



## The Role of Unmanned Aerial Vehicles (UAVs) In Monitoring Rapidly Occuring Landslides

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**Abstract:** This study used the Unmanned Aerial Vehicle (UAV), which was designed and produced to monitor rapidly occurring landslides in forest areas. It was aimed to determine the location data for the study area using image sensors integrated into the UAV. The study area was determined as the landslide sites located in the Taşlıçiftlik Campus of Gaziosmanpaşa University, Turkey. It was determined that landslide activities were on going in the determined study area and data was collected regarding the displacement of materials. Additionally, it was observed that data about landslides may be collected in a fast and sensitive way using UAVs, and this method is proposed as a new approach. Flights took place over a total of five different periods. In order to determine the direction and coordinate variables for the developed model, eight Ground Control Points (GCPs), whose coordinates were obtained with the GNSS method, were placed on the study area. In each period, approximately 190 photographs were investigated. The photos obtained were analysed using the PIX4D software. At the end of each period, the RMS and Ground Sample Distance (GSD) values of the GCPs were calculated. Orthomosaic and Digital Surface Models (DSM) were produced for the location and height model. The results showed that max RMS=±3.3 cm and max GSD=3.57cm/1.40 in. When the first and fifth periods are compared; the highest spatial displacement value  $\Delta S = 111.0$  cm, the highest subsidence value  $\Delta h = 37.3$  cm and the highest swelling value  $\Delta h = 28.6$  cm as measured.

**Keywords:** Unmanned Aerial Vehicles (UAV); landslides; ground sample distance (GSD); digital surface model (DSM); orthomosaic

### 1. Introduction

Landslides are a worldwide phenomenon that create dramatic physical and economic effects and sometimes lead to tragic deaths. During landslides two main factors occur, which are human and environmental effects. The human factors may be controlled; however, it is very difficult to control the topography and soil structure (Turner et al., 2015). Thus, landslides cause disasters on a global scale each year. These disasters are increasing in number due to the incorrect usage of the land. The main reason for the increase in landslide disasters is the instability of the soil and erodibility on the surface. Surface soil erodibility takes place as a result of various issues, such as deforestation, an increase in consumption by an increasingly larger population, uncontrolled land usage, etc. (Nadim et al., 2006). Landslides are primarily disasters that take place in mountainous and sloped areas around the world (Dikau et al., 1996). Landslides do not always show characteristic occurrences, however, they are usually triggered by increased stress on sloped surfaces. This triggering can occur faster because of short or long periods of heavy rain, earthquakes, or subterranean activity (Lucier et al., 2014). During landslide monitoring, a number of factors need to be continuously assessed, including the: extent



47 of the landslide, detection of fissure structures, topography of the land and rate of  
 48 displacements that could be related to fracture (Niethammer et al., 2010). Understanding  
 49 the mechanism of landslides may be made easier by being able to measure the vertical  
 50 and horizontal displacements. This is possible by forming a Digital Surface Model (DSM)  
 51 of the landslide area.

52 The calculation of displacements by Differential GPS (DGPS), total station, airborne  
 53 Light Detection and Ranging (LIDAR) and Terrestrial Laser Scanner (TLS) techniques  
 54 have been used since the beginning of the 2000s (Nadim et al., 2006). Additionally,  
 55 remote sensing has been put into operation in combination with other techniques  
 56 (Mantovani et al., 1996). There are several platforms, which are used to monitor landslide  
 57 occurrences via the method of remote sensing, where displacement data can be collected.  
 58 These include remote sensing satellites, manned aerial vehicles, specially equipped land  
 59 vehicles and, as a new method, Unmanned Aerial Vehicles (UAV) (Rau et al., 2011).  
 60 These UAV are aerial vehicles that are able to fly without crew automatically or semi-  
 61 automatically based on aerodynamics principles. UAV systems have become popular in  
 62 solving problems in various fields and applications (Saripalli et al., 2003; Tahar et al.,  
 63 2011). In parallel with the developing technology, UAVs have been used in recent years  
 64 in integration with the Global Positioning System (GPS), Inertial Measurement Units  
 65 (IMU) and high definition cameras and they have also been used in remote sensing (RS),  
 66 digital mapping and photogrammetry in scientific studies. While satellites and manned  
 67 aerial vehicles are able to gather location data in high resolutions of 20-50 cm/pixel,  
 68 UAVs are able to obtain even higher resolutions of 1 cm/pixel, as they are able to fly at  
 69 lower altitudes (Hunt et al., 2010). Indeed, UAV Photogrammetry opens up various new  
 70 applications in close-range photogrammetry in the geomatics field (Eisenbeiss 2009).  
 71 Monitoring landslides using UAV systems is an integrated process involving ground  
 72 surveying methods and aerial mapping methods. All measurement devices that require  
 73 details are integrated to UAVs, which fly at lower altitudes than satellites or planes. All  
 74 positional data are collected safely from above, except for determining and measuring the  
 75 control points (Nagai et al., 2008).

76 This study was conducted in the landslide site at the Organized Industrial Zone near a  
 77 campus of Gaziosmanpaşa University. The area of the studied field was approximately  
 78 50 hectares. The Multicopter was produced by the Department of Geomatics Engineering  
 79 at Gaziosmanpaşa University (GOP) and the firm TEKNOMER was used for this study.  
 80 A Sony Alpha 6000 (Ilce 6000) camera, IMU and GPS systems, produced for moving  
 81 platforms, were integrated to the UAV. Five different flights took place on different dates  
 82 in the study area and an average of 290 photographs were obtained on each flight. Eight  
 83 ground control points (GCPs), which were well distributed over the data area, were set  
 84 up in the landslide area (Figure 6). The positional information about the ground control  
 85 points was collected using four dual-frequency Geodesic GNSS receivers (Trimble,  
 86 Topcon). Two hours of static GNSS measurements were analyzed in 3D using the Leica  
 87 LGO V.8.3 software in connection to the TUSAGA Active System.

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## 89 2. System Design



This study used the multicopter, which was produced by the department of Geomatics Engineering at Gaziosmanpaşa University (GOP) (Figure 1a and b). The designed multicopter consisted of a platform and camera systems.



Figure 1a. The UAV and environmental components

Figure 1b. The UAV in the air

### 2.1. UAV Platform

UAV platforms provide crucial alternative solutions for environmental research (Nex and Remondino, 2014). The UAV environmental components used in this study were integrated into the multicopter as seen Figure 2. The platform had a blade-span of 0.80 m, height of 0.36 m, weight of 4.4 kg and operating weight of 5 kg. All sensors were placed on the carrying platform to achieve operating integrity. The carrying platform operated at the speed of 14 m/sec while shooting photos. The multicopter had a stabilized camera gimbal to take nadir photos during the flight. The characteristics of the carrying platform are given in Table 1.



Figure 2. UAV environmental components



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Table 1. Platform technical specifications

Specification	Technical Details
Weight	4.3 kg
Wing Span	74 cm
Payload	4 kg
Height	34 cm with GPS Antenna
Range	4 km
Endurance	30 min
Speed	14 m/sec
Maximum Speed	70 km - 30 mm /sec
Radio Control	433 MHz
Frame Transponder (FPV)	2.4 GHz
Telemetry Radio	868 MHz
GPS	5 Hz – 72 channels
Battery	6S li-po 25C 1600 Mah
Monitor	40 Channels 5.8 GHz DVR 7 inch LED system
Gimbal	Mapping Gimbal
Motors	35 x 15 Brushless Motor
Frame	22 mm 3K Carbon
ESC	60 Ampere 400 Hz
Prop	15 x 55 inch Carbon

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## 115 2.2. Camera System

116 In this study, a Sony ILCE-6000 E16mm F2.8-16.0-6000x4000 (RGB) camera  
 117 was used for collecting visible imagery (Figure 3). Table 2 shows the characteristics of  
 118 the camera. The main controller of the UAV was programmed to shoot photos regularly,  
 119 every two seconds. This way, the shutter of the camera was triggered at the desired  
 120 frequency intervals.

121 The camera and the main flight controller card were connected using a special  
 122 cable. Vibration isolation materials were used between the camera and the UAV to  
 123 prevent the effects of flight vibrations on the camera. During the flight, all photos were  
 124 taken in the RAW format and stored in the memory of the camera.

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Figure 3. The camera used in the study

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134 Table 2. Technical properties of the camera  
 (<http://pdf.crse.com/manuals/4532055411.pdf> [Accessed 2017 May 10])



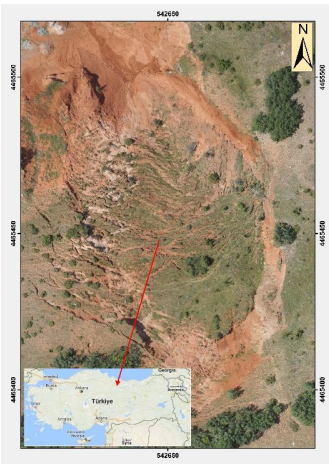
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Property	Technical Detail
Dimensions	4.72 x 2.63 x 1.78 in
Weight	10.05 oz (Body Only) / 12.13 oz (with battery and media)
Megapixels	12 MP
Sensor Type	APS-C
Sensor Size	APS-C type (23.5 x 15.6 mm)
Number of pixels (effective)	24.3 MP
Number of pixels (total)	Approx. 24.7 megapixels
ISO sensitivity (recommended exposure index)	ISO 100-25600
Clear image zoom	Approx. 2x
Digital zoom (still image)	L: Approx. 4x; M: Approx. 5.7x; S: Approx. 8x
LCD Size	3.0 in wide type TFT LCD
LCD Dots	921,600 dots
Viewfinder Type	0.39 in-type electronic viewfinder (colour)
Shutter speed	Still images: 1/4000 to 30 sec, Bulb, Movies: 1/4000 to 1/4 (1/3 steps) up to 1/60 in AUTO mode (up to 1/30 in Auto slow shutter mode)
Flash sync. Speed	1/160 sec.

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138 **3. Study Area**

139       This study was carried out in order to monitor the landslides with UAV in Tokat  
140 Province. The study area was selected to track the landslides that began in the area where  
141 factories and industrial enterprises are located. There is a great landslide risk in this  
142 industrial area, it is a preexisting situation and if the motion continues or accelerates it  
143 could mean great danger for the nearby factories. For this reason, the movement needs to  
144 be monitored.  
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Figure 4. The study area

The coordinates of the landslide area used for the study are given as 40° 19' 20.8" N, 36° 30' 0.6" E. The study area is shown in Figure 4.

### 3.1. Soil Properties of the Study Area

The oldest layer at the research area is Paleozoic aged metaophiolite (Metadunite, amphibolite/Metagabbro). The sedimentary layer, which is called eosin aged "Çekerek formation", is over the metaophiolite layer. This formation consists of sandstone, pebble, silt and clay (Sumengen, 1998).

Soil samples were collected from three different locations at 0-0.2 and 0.2-0.4 m depths and analyzed for soil particle distribution using the Bouyoucos hydrometer method (Gee and Bauder, 1986). The fraction greater than 2 mm diameter was separated and reported as coarse material (Gee and Bauder, 1986). The dispersion ratio was calculated using Equation 1 (Middleton 1930). The aggregate stability index was calculated by the wet sieving method (Yoder 1936).

$$\text{Dispersion Ratio} = \{D (\text{Silt} + \text{Clay}) / T (\text{Silt} + \text{Clay})\} \times 100 \quad (1)$$

Where D is dispersed silt + clay after 1kg of oven-dried soil in a litre of distilled water was shaken 20 times; T, is total silt + clay determined by the standard sedimentation method in a non-dispersed state. Some soil properties of the study area are presented in Table 3. The results of the mechanical analysis in most of the studied soils showed a high clay and silt and low sand content. The textural classes of the soil objects were determined as clay (C), clay loam (CL) and silt loam (SiL). The high clay and silt content of study area increased disaggregation by leading to imbalances in the moisture content of different soil layers instead of aggregation. This effect may result in high runoff, soil loss and weathering processes. When the topsoil and subsoil layers are compared, the clay content of the topsoil layer decreased, the silt content was the same and the sand content increased at study site one. At study site two, the higher clay and lower silt contents were detected more in the subsoil than in the topsoil. The same result was observed for study site three. Textural differences between the topsoil and subsoil created moisture differences in the soil layers and this situation may result in large mass movements. In the study area, the coarse material varied between 4.2 and 31.0%, depending on the mass transportation.

Table 3. Some soil properties of the study area

Study Site	Soil Depth (m)	Texture				Coarse Material %	Aggregate Stability %	Dispersion Ratio %
		Clay %	Sand %	Silt %	Class			
1	0.0-0.2	40.0	28.7	31.3	CL	13.0	34.3	36.9
	0.2-0.4	37.5	31.2	31.3	CL	31.0	41.3	60.0
2	0.0-0.2	50.0	11.2	38.8	C	4.2	13.9	57.8
	0.2-0.4	52.5	11.2	36.3	C	19.7	46.2	49.3
3	0.0-0.2	40.0	13.7	46.3	SiL	15.7	18.8	36.3
	0.2-0.4	42.5	13.7	43.8	SiL	6.6	13.1	47.9





To evaluate the forces on the soil resistance to the mass movement of the study area, aggregate stability and dispersion ratio indexes were used. The aggregate stability of the soil objects was under 46.2% and showed low aggregate stability with a high risk of soil movement. The dispersion ratio index indicated a sharp boundary between erodible and non-erodible soils, since a dispersion ratio greater than 10 indicated erodible soils and less than 10 indicated non-erodible soils. The dispersion values of the study area were greater than 10 with high erosion risk.

### 3.2. 3D Ground Control Points

A total of eight 3D GCPs were used in the study area. The GCPs were placed in a way so that they could be easily seen in photos taken from above, near the landslide site, but where future landslides would not affect them (Figure 5). All GCPs were placed as concrete blocks, which were topped with side wings with dimensions of 40x15 cm so they could be easily detected in the computer environment. The geometrical distribution of the GCPs in the study area is given in Figure 6.

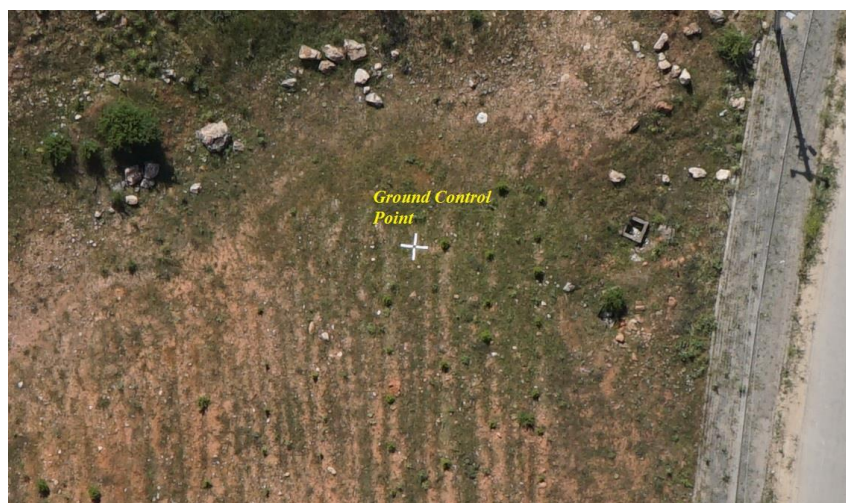


Figure 5. Ground Control Point (GCP)

The 3D positional information of the GCPs was collected by the CORS-TR System (Mekik et al., 2011) using Topcon GR3 dual-frequency GNSS (Global Navigation Satellite System) receivers. GNSS data was collected for a minimum of two hours for each point and it was computed via static analysis at the datum of ITRF96 and epoch of 2005.00. With the dual-frequency receivers used, the horizontal sensitivity of the GCPs were found to be  $\pm 3\text{mm} + 0.5\text{ ppm}$ , while the vertical sensitivity was found to be  $\pm 5\text{ mm} + 0.5\text{ ppm}$ .

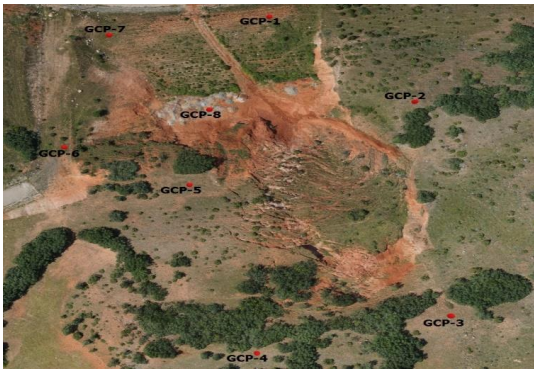


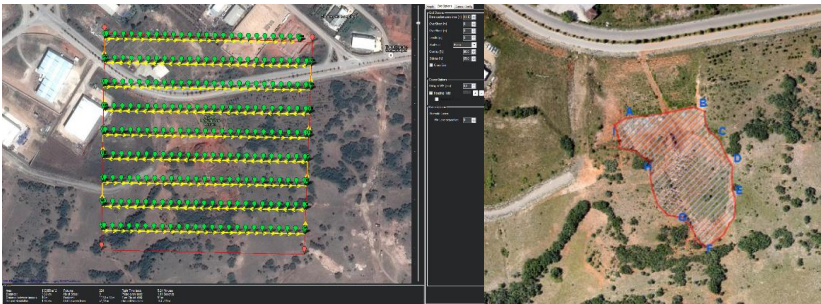
Figure 6. The geometric distribution of GCPs

### 3.3. Flight Planning and Shooting of the Photos

Flight plans were made following the GNSS measurements of the GCPs and obtaining their coordinates via analysis. The flights were carried out at five different periods following rainfall or snowfall, where the landslide area was the most active. The flight dates and flight altitude information are given in Table 4. The flight plan for the study area was set within the Mission Planner software with vertical overlapping of 80%, horizontal overlapping of 65%, a flight altitude of 100 meters and flying speed of 14 m/sec. A number of overlapping images were computed for each pixel of the orthomosaics. The green areas indicated an overlap of over five images for every pixel (Figure 8) (<http://ardupilot.org/planner/docs/common-history-of-ardupilot.html> accessed 2017 June 3, 2017). The prepared flight plan (Figure 7a, b) was uploaded onto the UAV and the photos of the study area were obtained. The same input parameters were used in all periods for the flights and an average of 190 photos were taken. Meteorological factors were considered in shooting the aerial photos and the most suitable time periods were chosen for the flights.

Table 4. Dates of flights

Period	Flight Date	Flight Altitude (m)
1	February 17, 2016	100
2	March 22, 2016	100
3	April 9, 2016	100
4	June 10, 2016	100
5	July 21, 2016	100







230 Figure 7a. Flight plan for the study area Figure 7b. Borders of the landslide area

### 231 3.4. Point Cloud, 3D Model and Orthomosaic Production

232 The photos obtained from each flight period were stored in a computer with an  
 233 empty storage space of 100 GB and 8 GB of RAM. The photos were analyzed by using  
 234 the Pix4D software.

235 In the first stage, quality checks were performed for the images, dataset, camera  
 236 optimization and GCPs and these were calculated and the software produced the quality  
 237 check report for each of the time periods. The Ground Sampling Distance (GSD) is the  
 238 distance between two consecutive pixel centers measured on the ground. The bigger the  
 239 value of the image GSD, the lower the spatial resolution of the image and the less visible  
 240 details; GCPs are used to correct the geographical location of a project.

241 At least three GCPs are required to produce point cloud, orthomosaics and 3D  
 242 models, which come from the desired datum from the photographs taken. Optimal  
 243 accuracy is usually obtained with 5 - 10 GCP [22]. GCPs should also be well distributed  
 244 over the data area. To orient and balance the point cloud and the 3D model, Helmert  
 245 Transformation was applied. The transformation process was carried out with seven  
 246 parameters, which were generated from a minimum of three GCPs and point cloud  
 247 relations (Niethammer et al., 2011; Watson, 2006; Crosilla and Alberto, 2002).

248  
 249 In this study, the geographical location of the project was oriented and balanced through  
 250 the use of eight GCPs. The RMS and GSD values of GCPs are given in Table 5.

251 Table 5. GCPs' mean RMS errors

Periods	RMS (mm)	GSD (cm/in)
#1	±23	3.11 / 1.22
#2	±29	3.04 / 1.20
#3	±28	3.50 / 1.38
#4	±33	3.27 / 1.28
#5	±18	3.57 / 1.40

254  
 255 The second stage increased the density of 3D points of the 3D model, which were  
 256 computed in the first stage. It represents the minimum number of valid re-projections of  
 257 this 3D point to the images. Each 3D point must be projected correctly in at least two  
 258 images. This option can be recommended for small projects, but it creates a point cloud  
 259 with more noise. The minimum number of matches is three in Pix4D, as a default, but up  
 260 to six can be chosen. This option reduces noise and improves the quality of the point  
 261 cloud, but it can calculate fewer 3D points in the endpoint cloud.

262 In this project, the number of matches was taken as three. The second stage results  
 263 are given in Table 6.

264 Table 6. Average density per m<sup>3</sup>

Periods	Average Density (per m <sup>3</sup> )	Grid DSM (cm)
#1	106.31	100
#2	104.15	100
#3	100.72	100
#4	128.15	100
#5	117.17	100



In the third stage, a Digital Surface Model (DSM) and an orthomosaic were formed for all periods. DSM formation was achieved by the triangulation method with 100 cm grid intervals. The aspect maps, showing the landslide motion direction for the first and last periods, were derived by using the DSMs of periods 1 and 5. The differences between these maps can be seen, especially in the western and northern areas (Figure 8). This means that there was a movement between periods.

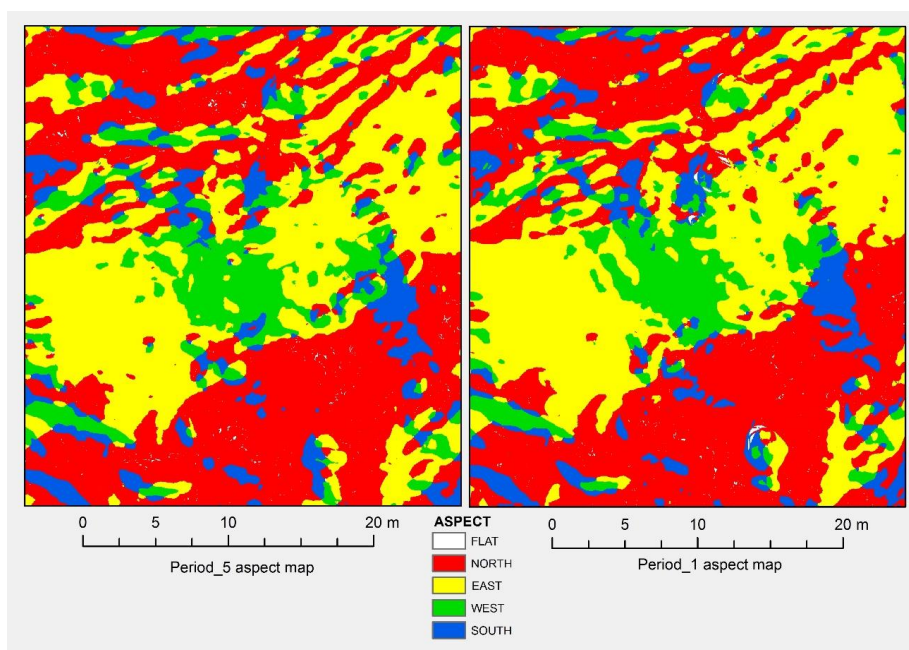


Figure 8. Aspect maps of period 5 (left) and 1 (right).

### 3.5. Analysis of the Point Clouds, 3D Models and Orthomosaics

Seventy-three object points were determined in the study area in order to monitor the speed and direction of the landslide movement (Figure 9). These points, which represent the topography, were chosen from the clearly visible details in the model and the field.

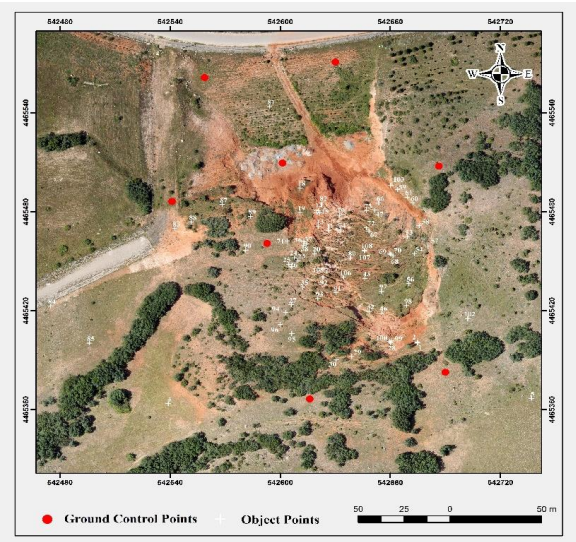


Figure 9. Ground Control and Object points

The 3D position information, orthomosaics and DSMs of the object points were produced in each period. The 3D position data were compared consecutively. As a result of these comparisons, differential displacements were calculated between T2 and T1, T3 and T2, T4 and T3, T5 and T4, and are given in Figures 10, 11, 12 and 13. Additionally, Figure 14 provides a diagram showing the two-dimensional position shift ( $\Delta s$ ) and height ( $\Delta H$ ) changes between T5 and T1 (the last and the first periods).

According to these diagrams and Table 7:

- a) Points shown with a star (\*) are at the centre of the area of motion and their positional displacement is higher than the median value ( $>21$  cm),
- b) Points shown without a star are outside the landslide area and their positional and height displacement values are lower than the median value ( $<21$  cm).

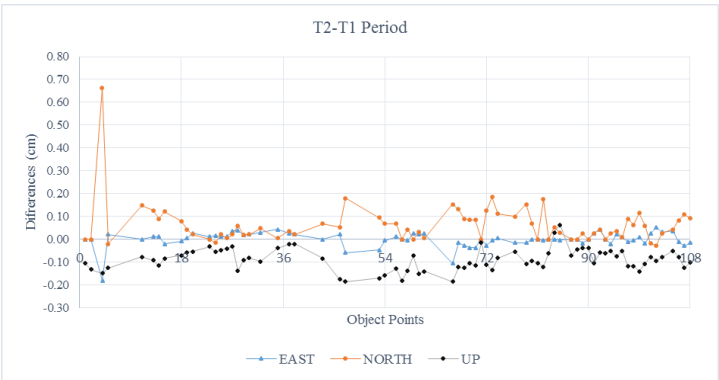


Figure 10. T2-T1 period differences

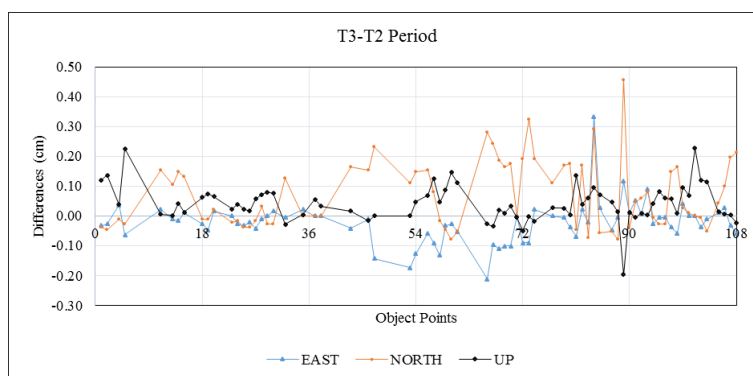


Figure 11. T3-T2 period differences

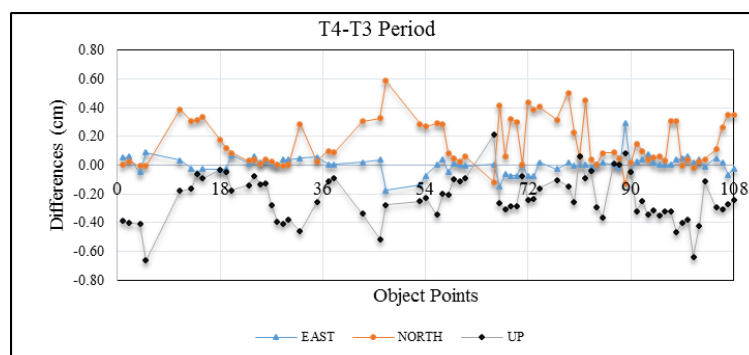


Figure 12. T4-T3 period differences

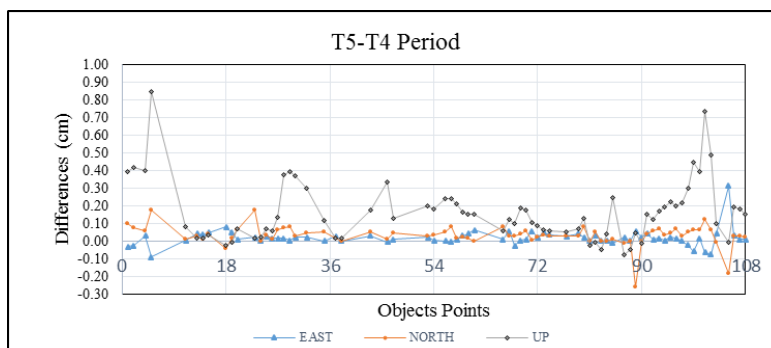


Figure 13. T5-T4 period differences

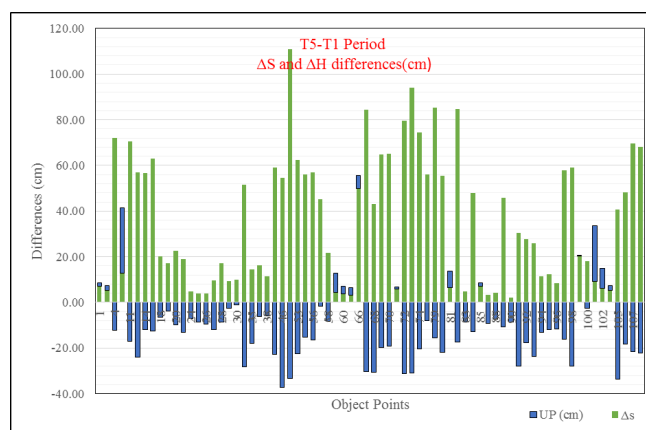


Figure 14. T5-T4 period  $\Delta S$  and  $\Delta H$  differences (cm)

The maps in Figure 8 show that the points with high positional displacement also had a change of height by 70%. The positional and height displacement correlation coefficient was calculated as  $\sigma=0.73$ . Thus, position and height changes are highly related to each other.





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Table 7. Vertical and horizontal motion magnitudes (cm) of the points

Bigger than median movement value (>21 cm)			Smaller than median movement value (<21 cm)		
Number of Object Points	Movement of Δs (cm)	Movement UP (cm)	Number of Object Points	Movement of Δs (cm)	Movement UP (cm)
47*	111.0	33.2	18	20.3	6.4
73*	94.0	31.0	23	19.0	13.3
79*	85.3	15.5	100	18.0	2.5
82*	84.8	17.4	28	17.2	8.6
67*	84.4	30.2	19	17.1	3.8
72*	79.7	31.2	37	16.4	6.3
74*	74.6	20.3	35	14.5	17.8
4*	72.1	12.2	5	12.9	5.0
11*	70.6	17.1	95	12.2	12.0
107*	69.7	21.7	94	11.4	13.2
108*	68.2	22.1	38	11.4	5.8
70*	65.1	19.2	30	9.9	1.1
69*	64.8	19.6	27	9.8	12.0
15*	63.0	12.5	29	9.5	2.5
53*	62.4	22.4	101	9.1	5.0
43*	59.1	22.9	96	8.5	11.6
98*	58.9	27.8	77	8.0	8.0
97*	57.8	16.1	85	7.2	1.5
13*	57.0	24.0	1	7.0	1.6
56*	56.8	16.6	81	6.4	7.2
14*	56.7	11.9	102	6.2	8.7
54*	56.1	15.3	71	5.8	1.0
80*	55.6	21.9	103	5.4	1.8
46*	54.7	37.3	2	5.3	2.0
32	51.6	28.2	66	5.0	5.6
106	48.3	18.1	83	4.9	8.7
84	47.9	13.0	24	4.8	7.2
89	45.7	10.6	59	4.3	8.4
57	45.3	1.7	88	4.1	7.5
68	43.0	30.7	26	4.0	9.4
105	40.8	33.8	25	3.8	8.6
91	30.3	27.8	60	3.7	3.4
93*	26.0	23.6	87	3.4	9.2
20*	22.6	9.7	61	3.2	3.1

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350 As a result of the positional movements obtained in the landslide area, point velocity  
 351 vectors ( $V_x$ ,  $V_y$ ,  $V_z$ ) were calculated using Equation 2 below, and they are given in Table  
 352 8. It was found that the general characteristic surface movement of the landslide took  
 353 place in the north-south direction (Figure 15).

354

$$355 \quad V\{x, y, z\} = \frac{\Delta V\{x, y, z\}}{\Delta t} \quad 365 \quad (2)$$

356 Here:

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358  $\Delta t$ : T5-T1 periods time difference,

359  $\Delta V\{x, y, z\}$ : The difference between Cartesian coordinate components between the T5 and  
 360 T1 periods.

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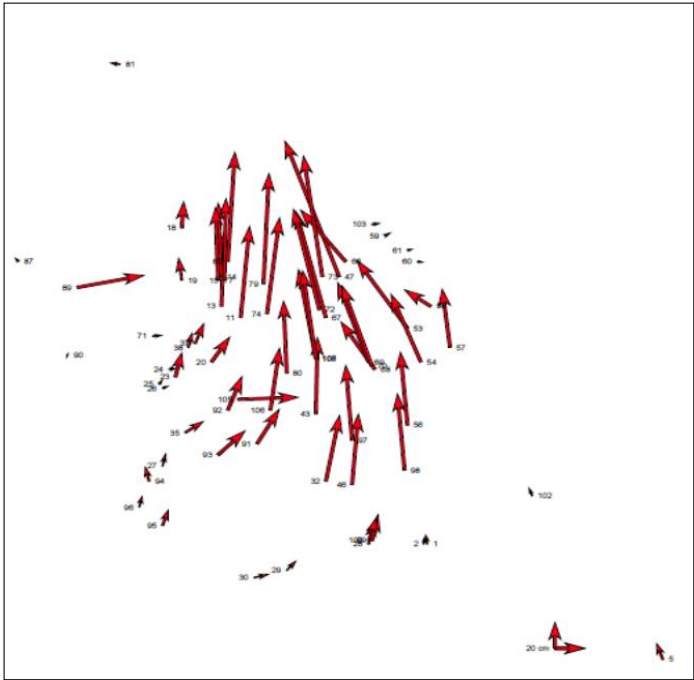


Figure 15. Characteristic surface movement of the landslide (m/year)

According to the velocity vectors, it may be seen that the landslide did not display a typical structure. The maximum movement was found to be  $v_x = -2.095$  m,  $v_z = -2.932$  m and  $v_y = 2.036$  m.

Table 7 and Figure 14 show that the object points numbered #47, 73, 79, 82, 67, 72, 74, 4, 11, 107, 108, 69, 70, which were at the centre of the movement and had positional (2D) displacement ( $>50$  cm). The object points numbered #29, 101, 77, 96, 01, 85, 71, 81, 102, 02, were outside the center of the movement and had positional (2D) displacement ( $<10$  cm).



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Table 8. Object points annual velocity vectors

#Object				#Object			
No	Vx (m/year)	Vy (m/year)	Vz (m/year)	No	Vx (m/year)	Vy (m/year)	Vz (m/year)
1	-0.068	-0.095	0.219	68	-0.851	-1.605	0.279
2	-0.064	-0.023	0.186	69	-1.111	-1.700	1.189
4	-1.214	-1.568	1.593	70	-1.122	-1.685	1.212
5	0.474	0.171	0.966	71	-0.108	0.172	0.036
11	-1.767	-1.035	1.480	72	-1.721	-2.010	1.362
13	-1.583	-1.084	0.968	73	-2.095	-2.077	1.772
14	-1.241	-0.996	1.233	74	-1.955	-1.063	1.505
15	-1.435	-1.001	1.387	77	-1.159	-0.913	1.306
18	-0.530	-0.333	0.392	79	-1.958	-1.268	1.908
19	-0.346	-0.343	0.364	80	-1.434	-1.139	0.981
20	-0.804	-0.064	0.285	81	0.265	-0.079	0.191
23	-0.707	-0.335	0.192	82	-2.009	-1.260	1.853
24	-0.261	0.013	-0.148	83	-0.052	-0.177	-0.293
25	-0.284	-0.118	-0.109	84	-1.588	0.275	0.615
26	-0.306	-0.066	-0.171	85	-0.147	0.016	0.206
27	-0.472	-0.255	-0.017	87	-0.200	-0.239	-0.136
28	-0.575	-0.234	0.246	88	-0.048	-0.151	-0.253
29	-0.311	0.037	0.133	89	-1.317	0.964	0.001
30	-0.268	0.214	0.043	90	-0.136	-0.124	-0.252
32	-1.716	-0.857	0.711	91	-1.379	-0.373	0.073
35	-0.776	-0.059	-0.181	92	-1.044	-0.355	0.289
37	-0.534	-0.140	0.263	93	-1.216	-0.108	-0.040
38	-0.380	-0.164	0.164	94	-0.429	-0.430	-0.002
43	-1.585	-1.112	1.050	95	-0.544	-0.240	0.037
46	-1.874	-1.190	0.605	96	-0.436	-0.238	-0.041
47	-1.863	-2.932	2.036	97	-1.307	-1.136	1.166
53	-0.734	-1.995	0.890	98	-1.564	-1.349	0.932
54	-0.865	-1.497	1.048	99	-0.437	-0.140	0.537
56	-1.285	-1.143	1.129	100	-0.479	-0.112	0.397
57	-0.747	-0.770	1.154	101	0.412	0.206	0.786
58	-0.051	-0.790	0.150	102	0.122	0.000	0.350
59	0.064	0.208	0.244	103	-0.089	0.163	0.069
60	0.007	0.165	0.063	105	-1.587	0.589	-0.723
61	-0.014	0.123	0.095	106	-1.385	-0.747	0.862
66	0.018	-1.281	1.183	107	-1.472	-1.579	1.336
67	-1.722	-2.124	1.498	108	-1.519	-1.493	1.297

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#### 392 4. Results and Conclusions

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As a result of this study, we found that unmanned aerial vehicles have undeniable advantages in disaster management and they have clear benefits over other methods. The monitoring process must be continued for taking necessary precautions in case of



continuity and acceleration of landslides. Monitoring the landslide velocity is not possible with conventional systems. Firstly, it is not possible to monitor an ongoing movement in areas where the ground movement is active using ground surveying methods. These movements have to be monitored by using remote measurements (remote sensing, photogrammetry and UAV). Aerial photogrammetry and remote sensing techniques are not usually preferred as they are expensive, measurements cannot be made at the desired time, and they cannot achieve the sensitivity obtained with UAVs.

This study was carried out with the aim of monitoring the landslide acceleration of movement of an area that could lead to great danger if it continues. In this study, GSD values of 3.11/1.22-3.57/1.40 cm/in were reached with a flight altitude of 100 m. It is not possible to reach these values with manned aerial vehicles or satellite images because flight altitudes will be higher in both cases and the result of this situation will decrease the sensitivity. Thus, it was concluded that the most effective situational awareness and monitoring might be achieved by UAVs. Additionally, if it is desired to increase sensitivity in monitoring landslides, GCPs should be assigned in a suitable distribution with a suitable geometry at places that are not affected by the landslide, and the area of flight should be widened based on these GCPs.

This study shows that UAVs are important tools in determining the speeds and directions of landslide movements. In addition, landslide movements may be monitored in real time using UAVs, allowing decisions to be made and precautions to be taken. In the light of the UAV data obtained, early warning may prevent more tragic disasters and the necessary precautions can be taken. Another important issue that needs to be emphasized at the end of this study is that, with other traditional methods, the monitoring of landslides and determination of the speed and direction of movement in real time is impossible.

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