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1 Coseismic deformation field derived from Sentinel-1A data and slip inversion of

- the 2015 Chile Mw8.3 earthquake
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9 Abstract. We obtain the coseismic surface deformation fields caused by the Chile Mw8.3 earthquake on 16 10 September 2015 through analyzing Sentinel-1A/IW InSAR data from ascending and descending tracks. The results 11 show that the main deformation field looks like a half circle convex to east with maximum coseismic displacement 12 of about 1.33m in descending LOS direction, 1.32m in ascending LOS direction. Based on an elastic dislocation 13 model in a homogeneous elastic half space, we construct a small-dip single plane fault model and invert the coseismic 14 fault slip using ascending and descending Sentinel-1A/IW data separately and jointly. The results show that the 15 patterns of the main slip region are similar in all datasets, but the scale of slip from ascending inversion is relatively 16 smaller. Joint inversion can display comprehensive fault slip. The seismic moment magnitude from the joint 17 inversion is Mw8.25, the rupture length along strike is about 340 km with a maximum slip of 8.16m near the trench 18 located at -31.04N, -72.49E, and the coseismic slip mainly concentrates at shallow depth above the hypocenter with 19 a symmetry shape. The depth where coseismic slip is near zero appears to a depth of 50km, quantitatively indicating 20 the down-dip limit of the seismogenic zone. From the calculated coseismic Coulomb stress change, we find 21 aftershocks locations correlate well with the areas having increased Coulomb stress and most areas with increased 22 Coulomb stress appeared beneath the main shock fault plane. 23 Keywords: Chile earthquake; InSAR; Coseismic deformation; slip distribution; Coulomb stress change

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25 1. Introduction

26 On September 16, 2015, a magnitude 8.3 offshore earthquake struck west of Illapel, Chile. About one million 27 people evacuated from their homes. A tsunami hit Coquimbo and other villages with waves close to 4 meter high (http://www.emsc-csem.org/Earthquake/237/M8-3-OFFSHORE-COQUIMBO-CHILE-on-September-16th-2015-28 29 at-22-54-UTC). This huge earthquake was the result from thrust faulting on the interface between the Nazca and 30 South America plates in central Chile, of which the epicenter is about 85 km to the Chile Trench. At the latitude of 31 this event, the Nazca plate is moving towards the east-northeast at a velocity of 65-74 mm/yr with respect to South 32 America, and begins its subduction beneath the continental South American plate at the Peru-Chile Trench. Located 33 on the subduction boundary of the two plates, Chile is one of the most earthquake-prone countries in the world 34 (Madariaga et al., 2010). The 2010 Mw8.8 Maule earthquake in central Chile ruptured a ~600 km (Tong et al, 2010; 35 Delouis et al, 2010; Pollitz et al, 2011) long section of the plate boundary south of this 2015 event and the 1985 36 Mw7.8 event (Barrientos,1995). This subduction zone hosted the largest earthquake on the record, the 1960 37 magnitude 9.5 Chile earthquake (National Earthquake Information Center (NEIC), 2010; Cifuentes et al. 1989). In 38 the past century, the region within 400 km to the event on September 16, 2015 has suffered 15 other earthquakes 39 with magnitude greater than 7 (http://earthquake.usgs.gov/earthquakes/eventpage/us20003k7a#general_summary). 40 Along the trench, most zones has been ruptured during the past earthquakes (Vigny et al., 2011) (Fig. 1).







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42 Figure 1. Tectonic setting around the 2015 Mw8.3 earthquake. Red dots: Epicenters of historical earthquakes near 43 this Illapel 2015 event (Mw8.4 in 1922, Mw8.3 in 1943, Mw7.8 in 1971, Mw7.8 in 1985, Mw8.8 in 2010). Yellow 44 dot: Epicenter of 2015 Mw8.3 Illapel event. Black circles: aftershocks (from http://earthquake.usgs.gov, as of 45 18/9/2015). The red barbed line is the Chile trench trace. Color stripes along the trench depict past earthquake rupture 46 zones (adapted from Vigny et al., 2011). ETOPO1 Digital Elevation Models 47 (http://www.ngdc.noaa.gov/mgg/global/global.html) were used to generate the background topography. The black 48 rectangle is the fault plane projected onto the surface.

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50 The information on the down-dip limit of the seismogenic zone and transition depth from seismic to aseismic 51 slip of thrust faulting earthquakes is important to understand Chile subduction zone. (Mendoza et al. 1994; Pritchard 52 et al. 2006). Modern geodetic technology can obtain small deformation of crust and could be used as a tool for 53 seismic hazard assessment (Ader et al. 2012). Inversion of the co-earthquake rupture depth constrained by a dense 54 geodetic data, e.g., deformation measurement from Synthetic Aperture Radar Interferometry (InSAR) and Global 55 Positioning System, permits to address this issue. For example, using InSAR and GPS data, Tong et al. (2010) 56 estimated the maximum rupturing depth of the 2010 Chile Mw8.8 event, which is 43-48km and is largely consistent 57 along the 600km-long rupture zone. For the same event and also using joint inversion of ALSO/PALSAR and GPS 58 data, Pollitz et al. (2011) suggested that the fault rupture of this event terminated at a depth of 35km, which is relative 59 shallow, and likely associated with the spherical layering Earth model used in their inversion. Using joint inversion 60 of teleseismic records, InSAR and high rate GPS (HRGPS) data, Delouis et al. (2010) constrained the maximum 61 down-dip depth as 50km for the 2010 Chile great shock. These studies on the rupturing depth of the great earthquakes 62 can provide evidence for determining the seismogenic depth, lower limit of stick-slip and the boundary between 63 seismic and aseismic layers in the subduction zone beneath central Chile.

In this work, both the descending and ascending track of Sentinel-1A/IW data have been downloaded and processed to reconstruct the coseismic deformation field of the 2015 Chile event. Then, we inverted the slip distribution on the seismogenic fault plane of this earthquake with three different constraints of descending and ascending measurements separately and jointly. Thirdly, we discussed the observation and inversion results.





68 Additionally, inversion results (e.g., rupture depth) from each track (ascending, descending) and join tracks has been 69 analyzed. Finally, in order to identify the promoting relationship between the main shock and aftershocks, we 70 estimated the shear stress in the aftershock area of the main shock event. The complete InSAR coverage over the 71 rupture area provided a unique information to derive a detailed slip model, which is needed to estimate the spatially 72 varied stress change from the event.

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2. Sentinel-1A InSAR data and processing

75 We investigated the crustal deformation triggered by the 2015 Mw8.3 Chile earthquake using interferometric 76 synthetic aperture radar (InSAR) with Sentinel-1A Interferometric Wide Swath (/IW) mode data in both descending 77 and ascending orbits. Sentinel-1A satellite was launched by ESA on April 3, 2014, and its IW Mode used the 78 technology advanced TOPSAR (Terrain Observation with Progressive Scans SAR) 79 (https://sentinel.esa.int/web/sentinel/user-guides/sentinel-1-sar/applications). The radar image in IW model has a 80 swath width up to 250km, spatial resolution of 5m×20m (single look), and revisit period of 12 days, providing a 81 good data source for large-scale monitoring of ground deformation. At present, Sentinel-1A satellite data can be 82 accessed through ESA data hub (https://scihub.esa.int/). It is one and three days after the 16 September 2015 Chile 83 event, i.e. 17 September and 19 September that Sentinel-1A acquired descending and ascending data covering the 84 coseismic area. The selected post-earthquake images are close to the event time, whereas the pre-image can be 85 acquired long before the event. Because data very close to the mainshock time, permit to study the coseismic 86 deformation of this event without much aftershock deformation. As the affected area of this great event is very large, 87 we use three adjacent frame along the same descending track to get a full coseismic deformation field. Since, in the 88 ascending track, only two frames are available, we get only part of coseismic deformation field. The SAR data and 89 its parameters used in this paper are shown in Table 1.

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Table 1. The Sentinel-1A/IW data used in this study

Number	Track	Master	Slave	Average Perpendicular Baseline(m)	Average Ambiguity Height(m)
1	Descending	20150707	20150917(north)	1	13667
2	Descending	20150707	20150917(middle)	-1	13667
3	Descending	20150707	20150917(south)	-3	4556
4	Ascending	20150826	20150919(north)	73	187
5	Ascending	20150826	20150919(south)	70	195

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92 We used the GAMMA software to process the Sentinel-1A data. The interferograms have been processed 93 separately for each frame along the same track, and then mosaicked to a signal wrapped differential interferogram. 94 To reduce noise, multi-look processing of 10-sight in range and 2-sight in azimuth directions were performed to the 95 interferograms. It requires a very high SLC (single look complex image) registration accuracy in azimuth direction 96 (Meta et al., 2010). To achieve an accuracy of a very small fraction of an SLC pixel nearly 0.1/% in azimuth direction, 97 we performed intensity image based and iterating offset estimation for many times until the azimuth offset correction 98 became at least smaller than 0.02 SLC pixel. Meanwhile, the adaptive filters based on interferometric fringe 99 frequency and gradually decreasing windows were applied to interferograms so that their ratio of signal to noise was 100 highly enhanced, fringes associated with seismic deformation were highlighted. The algorithm of minimum cost 101 flow (Werner et al., 2002) was implemented for phase unwrapping with Delaunay triangle network that is suitable





102 for low coherent areas. To make phase continuous and smooth, before integration of mosaic three adjacent 103 interferograms on descending track, we firstly unwrapped the interferogram in the southernmost of the study area, 104 and used the far field to its south as the start point for unwrapping. It was followed by unwrapping the interferogram 105 in the middle, using the same-place point in superposed portion of the two adjacent interferograms as the reference 106 and initial phase value for unwrapping it. Similarly, the interferogram in the north was unwrapped. Consequently, 107 the interferogram from integrating these three images was featured by continuous phase without signature of 108 boundaries. When doing this, we removed topographic phase by the generating simulated interferogram using 109 ASTER GDEM data (30m×30m) (http://gdem.ersdac.jspacesystems.or.jp/search.jsp).



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Figure 2. Earthquake mainshock, as seen from radar satellites that allow quantifying displacements in the Line of Sight (LOS) as indicated by green arrow in (A-D). Upper row is the data (A, C, coseismic deformation field from descending track; B, D, coseismic deformation field from ascending track). Center row (E-H) is the model solution (the model in black dashed area is constrained by descending data, in blue dashed area is constrained by ascending data, in red dashed line is constrained by ascending and descending data combine). Bottom row (I-L) shows the residual after subtracting the model from the data. Red dot depicts the location of the mainshock epicenter from USGS, about 10km to the coast. The red barbed line is the trench trace.

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119 3. Coseismic deformation fields derived from Sentinel-1A ascending and descending InSAR data

As mentioned above, the deformation field from descending data was generated by integrating three
 interferograms along the same track, which covers almost the whole affected area of the 2015 Chile earthquake (Fig.
 2A). Towards the continent, the fringes become progressively sparse, implying decreasing gradients of deformation.





123 While we set the deformation in far field, without any phase change, to zero, the maximum LOS displacement is -124 133cm near the coast. It looks like a half circle convex to east, with most of data being negative, which means 125 subsidence in descending LOS direction. According to the full descending track fringes, the deformation area is 126 within 300km long in the NS direction or along the coast, and 190km in the EW direction. Although the deformation 127 field derived from the ascending data is only based on two frame, it also covers the major part of the seismic 128 deformation area (Fig 2B), consistent with that from the descending data. This field is also of a half circle convex to 129 east with maximum LOS displacement 132cm (far field deformation be zero). Deformation in LOS being positive, 130 means uplift in ascending LOS direction. The positive and negative with similar magnitude of LOS deformation 131 from ascending and descending data suggest that the crustal deformation caused by this earthquake is dominated by 132 horizontal motion.

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134 4. Fault slip inversion and interferogram simulation

135 4.1 Inversion method and fault model construction

136 USGS Focal mechanism solutions GCMT given by (http://www.usgs.gov/) and 137 (http://www.globalcmt.org/CMTsearch.html) show that the seismogenic fault of this earthquake is thrust with a small 138 dip angle. Its surface trace closely follows the trench axis. Based on the focal mechanism solutions, aftershock 139 distribution and InSAR deformation fields obtained in this work, we built a single-plane fault model in elastic half-140 space (Okada Y. 1985) to invert the static coseismic slip distribution on the rupture surface constrained by the 141 Sentinel-1A descending and ascending data both separately and jointly. The linear-inversion, Sensitivity Based 142 Iterative Fitting (SBIF) method (Wang et al., 2008) was employed. Firstly, the fault plane was divided into multiple 143 fault patches. Each patch was presumed to slip uniformly. In this way, the non-linear problem can be transformed 144 into a linear problem. Then we used the mean square deviation reducing function to quantify the misfit between the 145 simulated interferogram and the observed one. Using this function, by minimizing mean square deviation, non-146 uniform slip distribution on the fault plane can be determined. The mathematical formulation of the inversion is 147 expressed by:

$$f(s) = \sum_{k=0}^{K} \left\| D_k - D_k^0 - G_k s(x) \right\|^2 + \beta^2 \left\| Hs \right\|^2 \to \min$$

149 Where's(x)' is slip vector, 'k' is the patch index of different input data set. 'D' is the matrix of observation data, 'D⁰' 150 is the static offset of the observations, 'G' is the Green's function for an elastic half-space, which describes the 151 relation between the model prediction and the observation. ' β ' is defined as the smoothing factor, 'H' is the Laplacian 152 operator, and $||H_S||^2$ represents the slip roughness. Assuming a Poisson ratio of 0.25 and using SBIF program, we 153 calculate the Green's functions of the homogeneous elastic half-space model using Okada.

154 Also, we resampled the InSAR deformation field by the quad-tree resampling method for inversion (J ánsson 155 et al., 1999; Lohman et al., 2005). The reason to do quad-tree is to reduce computation load and also to keep the 156 pattern of deformation map. In the resampling process, we have 12763 sampled points from Sentinel-1A descending 157 data and 9196 sampled points from Sentinel-1A ascending data, respectively, which still have a much higher spatial 158 density than other geodetic data (e.g., GPS). The initial fault geometry is a single planar surface striking N4.6 E and 159 dipping toward the east, where it takes trial values between 10 ° and 30 °. The rake angles are in the range of 80 °~150 °. 160 The upper boundary of the fault is to surface. The initial fault model is steadily modified through optimal fitting to 161 the deformation fields derived from both Sentinel-1A descending and ascending data sets in joint inversion. The 162 final fault model is that dip angle is 18.3 $^{\circ}$, strike is 4.6 $^{\circ}$, and the fault dimensions are 535 km along-strike and 163 200 km down-dip, with fault plane divided into many rectangular patches whose grid is 10km×10km from best fault 164 resolution test (Table 2).

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Table 2. Main parameters of the optimal fault model

Parameters	Lat_Ref(%	Lon_Ref(%	Strike()	Dip()	Length(km)	Rake()	Width(km)	Top_Depth(km)
Final values	-33.3	-72.75	4.6	18.3	535	80~150	200	0

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4.2 Fault slip inverted from Sentinel-1A descending and ascending data separately and jointly

168 Using the fault model and resampled data points described above, we inverted slip distribution on the fault 169 plane of this Chile earthquake constrained by the Sentinel-1A descending and ascending observations separately and 170 jointly. The calculated residual maps between the observed and simulated ones are shown in Figure 2. The result 171 shows that when the inversion is constrained by Sentinel-1A descending data alone, the preferred slip model shows 172 a preponderant fault rupture zone located in the shallow part of the up-dipping thrust fault above the hypocenter (Fig. 173 3B). The maximum fault slip is over 8 m at a shallow depth, located in the northwest of the epicenter. The down-dip 174 boundary of the rupture zone is relatively clear, and its depth is only about 35km under the surface. The rupture 175 length of the slip area is about to 340km, comparable to 335 km of the major axis of aftershock distribution in north 176 and south direction. But the main slip is concentrated in a shallow region that is 15km deep and 200 km long on the 177 subduction interface. The mean rake angle from inversion is 110°, consistent with the thrust fault motion. The 178 simulated interferogram is reconciled well with the observed one, with fitting degree 99.99%. The seismic moment 179 magnitude is Mw8.27.

When the inversion is constrained by the Sentinal-1A ascending data alone, the resulted fault slip magnitude and its scope are all smaller than that constrained by the Sentinal-1A descending data, although the overall patterns of the slip region in both cases are similar (Fig. 3A). The probable reason is that the ascending data do not fully cover the deformation field, since only two frame images are available. The maximum slip from this inversion is only about 3.43m. The mean rake angle is 102.42 °. The simulated interferogram fits the observed one very well with the fitting degree 99.97%. The seismic moment magnitude is Mw8.09. It should be pointed out that the down-dip boundary of the rupture zone is much deeper, with the depth about 50km under the surface.

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 Table 3. Fault plane and source parameters of the 2015 Chile earthquake given by teleseismic focal mechanism solutions and this study

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Source	Latitude ()	Longitude ()	Depth (km)	Mw	Strike	Dip ()	Rake	Scalar Moment(N.m)
GCMT	-31.22	-72.27	17.8	8.2	5	22	106	2.455×10^{21}
USGS	-31.57	-71.67	20.7	8.3	5	22	106	3.467×10^{21}
Descending	-	-	-	8.27	4.6	18.3	116.41	3.126×10 ²¹
Ascending	-	-	-	8.09	4.6	18.3	102.42	1.679×10^{21}
Jointly	-	-	-	8.25	4.6	18.3	103.24	2.917×10 ²¹

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We implemented a fault slip inversion jointly using the Sentinel-1A ascending and descending data with equal weight. The result falls between the two inversion results by using the two data alone (Fig. 3C). The shape of slip area seems to be symmetrical. The inversion result indicates that the mean rake angle is about 103.24°, which is in agreement with a thrust fault. The fitting degree is also very good, about 99.97%. The maximum slip is about 8.16m at shallow depth near the trench. The seismic moment magnitude is Mw8.25. The final inversion results are shown in Table 3 and Figure 3. It seems that combination of descending and ascending InSAR data used in inversion helps to derive a more comprehensive fault slip distribution.

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Figure 3. Fault slip distribution inverted by using Sentinel-1A ascending and descending data. The fault trace at the surface is from (-33.3N, -72.75E) in south to (-28.5N, -72.30E) in north, strike is N4.6 E. The blue rectangle is the fault plane projected onto the surface. Number with white background is the depth of the fault in kilometer. Red dot is the position of epicenter from USGS. Aftershocks (from http://earthquake.usgs.gov, as of 18/9/2015) are represented by black circle. (A) Fault slip distribution inverted by ascending data. (B) Fault slip distribution inverted by descending data. (C) Fault slip distribution inverted by ascending and descending data jointly as constraints.

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207 4.3 Static Coulomb stress changes

208 In order to identify the promoting relationship between the main shock and aftershocks, we calculated the 209 coseismic Coulomb Failure Stress (CFS) change on the fault plane and surrounding medium by using the optimal 210 slip model (Lin 2004; Toda 2005), which comes from inversion by ascending and descending jointly. Computing the 211 CFS change following an earthquake tells whether a fault has been brought closer or away from rupture (Stain 1999). 212 Many researches suggest that 0.1bar shear stress change can have a great influence in earthquake activities (King et 213 al., 1994). From the location of aftershocks, we found most of the aftershocks happened under our inverted fault 214 plane (Fig. 4B red line). The distribution of aftershocks reflected a special plane (Fig. 4B dash line in blue) whose 215 dip angle is about 31 °, much bigger than the dip angle (18.3 °) from our main shock inversion and results from USGS 216 (dip=19 °) and GCMT (dip=22 °). So in our models we set the receiver plane dip angle 31°, with strike 4.6 ° and rake 217 105 °, to see what the static coulomb stress the main shock promoted to aftershock is. From the coseismic Coulomb 218 stress profile at 30km depth (Fig. 4A), we estimate the coseismic shear stress change ranged from -12 bar (stress 219 drop) to 8 bar (stress increase) and find aftershocks (depth in 20km-30km) locations correlate well with the areas 220 having increased Coulomb stress. The three special profiles in vertical (dip=90 °) reflected most areas with increased 221 Coulomb stress appeared beneath the main shock fault plane, which is consistent with the location where aftershocks 222 took place. At the same time, we can see static Coulomb stress up the main shock fault plane is released (Fig. 4C). 223 A frictional ratio of 0.4 and rake angle 105 were used in these results, but we also explored different frictional ratios 224 (0.3-0.7) and rake angles of receiver plane (100 °-110 °). No significant difference was observed for the obtained CFS, 225 implying that the models are robust. 226

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229 Figure 4. (A) Coulomb Failure Stress (CFS) changes (in bar) due to 2015 September 16 main shock is calculated at 230 a depth of 30km. The red circle marks the main shock and black circle is the location of other aftershocks (Mw>4) 231 in the depth from 20km to 30km. (B) Location of aftershocks (from http://earthquake.usgs.gov, as of 11/10/2015) in 232 vertical plane. The main shock is the red dot and the red line is the fault plane in our inversion whose dip angle is 233 18.3 °. Blue dash line is the receiver plane which is best-fit from the location of aftershocks. The dip angle of the 234 receiver plane is about 31 °. (C) Cross section with the main fault lines (red line) and CFS calculated by the coseismic 235 mainshock slip model, where red denotes a stress built up, and blue a stress shadow. The areas beneath the fault 236 plane receive large CFS built up.

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238 5. Discussion

239 This paper presents a study of 2015 Chile Mw8.3 earthquake based on Sentinel-1A InSAR data of ascending 240 and descending tracks. The purpose is to investigate the coseismic deformation and invert the slip distribution on its 241 fault plane and rupture depth. The results show that the overall slip area is located in the shallow portion of the 242 subduction interface between the source and the trench, with a NS symmetric pattern. The moment magnitude (8.25) 243 and seismic moment (2.917×10²¹Nm) are between the results of GCMT (Mw=8.2, M_0 =2.455×10²¹) and USGS $(Mw=\!8.3,\ M_0\!=\!3.467\times\!10^{21})\ \text{, consistent with focal mechanism solutions from seismic waves. It indicates that the additional set of the set of t$ 244 245 inversion results of this work are reliable, including the dip angle 18.3 °which is consistent with result from USGS 246 (dip=19°) and GCMT (dip=22°). Fault slip is likely related with the ground broader deformation field in EW 247 direction from our work. To assess the resolution capabilities and stability of the fault model, we conducted fault 248 resolution tests of slip identification and find sub-fault grid 10km×10km is best.

249 The coseismic deformation fields of the Chile event derived from Sentinel-1A descending and ascending data 250 are roughly consistent in the shape. The positive and negative with similar magnitude of LOS deformations from ascending and descending data suggest that the crustal deformation caused by this earthquake is dominated by 251 252 horizontal motion. The fault-slip distributions of the Chile event from inversions constrained by different data sets 253 (Sentinel-1A descending, Sentinel-1A ascending, and jointly) have both similarities and disparities. The common 254 points include that the mean rake angles (102 °106 °), indicating a thrust fault with slight right lateral slip, and the 255 outlines of slip regions are about in the same area from the three inversions. There are differences between the 256 estimated slip (~3m) from inversion using Sentinel-1A ascending data alone and slip (~8m) from inversion using 257 Sentinel-1A descending data alone or inversion jointly. An alternative explaination is that the ascending displacement 258 field is smaller than the actual one because two-frame images cannot cover the whole coseismic deformation field.





With reference to all the results, we suggest that the slip-distribution from the inversion using Sentinel-1A descendingand ascending data jointly seems to be more convincing.

261 Here we also compare the surface deformation fields and slip distributions on the fault planes of the 2015 262 Mw8.3 and 2010 Mw8.8 Chile events. Although the South American subduction zone hosts a significant number of 263 large earthquakes, only these two events have InSAR data available for such a comparison. InSAR data, owing to 264 the advantages of dense sampling, can provide the best constraint on the slip location, distribution and depth on the 265 rupture plane by quantitative measuring the static displacement on the ground surface caused by an earthquake. We 266 find that the two events are different in coseismic deformation. For the 2010 event, the deformation spreads along 267 the coast with at least two centers (Tong et al., 2010; Bertrand et al, 2010). The slip distribution from inversion is 268 also of a narrow long strip, rupturing over 600km. The slip is concentrated on the north and south of the source, 269 mostly at depths of 15km-25km, and no large slip at the trench. In contrast, the deformation field of the 2015 event 270 is a complete half circle shape. The inverted slip concentration area is nearly NS symmetric, close to the shallow 271 trench. The 2015 event is located over 400km north of the 2010 shock, both on the subduction slab of the Nazca 272 plate beneath the South American plate. Both events are interplate thrusts with similar tectonic and dynamic settings. 273 But as mentioned above their rupture features are different. The analysis suggests that the 2015 event has a shallow 274 source (25km) and a connective rupture in up-dip direction above the source reaching the trench. Meanwhile its main 275 shock occurred on a big barrier. While the 2010 event is relatively deeper (33km), and at least ruptured two big 276 barriers. It may induce to speculate that the subduction zone has many barriers of varied sizes on different segments. 277 And the coupling or locking degrees are variable at different sections of the subduction zone.

However, the maximum rupture depth (50km) of the 2015 Mw8.3 event from the model of this work is roughly
consistent with the rupture depth of the 2010 Mw8.8 shock derived from inversion of previous studies, which are
based on InSAR plus GPS or InSAR, GPS, and seismic wave data (Tong et al., 2010; Bertrand et al, 2010). It is also
in accordance with the depths of the subduction zone in northern Chile (Tichelaar et al., 1993; Delouis et al. 1997)
and sourthern Chile (Delouis et al. 2009) and the locking depth of this zone from GPS data (Ruergg et al., 2009).
Previous studies suggest that this depth is the transition between the seismic and aseismic layer in the subduction
zone beneath the South American plate. This work further confirms this conclusion.

286 6 Conclusions

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287 In this work, we obtained the coseismic deformation field of the 2015 Chile Mw8.3 earthquake using Sentinel-288 1A descending and ascending data. The positive and negative with similar magnitude of LOS deformation from 289 ascending and descending data suggest that the crustal deformation is dominated by horizontal motion. The inversion 290 constrained by Sentinel-1A ascending and descending data jointly can display comprehensive fault slip. We find the 291 strike angle N4.6 E, the fault dimension 535km (along-strike) \times 200km (down-dip), and the dip angle 18.3 can fit 292 our model better. Mean rake angle from inversion is 103.24 °, which indicates a thrust fault with slight right-lateral 293 slip. A maximum slip of 8.16m on the fault plane appears near the trench, the length of rupture reaches about 340km 294 along strike but mainly extending to north side of the epicenter, and the overall slip pattern is moderately symmetrical, 295 with the down-dip end of the rupture at about 50km which is roughly consistent with the rupture depth of the 2010 296 Mw8.8 shock. The seismic moment magnitude is Mw8.25, the scalar moment from jointly inversion is 297 $(2.917 \times 10^{21} \text{N m})$, and the fitting degree of the whole field is 99.97%. Coseismic Coulomb stress change reflected 298 most areas with increased Coulomb stress appeared beneath the main shock fault plane, which is consistent with the 299 location where aftershocks took place. At the same time, we can see static Coulomb stress above the main shock 300 fault plane is released.

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