 2.83 | 2.15 | 2.83 | 2.15 | 2.83 | 2.15 |

| | | Neap tide | 1.54 | 0.86 | 1.54 | 0.86 | 1.54 | 0.86 |
|-----|-----------|-------------|------|------|------|------|------|------|
| 215 | High Tide | Spring tide | 6.16 | 5.48 | 6.16 | 5.48 | 6.16 | 5.48 |
| | | Neap tide | 4.86 | 4.18 | 4.86 | 4.18 | 4.86 | 4.18 |
| | Low Tide | Spring tide | 4.93 | 4.25 | 4.93 | 4.25 | 4.93 | 4.25 |
| | | Neap tide | 3.63 | 2.95 | 3.63 | 2.95 | 3.63 | 2.95 |
| 230 | High Tide | Spring tide | 7.20 | 6.52 | 7.20 | 6.52 | 7.20 | 6.52 |
| | | Neap tide | 5.91 | 5.23 | 5.91 | 5.23 | 5.91 | 5.23 |
| | Low Tide | Spring tide | 5.97 | 5.29 | 5.97 | 5.29 | 5.97 | 5.29 |
| | | Neap tide | 4.68 | 3.99 | 4.68 | 3.99 | 4.68 | 3.99 |

To identify the critical location of breaching, simulation results of the scenarios simulated with HEC-RAS corresponding to the three worst case scenarios S1, S2 and S3 were compared based on the total area flooded and estimated damage due to flooding. Using the calculated damage and occurrence probability of the event, a risk map was generated for the critical

5 locations of the sea facing dike. A probabilistic flood map (PFM) was generated from the flood maps of the 72 scenarios (Table 2; Output 2 in Figure 2)). As the storm surge height suggested by Islam *et al.*, (2013) corresponds to an event of 25 year return period, the PFM generated in this study is corresponds to probabilistic inundations maps for a single event of 1 in 25 year return period-in which a breach occurs.

10 **3.3 Estimation of damage due to floods**

A comprehensive damage calculation should involve both direct and indirect damages due to floods (Büchele *et al.*, 2006). Direct damage is caused by physical contact of properties and human beings with flood water. Indirect damage is caused by interruption of services, production and transportation and degradation of health due to floods. Due to lack of data, only the direct damage to properties were calculated for the study area. The damage was considered as a function of flood depth. The

15 land use of the study area was classified by the Ministry of Land of Bangladesh as settlements, rice fields, shrimp ponds and water bodies (rivers/canals). Only the tangible damage was considered and no environmental damage was calculated. Damages to the canal network was not considered. The damage in a flood event was calculated using Eq. (3).

$$D = \left(\sum_{i=0}^{n} x_i \times f(x_i)\right) \times A_i \tag{3}$$

Where, D = total direct tangible damage in a flood event, n = total number of computational cells within the flooded area, x_i = 20 flood depth of cell *i*, $f(x_i)$ = damage function for the land use of the flooded cell *i* and A_i = area of cell *i*.

Depth-damage curves for different land classes for the study area were developed by adapting depth-damage curves found in the literature (Figure 7Figure 7). Reese *et al.* (2010) calculated flood damage as a percentage of the property value of buildings categorised based on the construction material. The buildings of the study area are primarily built of timber due to its low cost

and easy availability. The depth-damage curve suggested by Reese *et al.* (2010) for buildings made of timber was used as a basis for generating the depth-damage curve for the settlements (residential area). Simple Action for the Environment (SAFE) carried out a research on the average value of properties in rural areas of Bangladesh (SAFE, 2011). This property values were used to update the damage values used by Reese *et al.* (2010). Muktadir and Hasan (1985) reported that rural houses of

- 5 Bangladesh are built with a large courtyard and as a result houses have a lot of open and unoccupied space around buildings. The damage curve considered for the residential area was used for the damage to the buildings and not for the courtyard. Moreover, the satellite image of the area also indicated that about half of the settlement -was without buildings. <u>Satellite image</u> from google earth was used for analysis. The satellite image of the area was downloaded and georeferenced. Then, the areas for buildings and open areas for households were manually calculated using ARCGIS. Therefore, 50% of the settlement area
- 10 was considered with no damages.

et al. (2014) was used in this study (Figure 7Figure 7).

15

The cultivation of rice involves flooding the rice field with water up to a few cm. However, if the height of water increases and the rice plant goes under water then the productivity decreases. The damage to rice plants also depends upon the flood duration. If the rice plant is continuously under water for more than 2-3 days then the damage can be up to 80% (Chau *et al.*, 2014). The <u>simplified (with regards to flow velocity and flood duration)</u> depth-damage curve for rice fields suggested by Chau

- Shrimp ponds are surrounded by embankments so that there is no damage to shrimp ponds till the flood level crosses the embankment level. However, after when the flood level is higher than the embankment level shrimps escape causing a loss of the total investment. To take this into account, the investment made by farmers was assessed using a study conducted by Fatema *et al.* (2011). According to the study the investment for shrimp pond in the study area was about $\notin 0.09/m^2$. Based on
- 20 the practices in the study area the banks of the shrimp ponds were considered as 2 meter above the adjacent land and the depth-damage curve (Figure 7Figure 7) was modified accordingly. The adapted depth-damage curves are obviously simplistic ones. Further research is needed for improving them.

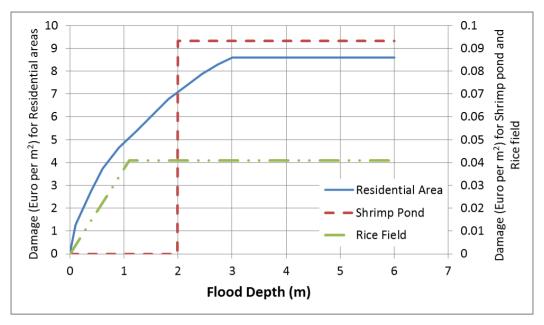


Figure 7: Depth-damage curves for different land use classes.

The damage calculations were carried out using ArcGIS. The simulated flood depth and landuse for each grid cell was used as the input and the damage in each grid cell was computed by using the -depth-damage curve corresponding to that landuse. The damage for each scenario was estimated using this procedure.

3.4 Calculation of flood risk and generation of risk map

5

Flood risk assessment is an essential part of risk management. Spatial distribution of risk and areas requiring mitigation measures can be identified from flood risk maps (Helm, 1996). To examine the spatial variation of risk, flood risk analysis was carried out and a risk map was generated considering dike breaching at the critical location. Van Manen and Brinkhuis (2005)
and Klijn (2009) under FLOOD*site* project carried out research to quantify the flood risk for the polders in The Netherlands for dike failure defining the risk as a product of the occurrence probability of the event and the consequences which was defined by Helm, (1996). Eq. (4) was used to calculate the risk due to flooding:

$$R = P_F * S \tag{4}$$

Where, R = risk, $P_F = \text{probability of occurrence of the flood hazard and } S = \text{consequences}$

15 The exceedance probability (return period) of the cyclone induced storm surge was used as the probability of occurrence of the hazard. The probability of flooding within a protected area is not the same as the probability of the hazard and depends also upon the probability of failure of the dike. It is a difficult probability to compute as the probability of dike failure also depends upon the dike maintenance, information about which were not available. Here we have assumed that the probability of occurrence of the hazard and the probability of failure of dike are the same.

3.5 Probabilistic flood map

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Purvis *et al.* (2008) stated that the risk assessment for the most probable scenario cannot take into account the impact of the scenario of low probability₂ stressing the necessity of a probabilistic risk analysis. The equation suggested by Purvis *et al.* (2008) for probabilistic risk analysis was adjusted and used for this research to calculate the probability of flooding of each cell and is presented below in Eq. (5):

$$P_{i(i=1\ toN)} = \frac{\sum_{j=1}^{M} F_{ij} \times P_{fj}}{\sum_{j=1}^{M} P_{fj}} \text{ and } F_{ij} = \begin{cases} 1, \ if \ flooded\\ 0, \ if \ dry \end{cases}$$
(5)

Where, P_i is probability of flooding at cell *i*, P_{fj} is the probability of reaching a certain storm surge level in simulation number *j*, F_{ij} is the binary value indicating if the cell *i* is flooded or not in simulation *j*, *j* =1,2,3, ..., *M* where *M* is the number of Scenarios considered (=72), *i* =1,2,3,..., *N* are the computational grid cells on the polder area and *N* is the number of cells.

Equation (5) was used in this study to calculate the probability of flooding at each cell. The probabilistic flood map (PFM) was calculated using the results of all the scenarios.

4. Results and discussion

The developed 1D-2D modelled for the present study was calibrated for the 1D part by comparing the observed and simulated

- 15 values for discharge and water level. The corresponding performance indicators used for evaluation were coefficient of determination (R^2), root mean square error (RMSE) and mean absolute error (MAE) for which values of 0.98, 2.15 m³/s and 1.68 m³/s respectively were obtained for discharge; and 0.98, 0.09 m and 0.08 m respectively for water level. The average value of the discharge and water level for the considered simulation period was 5.68 m³/s and 0.82 m respectively. The period of simulation for calibration coincided with the surges corresponding to cyclone Sidr (from November 14 to November 17,
- 20 2007). The simulation results indicates that the dike facing the seaside was overtopped and the area inside the polder was inundated. This conclusion is in line with the survey conducted by Japan Society of Civil Engineers (JSCE) (Hasegawa, 2008). The coupled 1D-2D model has not been calibrated because there were no flood maps showing flood extents available for recent cyclones. However, the 2D part of the model was pseudo-calibrated considering MODIS reflectance data. Such data was used in order to analyse -the inundation extent, though this also posed considerable challenges due to the cloud coverage during the
- 25 cyclones. The survey conducted by JSCE after cyclone Sidr was collected to investigate the flood extent and depth, which provided flood depth for only one location inside the study area. This location was used for the calibration of 2D model. The error difference between the reported and in the simulated flood depth was 4.5%. Prior to the calibration of the 2D model, sensitivity analysis was carried out regarding the roughness coefficient (Manning's *n*). The analysis indicated that the inundation model is not highly sensitive to the roughness coefficient and the areas of low flows (locations furthest from the
- 30 dike breach) are most sensitive. The sensitivity analysis was done for the breaching on the western part of the dike only. It was

considered that the breaching at other locations will have similar effects as the area inside the polder is flat and low lying with mostly farmlands near the dike.

This 1D-2D model, which had limited calibration points, was further used in simulating the developed scenarios. The simulated results were used to analyse flood depth, extent and damages due to flood. The FRM and the PFM were generated based on

5 flood results of the model.

4.1 Inundation corresponding to three worst case Scenarios

Among the simulated scenarios, the results of three worst case scenarios (Scenario $\underline{S}1$, $\underline{S}2$ and $\underline{S}3$) were compared for identifying the critical location of breaching. The corresponding flood maps for the worst case scenarios are presented in <u>Figure 8</u>.

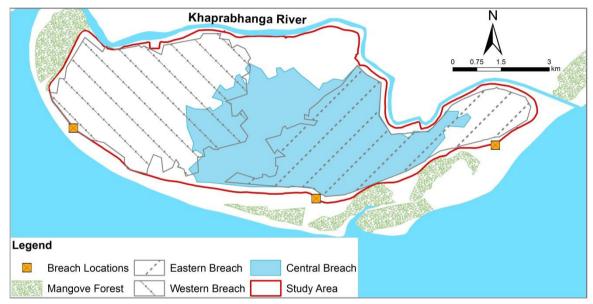


Figure 8: Flood extent corresponding to three worst case scenarios of dike breaching in the central, eastern and western section of the dike.

10 Flood extents corresponding to all different scenarios presented in Table 1 were compared to understand the effect of SLR, diurnal and seasonal tidal variation and angle of cyclone at landfall. The flood extents of different scenarios considering the breaching at central part of the sea facing dike is presented in Figure 9Figure 9.

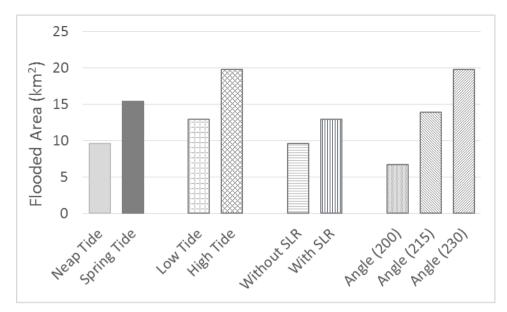


Figure 9: Comparison of flooded areas corresponding to different Scenarios <u>considering the breaching at central part of</u> <u>the sea facing dike</u>.

5

Moreover different land classes were considered while computing the flood extent for the three worst case scenarios (Table 3). The analysis of the flood extent for different flood depths, based on the considered land uses are presented in Figure 10. The highest storm surge height among all the developed scenarios were 7.2 m PWD (Table 2). This storm surge height with breaching at the -western, central and eastern parts of the dike -were considered as the worst case scenarios and were denoted as Scenario S1, S2 and S3 respectively.

| Land Classes | Flooded Area (km ²) | | | |
|--------------|---------------------------------|---------------------|---------------------|--|
| | Scenario <u>S</u> 1 | Scenario <u>S</u> 2 | Scenario <u>S</u> 3 | |
| Rice fields | 15.3 | 16.4 | 12.3 | |
| Settlements | 3.1 | 3.1 | 2.1 | |
| Shrimp ponds | 0.2 | 0.1 | 0.1 | |
| Canals | 1.2 | 1.7 | 1.2 | |
| Total | 19.8 | 21.2 | 15.8 | |

| Table 3: Flooded areas | of different land o | classes corresponding | g to the three w | orst case Scenarios. |
|------------------------|---------------------|-----------------------|------------------|----------------------|
| | | | | |

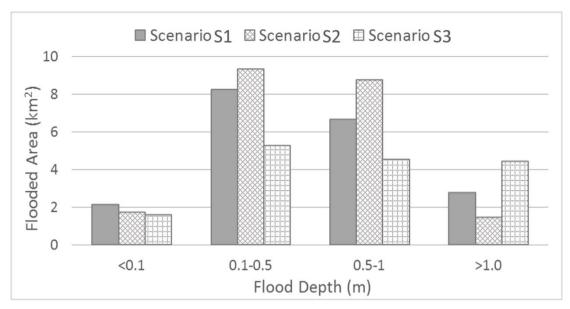


Figure 10: Flooded areas for different ranges of flood depths corresponding to different Scenarios.

4.2 Comparison of calculated damages

The damage due to flooding was calculated using the depth-damage curves for different land classes. The calculated damages for different land classes and damages for different flood depths corresponding to the three worst case scenarios are presented in <u>Table 4Table 4</u> and <u>Figure 11Figure 11</u>.

| Table 4: Calculated flood | l damages for different land | classes corresponding to | different scenarios. |
|---------------------------|------------------------------|--------------------------|------------------------|
| Table 4. Calculated hood | i damages for different land | clusses corresponding to | uniter ente scenarios. |

| Land Classes | Estimated flood damage (million Euros) | | | |
|--------------|--|---------------------|---------------------|--|
| | Scenario <u>S</u> 1 | Scenario <u>S</u> 2 | Scenario <u>S</u> 3 | |
| Rice Fields | 0.4 | 0.4 | 0.3 | |
| Settlements | 10.3 | 10.3 | 8.3 | |
| Shrimp Ponds | 0.0 | 0.0 | 0.0 | |
| Total | 10.7 | 10.7 | 8.7 | |

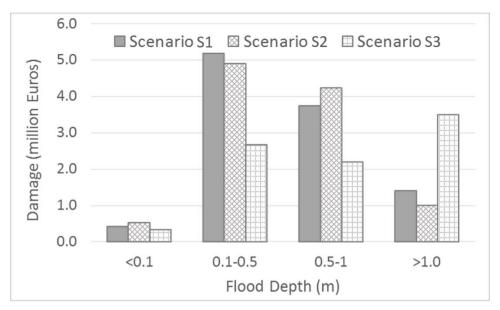


Figure 11: Variation of estimated flood damages with varying ranges of flood depths corresponding to Scenario $\underline{S}1$, $\underline{S}2$ and $\underline{S}3$.

Figure 10Figure 10 and Figure 11Figure 11 corresponds to the flooded area and damage due to different range of inundation respectively. The flood area and damage wereas highest for the inundation depth of 0.5 m to 1.0 m_{π}.

4.3 Risk map for the worst case scenario

5

The flood risk map for the scenario with the critical location of breaching of dike is presented in <u>Figure 12Figure 12</u>. The risk map presents the assessed risk of flooding due to breaching at critical locations of the dike. <u>Comparison of flooded area and damage due to flood for the three worst case scenarios lead to the identification of Scenario S1 as the critical location of breaching.</u> The identification of the critical location of breaching is described in section 4.5.

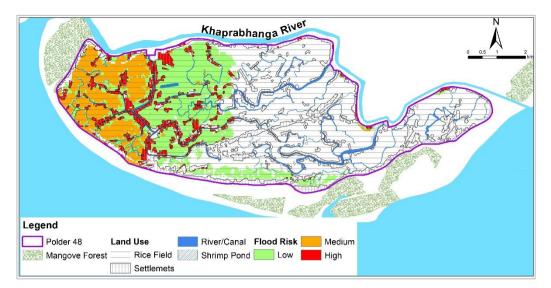


Figure 12: Flood risk map corresponding to the dike breach at the critical location of the dike. The following three classes of risk are shown: high, medium and low. The considered four landuses are shown as well.

4.4 Probabilistic flood map

5

Although the inundation maps are widely used for spatial planning and flood mitigation measures, the uncertainty of mathematical modelling affects the output of inundation maps (Alfonso *et al.*, 2016). In order to account for uncertainty, probabilistic flood maps are suggested to be used (Domeneghetti *et. al.*, 2013). The probabilistic flood map was calculated from the inundation maps corresponding to the 72 scenarios considered in the study. Probabilistic flood maps were calculated for a threshold of flood depth greater than 0.5 m. The developed damage curves suggest that the damage for flood depth below 0.5 m is minimal. Moreover, considering the widely accepted 'living with floods' philosophy in Bangladesh a threshold of 0.5m was adopted. This arbitrary threshold was used in developing the PMFs<u>_and_. This threshold was not considered while</u> the estimation of damage due to flood <u>was conducted</u> was not affected. The calculated probabilistic flood maps are presented

10 in Figure 13Figure 13. The probabilistic flood map indicates the likelihood of being flooded. This will assist the planning for future land use zoning, which can be used to restrict further developments in the floodplains.

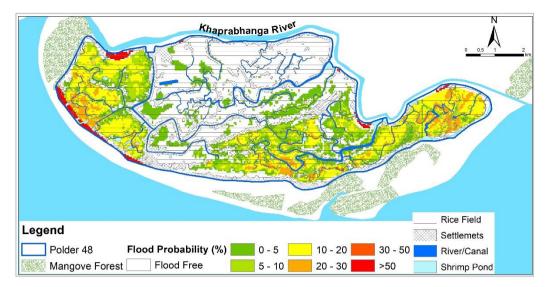


Figure 13: Probabilistic flood map of the study area. Varying colours indicate probabilities of obtaining flood depths more than 0.5m.

4.5 Discussion on the results

The flood extent for the simulated result of 72 scenarios were compared. Flood extent varies for different scenarios with different conditions such as the daily (high and low tide) and biweekly (spring and neap tide) tidal variation, sea level rise and angle of landfall (Figure 9Figure 9).

- 5 Three worst case scenarios (Scenario S1, S2 and S3) were compared by generating flood maps, calculating total flooded areas and total damages. The flood maps for Scenario S1, S2 and S3 (Figure 8Figure 8) demonstrated that a large area wais flooded for all the breach locations. However, Figure 9 indicates that the flood extent is different for different scenarios. More thanAt least 25% of the total area of Polder 48 was inundated for the three scenarios (Table 3). In the case of all three considered scenarios, the inundation area having flood depths from 0.5 to 1.0 m, was larger than the inundation areas with other flood
- 10 depths (Figure 10Figure 10). The inundation area with flood depths more than 1m was largest for Scenario <u>S</u>3, due to the depressions close to the dikes (Figure 10Figure 10). The rice fields were flooded most while the shrimp ponds were flooded least in all the scenarios (Table 3).

Flood risk was quantified with damage due to floods (negative consequences) and probability of occurrence. The total estimated damages due to flooding for Scenario S1, S2 and S3 were 10.7, 10.6 and 8.6 million Euros, respectively (Table

15 <u>4Table 4</u>). For all the scenarios, a 1-in-25 year cyclone event was considered. The damage to the settlements was greater than other land classes for all the scenarios (<u>Table 4Table 4</u>). Rice fields were flooded most but they did not experience the highest damage compared to other landuse classes (Table 3 and <u>Table 4Table 4</u>). This can be explained by the high damages in settlements compared to rice fields (<u>Table 4Table 4</u>). The damage to crops depends on the flood depth, duration and overland flow velocity. For simplification, only the damage related to flood depth was used. As the probability of cyclones were

considered the same for all the scenarios, the calculated damage governed the estimated flood risk, i.e., higher damage to the settlements translated as higher risk of flooding. The primary economic activity of the inhabitants of the study area is farming (BBS, 2011) and most of the inhabitants are poor (with a poverty rate of 0.628) (Alamgir *et al.*, 2018). Even though the estimated damage and risk of flooding to crops were much less compared to other land uses, it will affect the people living in

5 the study area most as they depend on the farming of rice for their livelihood (Nasreen *et al.*, 2013). Hasan *et al.* (2004) found out that the dependence on fishing (in the sea) by the inhabitants of Polder 48 are increasing due to loss of crops by flood, loss of productivity, lack of jobs and poverty. Fishing in the sea is a risky profession forin the coastal region of Bangladesh as it yields lower economic returns leading to enhanced poverty (Hasan *et al.*, 2004).

The damage was maximum with flood depths 0.1 to 0.5m for all the scenarios (Figure 11Figure 11). The damage due to 10 inundation less than 0.1m was small and insignificant. The damage is a function of flood depth but the unit is per unit area(per m²). Therefore, if the flood extent for higher depth is lower, the damage due to flood might be lower even though the flood damage increases significantly for inundation more than 0.5m according to the developed depth damage curves (Figure 7Figure $\frac{7}{2}$).

Generated PFM indicated that the areas adjacent to the dike facing the seaside, have higher probability of flooding and the rice

15 fields are more prone to flooding (Figure 13Figure 13). Moreover, the areas protected by mangrove forest might also be flooded due toif breaching of the unprotected location of the dike is breached (Figure 13Figure 13), stressing the importance of proper maintenance of the dike everywhere.

Scenario 1 had higher risk of flooding as the <u>The</u> damage due to flooding was maximum for Scenario <u>S</u>1 which results in higher risk of flooding for scenario <u>S</u>1. Total flooded area for settlements of Scenario <u>S</u>1 was lower than Scenario <u>S</u>2 (Table 3) but

- 20 the estimated damage for settlements of Scenario <u>S</u>1 was more than Scenario <u>S</u>2 (<u>Table 4Table 4</u>). This indicates that the settlements for Scenario <u>S</u>1 were exposed to greater flood depth and higher risk of flooding than Scenario <u>S</u>2. Furthermore, Scenario <u>S</u>1 had similar total damage due to flood with lower flood extent than Scenario <u>S</u>2 (Table 3 and <u>Table 4Table 4</u>). Considering these facts, Scenario <u>S</u>1 was selected as the worst case Scenario and breaching at the western part of the sea facing dike was identified as the critical location for breaching during cyclone.
- 25 The scenarios with the effect of climate change (sea level rise) had more damage compared to the scenarios without climate change. Scenario_S1, scenario_S2 and scenario_S3 were associated with had-the highest storm surge height. With the same set of conditions without climate change (sea level rise) the storm surge height was 6.52 m PWD (Table 2). The damage corresponding to breaching of eastern, central and western locations of the dike due to the storm surge without climate change impactfor breaching of eastern, central and western breach were 23.3%, 20.5% and 21.7% lower-respectively lower than the
- 30 <u>damages with the climate change. and t</u>The corresponding values for the flood extent were 30.1%, 21.67% and 27.21% <u>lower</u>, respectively lower than the flood extent areas with the climate change impact.

The probability of occurrence of the storm surge and damage caused by inundation were taken into consideration for the risk calculation. In case of breaching of the dike, the probability of flooding was considered the same as the probability of occurrence of storm surge. The depicted risk map (Figure 12Figure 12) shows the areas adjacent to the dike breach is at higher risk and the risk reduces as the flood propagates towards east.

5 Canals are used as a mode of transportation by the inhabitants of the area. Most of the economic activities and residential areas are by the canals. The risk analysis show that the areas at highest risk are the settlements by the canals (Figure 12Figure 12). Therefore, although canals plays a crucial role in the economy and social life of the area, they also increase the risk of flooding and probability of higher damage to the adjacent areas.

Land use plan plays an important role in reduction of vulnerability to disasters (Burby, 1998). Probabilistic flood maps (PFM)
can be used for land use planning (Alfonso *et al.*, 2016). For better understanding of the area at risk of flooding due to breaching of dike, probabilistic flood maps (PFM) were generated for the study area (Figure 12Figure 12 and Figure 13Figure 13). The results of 72 Scenarios from Scenario matrix was used for calculation of PFM. The areas adjacent to the sea dikes had higher probability of flooding due to breaching of dike for both PFMs. The areas inland had lower probability of flooding. Existing land use indicates that the areas with lower probability of flooding are mostly rice fields (Figure 12Figure 12 and Figure 13Figure 13). Land use zoning and management using the PMF can reduce the vulnerably.

5. Conclusions

A 1D-2D coupled model was developed to investigate the inundation pattern inside a polder -due to breaching of a dike by cyclone induced storm surges. Different second se

- 20 results of The three worst case the results of these SSs cenarios S1, S2 and S3 were compared based onusing the total flooded area and estimated damage. The comparison led Estimated damage and flood extent were compared to the identifyication of the critical location of dike breaching during a cyclone. The fFlood risk map and probabilistic flood map were generated for the dike breaching during a storm surge using the results of the developed sScenarios to identify the areas at higher risk and higher probability of flooding.
- 25 Flood iInundation for the three worst case sScenarios S1, S2 and S3 indicated that the maximum flooded area was obtained corresponding to occurs during for the breaching of the central part of the sea facing dike. Most flooded area had For all three breaching locations most of the flooded aArea had with -flood depth of 0.1 to 0.5 m. was largest for all three breaching locations, The highest depth was obtained corresponding to witch Sscenario S2 (when breaching is in the central part) having the highest depth. The dDamage for sScenarios S1 (breaching inat the western part) and Scenario S2 (breaching inat the central part).
- 30 part) were equal., <u>In scenario S1 the damage was higher corresponding to whereas Scenario 1 had higher damage for flood</u> depth of 0.1m to 0.5 m than to 0.5 to 1 m whereas in and Sscenario S2 the had higher damage was higher corresponding to for flood depth of 0.5m to 1.0m than to 0.1 to 0.5m. From these findings it can be concluded that the flood extents, flood depth

and damage due to flood in case of breaching of the dike dependeds on the breach location. Moreover, the comparison of the flood damages and flood extent led to identification of <u>s</u>Scenario <u>S</u>1 as the worst case <u>s</u>Scenario and <u>the</u> western part of the sea facing dike as the critical location for breaching.

The scenarios considering the effect of-climate change (sea level rise) indicated that the flood extent and damage due to flood

5 will increase with sea level rise.

<u>Flood risk was calculated as the product of occurrence probability of flood event and negative consequences (damage).</u> The generated flood risk maps indicated that for all the <u>s</u>-scenarios areas adjacent to the dike and canals inside the polder had higher risk of flooding. For better access to the canals, for transportation and livelihood, development of infrastructure and households nearby the canals- increases <u>the</u> vulnerability. Similarly, developing land for infrastructure and household on the country side

10 of the dikes increases vulnerability. Combining effect of increased vulnerability and higher flood depth results in elevated risk of flooding due to dike breach during a cyclone.

Inundation maps of all 72 scenarios were compared to generate the probabilistic flood map. Probabilistic flood maps generated by considering all the Scenarios-which indicated that the areas with rice fields and settlements are the least and the settlements are the most probable areasland use to be <u>for-floodedingrespectively</u>. Although the inhabitants are mostly dependent on

- 15 agriculture, the flooding of settlements will cause most damage and forced relocation. Measured storm surge level for previous cyclones were unavailable. Therefore, for this research synthetic water level time series wasere generated considering the storm surge height presented by Islam *et al.*₇(-2013), for a cyclone of 25 year return period. The probability of flooding in a protected area is complicated and Furthermore, it was assumed that the eyclone will always cause breaching which resulted in probability of storm surge occurrence and breaching are the same having the same
- 20 probability of occurrence. Limited number of field observations were available to compare the results of 2D model. The limited calibration possibility of hydraulic models is stresses the importance of field observations pre_, post_ and during_flood_events. As the future land use data were not available, current land_use has been used for the future second as well. The primary objective of the research was to present a methodology for generating FRM and PFM for the breaching of dike

during a cyclone. Due to the lack of data on the existing condition and previous history of breaching of the dike, the probability

- of the dike breaching could not be determined. Comprehensive surveys should <u>mustshould</u> be conducted to determine the pphysical condition of the existing embankments and their breach history. Using this data, a joint probability of flooding due to storm surges and breaching <u>mayshould</u> be considered <u>infor</u> future studies. As the sea beach outside the dike on the sea side was not included in the 2D model, the effect of mangrove forest could not be determined. <u>A s</u>Single breach <u>location</u> was considered for all the developed sScenarios. The probability of multiple dike breaching for a polder should be studieds as well.
- 30 Moreover, due to lack <u>of</u> data, the storm surge height for <u>the</u> present <u>s</u>Scenarios was used for future <u>s</u>Scenarios as well. As the sea surface temperature will change in the future due <u>to climate change</u>CC, the height and <u>the</u>-intensity of the storm surges will be <u>a</u>effected as well. Research on the change of storm surge height and intensity due to <u>climate change</u>CC should be conducted in the future. <u>Bathymetric data with coaurse grid resolution from GEBCO was used for sea Aa</u>s <u>the</u> the-measured bathymetric data for the sea was not available, the data provided by GEBCO was used which has coarse grids</u>. Furthermore,

the study relied on the previous literatures for developing depth damage curves. Conducting field survey to generate these curves will provide more reliable damages due to flood. The developed and simulated model depended on the field measurements and logical assumptions which might be the source of errors. For damages, only direct damages were included. Inclusion of indirect damages will provide more realistic estimates.

- 5 Bangladesh is a hazard prone country and cyclone induced storm surge is one of many natural disasters experienced by the coast of Bangladesh. The storm surges cause severe damage to the earthen embankment/dikes protecting the coastal polders and flood the area inside the coastal polders. The methodology presented in this paper to develop the 1D-2D inundation model, PFM, risk maps and to identify the critical locations for breaching can assist in better preparedness against flooding and help in by improved flood risk assessment, damage reduction by land use zoning and management, improved monitoring and
- 10 maintenance of the dike at the critical location and flood forecasting. Land use zoning using the risk maps and PFM can lead the settlements, growing tourism and dry fish industry of the study area to safe or flood free zone for future development and relocation. At present, the PFM and FRM due to storm surges and breaching of the dikes are not available for the coastal polders. The methodology to generate PFM and FRM presented in this research has the potential to provide the PFM and FRM for coastal polders of the Bangladesh.
- 15 Climate change will likely cause increase in the frequency and intensity of the cyclone around the world. This will call for large investments for the improvement of existing or new protection works for the deltas. Identification and prioritising maintenance of critical locations of dike breaching can potentially prevent a disaster. Non-structural tools such as land use zoning with the help of flood risk maps and probabilistic flood maps have the potential to reduce the risk and the damage due to flood due to dike breaching. The method presented in this research can potentially be utilized for the deltas around the world
- 20 to reduce vulnerability and flood risk due to dike breach caused by cyclone induced storm surges.

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