Earthquake Safety Analysis of Masonry Historical Building 1 2 Case Study: Historical Konya Gazi High School 3 4 M. Sami Donduren¹, Seyit Uguz² 5 6 7 Selcuk University, Faculty of Engineering, Department of Civil Engineering, 42060, Konya, Turkey 8 Uludag University, Department of Biosystems Engineering, 16150, Bursa, Turkey 9 10 Abstract. SUMMARY 11 It is substantially significant to protect insulate historical structures, which are an important part of our culture, 12 against for natural disasters such as earthquakes and to be transmitted to future generations. The structural 13 behaviour of historical buildings must beis difficult to well knowncharacterized to protect such structures 14 order to be able to determine how safe the historic buildings are against the earthquake effect, it is necessary to 15 determine the earthquake performance of the historical buildings in order to determine how safe the historical 16 buildings are for the earthquake effect. Nowadays, the most commonly used method for the modelling and 17 structural analysis of historical buildings systems with complex geometries is the finite element method. 18 In this study, Historical Konya Gazi High School was examined according to the present situation regarding the 19 design and construction features with "Regulations on buildings to be built in earthquake regions" and structural 20 analysis was performed in ETABS program. Graphs showing displacements, moments, shear forces and axial 21 forces are used to interpret the results of the finite element analysis of the Historical Gazi High School. It has 22 been informed about the stresses and damages that may be caused by any earthquake to this building, which has 23 been serving the students for 97 years. It is aimed that this work will be a study to suggest a solution in terms of 24 not losing the ourour historical values and delivering it to future generations. 25 Keywords: Earthquake, finite element methods, historical buildings 26 1. INTRODUCTION 27 28 Earthquakes cause damages and loss of lives in urban centres and cause significant losses in rural areas as well. 29 Almost all of the whole buildings in the countryside, and also a large part of the old buildings in the city centre 30 are masonry buildings. In addition, many of the historical buildings were built as masonry, wood and a mixture 31 of them. There is no regulation that can be used in analysing the structural systems of such buildings. Today, 32 regulations used in the design of masonry buildings are prepared for new structures, it is of the 33 substantially difficult to use these current regulations in the study of historical structures -because of these 34 regulations used in the design of masonry buildings are prepared for new structures. 35 Analysis of masonry buildings is rather exhausting complicated compared to reinforced buildings. Analysis 36 made by package Package programmes used to analyse for these kindkindse of buildings is are in-adequate. In 37 recent years, through the use of computer technology, plastic analysis method, -which the nonlinear material 38 properties and joints are taken into consideration, has become more and more widely used from than the classical 39 analysis methods on the analysis of for masonry structures. There are two types of approaches in the modelling 40 of masonry structures; micro modelling and macro modelling. In the micro modelling, masonry Masonry units 41 composed of bricks and mortar are modelled by separately in the micro modelling. Therefore, in the micro 42 modelling, the mechanical properties of the materials and binding materials of the structure need to be known

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characterized exactly. Micro modelling, which usually involves a large computational load, is suitable for local 43 44 analysis, but is not preferred for large-scale analysis. (Dabanli, 2008). Applications in this model are done by 45 using finite element methods, discrete elements and limit analysis. In the macro model used for plastic analysis, 46 the mechanical material properties of structure are defined by assuming as if the masonry structure materials are 47 homogeneous (<u>Cakti-Cakti</u> et al., 2013). The finite element methodFEM is generally used in the structural 48 analysis of masonry structures. In this analytical method, the structure is modelled and analysed by separating it 49 into finite elements in an appropriate number with regard to purpose of analysis. Package programs such as 50 ETABS and SAP2000 are widely used for the structural analysis done by using finite element methods.FEM. 51 In this study, the earthquake safety of the historical Konya Gazi High School was investigated according to the 52 present situation. This article provides information about the stresses and damages that may reveal due to any 53 earthquake in this building. which has been serving the students for 97 years. So that, tThis study will suggest 54 about protection of our historical values and delivering them to future generations. Earthquake safety of the 55 building was investigated by the ETABS programme which is one of the computer programmes used for 56 nonlinear static analysis. The ETABS program is software of the CSI Company and is especially designed for 57 3D static analysis of buildings. Structural analysis is done by using finite element method in the program.

58 2. CASE STUDY: HISTORICAL KONYA GAZI HIGH SCHOOL

59 2.1. Information about the buildingdentity of the Structure

The architecture of Konya Gazi High School, which is the subject of this study, is Mimar Muzaffer. The construction of the building started in 1914 and was completed in 1917. The building, which was opened in 1917, was used as Military High School until 1923. It was used as The name of the school was "Dar'ül Muallim"
between 1923-1934, "Konya Idadi" between 1934 and 1972 and Konya High School until 1972. The layout plan of Gazi High School is given in Figure 2.1.



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2.2. Architectural features

Figure_-2.1. The layout plan of Gazi High School

The historical Gazi High School is located in Konya city centercentre, at the intersection of Atatürk Street and Amber Reis Street. The building is positioned the south of the school area. There are other schoolhouse. buildings for sports hall, laboratories and conference halls in the school garden. The observed building is positioned the school area. The empty space in the middle of the set three buildings is used as a sports and ceremonial space. Because the building is a historical building, there-There is no architectural or static project of this historical e-building. For this reason, the architectural project of the building was made by taking

the relievo. Konya Gazi high school has a basement floor, ground floor and two normal floors. The height of the floors differs from floor to floor. Basement and ground floor heights are $5_{\frac{1}{2}}00$ m, first floor and second floor

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76 heights are 4,...50 m. In general, the condition of the building is good although some of the bearing walls have

77 local cracks, deterioration of mortar or stone, roof elements.

78 2.3. Structural System and Material Properties

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79 The building is not exactly symmetric and also is built with masonry structural system. The form of the structural 80 system varies with each floor. It was observed that rubble stone was used as material in the walls. It is thought 81 that the rubble stones used in this structure are brought from the Sille region in Konya. When the walls of the 82 structural system elements are examined, it is observed that the basement wall thickness is 90 cm, the ground 83 floor wall thickness is 80 cm, the first floor wall thickness is 75 cm and the second floor wall thickness is 70 cm. 84 It is known that the second floor of the building was rebuilt with renovation for restoration, but it could not be 85 verified because there were not enough resources.- The basement floor, the ground floor and the second floor 86 slabs are not visible from the coatings. However, it has been observed that horizontal beams were used in the 87 first story. Figure 2.2 shows the image of the first floor slab.



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89	Figure 2.2. Horizontal beams at the first 1 st floor
90	3.2.4. Structural ModellingANALYSIS PRO GRAMME
91	The program used to static analysis of building is the software ETABS 2015, a specialist program for the three
92	dimensional analysis and design of building systems. Finite Element Method model was formed to calculate the
93	response of the structure with this program. The finite element mesh shows the real mass distribution for the
94	ideal concentration of the masses at the nodes.
95	The ETABS program is one of the computer programs used for nonlinear static analysis. The program is
96	software of CSI Company with ISO9001 quality certification and is specially designed for 3D static analysis of
97	building type structures.
98	The CSI Company was founded in 1975 and is the manufacturer of programs, which are used in more than 160
99	countries worldwide. This program is also used in project designs of buildings such as Taipei Finance Centre in
100	Taiwan, One World Trade Centre in New York and Beijing National Stadium. ETABS program analyses by
101	using the finite element method (Sırlıbaş, 2013).
102	3.1. Modelling and analysis in ETABS 2015 program
103	Structural Modelling
104	In order to assessment the earthquake performance of the building, the DBYBHY, 2007 (The Regulations on
105	Buildings to be <u>built</u> done in Earthquake Regions) (DBYBHY, 2007) was followed in order to assessment the
106	earthquake performance of the building However, FEMA 356 (Prestandard and Commentary for Seismic
107	Rehabilitation of Buildings) regulation is used in cases where our current earthquake regulations may be



Equivalent Seismic Load was chosen as the method of earthquake analysis. Equivalent Seism	ic Load is defined			
as the user coefficient in ETABS. The loads are defined separately using positive and negative	ve eccentricity for			
both X and Y directions.				
$C = A_0 \times I \times \frac{S(T)}{B} = 0_7.125 \qquad \text{Eq.(1)}$				
In the considered earthquake direction, the seismic mass (wi) to be used in calculating the ear	rthquake loads of	A. C. LAND		
the building is given on DBYBHY 2007 as;		TTTTT -		
wi=gi+nqi Eq. (2)				
Here, the live load participation coefficient is given in Table 23.1. Since the building is a sch	ool building, n is			
taken as 0.6. Accordingly, seismic mass will affect the structure is defined as G+ 0.6Q accor	ding to the	1		
regulation. Figure 2.53.3 shows the definition of the seismic mass defined as $G + 0.6Q$ according to the				
regulation in program.				
Table 23.1. Live load participation coefficient (DBYBHY, 2007)				
Binanın Kullanım AmacıPurpose of Building uşe	n			
Depo, antrepo, vb.Warehouse, Storehouse etc.	0 <u>.</u> ,80	-		
School, student dormitory, sports facility, cinema, theater, concert hall, garage,		A		
restaurants, shops, etc. Okul, öğrenci yurdu, spor tesisi, sinema, tiyatro, konser salonu, garaj,	0 , .60	annan a		
lokanta, mağaza, vb	_	1000000		
<u>Residential, office, hotel, hospital, etc. Konut, işyeri, otel, hastane, vb.</u>	0 , .30	•		
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Vertical Loads

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The vertical loads affecting the building are shown in Table 23.2 as dead and live loads. Vertical loads were defined as linear load on horizontal beams and distributed load on the slabs. Hereby, the unit volume of the masonry walls in the building is taken as 1800 kg/m^3 . For Floor, secondary wall and dead load of roof, the predicted load values were examined in place of the building were taken. Live and snow load are taken according to the values given in TS 498 (Turkish Standards).

Figure 2.53.3. Definition of seismic mass

 Table 23.2. Equivalent earthquake load values

Yükleme Adı<u>Load</u> <u>Name</u>	Yükleme Tipi<u>Type</u> of Load	Değer <u>Load</u>	
SabitDead-KendiWeight	<u>Weights of Structural Elements</u> Yapısal " Elemanların Kendi Ağırlıkları	1800 kg/m ³	
Sabit Dead- KaplamaSurfacing	<u>Floor Covering LoadsDöşeme Üzeri</u> Kaplama Yükleri	-100 kg/m ²	
SabitDead-Tali DuvarSecondary wall	Taşıyıcı Olmayan Duvar Yükleri<u>Non-</u> Bearing Wall Loads	-300 kg/m ²	
<u>Sabit-Çat1Dead-Roof</u>	Çatı Sabit YüküWeight of Roof	200 kg/m ²	
Hareketli-KullanimLive	TS 498 Hareketli YükLive Load (TS498)	350 kg/m ² ve 500 kg/m ²	
Hareketli-KarLive-Snow	Snow Load for Konya Region (TS498) TS 498 Konya Bolgesi Kar Yuku	100 /m ²	

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of the structure influences and incorporates into the resonance motion by the mass participation rate. <u>In the</u>
earthquake regulation, <u>A</u> lower minimum limit is given for the sum of modal masses in the earthquake
regulation.

	Mode	Period (sn)	Mass Participation in	Mass Participation in	/	
230 231	Table 34.1. X-Y mass partic	ipation of modal a	nalysis		~	
229		Figure <u>-34</u> .1	I. Modal Analysis Param	eters	Ś	
228			OK Cancel			
		Convergence Tolerance Allow Auto Frequency Shifting	1E-09			
		Frequency Shift (Center) Cutoff Frequency (Radius)	0	yc/sec		
		Minimum Number of Modes	1			
		Other Parameters	12			
		Loads Applied Advanced Load Data Does NOT Exis	ŧ	Advanced		
		Nonlinear Case				
		Use Preset P-Delta Settings Use Nonlinear Case (Loads at En	None Modify/Show d of Case NOT Included)			
		P-Delta/Nonlinear Stiffness				
		Exclude Objects in this Group Mass Source	Not Applicable Mass			
		Modal Case Sub Type	Eigen ~	Notes		
		General Modal Case Name	Modal	Design		
	13	Modal Case Data		×		
227	no displacement in the X an	d Y directions, bu	t buckling occurs in the	structure.		
226	participation in the second m	ode_ , there is no m	ass participation in either	way. As shown in Figure 34.3 , there is	~	
225	and a displacement in the	X direction is see	en (Figure $\underline{34.4}$). Again,	when we look at thethere is no mass		
224	at the mass participation in th	e X direction, we	can see that there is a 709	% mass participation in the third mode		
223	an ection exceeds 70% in the	$\frac{111}{111} = \frac{1100}{1100} = \frac{1100}{1100} = \frac{1100}{1100} = \frac{1100}{1000} $	rear and that there is 700	e i direction. Similarly, when we look		
222	direction exceeds 70% in the	first mode and the	rais a displacement in th	a V direction Similarly, when we look		
222	are given in Table 34.1 Acc	ordingly up socit	can be seen that the mass	participation of the structure in the V		
220	Figure 3.1 and result mass di	stributions in the X	K and V directions of the	modal analysis parameters are given in		
220	buckling and third mode is 0	314 second in the	direction of "X" The	nodal analysis parameters are given in		
219	building is 0.50 second (the	vibration period	is in the "Y" direction)	the second mode is 0.404 second in		
218	historical buildings, it is very difficult to catch this limit. As a result of the analysis, the first mode of the					
217	each mode is never less than 90% of the total building mass. However, if fewer modes are used in the analysis of					
216	earthquake directions, will be	determined accor	ding to the rule that the s	sum of the active calculated masses for		
215	According to the regulation,	it is stated that th	he number of sufficient	vibration modes in each of the x and y		

X direction

0.000

0.001

0.769

Y direction

0.725

0.000

0.000

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Numbers

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0.501

0.404

0.314





263	accordance with the above figures and local axes. According to DBYBHY-2007, Safe shear stress is calculated		
264	according to the following equation;		
	$\tau_{em} = \tau_0 + \mu \sigma$		Biçimlendirilmiş: Yazı tipi: 10 nk
265	$\tau_{em} = \tau_0 + \mu \sigma$		Biçimlendirilmiş: Yazı tipi: 10 nk
266	Where: σ is the axial stress due to the vertical loads, and μ is the friction coefficient. In our earthquake	M/	Biçimlendirilmiş: Yazı tipi: 10 nk
267	regulations, it is clear that the coefficient of friction can be taken as 0.5 in head 5.3.3.4 in Turkish Farthquake	$\{(\cdot,\cdot)\}$	Biçimlendirilmiş: Yazı tipi: 10 nk
207	Permission $C = 0.60$ ups taken into account in accordance with		Biçimlendirilmiş: Yazı tipi: 10 nk
200	<u>Regulations</u> . In the calculation of vertical tension, G + 0.0Q was taken into account in accordance with		Biçimlendirilmiş: Yazı tipi: 10 nk
269	earthquake mass.		Biçimlendirilmiş: Yazı tipi: 10 nk
270	Average axial stress due to vertical load $= 0.13$ MPa		Biçimlendirilmiş: Yazı tipi: 10 nk
271	Found as;		
	$\sigma_{am} = 0.1 + 0.5 \times 0.13 = 0.165 MPa$		Biçimlendirilmiş: Yazı tipi: 10 nk
272	$\tau_{em} = 0.1 + 0.5 \times 0.13 = 0.165 Mpa$		Biçimlendirilmiş: Yazı tipi: 10 nk
273	As it can be seen from the figures given above, it is seen that the shear stresses in the local regions (especially		Biçimlendirilmiş: Yazı tipi: 10 nk
274	around the spaces) reach to 0.3 MPa. However, $\frac{1}{10000000000000000000000000000000000$		Biçimlendirilmiş: Yazı tipi: 10 nk
275	by the formula in DRVRHV is not exceeded throughout the system		Biçimlendirilmiş: Yazı tipi: 10 nk
275	by the formula in DDTDTT is not exceeded throughout the system.		Biçimlendirilmiş: Yazı tipi: 10 nk
276	<u>34.4. Relocation Displacement results</u>		Biçimlendirilmiş: Yazı tipi: 10 nk
277	Since DBYBHY 2007 did not observe the displacement criterion for masonry structures, displacement controls		
278	were carried out in accordance with FEMA 356 regulation. In FEMA 356, performance Performance aimtargets,		
279	performance lperformance levels and ranges of structural and non-structural elements, earthquake impact levels		
280	are defined in FEMA 356. In this regulation, There are essential explanations are made about the modelling of		
281	masonry structures in this regulation. In Turkey, FEMA 273/356 standards are used in evaluating existing		
282	structures in addition to DBYBHY 2007 in evaluating existing structures in our country. Figures 34.7-34.8-34.9-		Bicimlendirilmis: Yazı tipi: 10 nk
283	<u>34.10 show the maximum displacements in the X and Y directions of the model.</u>		Biçimlendirilmiş: Yazı tipi: 10 nk
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satır

302	5.4. DISCUSSIONCONCLUSION		Biçimlendirilmiş: İki Yana Yasla,
303	In this study, performance		Girinti: Sol: 0,12 cm, Satır aralığı: 1,5 satır
304	constructed as masonry structure, <u>and</u> was investigated by static analyse. As a result of the analyse studys made,		Biçimlendirilmiş: Yazı tipi: 10 nk
305	it has been determined that the most-forced stressed parts of the building in the static condition are the edges of	())	Biçimlendirilmiş: Yazı tipi: 10 nk
306	the window and door openings. The bearing wall lengths, floor heights, void ratios in the building do not provide		Biçimlendirilmiş: Satır aralığı: 1,5 satır
307	the regulation requirements when the present state of the structure is examined according to the requirements of		Bicimlendirilmis: Yazı tipi: 10 nk
308	today's regulations. Moreover, it is seen that the most difficult stressed parts of the construction are the edges of		Biçimlendirilmiş: Yazı tipi: 10 nk
309	windows and door doorsedges according the results of analysis of analysis on ETABS. Thin and deep cracks on		
310	the edges of the doors and windows were also observed in the buildingsit is recommended to repair of cracks		
311	in these areas.		
312	-The detailed results of analyses carried out in order to determine the performance of the building under the		
313	effects of earthquake loads are presented in the above sections. The summaries of the results obtained are		
314	indicated below.		
315	• The lateral displacement of the structural system is 30mm / 19000mm = 0.16% and provides the criteria		
316	of FEMA 356 regulation.		
317	• The axial pressure stresses in the structural system are lower than 0.3 MPa on average.		
318	• Although the axial stresses reach 1.0 MPa in local areas, they are below the characteristic compressive		
319	strength (1.2 MPa).		
320	• The shear stresses in the structural system are less than 0.15 MPa on average. Although the shear		
321	stresses reach 0.3 MPa in the local regions, they are below the shear stress (0.7 MPa) calculated		
322	according to the characteristic compressive strength.		
323	• It is thought that some of the cracks seen in the building may originate in the settlement of the building.		
324	Therefore, it is considered appropriate to take precautions related to the foundation of the building.		
325	• And also, it will be useful for the next lifetime of the building if the cracks observed in the building are		
326	repaired according to the strengthening methods.		
327	• Since the back wall of building is painted with complex -plaster, the historic texture of the building is		
328	distorted and ruins the historical texture of building . It is suggested that such applications should not be		
329	repeated.		
330	It is thought that the analyses made in the scope of the study and the results obtained are very important for		
331	carrying out similar studies related to such subjects in future works- related to such subjects- and also for the		
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