

1 Application of a physically-based model to forecast shallow 2 landslides at regional scale

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10 Abstract.

11 In this work, we apply a physically-based model, namely the HIRESSS (High RESolution Stability Simulator) model, to
12 forecast the occurrence of shallow landslides at regional scale. HIRESSS is a physically based distributed slope stability
13 simulator for analysing shallow landslide triggering conditions during a rainfall event. The software is made of two
14 parts: hydrological and geotechnical. The hydrological model is based on an analytical solution of an approximated
15 form of the Richards equation while the geotechnical stability model is based on an infinite slope model that takes into
16 account the unsaturated soil condition. The test area is a portion of the Valle d'Aosta region, located in North-West
17 Alpine mountain chain. The geomorphology of the region is characterized by steep slopes with elevations ranging from
18 400 m a.s.l of Dora Baltea's river floodplain to 4810 m a.s.l. of Mont Blanc. In the study area, the mean annual
19 precipitation is about 800-900 mm. These features lead to the territory to be very prone to landslides, mainly shallow
20 rapid landslides and rock falls. In order to apply the model and to increase its reliability, an in-depth study of the
21 geotechnical and hydrological properties of hillslopes controlling shallow landslides formation was conducted. In
22 particular, two campaigns of on site measurements and laboratory experiments were performed with 12 survey points.
23 The data collected contributes to generate input map of parameters for HIRESSS model. In order to consider the effect
24 of vegetation on slope stability, the soil reinforcement due to the presence of roots has been also taken into account
25 based on vegetation maps and literature values of root cohesion. The model was applied in back analysis on two past
26 events that have affected Valle d'Aosta region between 2008 and 2009, triggering several fast shallow landslides. The
27 validation of the results, carried out using a database of past landslides, has provided good results and a good prediction
28 accuracy of the HIRESSS model both from temporal and spatial point of view.

29 1 Introduction

30 Landslide prediction at regional scale can be performed following two approaches: a) rainfall thresholds based on
31 statistical analysis of rainfall and landslides and b) physically-based deterministic models. While the first approach is
32 currently extensively used at regional scale (Aleotti, 2004; Cannon et al., 2011; Martelloni et al., 2012; Rosi et al.,
33 2012; Lagomarsino et al., 2013), the latter is more frequently applied at slope or catchment scale (Dietrich and
34 Montgomery, 1998; Pack et al., 2001; Baum et al., 2002, 2010; Lu and Godt, 2008; Simoni et al., 2008; Ren et al.,
35 2010; Arnone et al., 2011; Salciarini et al., 2012, 2017; Park et al., 2013; Rossi et al., 2013). The poor knowledge of
36 hydrological and geotechnical parameters spatial distribution, caused by the extreme heterogeneity and inherent
37 variability of soil at large scale (Mercogliano et al., 2013; Tofani et al., 2017), mainly avoid the physically-based model
38 application at regional scale. On the other hand, physically-based models allow to predict spatially and temporally the

39 occurrence of landslides with high accuracy producing accurate hazard maps that can be of help for landslide risk
40 assessment and management.

41 In this work, we apply the physically based model, named HIRESSS (Rossi et al., 2013) in Eastern part of Valle
42 d'Aosta region (Italy), in North-West Alpine mountain chain in order to test the capacity of the model to forecast the
43 occurrence of shallow landslides at regional scale. In particular, the objectives of the work are: i) to properly
44 characterise the geotechnical and hydrological parameters of the soil to feed the HIRESSS model and to spatialize this
45 punctual information in order to have spatially-continuous maps of the model input data ii) to test the HIRESSS code
46 for two selected rainfall events that have triggered several shallow landslides and to validate the model results.
47 HIRESSS is a physically based distributed slope stability simulator for analysing shallow landslide triggering
48 conditions in real time and in large areas using parallel computational techniques. In the area selected, an in-depth study
49 of the geotechnical and hydrological properties of hillslopes controlling shallow landslides formation was conducted,
50 performing two campaigns (12 survey points) of in-situ measurements and laboratory tests. Furthermore, the HIRESSS
51 model has been modified to take into account the effect of the root reinforcement to the stability of slopes based on
52 plant species distribution and literature values of root cohesion.

53 **2 Study area and rainfall events**

54 The study area, called alert Zone B by the regional civil protection authorities, is located in eastern part of Valle
55 d'Aosta region, in North-West Alpine mountain chain (Fig. 1). The area is characterized by three main valleys:
56 Champorcher valley, Gressoney or Lys valley, and Ayas valley. The first is located on the right side of Dora Baltea
57 water catchment, and represents the southern part of the study area. The second and third valleys show N-S orientation,
58 and they are delimited to north by Monte Rosa massif (4527 m a.s.l) and to south by Dora Baltea river.

59 From a geological point of view, the Valle d'Aosta is located NW with respect to the Insubrica Line, in particular, there
60 are three systems of Europa chain: the Austroalpino, the Pennidiche and the Elvetico-Ultraelevato systems (De Giusti,
61 2004). Fig. 2 shows the lithological map of the study area obtained by reclassifying the geological units according to 11
62 lithological groups: landslides, calcareous schist, alluvial deposits, glacial deposits, colluvial deposits, glacier, granites,
63 mica schists, green stone, black schists and serpentinites. In detail in the study area the main lithologies outcropping are
64 metamorphic and intrusive rocks, in particular granites, metagranites, schists and serpentinite.

65 The geomorphology of the region is characterized by steep slopes and valleys shaped by glaciers. The glacial modelling
66 is shown in the U-shaped of Lys and Ayas valleys, and the erosive depositional forms found in the Ayas valley. The
67 three valleys' watercourses, the Lys creek, the Evançon creek, and the Dora Baltea river, contributed to the glacial
68 deposits modelling with the formation of alluvial fans. The climate of the region is characterized by high variability
69 strongly influenced by altitude (ranging from 400 m a.s.l of Dora Baltea's river floodplain to 4810 m a.s.l. of Mont
70 Blanc), with a continental climate in the valleys floor and an Alpin climate at high altitudes.

71 The slope steepness, together with mean annual precipitation of 800-900 mm are the main landslide triggering factors.
72 These features lead the study area to be prone to landsliding, in particular rock falls, deep seated gravitational slope
73 deformations (DSGSD), rocks avalanches, debris avalanches, debris flows, and debris slides (Catasto dei Dissesti
74 Regionale – form Val d'Aosta Regional Authorities). In this work we model the triggering conditions of shallow
75 landslides, i.e. soil slips and translational slides and we do not take into account the other types of movement.

76 The HIRESSS model simulated two past events, one in 2008 and one in 2009, and the validation of the model
77 performance was carried out comparing the results with the landslide regional database.

78 In particular:

- 79 • 24 - 31 May 2008: on 28 and 29 May 2008 intense and persistent rainfall was recorded across the Valle d'Aosta
80 region with a total precipitation in the study area of about 250 mm causing flooding, debris flows and rockfalls.
- 81 • 25 - 28 April 2009: from 26 April to 28 April 2009 heavy rainfall affected the south-eastern part of the Valle
82 d'Aosta region, with the highest precipitation recorded at the Lillianes Granges station of about 268 mm. This
83 precipitation triggered several landslides.

84 3 Methodology

85 3.1 HIRESSS description

86 The physically-based distributed slope stability simulator HIRESSS (Rossi et al., 2013) is a model developed to analyse
87 shallow landslide triggering conditions on large scale at high spatial and temporal resolution using parallel calculation
88 method. Two parts compose the model: hydrological and geotechnical (Rossi et al., 2013). The hydrological part is
89 based on a dynamical input of the rainfall data which are used to calculate the pressure head and provide it to the
90 geotechnical stability model. The hydrological model is initiated as a modelled form of hydraulic diffusivity, using an
91 analytical solution of an approximated form of the Richards equation under the wet condition (Richards, 1931). The
92 equation solution allows us to calculate the pressure head variation (h), depending on time (t) and depth of the soil (Z).
93 The solutions are obtained by imposing some boundary conditions as described by Rossi et al. (2013).

94 The geotechnical stability model is based on an infinite slope stability model. The model considers the effect of matric
95 suction in unsaturated soils, taking into account the increase in strength and cohesion. The stability of slope at different
96 depths (Z values) is computed since the hydrological model calculates the pressure head at different depths. The
97 variation of soil mass caused by water infiltration on partially saturated soil is also modelled. The original FS equations
98 (Rossi et al., 2013) were modified taking into account the effect of root reinforcement (c_r) as an increase of soil
99 cohesion (c') according to the Eq. 1:

$$100 \quad c_{tot} = c' + c_r$$

$$101 \quad (1)$$

102 Regarding the geotechnical influence of roots on the soil strength, roots seem to affect the cohesion parameter only,
103 while the friction angle would be poorly or not at all interested by reinforcement (Waldron and Dakessian, 1981; Gray
104 and Ohashi, 1983; Operstein and Frydaman, 2000; Giadrossich et al., 2010). Therefore, is necessary to consider the root
105 cohesion in calculating FS and consequently in applying HIRESSS model.

106 The root reinforcement (or root cohesion) can be considered equal to (Eq. 2):

$$107 \quad c_r = kT_r(A_r/A)$$

$$108 \quad (2)$$

109 where T_r is the root failure strength (tensile, frictional, or compressive) of roots per unit area of soil, A_r/A the root area
110 ratio (proportion of area occupied by roots per unit area of soil), k a coefficient dependent on the effective soil friction
111 angle and the orientation of roots. The measure of c_r varies with vegetal species, within a single species depends on how
112 plants respond to environmental characteristics and fluctuations.

113

114 The new equation of FS at unsaturated conditions is therefore (Eq. 3):

115
$$FS = \frac{\tan \varphi}{\tan \alpha} + \frac{c_{tot}}{\gamma_d y \sin \alpha} + \frac{\gamma_w h \tan \varphi \left\{ 1 + (h_b^{-1} |h|)^{\lambda+1} \right\}^{\frac{\lambda}{\lambda+1}}}{\gamma_d y \sin \alpha}$$

116 (3)

117 where φ is the friction angle, α is the slope angle, γ_d is the dry soil unit weight, y is the depth, γ_w is the water unit
 118 weight, h is the pressure head, h_b is the bubbling pressure, and λ is the pore size index distribution. In saturated
 119 condition the equation of FS (Rossi et al., 2013) becomes (Eq. 4):

120
$$FS = \frac{\tan \varphi}{\tan \alpha} + \frac{c_{tot}}{(\gamma_d(y-h) + \gamma_{sat}h) \sin \alpha} - \frac{\gamma_w h \tan \varphi}{(\gamma_d(y-h) + \gamma_{sat}h) \tan \alpha}$$

121 (4)

122 where γ_{sat} is the saturated soil unit weight.

123 One of the major problems, associated with the deterministic approach employed on a large scale, is the uncertainty of
 124 the static input parameters or geotechnical parameters of the soil. The method used for the estimation of parameters
 125 spatial variability is the Monte Carlo Simulation. The Monte Carlo simulation achieves a probability distribution of
 126 input parameters providing results in terms of slope failure probability (Rossi et al., 2013). The developed software uses
 127 the computational power offered by multicore and multiprocessor hardware, from modern workstations to
 128 supercomputing facilities (HPC), to achieve the simulation in reasonable runtimes, compatible with civil protection real
 129 time monitoring (Rossi et al., 2013). The HIRESSES model loads spatially distributed data arranged as 12 input raster
 130 maps and the maps of rainfall intensity. These input raster maps are: slope gradient; effective cohesion (c'); root
 131 cohesion (c_r); friction angle (φ'); dry unit weight (γ_d); soil thickness; hydraulic conductivity (k_s); initial soil saturation
 132 (S); pore size index (λ); bubbling pressure (h_b); effective porosity (n); and residual water content (q_r). and rainfall
 133 intensity.

134

135 3.2 HIRESSES input data preparation

136 The input parameters can be divided in two classes: the static data and the dynamical data. Static data are geotechnical
 137 and morphological parameters while the dynamical data is represented by the hourly rainfall intensity. Static data are
 138 read only once at the beginning of the simulation while dynamical inputs are continuously updated.

139 The HIRESSES input are in raster, therefore point data and parameters have to be adequately spatially distributed. In this
 140 application the spatial resolution was 10 m.

141 Static data

142 The slope gradient was calculated from the DEM (Digital Elevation Model). The DEM has a resolution of 10 m and is
 143 dated 2006. Effective cohesion, friction angle, hydraulic conductivity, effective porosity and dry unit weight, were
 144 obtained, spatializing according to lithology, the soil punctual parameters derived from the in situ and laboratory
 145 geotechnical tests and analysis.

146 In particular, the properties of slope deposits were determined by in situ and laboratory measurements (Bicocchi et al.,
 147 2016; Tofani et al., 2017) at 12 survey points. To carry out the in situ tests the survey points were selected following
 148 these characteristics: i) physiography, ii) landslides occurrence, and iii) geo-lithology (Fig. 2). Regarding the first point,
 149 a high-resolution DEM (from Val d'Aosta Regional Authorities) together with a careful first surveys were used to
 150 identify the most suitable slopes. The surveys took place in two sessions, the first one in August 2016, and the second
 151 one in September 2016. The following analyses were conducted:

- 152 • registration of geographical position using a GPS and photographic documentation of the site characteristics
153 (morphology and vegetation);
- 154 • in situ measurement of saturated hydraulic conductivity (k_s) by means of the constant-head well permeameter
155 Amoozemeter;
- 156 • sampling of an aliquot (~2 kg each) of the material for laboratory tests, including grain size distributions, index
157 properties, Atterberg limits and direct shear tests.

158 The permeability in-situ measurements and the soil samplings were made at depth ranging from 0.4 to 0.6 m below the
159 ground level. The evaluation of the k_s (saturated hydraulic conductivity or permeability) was made with the
160 *Amoozemeter* permeameter (Amoozegar, 1989). The measurement was obtained by observing the amount of water
161 required to maintain a constant volume of water into the hole. In situ measurements are then applied into the Glover
162 solution (Amoozegar, 1989), which calculates the saturated permeability of the soils. The k_s is a very useful parameter
163 not only for slope stability modelling but also for many other hydrological problems (groundwater, surface water runoff
164 and sub-surface, flow calculation of water courses).

165 In addition, the *in situ* collected samples were examined in the laboratory to define a wide range of parameters to
166 characterize more extensively the deposits. In particular, the following tests were performed in order to classify the
167 analysed soils:

- 168 • grain size distribution (determination of granulometric curve for sieving and settling following ASTM
169 recommendations), and classification of soils (according to AGI and USCS classification, Wagner, 1957);
- 170 • determination of the main index properties (porosity, relationships of phases, natural water content w_n , natural
171 and dry unit weight γ and γ_d) following the ASTM recommendations;
- 172 • determination of Atterberg limits (liquid limit LL, plastic limit PL, and plasticity index PI);
- 173 • direct shear test on selected samples.

174 Soil thickness was calculated by the GIST model (Catani et al., 2010; Del Soldato et al, 2016). Soil characteristic curves
175 parameters (pore size index, bubbling pressure, and residual water content) were derived from literature values (Rawls
176 et al., 1982).

177 Root cohesion variations in the area (at the soil depth chosen for the physical modelling with HIRESSS) were obtained
178 firstly, identifying the plant species and determining their distribution from *in situ* observations and vegetational maps
179 (Carta delle serie di vegetazione d'Italia, Italian Ministry of the Environment and Protection of Land and Sea). Then,
180 the measure of cohesion due to the presence of roots was assigned to each subarea according to the dominant plant
181 species and literature root cohesion for that species (Bischetti, 2009; Burylo et al., 2010; Vergani et al., 2013, 2017) that
182 were calculated considering the Fiber Bundle Model (Pollen et al., 2004). The measure of c_r varies with vegetal species,
183 within a single species depends on how plants respond to environmental characteristics and fluctuations, so map of root
184 cohesion variations obtained as mentioned is a simplification of reality. This is a necessary simplification as the known
185 methods to evaluate root cohesion variations are not suitable for wide areas and acceptable measurement times.

186 The last static input data, in this case of study, is the exposure rock mask. This was defined considering the lithological
187 and land use maps, so that HIRESSS model avoided the simulation on steep slopes made of bare rocks.

188 The geotechnical properties and root cohesion of the soils have been spatialized with respect to a lithological
189 classification.

190 For each lithological class and plant species the mean value has been selected in order to obtain the HIRESSS input
191 raster parameters.

192

193 Dynamic data

194 In the study area, the rainfall hourly data from 27 pluviometers were available, therefore it was necessary to spatially
195 distribute them to generate 10x10 m cell size input raster to ensure the correct program operation. The rainfall data were
196 elaborated applying the Thiessen's polygon methodology (Rhynsburger, 1973) modified to take into account the
197 elevation. Thiessen's polygon methodology, in fact, allows us to divide a planar space in some regions, and to assign the
198 regions to the nearest point feature. This approach defines an area around a point, where every location is nearer to this
199 point than to all the others. Thiessen's polygon methodology do not consider the morphology of the area, so the alert
200 Zone B was divided in three catchment areas and the polygons were calculated for each rain gauges considering the
201 reference catchment basin (Fig. 3).

202 **4 Results**

203 4.1 HIRESSS input data

204 The results of the geotechnical and hydrological characterization of the soils of the 12 survey points are shown in Table
205 1 for all survey sites.

206 The results of granulometric tests show that the analysed soils are predominantly sands with silty gravel (Fig. 4 and
207 Table 1). Regarding the index properties, the natural soil water content values were predominantly about 20% by
208 weight, with a maximum and minimum values of 5.1% and 26.2%, respectively. These values reflect their different
209 ability to hold water in their voids. The measured natural unit weight (γ) was variable between 15.3 kN/m³ and 21.7
210 kN/m³, depending not only on the different grain size distribution but also by different thickening and consolidation
211 states. Regarding saturated unit weight (γ_{sat}) the measured values range between 18.2 kN/m³ and 21.5 kN/m³ (Table 1).
212 The Atterberg limits (LL and PL) were measured on samples with a sufficient passing fraction (> 30% by weight)
213 through 40 ASTM (0.425 mm) sieve. For sandy prevalent samples, LL values are predominantly around 40% of water
214 content (% by weight), while the PL is around 30% (Table 1).

215 The effective friction angle varies between a minimum of 25.6° and a maximum of 34.3°, while the effective cohesion
216 ranges from a minimum of 0.0 kPa to a maximum of 9.3 kPa. Consistent with the presence of sandy soils, the saturated
217 permeability values were around a medium-high value of 10⁻⁶ m/s. The minimum and maximum values were found
218 between 1.36·10⁻⁷ m/s and 1.54·10⁻⁵ m/s. Considering the poor variability of samples, the permeability values were
219 relatively homogeneous and in accordance with the values reported in the literature (Table 1).

220 The additional cohesion induced by roots assumes different values not only depending on plant species and
221 environmental characteristics, but also on depth of soil, as roots diameter and density vary with latter. Because of such
222 evidence, studies on roots cohesion of different species report values as function of depth of soil. In the area of the case
223 study, soils have thinner thickness than those ones in which these studies are carried out. In such thin soils, root systems
224 organize their growth depending on available space not reaching the same depth of roots of thick soils. Consequently, in
225 this context root cohesion of species at the different depth is dissimilar related to literature values. Considering this,
226 map for variation of root cohesion is processed taking for each species the minimum cohesion (among those specified
227 for each species at the different depth) reported in literature. By doing this, contribution of vegetation to stability of
228 slopes is considered in FS calculate and at the same time, it is avoided an overestimate of root cohesion.

229 In the area, root cohesion defined as mentioned above ranges from a minimum of 0.0 kPa (mainly in the outcrop area)
230 to maximum of 8.9 kPa (area occupied by mountain maple on the left bank of river Dora Baltea).

231 In Table 2, the mean values of each input parameters respect to lithological class were reported.

232 The pore size index, bubbling pressure and residual water content are constant in whole area of: 0,322 (-); 0,1466 m and
233 0,041 (-), respectively.

234 The distributed soil parameters maps are shown in Fig. 5. The results of rainfall data elaborated using Thiessen's
235 polygon methodology are 192 and 96 rainfall hourly maps for the 2008 and 2009 event, respectively. In Fig. 6 are
236 reported the cumulative maps of each event.

237

238 4.2 HIRESSS simulation

239 The HIRESSS model has simulated two past events; one in 2008 (24 - 31 May) and the other in 2009 (25 - 28 April)
240 which have triggered several landslides in the study area.

241 The HIRESSS input data have been inserted in the HIRESSS model to obtain day-by-day maps of landslide occurrence
242 probability. The main characteristics of simulation are shown in Table 3.

243 The results of the simulations for both events have shown that the first day of simulation pixels with high probability of
244 occurrence in absence of rainfall. These pixels are false positive, (i.e. pixels identified unstable by the model but not
245 real unstable) because of morphometric reasons, predominantly high slope angles. To remove these false positive, a
246 numeric mask was applied. Using the GIS software commands, it was possible to calculate the number of pixels of the
247 first simulation day with a trigger probability value greater than 80% and delete them (Fig. 7). The mask was then
248 applied to the rest of landslide occurrence probability maps. The resulting maps for each days of the simulated events
249 are shown in the Fig. 8 and Fig. 9.

250 The results of the first simulated event (24 - 31 May 2008) are shown in Fig. 8. The failure probability in the whole area
251 is negligible for the first four days (from 24 to 27 May 2008) (Fig. 8a). The rainfall intensity increased since 27 May,
252 reaching the highest value on 29 May, when the precipitation value was around 100 mm in the eastern sector of study
253 area. The HIRESSS model well simulate this passage: the 28 May and 29 May 2008 landslide occurrence probability
254 maps show a considerable increase of the probability of failure with maximum values around 90% at the East of alert
255 Zone B (Fig. 8b, c). In the following days rainfall intensity decreases, and also the probability slowly decreases, being
256 anyway still high on 30 May 2008.

257 Concerning the second event (25 - 28 April 2009) landslide occurrence probability is negligible for the first two days
258 (25 and 26 April 2009) in the whole area (Fig. 9a, b), because of the low rainfall intensity. From 27 April 2009 rainfalls
259 become more intense, especially in the southeast sector of the region, where the cumulated rainfall average was about
260 151 mm. The probability maps show high values during these days (Fig. 9c, d). This event led to many landslides
261 triggered during these days (as reported in the database).

262 In order to validate the HIRESSS simulations the database of landslides triggered during the two events have been
263 compared with the models results.

264 In general, for both events temporal validation shows that the daily highest probability of occurrence, computed by
265 HIRESSS, correspond with the days with landslide occurrence and with the most intense precipitation.

266 For the first simulated event landslides reported in the database are dated 30 May and 31 May 2008 (Fig. 8d) which
267 correspond to the days with highest probability of occurrence. The same is for the second event; many landslides have
268 triggered during 27 and 28 April 2009 (as reported in the database).

269 In Table 4 the results over 75% of slope failure probability for both events are highlighted and confirm the correct
270 temporal occurrence of landslides. In particular we can notice that for the first event (2008) the number of unstable
271 pixel (failure probability > 75%) increases the 29th of May with a total extension of the unstable area of about 24 km²,
272 while for the event of 2009, the number of unstable pixel increases the 27th of April with an extension of 33 km².

273 The temporal validation was also carried out considering daily cumulative rainfall compared to the landslide failure
274 probability. In particular, a median of landslide occurrence probability was calculated for four pluviometric areas
275 identified by Thiessen's polygons methodology, modified according to limits of river basins, both for the event of May
276 2008 and for the April 2009 event (Fig. 10a, b). As it could be expected, the results show that when the highest rainfall
277 intensity is measured, the highest probability of occurrence is computed for the all areas and for both events.

278 Spatial validation was performed following a pixel by pixel method: this method is the most complex since it consists in
279 comparing the probability of instability of each pixel with the pixels involved in the actual event that occurred. This
280 validation implies a great deal of uncertainty in the results since the reports of landslide events may have errors on the
281 precise spatial location and on the size of the phenomenon. To overcome this problem and taking into account probable
282 errors caused by the actual spatial location in the database, an area of 1 km² (called influence area) around the point of
283 the landslide were considered in the validation analysis. Inside the influence area, pixels that have the 75% of
284 probability of failure were considered instable.

285 Figure 11 shows an example of landslide event occurred in the Arnad municipality on 30 May 2008. The model
286 computes a low failure probability on 24 May 2008 and an increase of probability on 30 May 2008. In Fig. 11a and b it
287 is possible to note that inside the red circle the red and yellow area increase on 30 May with respect to 24 May. In this
288 case, the model is able to identify correctly such movement. To better highlight this validation, Figure 11c shows the
289 number of pixels above 75% of probability calculated by the model, within the circular area of about 1 km² around the
290 all landslides occurred during the event of 2008. For some of the reported landslide events, the number of pixels above
291 75% increases on 30 May 2008, only in case of the Champdepraz and Montjovet 2 events the probability does not
292 increase. This may be caused by the low precision of location of the reported landslide, and maybe because some of the
293 real landslides reported are other types of movements (rockfalls, rotational slides) that cannot simulated by the
294 HIRESSS model.

295 **5 Discussion**

296 The application of the HIRESS model to a portion of the Valle D'Aosta region has provided good results in term of
297 spatial and temporal accuracy of the model as highlighted in section 4.2. The advantage of the regional physically-based
298 model, with respect to rainfall-thresholds one, is that is possible to predict with metric spatial resolution and hourly
299 temporal resolution the occurrence of shallow landslides.

300 On the other hand, the application of the HIRESSS model has highlighted some important drawbacks, mainly related to
301 the i) validation of the models results, ii) uncertainty of the input parameters.

302

303 Validation of the model results

304 To perform a solid validation is necessary to have information on spatial location and temporal occurrence of
305 landslides. In particular, the time of occurrence is very rarely known with hourly precision, and usually landslides are
306 related to a rainstorm, without any more precise information on time of occurrence (Rossi et al., 2013). Concerning the
307 spatial landslides locations, in many cases they are included in the database only as points without any information on
308 the area involved. In our database, provided by the local authorities, landslides are points with information on the day of
309 occurrence.

310 In synthesis the main problems encountered during the model validation are:

- 311 • Incompleteness of landslide dataset: in general event-based database are incomplete due to a lack of reporting
312 in mountainous areas scarcely populated while most of reported landslides involve infrastructure or water
313 streams (Mercogliano et al., 2013, Tofani et al., 2017). In our case we have two datasets for the two events
314 simulated (2008 and 2009) with 9 and 11 landslides respectively. The number of reported landslides is very
315 low and not suitable to perform a correct validation for the whole area. Infact in both events there are some
316 areas that show an high failure probability even though there are no landslides reported. For example for the
317 2008 event (Fig. 8), the municipalities of Gressoney Saint Jean and Gaby in the NE portion of the study area
318 and the municipalities of Pontboset and Issogne in south part of the study area show high failure probabilities
319 ($> 75\%$) but no landslides reported. The same happens for the event of 2009 (Fig. 9) when again Gressoney
320 Saint Jean and Pontboset as well as Lillianes and Fontainemore in the SE portion of the study area show high
321 failure probabilities but no recorded landslides. In these cases, we are not able to discriminate if the model has
322 overestimated the landslide occurrence or it has correctly predicted landslide occurrence since we are not sure
323 about the completeness of the database.
- 324 • Correct spatial location: In our validation landslide dataset the accuracy of the spatial location is very low and
325 the landslides are reported as points (yellow dots in Fig. 8 and Fig. 9). Anyway we don't know exactly if these
326 points correspond to the triggering area, that would constitute the desirable situation, or the deposition one or,
327 even worst, to the position of the elements at risk (house, road, river) interested by the landslides. For this
328 reason, we have performed the spatial validation considering an area of 1km^2 around the point in order to take
329 into account the error in the spatial location of the landslides (Fig. 11). In these cases of uncertain position of
330 the landslides, an alternative solution could be to perform a validation aggregating the results using different
331 spatial units, for example first or second order basins as proposed in Rossi et al., (2013). If the spatial
332 aggregation overcome the problem of the correct location of the landslides for the validation, on the other hand
333 it allows to loss the high spatial resolution of the HIRESSS model that is on the major benefit of the analysis.
334 The ideal situation would be to have a landslide database realized with the same resolution of the HIRESSS
335 model.
- 336 • Temporal occurrence: The event landslide database has the information concerning the day of the occurrence
337 of the landslides. The HIRESSS has a higher temporal resolution since it is able to provide hourly failure
338 probability maps (Table 3). In order to make a temporal validation, model outcomes have been temporally
339 aggregated in daily maps (Fig. 8 and Fig. 9).The results of the temporal validation are quite satisfactory,
340 anyway due the insufficient information of the landslide database, we are not able to make a real validation of
341 the model performance on hourly basis. Also in this case a satisfactory analysis of the model performance
342 could have been carried out only if available information on the exact time of failure.

343

344 Uncertainty of the input parameters

345 Another important limitation related to the application and the accuracy of the physically-based model is the availability
346 of detailed databases of physical and mechanical properties of soils in the study areas. The performance of a model can
347 be strongly influenced by the errors or uncertainties in such input data (Segoni et al., 2009; Jiang et al., 2013).
348 Furthermore, the punctual information of soil properties have to be spatialized and in general they are characterized by
349 high spatial variability and their measurement is difficult, time-consuming and expensive, especially when working on
350 large, geologically complex areas (Carrara et al., 2008; Baroni et al., 2010; Park et al., 2013; Biccocchi et al., 2016;
351 Tofani et al., 2017).

352 In order to prepare the raster maps of the input data and to feed the physically based models, we have adopted a set of
353 constant values of the parameter for distinct lithological units, as derived from direct measurements. In particular we
354 have measured soils parameters in twelve survey points (Table 1, Fig. 2) and then we have spatialized the punctual data
355 according to different lithologies (Table 2). Then, within the HIRESSS model the soil parameters are treated with the
356 Monte Carlo simulation, using a equiprobable distribution for each of them.

357 The HIRESSS model, fed with these parameters has provided good results (section 4.2), although all the limitations of
358 the validations process described above.

359 Anyway further analysis has to be carried out in the study area in order to define the impact of the uncertainties of the
360 input parameters on model results and to set-up the correct approach to increase the efficiency of the model. In
361 particular:

- 362 • Increase the number of survey points in order a sufficient number of points for each lithology;
- 363 • Use inside the Monte Carlo simulation of the normal Gaussian frequency model instead of equiprobable one
364 for some soil parameters. The normal distribution model, when applicable, allow to obtain more accurate
365 results than using an equiprobable one: given a mean value and a standard deviation obtained from the
366 normally distributed samples analysed, extremely low or high values are associated to low probability of
367 occurrence, moreover dramatically reducing the simulation time. (Bicocchi et al., 2016, Tofani et al., 2017);
- 368 • To test another approach to spatialize the soil parameters based for example on the soil parameters values as
369 random variables using a probabilistic or stochastic approach as proposed by Fanelli et al., (2016) and
370 Salciarini et al. (2017).

371 **6 Conclusion**

372 The HIRESSS code (a physically-based distributed slope stability simulator for analysing shallow landslide triggering
373 conditions in real time and in large areas) was applied to the eastern sector of Valle d'Aosta region in order to test its
374 capability to forecast shallow landslides at regional scale. The model was applied in back analysis to two past rainfall
375 events that have triggered in the study areas several shallow landslides between 2008 and 2009. In order to run the
376 model and to increase its reliability, an in-depth study of the geotechnical and hydrological properties of hillslopes
377 controlling shallow landslides formation was conducted. In particular, two campaigns of on site measurements and
378 laboratory experiments were performed with 12 survey points. The data collected contributes to generate input map of
379 parameters for HIRESSS model according to lithological classes. The effect of vegetation on slope stability in terms of
380 root reinforcement has been also taken into account based on the plant species distribution and literature values of root
381 cohesion to product a map of root reinforcement of the study area. The outcomes of the model are daily failure
382 probability maps with a spatial resolution of 10 m. To evaluate the model performance both temporal and spatial
383 validation were carried out, and in general for both the simulated events the computed highest daily probability of
384 occurrence corresponds to the days and the areas of real landslides.

385 The application has highlighted also some drawbacks that are mainly related to the validation of the model performance
386 and to the uncertainty of the model input parameters. In particular, a satisfactory validation of the model is possible
387 only if available a complete event database of landslides with spatial and temporal resolution equal to the HIRESSS
388 model ones. On the other hand a correct geotechnical and hydrological characterization of the soil parameters as input
389 data of the model, as well as a correct approach to spatialize the data are both fundamental to apply the model and to
390 have sound result at regional scale.

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