



47 of the landslide, detection of fissure structures, topography of the land and rate of
48 displacements that could be related to fracture (Niethammer et al., 2010). Understanding
49 the mechanism of landslides may be made easier by being able to measure the vertical
50 and horizontal displacements. This is possible by forming a Digital Surface Model (DSM)
51 of the landslide area.

52 The calculation of displacements by Differential GPS (DGPS), total station, airborne
53 Light Detection and Ranging (LIDAR) and Terrestrial Laser Scanner (TLS) techniques
54 have been used since the beginning of the 2000s (Nadim et al., 2006). Additionally,
55 remote sensing has been put into operation in combination with other techniques
56 (Mantovani et al., 1996). There are several platforms, which are used to monitor landslide
57 occurrences via the method of remote sensing, where displacement data can be collected.
58 These include remote sensing satellites, manned aerial vehicles, specially equipped land
59 vehicles and, as a new method, Unmanned Aerial Vehicles (UAV) (Rau et al., 2011).
60 These UAV are aerial vehicles that are able to fly without crew automatically or semi-
61 automatically based on aerodynamics principles. UAV systems have become popular in
62 solving problems in various fields and applications (Saripalli et al., 2003; Tahar et al.,
63 2011). In parallel with the developing technology, UAVs have been used in recent years
64 in integration with the Global Positioning System (GPS), Inertial Measurement Units
65 (IMU) and high definition cameras and they have also been used in remote sensing (RS),
66 digital mapping and photogrammetry in scientific studies. While satellites and manned
67 aerial vehicles are able to gather location data in high resolutions of 20-50 cm/pixel,
68 UAVs are able to obtain even higher resolutions of 1 cm/pixel, as they are able to fly at
69 lower altitudes (Hunt et al., 2010). Indeed, UAV Photogrammetry opens up various new
70 applications in close-range photogrammetry in the geomatics field (Eisenbeiss 2009).
71 Monitoring landslides using UAV systems is an integrated process involving ground
72 surveying methods and aerial mapping methods. All measurement devices that require
73 details are integrated to UAVs, which fly at lower altitudes than satellites or planes. All
74 positional data are collected safely from above, except for determining and measuring the
75 control points (Nagai et al., 2008).

76 This study was conducted in the landslide site at the Organized Industrial Zone near a
77 campus of Gaziosmanpaşa University. The area of the studied field was approximately
78 50 hectares. The Multicopter was produced by the Department of Geomatics Engineering
79 at Gaziosmanpaşa University (GOP) and the firm TEKNOMER was used for this study.
80 A Sony Alpha 6000 (Ilce 6000) camera, IMU and GPS systems, produced for moving
81 platforms, were integrated to the UAV. Five different flights took place on different dates
82 in the study area and an average of 290 photographs were obtained on each flight. Eight
83 ground control points (GCPs), which were well distributed over the data area, were set
84 up in the landslide area (Figure 6). The positional information about the ground control
85 points was collected using four dual-frequency Geodesic GNSS receivers (Trimble,
86 Topcon). Two hours of static GNSS measurements were analyzed in 3D using the Leica
87 LGO V.8.3 software in connection to the TUSAGA Active System.

88

89 2. System Design



90 This study used the multicopter, which was produced by the department of
91 Geomatics Engineering at Gaziosmanpaşa University (GOP) (Figure 1a and b). The
92 designed multicopter consisted of a platform and camera systems.

93



100 Figure 1a. The UAV and environmental components

Figure 1b. The UAV in the air

101 **2.1. UAV Platform**

102 UAV platforms provide crucial alternative solutions for environmental research
103 (Nex and Remondino, 2014). The UAV environmental components used in this study
104 were integrated into the multicopter as seen Figure 2. The platform had a blade-span of
105 0.80 m, height of 0.36 m, weight of 4.4 kg and operating weight of 5 kg. All sensors
106 were placed on the carrying platform to achieve operating integrity. The carrying platform
107 operated at the speed of 14 m/sec while shooting photos. The multicopter had a stabilized
108 camera gimbal to take nadir photos during the flight. The characteristics of the carrying
109 platform are given in Table 1.



110

111

Figure 2. UAV environmental components

112



113

Table 1. Platform technical specifications

Specification	Technical Details
Weight	4.3 kg
Wing Span	74 cm
Payload	4 kg
Height	34 cm with GPS Antenna
Range	4 km
Endurance	30 min
Speed	14 m/sec
Maximum Speed	70 km - 30 mm /sec
Radio Control	433 MHz
Frame Transponder (FPV)	2.4 GHz
Telemetry Radio	868 MHz
GPS	5 Hz – 72 channels
Battery	6S li-po 25C 1600 Mah
Monitor	40 Channels 5.8 GHz DVR 7 inch LED system
Gimbal	Mapping Gimbal
Motors	35 x 15 Brushless Motor
Frame	22 mm 3K Carbon
ESC	60 Ampere 400 Hz
Prop	15 x 55 inch Carbon

114

115 2.2. Camera System

116 In this study, a Sony ILCE-6000 E16mm F2.8-16.0-6000x4000 (RGB) camera
 117 was used for collecting visible imagery (Figure 3). Table 2 shows the characteristics of
 118 the camera. The main controller of the UAV was programmed to shoot photos regularly,
 119 every two seconds. This way, the shutter of the camera was triggered at the desired
 120 frequency intervals.

121 The camera and the main flight controller card were connected using a special
 122 cable. Vibration isolation materials were used between the camera and the UAV to
 123 prevent the effects of flight vibrations on the camera. During the flight, all photos were
 124 taken in the RAW format and stored in the memory of the camera.

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Figure 3. The camera used in the study

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Table 2. Technical properties of the camera

134

(<http://pdf.crse.com/manuals/4532055411.pdf>[Accessed 2017 May 10])



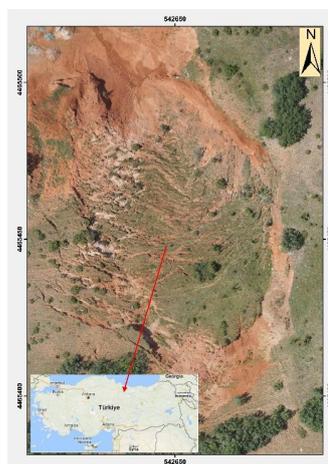
135

Property	Technical Detail
Dimensions	4.72 x 2.63 x 1.78 in
Weight	10.05 oz (Body Only) / 12.13 oz (with battery and media)
Megapixels	12 MP
Sensor Type	APS-C
Sensor Size	APS-C type (23.5 x 15.6 mm)
Number of pixels (effective)	24.3 MP
Number of pixels (total)	Approx. 24.7 megapixels
ISO sensitivity (recommended exposure index)	ISO 100-25600
Clear image zoom	Approx. 2x
Digital zoom (still image)	L: Approx. 4x; M: Approx. 5.7x; S: Approx. 8x
LCD Size	3.0 in wide type TFT LCD
LCD Dots	921,600 dots
Viewfinder Type	0.39 in-type electronic viewfinder (colour)
Shutter speed	Still images: 1/4000 to 30 sec, Bulb, Movies: 1/4000 to 1/4 (1/3 steps) up to 1/60 in AUTO mode (up to 1/30 in Auto slow shutter mode)
Flash sync. Speed	1/160 sec.

136
 137

138 3. Study Area

139 This study was carried out in order to monitor the landslides with UAV in Tokat
 140 Province. The study area was selected to track the landslides that began in the area where
 141 factories and industrial enterprises are located. There is a great landslide risk in this
 142 industrial area, it is a preexisting situation and if the motion continues or accelerates it
 143 could mean great danger for the nearby factories. For this reason, the movement needs to
 144 be monitored.
 145



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 147



148

Figure 4. The study area

149

The coordinates of the landslide area used for the study are given as 40° 19' 20.8"

150

N, 36° 30' 0.6" E. The study area is shown in Figure 4.

151

152

3.1. Soil Properties of the Study Area

153

The oldest layer at the research area is Paleozoic aged metaophiolite (Metadunite, amphibolite/Metagabbro). The sedimentary layer, which is called eosin aged “Çekerek formation”, is over the metaophiolite layer. This formation consists of sandstone, pebble, silt and clay (Sumengen, 1998).

154

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157

Soil samples were collected from three different locations at 0-0.2 and 0.2-0.4 m depths and analyzed for soil particle distribution using the Bouyoucos hydrometer method (Gee and Bauder, 1986). The fraction greater than 2 mm diameter was separated and reported as coarse material (Gee and Bauder, 1986). The dispersion ratio was calculated using Equation 1 (Middleton 1930). The aggregate stability index was calculated by the wet sieving method (Yoder 1936).

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$$\text{Dispersion Ratio} = \{D (\text{Silt} + \text{Clay}) / T (\text{Silt} + \text{Clay})\} \times 100 \quad (1)$$

164

Where D is dispersed silt + clay after 1kg of oven-dried soil in a litre of distilled water was shaken 20 times; T, is total silt + clay determined by the standard sedimentation method in a non-dispersed state. Some soil properties of the study area are presented in Table 3. The results of the mechanical analysis in most of the studied soils showed a high clay and silt and low sand content. The textural classes of the soil objects were determined as clay (C), clay loam (CL) and silt loam (SiL). The high clay and silt content of study area increased disaggregation by leading to imbalances in the moisture content of different soil layers instead of aggregation. This effect may result in high runoff, soil loss and weathering processes. When the topsoil and subsoil layers are compared, the clay content of the topsoil layer decreased, the silt content was the same and the sand content increased at study site one. At study site two, the higher clay and lower silt contents were detected more in the subsoil than in the topsoil. The same result was observed for study site three. Textural differences between the topsoil and subsoil created moisture differences in the soil layers and this situation may result in large mass movements. In the study area, the coarse material varied between 4.2 and 31.0%, depending on the mass transportation.

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Table 3. Some soil properties of the study area

Study Site	Soil Depth (m)	Texture				Coarse Material %	Aggregate Stability %	Dispersion Ratio %
		Clay %	Sand %	Silt %	Class			
1	0.0-0.2	40.0	28.7	31.3	CL	13.0	34.3	36.9
	0.2-0.4	37.5	31.2	31.3	CL	31.0	41.3	60.0
2	0.0-0.2	50.0	11.2	38.8	C	4.2	13.9	57.8
	0.2-0.4	52.5	11.2	36.3	C	19.7	46.2	49.3
3	0.0-0.2	40.0	13.7	46.3	SiL	15.7	18.8	36.3
	0.2-0.4	42.5	13.7	43.8	SiL	6.6	13.1	47.9

182



183 To evaluate the forces on the soil resistance to the mass movement of the study
184 area, aggregate stability and dispersion ratio indexes were used. The aggregate stability
185 of the soil objects was under 46.2% and showed low aggregate stability with a high risk
186 of soil movement. The dispersion ratio index indicated a sharp boundary between erodible
187 and non-erodible soils, since a dispersion ratio greater than 10 indicated erodible soils
188 and less than 10 indicated non-erodible soils. The dispersion values of the study area were
189 greater than 10 with high erosion risk.
190

191 **3.2. 3D Ground Control Points**

192 A total of eight 3D GCPs were used in the study area. The GCPs were placed in a way so
193 that they could be easily seen in photos taken from above, near the landslide site, but
194 where future landslides would not affect them (Figure 5). All GCPs were placed as
195 concrete blocks, which were topped with side wings with dimensions of 40x15 cm so
196 they could be easily detected in the computer environment. The geometrical distribution
197 of the GCPs in the study area is given in Figure 6.
198



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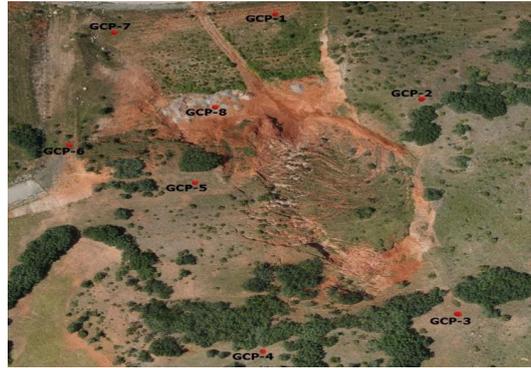
200

Figure 5. Ground Control Point (GCP)

201

202 The 3D positional information of the GCPs was collected by the CORS-TR
203 System (Mekik et al., 2011) using Topcon GR3 dual-frequency GNSS (Global
204 Navigation Satellite System) receivers. GNSS data was collected for a minimum of two
205 hours for each point and it was computed via static analysis at the datum of ITRF96 and
206 epoch of 2005.00. With the dual-frequency receivers used, the horizontal sensitivity of
207 the GCPs were found to be $\pm 3\text{mm} + 0.5\text{ ppm}$, while the vertical sensitivity was found to
208 be $\pm 5\text{ mm} + 0.5\text{ ppm}$.

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Figure 6. The geometric distribution of GCPs

212

3.3. Flight Planning and Shooting of the Photos

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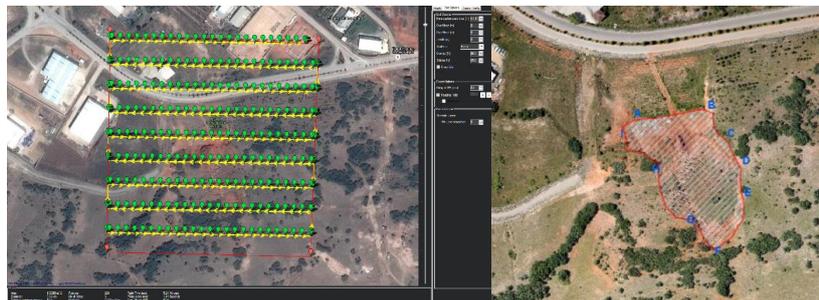
Flight plans were made following the GNSS measurements of the GCPs and obtaining their coordinates via analysis. The flights were carried out at five different periods following rainfall or snowfall, where the landslide area was the most active. The flight dates and flight altitude information are given in Table 4. The flight plan for the study area was set within the Mission Planner software with vertical overlapping of 80%, horizontal overlapping of 65%, a flight altitude of 100 meters and flying speed of 14 m/sec. A number of overlapping images were computed for each pixel of the orthomosaics. The green areas indicated an overlap of over five images for every pixel (Figure 8) (<http://ardupilot.org/planner/docs/common-history-of-ardupilot.html> accessed 2017 June 3, 2017). The prepared flight plan (Figure 7a, b) was uploaded onto the UAV and the photos of the study area were obtained. The same input parameters were used in all periods for the flights and an average of 190 photos were taken. Meteorological factors were considered in shooting the aerial photos and the most suitable time periods were chosen for the flights.

227

Table 4. Dates of flights

Period	Flight Date	Flight Altitude (m)
1	February 17, 2016	100
2	March 22, 2016	100
3	April 9, 2016	100
4	June 10, 2016	100
5	July 21, 2016	100

228



229



230 Figure 7a. Flight plan for the study area Figure 7b. Borders of the landslide area

231 **3.4. Point Cloud, 3D Model and Orthomosaic Production**

232 The photos obtained from each flight period were stored in a computer with an
 233 empty storage space of 100 GB and 8 GB of RAM. The photos were analyzed by using
 234 the Pix4D software.

235 In the first stage, quality checks were performed for the images, dataset, camera
 236 optimization and GCPs and these were calculated and the software produced the quality
 237 check report for each of the time periods. The Ground Sampling Distance (GSD) is the
 238 distance between two consecutive pixel centers measured on the ground. The bigger the
 239 value of the image GSD, the lower the spatial resolution of the image and the less visible
 240 details; GCPs are used to correct the geographical location of a project.

241 At least three GCPs are required to produce point cloud, orthomosaics and 3D
 242 models, which come from the desired datum from the photographs taken. Optimal
 243 accuracy is usually obtained with 5 - 10 GCP [22]. GCPs should also be well distributed
 244 over the data area. To orient and balance the point cloud and the 3D model, Helmert
 245 Transformation was applied. The transformation process was carried out with seven
 246 parameters, which were generated from a minimum of three GCPs and point cloud
 247 relations (Niethammer et al., 2011; Watson, 2006; Crosilla and Alberto, 2002).

248
 249 In this study, the geographical location of the project was oriented and balanced through
 250 the use of eight GCPs. The RMS and GSD values of GCPs are given in Table 5.

251
 252 Table 5. GCPs' mean RMS errors

Periods	RMS (mm)	GSD (cm/in)
#1	±23	3.11 / 1.22
#2	±29	3.04 / 1.20
#3	±28	3.50 / 1.38
#4	±33	3.27 / 1.28
#5	±18	3.57 / 1.40

254
 255 The second stage increased the density of 3D points of the 3D model, which were
 256 computed in the first stage. It represents the minimum number of valid re-projections of
 257 this 3D point to the images. Each 3D point must be projected correctly in at least two
 258 images. This option can be recommended for small projects, but it creates a point cloud
 259 with more noise. The minimum number of matches is three in Pix4D, as a default, but up
 260 to six can be chosen. This option reduces noise and improves the quality of the point
 261 cloud, but it can calculate fewer 3D points in the endpoint cloud.

262 In this project, the number of matches was taken as three. The second stage results
 263 are given in Table 6.

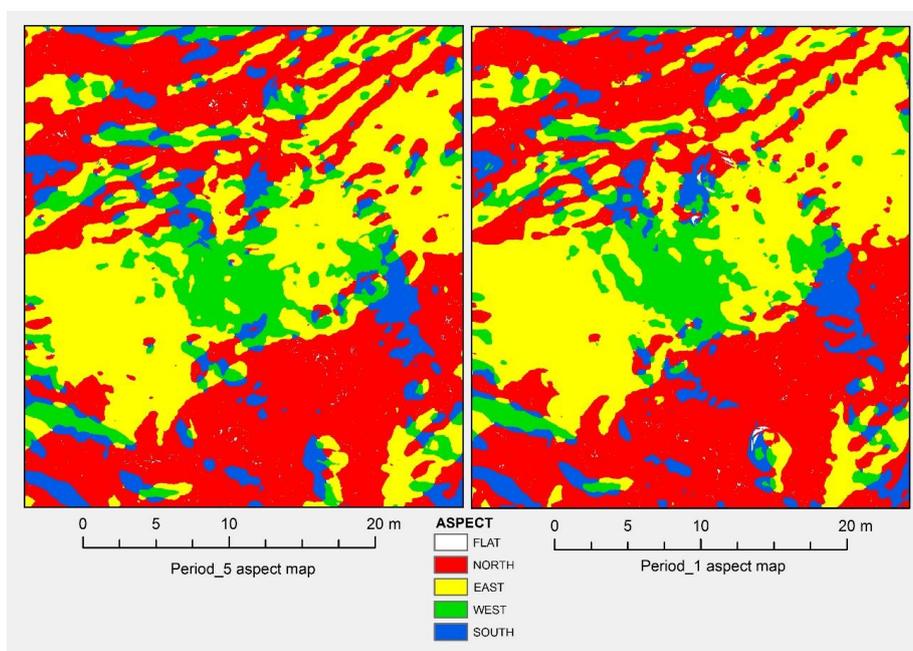
264
 265 Table 6. Average density per m³

Periods	Average Density (per m ³)	Grid DSM (cm)
#1	106.31	100
#2	104.15	100
#3	100.72	100
#4	128.15	100
#5	117.17	100



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In the third stage, a Digital Surface Model (DSM) and an orthomosaic were formed for all periods. DSM formation was achieved by the triangulation method with 100 cm grid intervals. The aspect maps, showing the landslide motion direction for the first and last periods, were derived by using the DSMs of periods 1 and 5. The differences between these maps can be seen, especially in the western and northern areas (Figure 8). This means that there was a movement between periods.



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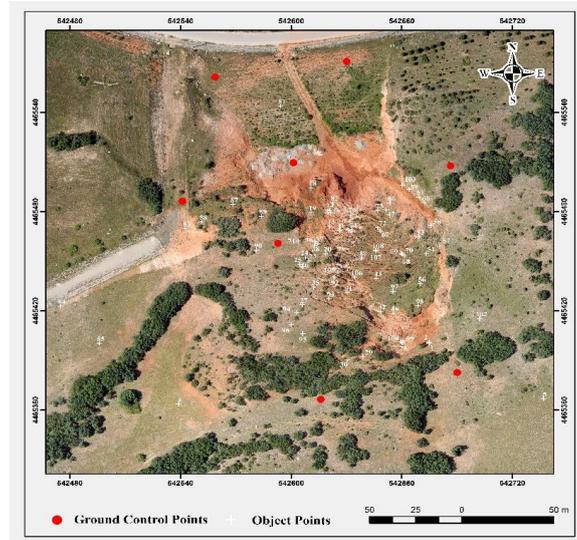
Figure 8. Aspect maps of period 5 (left) and 1 (right).

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3.5. Analysis of the Point Clouds, 3D Models and Orthomosaics

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Seventy-three object points were determined in the study area in order to monitor the speed and direction of the landslide movement (Figure 9). These points, which represent the topography, were chosen from the clearly visible details in the model and the field.



285

286

Figure 9. Ground Control and Object points

287 The 3D position information, orthomosaics and DSMs of the object points were produced
 288 in each period. The 3D position data were compared consecutively. As a result of these
 289 comparisons, differential displacements were calculated between T2 and T1, T3 and T2,
 290 T4 and T3, T5 and T4, and are given in Figures 10, 11, 12 and 13. Additionally, Figure
 291 14 provides a diagram showing the two-dimensional position shift (Δs) and height (ΔH)
 292 changes between T5 and T1 (the last and the first periods).
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According to these diagrams and Table 7:

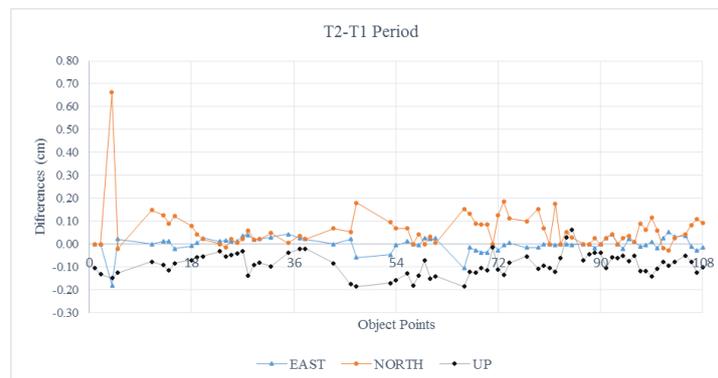
295

a) Points shown with a star (*) are at the centre of the area of motion and their
 296 positional displacement is higher than the median value (>21 cm),

297

b) Points shown without a star are outside the landslide area and their positional and
 298 height displacement values are lower than the median value (<21 cm).
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Figure 10. T2-T1 period differences

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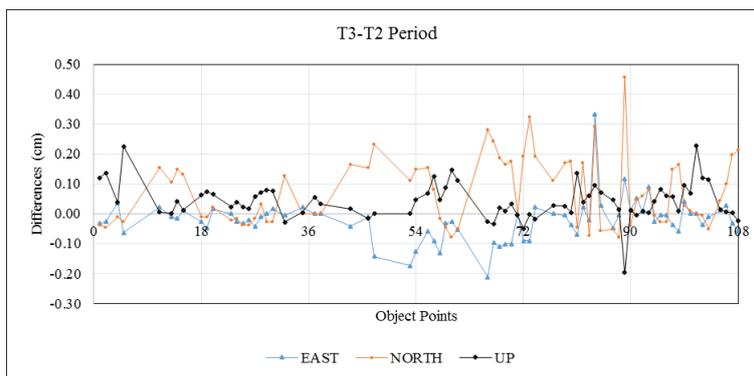


Figure 11. T3-T2 period differences

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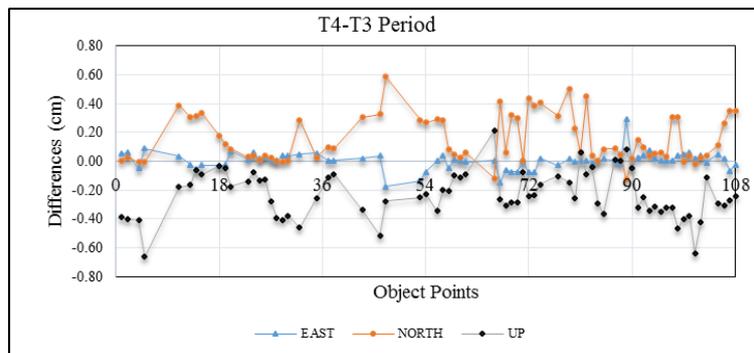


Figure 12. T4-T3 period differences

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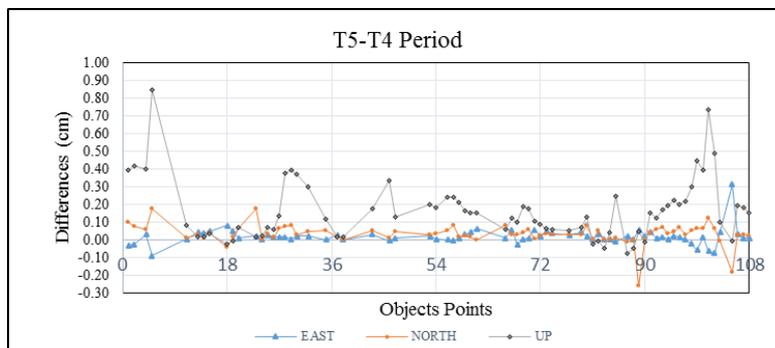
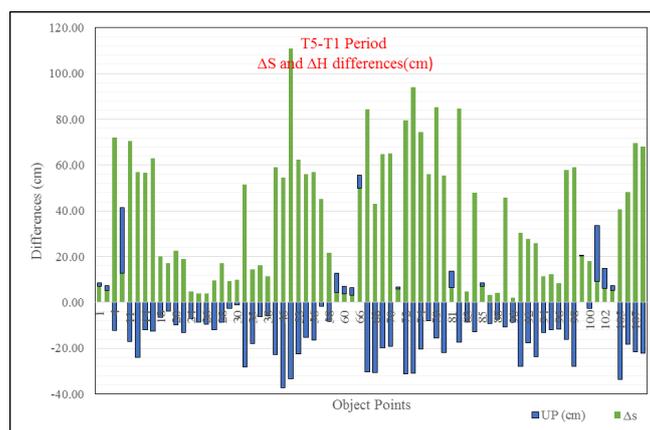


Figure 13. T5-T4 period differences



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Figure 14. T5-T4 period ΔS and ΔH differences (cm)

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The maps in Figure 8 show that the points with high positional displacement also had a change of height by 70%. The positional and height displacement correlation coefficient was calculated as $\rho=0.73$. Thus, position and height changes are highly related to each other.



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 348

Table 7. Vertical and horizontal motion magnitudes (cm) of the points

Bigger than median movement value (>21 cm)			Smaller than median movement value (<21 cm)		
Number of Object Points	Movement of Δs (cm)	Movement UP (cm)	Number of Object Points	Movement of Δs (cm)	Movement UP (cm)
47*	111.0	33.2	18	20.3	6.4
73*	94.0	31.0	23	19.0	13.3
79*	85.3	15.5	100	18.0	2.5
82*	84.8	17.4	28	17.2	8.6
67*	84.4	30.2	19	17.1	3.8
72*	79.7	31.2	37	16.4	6.3
74*	74.6	20.3	35	14.5	17.8
4*	72.1	12.2	5	12.9	5.0
11*	70.6	17.1	95	12.2	12.0
107*	69.7	21.7	94	11.4	13.2
108*	68.2	22.1	38	11.4	5.8
70*	65.1	19.2	30	9.9	1.1
69*	64.8	19.6	27	9.8	12.0
15*	63.0	12.5	29	9.5	2.5
53*	62.4	22.4	101	9.1	5.0
43*	59.1	22.9	96	8.5	11.6
98*	58.9	27.8	77	8.0	8.0
97*	57.8	16.1	85	7.2	1.5
13*	57.0	24.0	1	7.0	1.6
56*	56.8	16.6	81	6.4	7.2
14*	56.7	11.9	102	6.2	8.7
54*	56.1	15.3	71	5.8	1.0
80*	55.6	21.9	103	5.4	1.8
46*	54.7	37.3	2	5.3	2.0
32	51.6	28.2	66	5.0	5.6
106	48.3	18.1	83	4.9	8.7
84	47.9	13.0	24	4.8	7.2
89	45.7	10.6	59	4.3	8.4
57	45.3	1.7	88	4.1	7.5
68	43.0	30.7	26	4.0	9.4
105	40.8	33.8	25	3.8	8.6
91	30.3	27.8	60	3.7	3.4
93*	26.0	23.6	87	3.4	9.2
20*	22.6	9.7	61	3.2	3.1

349

350 As a result of the positional movements obtained in the landslide area, point velocity
 351 vectors (V_x , V_y , V_z) were calculated using Equation 2 below, and they are given in Table
 352 8. It was found that the general characteristic surface movement of the landslide took
 353 place in the north-south direction (Figure 15).

354

355
$$V\{x, y, z\} = \frac{\Delta V\{x, y, z\}}{\Delta t} \quad (2)$$

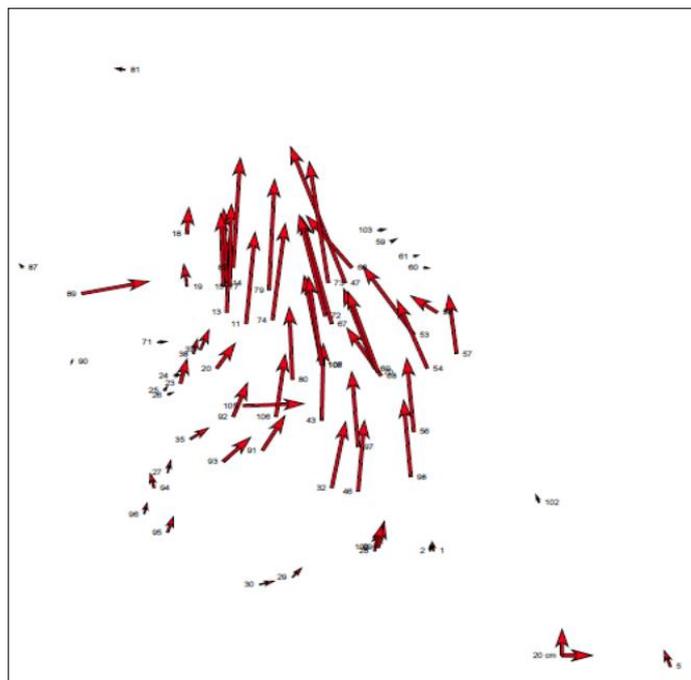
356 Here:

357

358 Δt : T5-T1 periods time difference,

359 $\Delta V\{x, y, z\}$: The difference between Cartesian coordinate components between the T5 and
 360 T1 periods.

361



362

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Figure 15. Characteristic surface movement of the landslide (m/year)

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According to the velocity vectors, it may be seen that the landslide did not display a typical structure. The maximum movement was found to be $v_x = -2.095$ m, $v_z = -2.932$ m and $v_y = 2.036$ m.

Table 7 and Figure 14 show that the object points numbered #47, 73, 79, 82, 67, 72, 74, 4, 11, 107, 108, 69, 70, which were at the centre of the movement and had positional (2D) displacement (>50 cm). The object points numbered #29, 101, 77, 96, 01, 85, 71, 81, 102, 02, were outside the center of the movement and had positional (2D) displacement (<10 cm).



389

Table 8. Object points annual velocity vectors

#Object				#Object			
No	Vx (m/year)	Vy (m/year)	Vz (m/year)	No	Vx (m/year)	Vy (m/year)	Vz (m/year)
1	-0.068	-0.095	0.219	68	-0.851	-1.605	0.279
2	-0.064	-0.023	0.186	69	-1.111	-1.700	1.189
4	-1.214	-1.568	1.593	70	-1.122	-1.685	1.212
5	0.474	0.171	0.966	71	-0.108	0.172	0.036
11	-1.767	-1.035	1.480	72	-1.721	-2.010	1.362
13	-1.583	-1.084	0.968	73	-2.095	-2.077	1.772
14	-1.241	-0.996	1.233	74	-1.955	-1.063	1.505
15	-1.435	-1.001	1.387	77	-1.159	-0.913	1.306
18	-0.530	-0.333	0.392	79	-1.958	-1.268	1.908
19	-0.346	-0.343	0.364	80	-1.434	-1.139	0.981
20	-0.804	-0.064	0.285	81	0.265	-0.079	0.191
23	-0.707	-0.335	0.192	82	-2.009	-1.260	1.853
24	-0.261	0.013	-0.148	83	-0.052	-0.177	-0.293
25	-0.284	-0.118	-0.109	84	-1.588	0.275	0.615
26	-0.306	-0.066	-0.171	85	-0.147	0.016	0.206
27	-0.472	-0.255	-0.017	87	-0.200	-0.239	-0.136
28	-0.575	-0.234	0.246	88	-0.048	-0.151	-0.253
29	-0.311	0.037	0.133	89	-1.317	0.964	0.001
30	-0.268	0.214	0.043	90	-0.136	-0.124	-0.252
32	-1.716	-0.857	0.711	91	-1.379	-0.373	0.073
35	-0.776	-0.059	-0.181	92	-1.044	-0.355	0.289
37	-0.534	-0.140	0.263	93	-1.216	-0.108	-0.040
38	-0.380	-0.164	0.164	94	-0.429	-0.430	-0.002
43	-1.585	-1.112	1.050	95	-0.544	-0.240	0.037
46	-1.874	-1.190	0.605	96	-0.436	-0.238	-0.041
47	-1.863	-2.932	2.036	97	-1.307	-1.136	1.166
53	-0.734	-1.995	0.890	98	-1.564	-1.349	0.932
54	-0.865	-1.497	1.048	99	-0.437	-0.140	0.537
56	-1.285	-1.143	1.129	100	-0.479	-0.112	0.397
57	-0.747	-0.770	1.154	101	0.412	0.206	0.786
58	-0.051	-0.790	0.150	102	0.122	0.000	0.350
59	0.064	0.208	0.244	103	-0.089	0.163	0.069
60	0.007	0.165	0.063	105	-1.587	0.589	-0.723
61	-0.014	0.123	0.095	106	-1.385	-0.747	0.862
66	0.018	-1.281	1.183	107	-1.472	-1.579	1.336
67	-1.722	-2.124	1.498	108	-1.519	-1.493	1.297

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392 4. Results and Conclusions

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As a result of this study, we found that unmanned aerial vehicles have undeniable advantages in disaster management and they have clear benefits over other methods. The monitoring process must be continued for taking necessary precautions in case of



397 continuity and acceleration of landslides. Monitoring the landslide velocity is not possible
398 with conventional systems. Firstly, it is not possible to monitor an ongoing movement in
399 areas where the ground movement is active using ground surveying methods. These
400 movements have to be monitored by using remote measurements (remote sensing,
401 photogrammetry and UAV). Aerial photogrammetry and remote sensing techniques are
402 not usually preferred as they are expensive, measurements cannot be made at the desired
403 time, and they cannot achieve the sensitivity obtained with UAVs.

404 This study was carried out with the aim of monitoring the landslide acceleration of
405 movement of an area that could lead to great danger if it continues. In this study, GSD
406 values of 3.11/1.22-3.57/1.40 cm/in were reached with a flight altitude of 100 m. It is not
407 possible to reach these values with manned aerial vehicles or satellite images because
408 flight altitudes will be higher in both cases and the result of this situation will decrease
409 the sensitivity. Thus, it was concluded that the most effective situational awareness and
410 monitoring might be achieved by UAVs. Additionally, if it is desired to increase
411 sensitivity in monitoring landslides, GCPs should be assigned in a suitable distribution
412 with a suitable geometry at places that are not affected by the landslide, and the area of
413 flight should be widened based on these GCPs.

414 This study shows that UAVs are important tools in determining the speeds and directions
415 of landslide movements. In addition, landslide movements may be monitored in real time
416 using UAVs, allowing decisions to be made and precautions to be taken. In the light of
417 the UAV data obtained, early warning may prevent more tragic disasters and the
418 necessary precautions can be taken. Another important issue that needs to be emphasized
419 at the end of this study is that, with other traditional methods, the monitoring of landslides
420 and determination of the speed and direction of movement in real time is impossible.

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