© Author(s) 2017. CC BY 4.0 License.





Developing fragility functions for aquaculture rafts and eelgrass in the case of the 2011 Great 1 East Japan tsunami 2

3

4 Anawat SUPPASRI¹, Kentaro FUKUI², Kei YAMASHITA³, Natt LEELAWAT⁴, Hiroyuki 5 OHIRA⁵, and Fumihiko IMAMURA⁶

- 6
- 7 ¹International Research Institute of Disaster Science, Tohoku University
- (468-1 Aramaki-aza Aoba, Aoba-ku, Sendai 980-0845, Japan) suppasri@irides.tohoku.ac.jp 8
- 9 ²Kanagawa Prefectural Office,
- (1 Nihon Odori, Naka-ku, Yokohama 231-8588, Japan) fukui19940616@gmail.com 10
- ³International Research Institute of Disaster Science, Tohoku University 11
- (468-1 Aramaki-aza Aoba, Aoba-ku, Sendai 980-0845, Japan) yamashita@irides.tohoku.ac.jp 12
- ⁴ Department of Industrial Engineering, Faculty of Engineering, Chulalongkorn University 13
- 14 (Phayathai Road, Pathumwan, Bangkok 10330 Thailand) natt.l@chula.ac.th
- 15 ⁵ Electric Power Development Co., Ltd.
- (6-15-1,Ginza, Chuo-ku, Tokyo,104-8165 Japan) Hiroyuki Oohira@jpower.co.jp 16
- 17 ⁶International Research Institute of Disaster Science, Tohoku University
- 18 (468-1 Aramaki-aza Aoba, Aoba-ku, Sendai 980-0845, Japan) imamura@irides.tohoku.ac.jp

19 20

Abstract

Since the two devastating tsunamis in 2004 (Indian Ocean) and 2011 (Great East Japan), new 21 22 findings have emerged on the relationship between tsunami characteristics and damage in terms 23 of fragility functions. Human loss and damage to buildings and infrastructures are the primary 24 target of recovery and reconstruction; thus, such relationships for offshore properties and marine 25 ecosystems remain unclear. To overcome this lack of knowledge, this study used the available data from two possible target areas (Mangokuura Lake and Matsushima Bay) from the 2011 Japan 26 tsunami. This study has three main components: 1) reproduction of the 2011 tsunami, 2) damage 27 28 investigation and 3) fragility function development. First, the source models of the 2011 tsunami 29 were verified and adjusted to reproduce the tsunami characteristics in the target areas. Second, the damage ratio of the aquaculture raft and eelgrass was investigated using satellite images taken 30 before and after the 2011 tsunami through visual inspection and binarization. Third, the tsunami 31 32 fragility functions were developed using the relationship between the simulated tsunami characteristics and the estimated damage ratio. Based on the statistical analysis results, fragility 33 34 functions were developed for Mangokuura Lake, and the flow velocity was the main contributor to the damage instead of the wave amplitude. For example, the damage ratio above 0.9 was found 35 36 to be equal to the maximum flow velocities of 1.3 m/s (aquaculture raft) and 3.0 m/s (eelgrass). This finding is consistent with the previously proposed damage criterion of 1 m/s for the 37 aquaculture raft. This study is the first step in the development of damage assessment and planning 38 39 for marine products and environmental factors to mitigate the effects of future tsunamis.

Keywords: 2011 Great East Japan tsunami, fragility functions, aquaculture raft, eelgrass 41

- 42
- 43
- 44 45





46 1. Introduction

47 Aquaculture and ecological systems provide many services and functions to humans and are important to the global economy (Costanza et al., 1997). The 2011 Great East Japan tsunami 48 49 caused devastating damage to inland and offshore properties. Considerable economic damage from 50 the loss of aquaculture products and the impact to ecological systems was also caused by this 51 tsunami. Since the 2004 Indian Ocean tsunami and the 2011 tsunami, numerous quantitative measures of tsunami vulnerability, such as fragility functions, have been developed for buildings 52 53 (Suppasri et al., 2016), infrastructures (Shoji and Nakamura, 2017) and marine vessels (Suppasri et al., 2014 and Muhari et al., 2015). However, only one criterion is based on a previous study of 54 55 the 1960 Chilean tsunami that struck the west of Japan: the damage to an aquaculture raft (pearl) begins to occur when the tsunami flow velocity is larger than 1 m/s regardless of the water level 56 (Nagano et al., 1991). No other criterion or study has been presented regarding the vulnerability 57 58 of marine plants.

59

60 1.1 Objectives

To quantitatively assess such damage to marine products and marine ecosystems, the main 61 objective of this study is to develop the fragility functions as the first step to understand the 62 relationship between the tsunami characteristics and the damage. After reviewing previous works, 63 this study comprises three main sections: 1) reproduction of the 2011 tsunami, 2) damage 64 investigation and 3) development of fragility functions. The first section presents a validation of 65 the proposed source models for the 2011 tsunami and the adjustment for tsunami reproduction in 66 67 the study areas. The second section presents the available damage data and damage quantification. 68 The third section presents statistical analysis methods to develop the fragility functions using the 69 results obtained from the first and second sections. Finally, new findings, recommendations and 70 the limitations of this study are discussed.

71

72 **1.2 Review of previous studies**

This section reviews selected previous studies related to the damage characteristics of offshore 73 74 facilities and marine plants against tsunamis. The first attempt was based on the 1960 Chilean tsunami that struck the west of Japan. The damaged aquaculture rafts were plotted against the 75 76 simulated maximum water level and flow velocity (Nagano et al., 1991). As shown in Fig. 1, the 77 damage to the aquaculture raft (pearl) begins to occur when the tsunami flow velocity is higher 78 than 1 m/s regardless of the water level. Similarly, Kato et al., (2010) applied identical criteria to 79 quantify the damage to aquaculture rafts in areas along the east coast of Japan, which were struck by the 2010 Chilean tsunami. They found that the damage on the east coast of Japan caused by the 80 2010 Chilean tsunami was accurately modeled by the proposed damage criteria developed from 81 the data of the 1960 Chilean tsunami in the west of Japan. 82

83 After the 2011 tsunami, Suppasri et al. (2014) and Muhari et al. (2015) developed fragility functions for fishing boats. Based on their results, the threshold water level and flow velocity 84 values for the complete destruction of small boats of less than 5 tons are 2 m and 1 m/s, respectively. 85 Keen et al. (2017) developed fragility functions for structural components in small craft harbors 86 87 based on actual damage caused by the 2011 tsunami on the US west coast. The 2016 Fukushima 88 tsunami caused no inland damage but some damage to aquaculture rafts and fishing boats in Sendai Bay (Suppasri et al., 2017). Nevertheless, no damage criteria or fragility functions have been 89 proposed for the 2011 tsunami. There have been limited studies on the relation between tsunami 90





91 characteristics and damage to sea plants. Sakamaki et al. (2016) and Tsujimoto et al. (2016) 92 reported the damage to eelgrass in Matsushima Bay but provided no direct consideration of the

effect of tsunami characteristics. Yamashita et al. (2016) noted possible relationships between the

sediment deposition and erosion caused by the 2011 tsunami and the damage to eelgrass.

95



96

Fig. 1 Damage criteria of the aquaculture raft based on the damage data from Kii Peninsula,
western Japan, from the 1960 Chilean tsunami (Adapted from Nagano et al., 1991)

99

100 1.3 Target areas of this study

Because the size of the 2011 tsunami was extremely large, most aquaculture rafts and other marine 101 plants were completely destroyed. There are only two well-suited locations with specific coastal 102 geography, namely, Mangokuura Lake and Matsushima Bay in Miyagi Prefecture (Fig. 2), where 103 the effects of the tsunami were comparatively small (Suppasri et al., 2012) and the aquaculture 104 rafts were undamaged and the eelgrass survived (University of Tokyo, 2016). Mangokuura Lake 105 106 has a notably narrow entrance from the Pacific Ocean through Ishinomaki Bay, and the average 107 sea depth is as shallow as 5 m or less. Matsushima Bay is protected by almost 300 small islands 108 around the bay front. Thus, the 2011 tsunami inundation and run-up heights in both areas were less than 1-2 m, whereas they were as high as 10 m in other nearby areas (Suppasri et al., 2012). As a 109 result, some aquaculture rafts and other marine plants survived in these two locations, which 110 enabled the development of fragility functions. 111







112 113

Fig. 2 Study areas: (a) Mangokuura Lake and (b) Matsushima Bay

114115 2. Reproduction of the 2011 tsunami

116 **2.1 Simulation conditions**

To obtain tsunami-related parameters, including the water level and flow velocity, the 2011 117 118 tsunami was reproduced using a numerical analysis. The 2011 tsunami was numerically simulated using a set of nonlinear shallow water equations, which were discretized using the staggered leap-119 120 frog finite difference scheme (TUNAMI model) with bottom friction in the form of Manning's formula, similar to previous studies (Suppasri et al., 2010, Charvet et al., 2015 and Macabuag et 121 al., 2016). Six computational domains were used as a nesting grid system of 1,215 m (Region 1), 122 405 m (Region 2), 135 m (Region 3), 45 m (Region 4), 15 m (Region 5) and 5 m (Region 6). The 123 tidal level of -0.42 m was set at the time of the tsunami occurrence, and the simulation time was 124 125 set to three hours to maximize the water level and flow velocity.









Fig. 3 Six computational areas for Mangokuura Lake (up) and Matsushima Bay (down)

128

129 2.2 Model calibration and verification

130 Three models of fault parameters were selected to reproduce the 2011 tsunami: Model 1: Tohoku 131 University model (Imamura et al., 2013); Model 2: Satake model (Satake et al., 2013); and Model 132 3: Japan Nuclear Energy Safety Organization (JNES) model (Sugino et al., 2013). The 133 corresponding fault parameters were used to estimate the seafloor deformation proposed by Okada 134 (1985), which later became the initial seafloor condition for the tsunami numerical simulation. The 135 simulated tsunami inundation and run-up height with the actual measured values (Mori et al., 2012) 136 were validated for each area using Aida's *K* and κ (Aida, 1978) as defined below.





$$\log K = \frac{1}{n} \sum_{i=1}^{n} \log K_i \tag{1}$$

$$\log \kappa = \sqrt{\frac{1}{n} \sum_{i=1}^{n} (\log K_i)^2 - (\log K)^2}$$
(2)

140

141

(3) $K_i = \frac{x_i}{y_i}$ 142 143

where x_i and y_i are the measured and simulated tsunami trace heights, respectively, at point *i*. 144 145 Consequently, K is considered a correction factor to adjust the modeled values to fit the actual tsunami averaged over several locations; κ is defined as a measure of the fluctuation or deviation 146 in K_i . The values of Aida's K and κ from each model are shown in Table 1. 147

For Mangokuura Lake, Model 3 produced the optimal values of Aida's K and κ . Because 148 149 K is slightly less than 1.0, the simulated tsunami heights are slightly larger than the measurement. Similarly, for Matsushima Bay, Model 2 produced the best Aida's K and κ . Because K is larger 150 151 than 1.0, the simulated tsunami heights are smaller than the measurement. To better obtain the 152 tsunami parameters, the fault slip was scaled by the K values of 0.96 and 1.29 for Mangokuura Lake and Matsushima Bay, respectively, so that the reproduced tsunami closely matched the 153 measured tsunami trace heights and satisfied the guideline of the Japan Society of Civil Engineers; 154 0.95 < K < 1.05 and $\kappa < 1.45$ (Suppasri et al., 2010). As a result, the accuracy of the simulated 155 tsunami parameters in both study areas was improved, as shown in Fig. 4. 156

157

158	Table 1	Aida'	s K	and κ	for	each	model	and	after	the	model	scaling
-----	---------	-------	-----	--------------	-----	------	-------	-----	-------	-----	-------	---------

159

Location	Value	Model 1	Model 2	Model 3	After scaling (Model 2)	After scaling (Model 3)
Mangalaura Laka	K	0.90	0.87	0.96	-	1.01
Mangokuura Lake	κ	1.65	1.49	1.45	-	1.41
Matauchima Day	K	1.53	1.29	1.35	1.06	-
Matsusiiiiia Day	κ	1.45	1.34	1.42	1.39	-







161 Calculation (m)
 162 Fig. 4 Comparison of the simulated and measured tsunami heights in Mangokuura Lake and
 163 Matsushima Bay

164

165 2.3 Reproduction results

The hydrodynamic properties of the 2011 tsunami were reproduced based on the model calibration
and verification as mentioned above. Fig. 5 shows that the average maximum water level and flow
velocity in the bay of Mangokuura Lake are approximately 0.5 m and 1-2 m/s, those of Matsushima
Bay are approximately 2 m and 3-5 m/s, and the average offshore maximum water level and flow
velocity in the other 2011 tsunami affected areas were much higher than these values (Suppasri et al., 2014).



Maximum Water Level (m)







174

Fig. 5 Simulated maximum water level and flow velocity in Mangokuura Lake and MatsushimaBay

177

3. Damage investigation of the aquaculture rafts and eelgrass

Damage inspection was performed using satellite images taken before and after the tsunamithrough a visual inspection for the aquaculture rafts and an image analysis for the eelgrass.

181

182 **3.1 Damage investigation of the aquaculture rafts**

In this study, only the long-line type of aquaculture raft (Fig. 6) had sufficient quantities to develop 183 184 the fragility function. This type of aquaculture raft is common in the study area and is used for oyster and seaweed farming. Examples of the visual inspection of the aquaculture rafts in the lake 185 before (Fig. 7a) and after the tsunami (Fig. 7b) are shown. Approximately half of the rafts remained 186 after the tsunami; the others were completely washed away. The remaining aquaculture rafts were 187 classified as undamaged, whereas the disappeared aquaculture rafts were classified as damaged. 188 Fig. 7 also shows the visual inspection results as polygons of the undamaged and washed-away 189 aquaculture rafts (long-line type) in Mangokuura Lake. Many damaged aquaculture rafts were 190 found near the entrance to and in the middle of the lake. Then, the created polygons were gridded 191 into 5×5 m² regions corresponding to the finest tsunami simulation grid (Region 6). The simulated 192 maximum water level and flow velocity were assigned to each grid. For Matsushima Bay, there 193 was an insufficient number of long-line-type aquaculture rafts, and many rafts could not be 194 classified into types. Therefore, only damaged aquaculture rafts in Mangokuura Lake were used 195 to develop fragility functions. 196







197 198 Fig. 6 Aquaculture raft (long-line type)

199



200 201

Fig. 7 Visual damage interpretation of aquaculture rafts (long-line type) (a) before and (b) after the 2011 tsunami

204

205 **3.2 Damage investigation of eelgrass**

Damage to eelgrass occurs in one of three modes: cut-off, deposition or erosion, as shown in Fig. 8. Although the deposition and erosion can be estimated using a sediment transport model, more detailed data and surveys are required to obtain the necessary data for the model input. This pilot study considered only the tsunami itself. In addition, the erosion was controlled primarily by the flow velocity. Therefore, the cut-off and erosion were considered damage from the horizontal force of the tsunami.







Fig. 8 Eelgrass (a) and its damage pattern: (b) cut-off, (c) sand deposition and (d) erosion

215

229

Color images from the actual satellite image before the 2011 tsunami and after the 2011 tsunami 216 were analyzed (University of Tokyo, 2016 and Tsujimoto et al., 2016). At this stage, the areas for 217 land, sea, aquaculture raft, eelgrass and mudflat were first identified. To identify only the eelgrass 218 area, the colored images were binarized to binary (black and white) images using the image 219 analysis software ImageJ which is being developed at the National Institutes of Health, the United 220 States (ImageJ, 2016). This binarization helps distinguish eelgrass and non-eelgrass areas. Figs. 9 221 and 10 show the eelgrass areas before and after the 2011 tsunami in Mangokuura Lake and 222 Matsushima Bay, respectively. The identified damage and undamaged areas for both aquaculture 223 rafts and eelgrass were gridded into 5×5 m² regions. Then, the damage ratio of each grid was 224 calculated, and the maximum simulated water level and flow velocity were assigned to each grid. 225 Finally, another process was performed to create a list of the simulated tsunami characteristics 226 (water level and velocity) and damage ratio to develop the fragility function, as explained in the 227 next section 228



Fig. 9 Areas of the eelgrass before (a) and after (b) the 2011 tsunami in Mangokuura Lake







231

Fig. 10 Areas of the eelgrass before (a) and after (b) the 2011 tsunami in Matsushima Bay

233234 4. Developing tsunami fragility functions

235 4.1 Preliminary analysis

236 A comparison of the aquaculture raft data in the cases of the 1960 Chilean tsunami (Fig. 1) and the 2011 Japan tsunami is shown in Fig. 11. Most of the undamaged aquaculture rafts in the 2011 237 tsunami were limited to the maximum flow velocity less than 1.5 m/s. For both target areas, the 238 239 damage probabilities for each range of the simulated water level and maximum flow velocity of 240 both aquaculture rafts and eelgrass were calculated and are shown against a median value in a 241 specific range of the grids. In Fig. 12, the preliminary scatter plot does not show any significant trend between the simulated maximum water level and the damage to the aquaculture rafts (Fig. 242 243 12a) and eelgrass (Fig. 12b) in Mangokuura Lake or between the simulated maximum flow 244 velocity and the damage to eelgrass in Matsushima Bay (Fig. 12c). Thus, another expected parameter was used to develop the fragility functions: the simulated maximum flow velocity in 245 Mangokuura Lake. To verify that our regression model is better than the predicted average value, 246 247 an analysis of variance (ANOVA) was performed. The ANOVA is a statistical test to verify whether the regression model is significantly satisfactory in terms of predicting the variable's value. 248 249 The analysis can test whether the proposed regression model provides a better estimation than 250 using the average value of the predicted variables. The result shows that the calculated models significantly predict the damage ratio (F aquaculture raft = 74.73; p aquaculture raft < 0.001; F 251 252 eelgrass = 89.70; p eelgrass < 0.001) in the model.









Maximum water level (m)
 Fig. 11 Comparison of the aquaculture raft data from the 1960 Chilean tsunami (Fig. 1) and the
 present study on the 2011 Japan tsunami



257 258

261

Fig. 12 Maximum water level and damage probability of the (a) aquaculture rafts and (b) eelgrassin Mangokuura Lake and (c) eelgrass in Matsushima Bay

262 4.2 Linear regression analysis

263 Only the simulated maximum flow velocity and damaged-eelgrass data in Mangokuura Lake could be used to develop the fragility functions. The tsunami fragility functions were developed by 264 265 applying the classical standardized lognormal distribution function throughout the linear regression analysis for both aquaculture rafts and eelgrass. For Mangokuura Lake, Fig. 12 shows 266 the histograms of the numbers of damaged and undamaged aquaculture rafts in every 100 grids 267 (Fig. 13a) and 0-50% damaged and 50-100% damaged eelgrass in every 5,000 grids (Fig. 13b) in 268 269 terms of the simulated maximum flow velocity range. Both histograms show that the damage data increase when the flow velocity increases. A linear regression analysis was performed to develop 270 the fragility function. The cumulative probability P of occurrence of the damage is given in Eq. 271 272 (4).

274
$$P(x) = \phi \left[\frac{\ln x - \mu'}{\sigma'} \right]$$
(4)
275





where Φ is the standardized lognormal distribution function, *x* is the hydrodynamic feature of the tsunami (simulated maximum velocity), and μ ' and σ ' are the mean and standard deviation of ln x, respectively. The statistical parameters μ ' and σ ' of the fragility function were obtained by plotting ln *x* against the inverse of Φ^{-1} on lognormal probability papers and performing least-squares fitting of this plot (Figs. 14a and 14b). Consequently, two parameters are obtained as the intercept (= μ ') and angular coefficient (= σ ') in Eq. (5).

(5)

 $\ln x = \sigma' \Phi^{-1} + \mu'$





288 289

Fig. 13 Histogram of the numbers of (a) damaged and undamaged aquaculture rafts and (b) 0-50%
damaged and 50-100% damaged eelgrass in terms of the simulated flow velocity range in
Mangokuura Lake.









294

Fig. 14 Least-squares fit on lognormal probability paper for the aquaculture rafts (a) and eelgrass (b) in Mangokuura Lake

297

298 4.3 Tsunami fragility functions for the aquaculture rafts and eelgrass

299 With the regression analysis, the parameters that best fit the fragility functions with respect to the 300 maximum flow velocity are shown in Table 2. The tsunami fragility curves for the aquaculture rafts and eelgrass were developed as shown in Figs. 15a and 15b, respectively. The proposed 301 fragility functions show that a damage ratio above 0.5 corresponds to the maximum flow velocity 302 of 0.8 m/s (aquaculture raft) and 1.0 m/s (eelgrass). A damage ratio above 0.9 corresponds to the 303 maximum flow velocity of 1.3 m/s (aquaculture raft) and 3.0 m/s (eelgrass). The results for the 304 aquaculture rafts are consistent with the previously proposed criteria (Nagano et al., 1991): at 1 305 306 m/s flow velocity, the damage ratio is almost 0.8.

307 308

Table 2 Parameters to create the tsunami fragility functions.

310

Item	μ'	σ'	R^2
Aquaculture raft	-0.2917	0.3464	0.65
Eelgrass	-0.0314	0.8750	0.74









312 313

Fig. 15 Tsunami fragility functions for the aquaculture rafts (a) and eelgrass (b) based on data from 314 Mangokuura Lake 315

316

317 5. Conclusions

5.1 Main findings 318

319 This study was the first attempt in this field to develop fragility functions for aquaculture rafts and 320 eelgrass. The careful selection of the study areas and availability of the damage data enabled this 321 attempt. First, we reproduced the hydrodynamic characteristics, i.e., the water level and flow 322 velocity of the 2011 tsunami, using the tsunami trace data for the model calibration and verification 323 based on the finest grid of 5×5 m² regions. The damage data for both aquaculture rafts and eelgrass 324 were investigated by visually inspecting and analyzing the satellite images before and after the 2011 tsunami. Then, the fragility functions for the aquaculture rafts and eelgrass were developed 325 326 using the data for Mangokuura Lake. This lake appears to be the only suitable location for a study based on tsunami characteristics because of its location and consequent damage range from no 327 damage to little damage to considerable damage. In addition, Matsushima Bay was exposed to a 328 stronger tsunami and had fewer undamaged aquaculture rafts and surviving eelgrass. The main 329 330 conclusions are as follows:

- 331 _ Based on the reproduced hydrodynamic characteristics of the 2011 tsunami, Matsushima Bay 332 was hit by a stronger tsunami than Mangokuura Bay (Fig. 5).
- The maximum water level is not related to the damage to aquaculture rafts and eelgrass (Fig. 333 _ 12). 334
- The threshold value (at 90% damage probability) of the maximum flow velocity for damage 335 _ to aquaculture rafts and eelgrass is 1.3 m/s and 3.0 m/s, respectively (Fig. 15). 336
- The proposed fragility function for the aquaculture rafts is consistent with the previously 337 proposed damage criteria and can further provide the values of the damage ratio at other flow 338 339 velocities in addition to the threshold value.
- This information on the tsunami damage in offshore areas is expected to be useful for marine 340 _
- product and environmental damage assessment and recommendations for aquaculture raft 341 zoning to mitigate the effects of tsunamis in the future. 342

© Author(s) 2017. CC BY 4.0 License.





343

344 5.2 Limitations, considerations and future studies

Although this study successfully developed fragility functions for aquaculture rafts and eelgrass
for the first time, certain limitations and considerations exist when applying the fragility functions,
and possible improvements to be pursued in future studies are as follows.

The developed fragility functions may underestimate the economic damage related to
 aquaculture rafts because the loss of marine products may occur even when the rafts remain.
 For example, although the aquaculture rafts were present in the satellite image, in some cases,

- For example, although the aquaculture rafts were present in the satellite image, in some cases, the marine products were completely washed away or damaged when the rafts collided with each other.
- This study simulated only the hydrodynamic characteristics of the tsunami, which can directly
 explain the damage caused by cut-off and erosion. However, the damage caused by deposition
 was not considered.
- The use of the actual surveyed damage to the aquaculture rafts and eelgrass and the application
 of a sediment transport model may increase the accuracy of the fragility functions.
- The fragility functions for both aquaculture rafts and eelgrass may differ based on the type of
 aquaculture raft and the environmental conditions of the eelgrass. Future studies of aquaculture
 rafts and eelgrass in other areas impacted by historical tsunami events may improve our
 understanding of these differences and the generalizability of the fragility functions.
- 362

363 Acknowledgments

- We thank the Miyagi Prefecture Fisheries Cooperative Association (JF Miyagi) Ishinomaki Bay
 branch for their information on the aquaculture rafts and Dr. Daisuke Sugawara (Museum of
 Natural and Environmental History, Shizuoka) for his help in developing the bathymetry and
 topography data. This study was funded by the Tokio Marine & Nichido Fire Insurance Co., Ltd.
 through IRIDeS, Tohoku University, Willis Research Network (WRN) and JSPS Grant-in-Aid for
 Young Scientists (B) "Applying developed fragility functions for the Global Tsunami Model
 (GTM)" (grant no. 16K16371).
- 371

372 References

- Aida, I. (1978) Reliability of a tsunami source model derived from fault parameters, J. Phys. Earth,
 26, 57–73.
- Costanza, R., D'Arge, R., Groot, R. D., Farber, S., Grasso, M., Hannon, B., Limburg, K., Naeem,
 S., O'Neill, R. V., Paruelo, J., Raskin, R. G., Sutton, P. and Van Den Belt, M. (1997) The value
 of the world's ecosystem services and natural capital, Nature, 387, 253-260.
- Charvet, I., Suppasri, A., Kimura, H., Sugawara, D. and Imamura, F. (2015) Fragility estimations
 for Kesennuma City following the 2011 Great East Japan Tsunami based on maximum flow
 depths, velocities and debris impact, with evaluation of the ordinal model's predictive accuracy,
 Natural hazards, 79(3), 2073-2099.
- 382 Fukuoka Fisheries and Marine Technology Research Center (2016): Longline type of aquaculture
- 383raftforoyster,availableathttp://www.sea-384net.pref.fukuoka.jp/gaiyo/naminami/vol8/nami8fukyuu.htm(In Japanese) (Accessed date: 10
- 385 May 2016)
- Kato, H., Tanji, Y., Fujima, K. and Shigihara, Y. (2010) Study on Measures against Drifting of
 Cultivation Rafts by Tsunami (Report on the result of 2010 Chili Earthquake Tsunami),

© Author(s) 2017. CC BY 4.0 License.





- Collection of articles published by the Japanese Institute of fisheries Infrastructure and
 Communities, 21, 111-120. (In Japanese with English abstract)
- Keen, A. S., Lynett, P. J., Eskijian, M. L., Ayca A. and Wilson, R. (2017) Monte Carlo-based
 approach to estimating fragility curves of floating docks for small craft marinas, J. Waterway,
 Port, Coastal, Ocean Eng., Vol. 143, No. 4, pp. 04017004.
- ImageJ (2016) ImageJ, Image Processing and Analysis in Java, available at:
 https://imagej.nih.gov/ij/index.html
- Imamura, F. (1996) Review of tsunami simulation with a finite difference method, in H. Yeh, P.
 Liu, and C. E. Synolakis (Eds.), "Long-Wave Runup Models," pp. 25-42, Singapore: World
 Scientific Publishing Co., 1996.
- Imamura, F., Koshimura, S., Mabuchi, Y., Oie, T. and Okada, K. (2011) Tsunami simulation of
 the 2011 Great East Japan Tsunami using Tohoku University model (Version 1.1), available at
 http://www.tsunami.civil.tohoku.ac.jp (In Japanese) (Accessed date: 7 November 2011)
- Latcharote, P., Leelawat, N., Suppasri, A. and Imamura, F. (2017) Developing estimating
 equations of fatality ratio based on surveyed data of the 2011 Great East Japan Tsunami, IOP
 Conf. Series: Earth and Environmental Science, Vol. 56, pp. 012011.
- Macabuag, J., Rossetto, T., Ioannou, I., Suppasri, A., Sugawara, D., Adriano, B., Imamura, F. and
 Koshimura, S. (2016) A proposed methodology for deriving tsunami fragility functions for
 buildings using optimum intensity measures, Natural Hazards, 84 (2), 1257-1285.
- Mori, N., Takahashi, T. and 2011 Tohoku Earthquake Tsunami Joint Survey Group (2012)
 Nationwide Post Event Survey and Analysis of the 2011 Tohoku Earthquake Tsunami, Coastal
 Engineering Journal, 54, 1250001.
- Muhari, A., Charvet, I., Futami, T., Suppasri, A. and Imamura, F. (2015) Assessment of tsunami
 hazard in port and its impact on marine vessels from tsunami model and observed damage data,
 Natural Hazards, 78(2), 1309-1328
- Nagano, O., Imamura, F. and Shuto, N. (1991) A numerical model for far-field tsunamis and its
 application to predict damages done to aquaculture, Natural Hazards, Vol. 4, pp. 235–255.
- Northwest Pacific Region Environmental Cooperation Center (NPEC), Atmosphere and Ocean
 Research Institute, The University of Tokyo (2016) Damage condition of seaweed bed and
 tideland based on the 2011 Great East Japan tsunami in Mangokuura Lake, available at
 http://ocean.nowpap3.go.jp/wp-content/uploads/2014/07/mangoku_higai.pdf (Accessed date:
 6 August 2016)
- Satake, K., Fujii, Y., Harada, T. and Namegaya Y. (2013) Time and Space Distribution of
 Coseismic Slip of the 2011 Tohoku Earthquake as Inferred from Tsunami Waveform Data, Bull.
 Seismol. Soc. Am., Vol. 103, No. 2B, pp. 1473-1492.
- Sakamaki, T., Sakurai, Y. and Nishimura, O. (2016) Tsunami impacts on eelgrass beds and acute
 deterioration of coastal water quality due to the damage of sewage treatment plant in
 Matsushima Bay, Japan, Tsunamis and earthquakes in coastal environments: Significance and
 restoration, Coastal Research Library, 14, 187-199.
- Shoji, G. and Nakamura, T. (2017) Damage assessment of road bridges subjected to the 2011
 Tohoku Pacific earthquake tsunami, Journal of Disaster Research, Vo. 12, No. 1, pp. 79-89.
- 429 Sugino, H., Wu, C., Korenaga, M., Nemoto, M., Iwabuchi, Y. and Ebisawa, K. (2013) Analysis
- 430 and verification of the 2011 Tohoku earthquake tsunami at nuclear power plant sites, Journal
- 431 of Japan Association for Earthquake Engineering, Vol. 3, No. 2, pp. 2-21. (In Japanese)

Natural Hazards and Earth System Sciences Discussions



- Suppasri, A., Koshimura, S. and Imamura, F. (2011) Developing tsunami fragility curves based on
 the satellite remote sensing and the numerical modeling of the 2004 Indian Ocean tsunami in
 Theiland Net Hagard Forth Size Vol. 11, No. 1, pp. 172–180.
- 434 Thailand, Nat. Hazard. Earth Sys, Vol. 11, No. 1, pp. 173-189.
- Suppasri, A., Latcharote, P., Bricker, J. D., Leelawat, N., Hayashi, A., Yamashita, K.,
 Makinoshima, F., Roeber, V. and Imamura, F. (2016) Improvement of tsunami
 countermeasures based on lessons from the 2011 great east japan earthquake and tsunami Situation after five years-, Coastal Engineering Journal, 58 (4), 1640011.
- Suppasri, A., Leelawat, N., Latcharote, P., Roeber, V., Yamashita, K., Hayashi, A., Ohira, H.,
 Fukui, K., Hisamatsu, A., Nguyen, D. and Imamura, F. (2017) The 2016 Fukushima Earthquake
 and Tsunami: Preliminary research and new considerations for tsunami disaster risk reduction,
- 442 International Journal of Disaster Risk Reduction, 21, 323-330.
- Suppasri, A., Mas, E., Charvet, I., Gunasekera, R., Imai, K., Fukutani, Y., Abe, Y. and Imamura,
 F. (2013) Building damage characteristics based on surveyed data and fragility curves of the
 2011 Great East Japan tsunami, Nat. Hazards, Vol. 66, No. 2, pp. 319-341.
- Suppasri, A., Muhari, A., Futami, T., Imamura, F. and Shuto, N. (2014) Loss functions of small
 marine vessels based on surveyed data and numerical simulation of the 2011 Great East Japan
 tsunami, J. Waterway, Port, Coastal, Ocean Eng., Vol. 140, No. 5, pp. 04014018.
- Tsujimoto, R., Terauchi, G., Sasaki, H., Sakamoto, S. X., Sawayama, S., Sasa S., Yagi, H. and
 Komatsu, T. (2016) Damage to seagrass and seaweed beds in Matsushima Bay, Japan, caused
 by the huge tsunami of the Great East Japan Earthquake on 11 March 2011, International
 Journal of Remote Sensing, 37(24), 5843-5863.
- Yamashita, K., Sugawara, D., Takahashi, T. and Imamura, F. (2016) Influence of sediment
 transport on seaweed bed dissipation in Shizugawa Bay, Miyagi Prefecture in the 2011 Great
 East Japan Earthquake, Abstract of the 2015 Annual Seminar of Tohoku Disaster Science
 Research (in Japanese).
- 457