



1 **A modified tank model including snowmelt and infiltration time lags for**
2 **deep-seated landslides in Alpine Environments (Aggenalm, Germany)**

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11

12 **Abstract**

13 Deep-seated landslides are an important and widespread natural hazard within alpine regions,
14 and can have a massive impact on infrastructure. Pore water pressure plays an important role
15 in determining the stability of hydro-triggered deep-seated landslides. We improve current
16 methods of groundwater level prediction by introducing a means to account for time lags
17 associated with groundwater supply caused by snow accumulation, snowmelt, and infiltration
18 in deep-seated landslides. In this study, we demonstrate a simple method to improve the
19 estimation of these time lags using a modified tank model to calculate groundwater levels. In
20 a deep-seated landslide in Bavaria, Germany, our results predict daily changes in pore water
21 pressure ranging from -1 to 1.6 kPa depending on daily rainfall and snowmelt. The inclusion
22 of time lags improves the results of standard tank models by ~36% (linear correlation with
23 measurement) after heavy rainfall and, respectively, by ~82% following snowmelt in a 1-2
24 day period. For the modified tank model, we introduced a representation of snow
25 accumulation and snowmelt, based on a temperature index and an equivalent infiltration
26 method, i.e. the melted snow water equivalent. This compares well to the in situ measurement
27 for the same time interval which reflect changes of pore water pressure with 0-8% relative
28 error in rainfall season (standard tank model: 2-16% relative error) and with 0-7% relative
29 error in snowmelt season (standard tank model: 2-45% relative error). Here we demonstrate a
30 modified tank model for deep-seated landslides that includes snow and infiltration effects and
31 can effectively predict changes in pore water pressure in alpine environments.



1

Nomenclature			
a	related coefficient between equivalent infiltration and increased ground water table, 1	q_i	drainage of i^{th} day, mm
a'	related coefficient between equivalent infiltration and increased pore water pressure, kPa/mm	PWP_i	pore water pressure of i^{th} day, kPa
b	average value of pore water pressure changed by drainage and ground water supply, kPa.	$\Delta PWP_{(g+q)i}$	PWP changed by drainage combined groundwater supply, kPa
a	related coefficient between pore water pressure of i^{th} day and $i+1^{th}$ day without infiltration, kPa.	ΔPWP_i	change of pore water pressure of i^{th} day, kPa
b	related coefficient between pore water pressure of i^{th} day and $i+1^{th}$ day without infiltration, 1	$R_i^{(n)}$	part of rainfall of i^{th} day to changed pore water pressure of i^{th} day, mm
ER_i	equivalent rainfall of i^{th} day, mm	RH	relative humidity, 1
ES_i	equivalent snowmelt of i^{th} day, mm	RH_i	threshold of relative humidity, 1
f_m	degree-day factor for snowmelt rate, mm/°C	M	time about effect of infiltration reducing to 50%, 1
F	canopy covers percent, 1	R_i	rainfall of i^{th} day, mm
g_i	ground water supply of i^{th} day, mm	$S_i^{(n)}$	part of snowmelt of i^{th} day to changed pore water pressure of i^{th} day, mm
h_i	ground water table height the i^{th} day, mm	S_i	rainfall of i^{th} day, mm
H	base water table, mm	T_d	daily average temperature, °C
M'	daily snowmelt, mm		

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1 **1 Introduction**

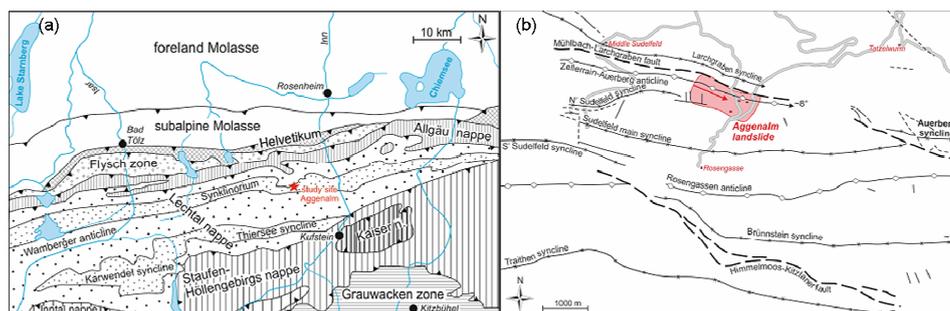
2 Deep-seated landslides in the eastern European Alps pose a certain hazard to people and
3 infrastructure (Mayer et al., 2002; Madritsch and Millen, 2007; Agliardi et al., 2009). It has
4 long been recognized that pore water pressure (PWP) changes by precipitation play a critical
5 role in hydrologically triggered deep-seated landslide activation. The rise in PWP causes a
6 drop of effective normal stress on potential sliding surfaces (Bromhead, 1978; Iverson, 2000;
7 Wang and Sassa, 2003; Rahardjo et al., 2010). The estimation of pore water pressure is of
8 great significance for anticipating deep-seated landslide stability. In past years, geotechnical
9 monitoring systems have revealed PWP change related to rainfall and snowmelt events
10 (Angeli et al., 1988; Simoni et al., 2004; Hong et al., 2005; Rahardjo et al., 2008; Huang et al.,
11 2010). The Green and Ampt Model and the Richards Equation are generally used to describe
12 groundwater infiltration and water table changes (producing PWP) in saturated homogeneous
13 material (Chen and Young, 2006; Weill et al., 2009). The Van Genuchten Equation (Schaap
14 and Van Genuchten, 2006) and the Fredlund and Xing (1994) method show better
15 performance in the evaluation of infiltration and groundwater table but require many
16 parameters which cannot be measured easily. Tank models typically describe infiltration and
17 evaporation in shallow soil materials (Ishihara and Kobatake, 1979). They are based on the
18 water balance theory, which means they account for flows into and out of a particular
19 drainage area. Multi-tank models involving two or three tank elements have been developed
20 to better estimate groundwater fluctuations within shallow landslides induced by heavy
21 rainfall (Michiue, 1985; Ohtsu et al., 2003; Takahashi, 2004; Takahashi et al., 2008; Xiong et
22 al., 2009). However, multi-tank models do often not predict groundwater changes well in
23 deep-seated landslides as they (i) require too many parameters to track groundwater flow
24 supplies in complicated geological structures and (ii) are presently not developed to replicate
25 time lags of increased infiltration, e.g., following snowmelt (Iverson, 2000; Sidle, 2006;
26 Nishii and Matsuoka, 2010)

27 In this study, we introduce a simple method to estimate time lags by a modified standard tank
28 model which predicts changes in pore water pressure. We apply our mode to a case study on
29 the Aggenalm landslide, Bavaria, Germany, where predicted PWP changes can be verified
30 against monitoring data. The monitoring network design and installation, as well as detailed
31 monitoring data, and the introduction of monitoring devices have been described perviously



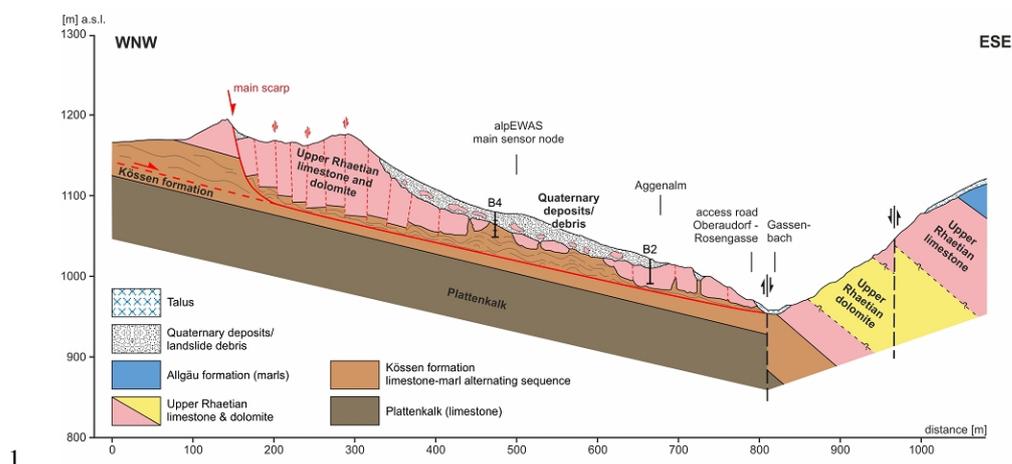
1 in detail (THURO et al., 2009; Thuro et al., 2011a; Thuro et al., 2011b; Festl et al., 2012; Thuro
2 et al., 2013).

3 2 Site descriptions



4
5 Figure 1 (a) Tectonic map of the Northern Calcareous Alps between Lake Starnberg and
6 Chiemsee. The Aggenalm Landslide is situated in the Lechtal Nappe within the Synklinorium,
7 a major syncline–anticline–syncline fold belt, which can be traced through the whole region.
8 (b) Detailed tectonic map showing the main tectonic features in the Aggenalm landslide area.
9 Here the Synklinorium has a complex structure with several additional minor syn- and
10 anticlines, of which the eastward dipping of the Zellerrain-Auerberg Anticline is responsible
11 for the nearly slope parallel orientation of the rock mass within the Sudelfeld landslide
12 (modified from Festl 2014).

13 The Aggenalm Landslide is situated in the Bavarian Alps in the Sudelfeld region near
14 Bayrischzell (Fig. 1). During the Alpine orogeny, the rock mass was faulted and folded into
15 several large east-west oriented synclines, of which the Audorfer Syclinorium is responsible
16 for the nearly slope-parallel bedding orientation of the rock mass in the area of the Aggenalm
17 Landslide (Fig. 2). The Aggenalm Landslide is underlain by Late Triassic well-bedded
18 limestones (Plattenkalk, predominantly Nor), overlain by Kössen Layers (Rhät,
19 predominantly marly basin facies) and the often more massive Oberrhät Limestones and
20 Dolomites (Rhät) (Fig. 2). The marls of the Kössen Layers are assumed to provide primary
21 sliding surfaces and are very sensitive to weathering as they decompose over time to a clay-
22 rich residual mass (Nickmann et al., 2006). The landslide mechanism can be classified as a
23 complex landslide dominated by deep-seated sliding with earth flow and lateral rock
24 spreading components (Singer et al., 2009). A major activation of the landslide occurred in
25 1935, destroying three bridges and a local road. Slow slope deformation and secondary debris
26 flow activity has been ongoing since this time.



1

2 Figure 2 Geological profile of the Aggenalm Landslide (modified from Festl, 2014)

3 3 Data and Methods

4 3.1 Monitoring data

5 Monitoring data for this study is derived from a rain gauge and humidity sensor (alpEWAS
6 central station), and a pore water pressure sensor (PWP) installed in boreholes close to the
7 assumed shear zone (B4, 29.4 meter deep) (Fig. 2) (Singer et al., 2009; Festl, 2014). A heated
8 precipitation gauge provides data on the snow-water equivalent of snowfall. Short term noise
9 in raw data was filtered. PWP, temperature, and humidity are averaged over a 24-hour period
10 (Festl, 2014). The monitoring period lasts almost from February 2009 to December 2011.
11 Considering data loss in some months, we have approximately 24 months of valid data. We
12 use data from the 13 months (May 2009 to June 2009; September 2009 to December 2009;
13 February 2010 to August 2010) to parametrize the modified tank model. The 55 days of
14 rainfall (July 2009 to August 2009) and 44 days of snowmelt (March 2009 to April 2009) are
15 used to validate the modified tank model. In addition, simulation of two years PWP levels are
16 compared to the whole two years of monitoring data of PWP levels bridging the data gaps.



1 3.2 The modified tank model including snowmelt and infiltration

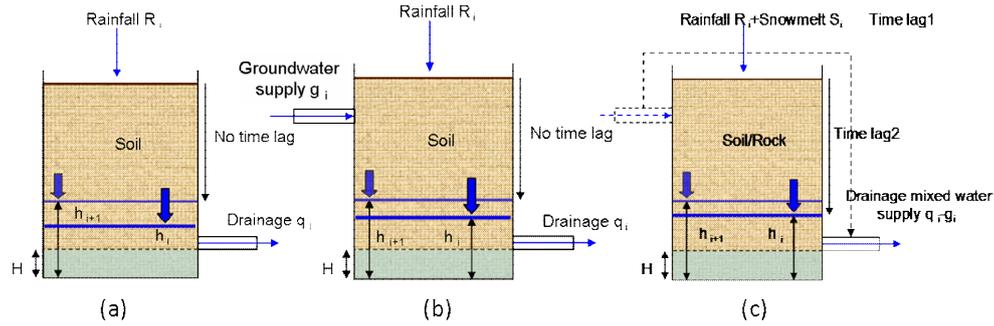


Figure 3 Generation of the modified tank model. (a) Original tank model considering the vertical infiltration and drain affecting water table. (b) Considering both vertical infiltration and horizontal water flow. (c) Modified tank model including water supply and two time lags (snowmelt and infiltration).

2 Figure 3 demonstrates the changes from the original tank model (Ishihara and Kobatake, 1979;
 3 Michiue, 1985; Ohtsu et al., 2003; Uchimura et al., 2010) to our modified model. Fig. 3a
 4 shows the basic concept of the original tank model, the daily change in the groundwater table
 5 height $h_{i+1} - h_i$ is

$$6 \quad h_{i+1} - h_i = R_i - q_i \quad (1)$$

7 where R_i is the rainfall and q_i is the drainage of the i^{th} day. h_i is groundwater table height the
 8 i^{th} day.

9 Concepts illustrated in Fig. 3b are now incorporated in the water flow supply tank model
 10 including groundwater supply. The daily change in groundwater table height $h_{i+1} - h_i$ is

$$11 \quad h_{i+1} - h_i = R_i - (q_i - g_i), \quad (2)$$

12 where g_i is groundwater supply of the i^{th} day from the upper slope.

13 Another aspect, snowmelt also plays an important role in producing groundwater supply in
 14 Fig. 3c. Thus, the equation (3) should be written as

$$15 \quad h_{i+1} - h_i = R_i + S_i - (q_i - g_i), \quad (3)$$

16 where, S_i is the snowmelt of the i^{th} day.



1 More importantly, snow accumulation and snowmelt produces our first time lag (*time lag 1*)
 2 as a result of the effects of ambient temperature on snowmelt. Both the groundwater response
 3 snowmelt and rainfall are compounded by long infiltration paths as, for example, water
 4 infiltration often takes one or more days to reach the water table in deep-seated landslide
 5 masses (*time lag 2*) (Fig. 3c). This can be described: the infiltration in i^{th} day does not only
 6 affect the groundwater table in i^{th} day but also the groundwater table over the following n
 7 days if the *time lag2* (n days) is considered ($n > 1$). In other words, R_i and S_i are divided into n
 8 parts ($R_i = \sum_{n=1}^N R_i^{(n)}$ and $S_i = \sum_{n=1}^N S_i^{(n)}, i, n \geq 1$). Each component ($R_i^{(n)}$ and $S_i^{(n)}$) contributes to daily
 9 changes in the groundwater table ($h_{i+n} - h_{i+n-1}$). Thus, for example, total daily variations (h_{i+2} -
 10 h_{i+1}) in response to rainfall and snowmelt can be described by $R_{i-1}^{(3)} + S_{i-1}^{(3)}, R_i^{(2)} + S_i^{(2)},$
 11 $R_{i+1}^{(1)} + S_{i+1}^{(1)}$ when time lag is 2 days as shown in Fig. 4. (Considering that the groundwater
 12 table in $i+1^{th}$ day is not only affected by the infiltration today but also the infiltration of
 13 previous two days)

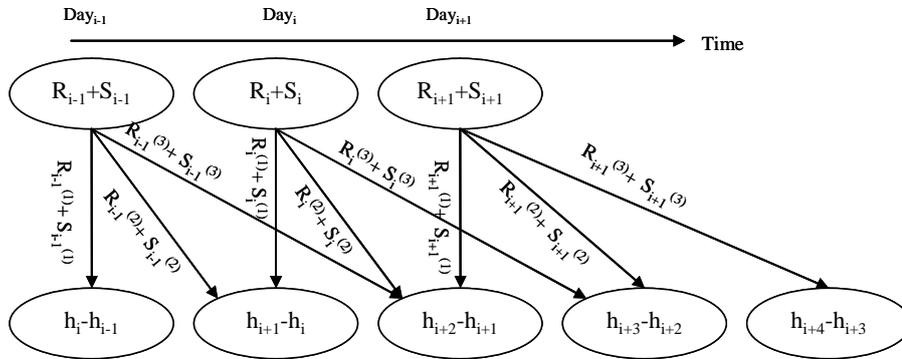


Figure 4 Schematic diagram of water infiltration from the surface to the groundwater table producing *time lag 2* (time lag is 2 days)

Groundwater changes on a given day (Day_{i+1}) result from infiltration over the previous three days (Day_{i-1} , Day_i , and Day_{i+1}).

14 Antecedent Precipitation Index (API) can reduce this *time lag 2* by estimating the current
 15 water content of the ground affected by previous precipitation (Chow, 1964). This is
 16 equivalent to the infiltration calculations of (Suzuki and Kobashi, 1981; Matsuura et al., 2003;
 17 Sumio Matsuura et al., 2008) who define equivalent infiltration as

$$18 \quad ER_i + ES_i = (0.5)^{1/M} R_i + (0.5)^{1/M} ER_{i-1} + (0.5)^{1/M} S_i + (0.5)^{1/M} ES_{i-1}. \quad (4)$$



1 where ER_{i-1} and ES_{i-1} represent the equivalent rainfall and snowmelt of $i-1^{th}$ days, respectively;
2 R_i and S_i mean the rainfall and snowmelt of i^{th} day; $(0.5)^M$ means the effect of infiltration
3 reduces to 50% in M days (where M is determined from field observations). Therefore, the
4 whole modified tank model with an equivalent infiltration method could substitute both, *time*
5 *lag 1* by integrating snow accumulation and snowmelt (section 2.4) and *time lag 2*.

6 The relationship between infiltration and water table is often proportional in slopes
7 (Matsuura et al., 2008; Schulz et al., 2009; Thuro et al., 2010; Yin et al., 2010;). Therefore,
8 the conceptual equation of changed water table should be like:

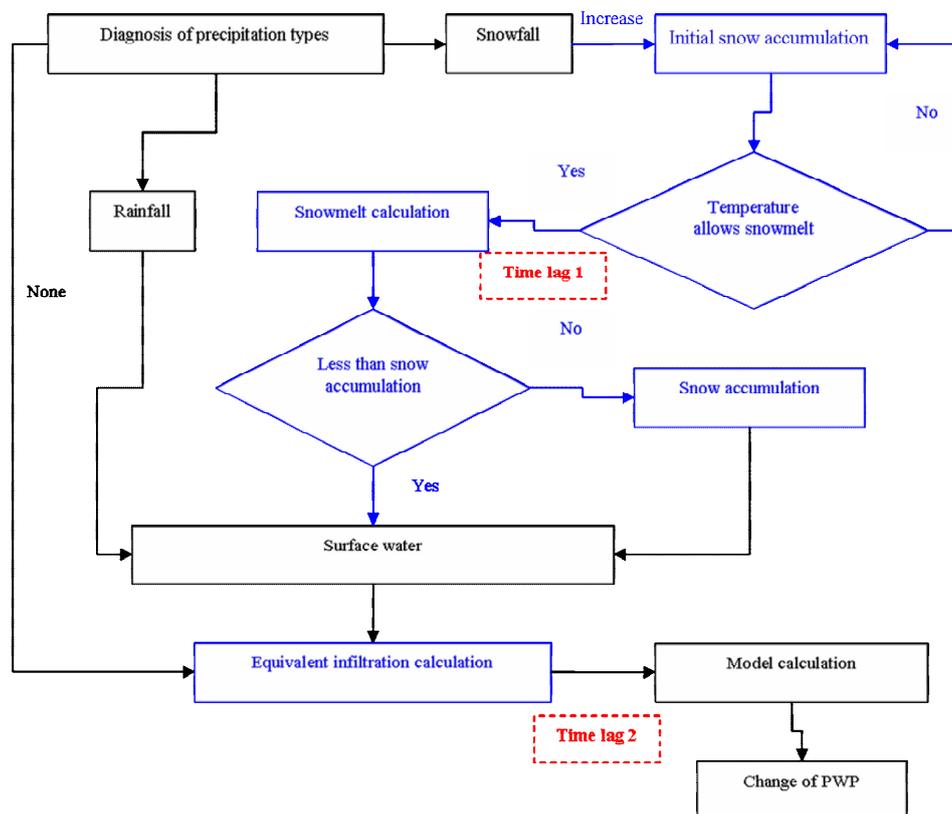
$$9 \quad \Delta h_i = h_{i+1} - h_i = a(ER_i + ES_i) - (q_i - g_i). \quad (5)$$

10 where a is a proportional coefficient (only for ideal tank model, a is one).

11 Assuming seepage forces are negligible, PWP can be linearly correlated to groundwater levels
12 such that:

$$13 \quad \Delta PWP_i = a'(ER_i + ES_i) - \Delta PWP_{(g+q)i}. \quad (6)$$

14 where, $\Delta PWP_{(g+q)i}$ is the PWP changed by subsurface inflows and outflows on the i^{th} day This
15 allows us to evaluate changes in PWP resulting from infiltration, drainage, and groundwater
16 supply. The workflow chart of our modified tank model for change of PWP_i is indicated in
17 Fig. 5.

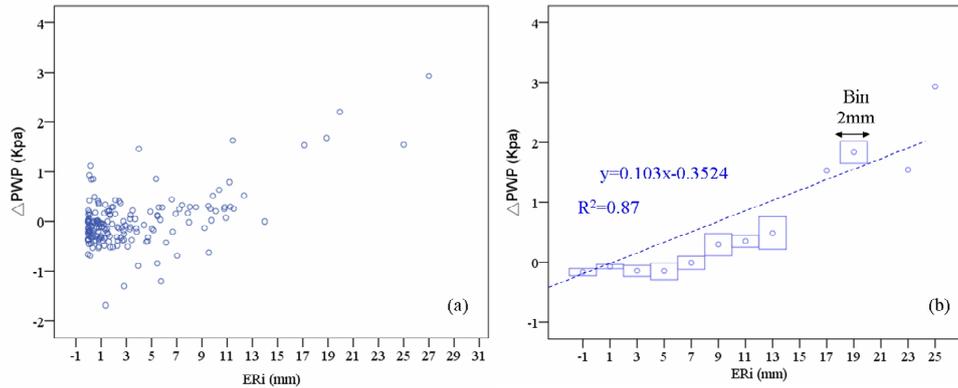


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2 Figure 5 Workflow chart of the modified tank model with respect to the original model are
 3 highlighted in blue including time lags from snow accumulation/snowmelt and infiltration.

4 3.3 Determining the parameter of PWP calculation in the modified tank 5 model

6 In order to determine an appropriate value of a' for the monitoring location on the Aggenalm
 7 Landslide, we use 13 months data as training data to fit the relationship between equivalent
 8 rainfall and ΔPWP (Fig. 6 and Fig. 7).



1

2 Figure 6 (a) Daily equivalent rainfall ER_i versus daily change of pore water pressure ΔPWP_i
 3 in absolute values for 13 months (Sep.2009-Feb.2010 and May.2010-Nov.2010). (b) ΔPWP_i
 4 has been aggregated in bins of mean values for discrete steps of daily equivalent rainfall
 5 (mean+1 sigma error).

6 The linear relationship between daily change of pore water pressure (ΔPWP_i) and daily
 7 equivalent rainfall (ER_i) for absolute data is shown in Fig. 6a. However, this does not
 8 produce a functional link between ΔPWP_i and ER_i . We consider using the mean value of
 9 daily change of pore water pressure given for certain daily equivalent rainfall such as in *Bin*
 10 (Fig. 6b) to replace the data of the same width (Fig. 6a) (Freedman et al., 1998). The result
 11 shows change of PWP_i as

$$12 \quad \Delta PWP_i = a' ER_i - b . \quad (7)$$

13 where, a' [kPa/mm] is 0.103, thus relates rainfall to pore pressure increase and b (-0.3524)
 14 [kPa] is the average decrease of pore water pressure by drainage (Thus at a day without
 15 infiltration by snowmelt and rainfall the pore water pressure drops by 0.35 kPa, i.e. the water
 16 column drops by 35mm). According to the tank model theory, b , as a constant, is quite rough.
 17 The original tank theory demonstrates that the decrease of pore water pressure rate depends
 18 on the current pore water pressure (Michiue 1985; Ohtsu et al. 2003; Takahashi 2004;
 19 Takahashi et al., 2008; Xiong et al., 2009; Uchimura et al., 2010). In reality, the relationship
 20 can only be calculated by monitoring an extended period without infiltration. As shown in Fig.
 21 7a, the observation of PWP is within 48 days without rainfall input which means these
 22 processes only include the information of drainage combined with groundwater supply for



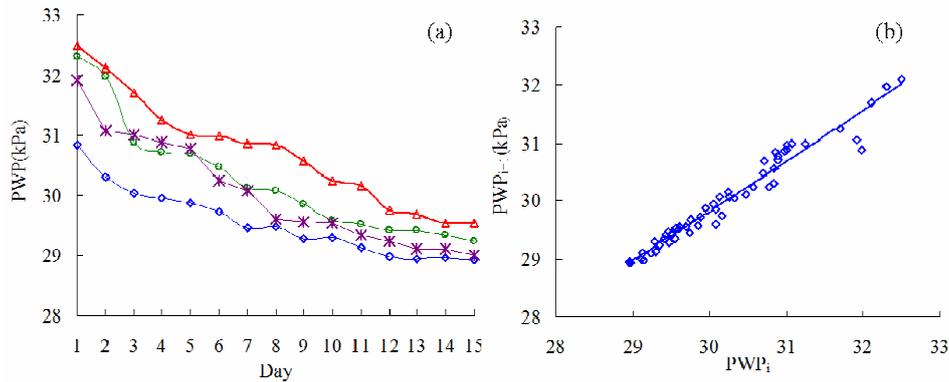
1 this test point. The relation between PWP_{i+1} and PWP_i without rainfall infiltration is shown in
 2 Fig. 7b and equation (8).

$$3 \quad PWP_{i+1} = ae^{bPWP_i}. \quad (8)$$

4 where a (13.4) and b (0.02664) are fitted coefficients.

5 Thus, ΔPWP_i calculation could be rewritten as:

$$6 \quad \Delta PWP_i = a'(ER_i + ES_i) - (PWP_i - ae^{bPWP_i}). \quad (9)$$



7
 8 Figure 7 (a) Observation of PWP vs. time for four fifteen-day-long periods without rainfall or
 9 snowmelt. (Number of samples: $n=48$) (b) PWP_i vs. PWP_{i+1} (i^{th} day of PWP correlates to
 10 $i+1^{th}$ day of PWP for four fifteen-day-long periods without rainfall or snowmelt (Number of
 11 samples: $n=48$).

12 3.4 Snowmelt calculations in modified tank model

13 3.4.1 Diagnosis of precipitation types

14 A threshold temperature under which the precipitation falls as snow solid is a key factor for a
 15 snow accumulation model. However, diagnosis of precipitation is difficult, and there are no
 16 parameters with which the type of precipitation can be determined for certainty (Wagner,
 17 1957; Koolwine, 1975; Bocchieri, 1980; Czys et al., 1996; Ahrens, 2007). Until now, the
 18 most common approach is still to derive statistical relationships between some predictors and
 19 different precipitation types (Bourgouin, 2000). We therefore select a statistical model based
 20 on hundreds of observation samples in Wajima Japan, between 1975 and 1978 to estimate



1 precipitation types (Matsuo and Sasyo, 1981). The threshold of relative humidity calculated
2 by T_d (daily average temperature) is as follows:

$$3 \quad RH_t = 124.9e^{-0.0698T_d} . \quad (10)$$

4 If the real relative humidity RH is smaller than RH_t , the precipitation is usually snowfall
5 (Häggmark and Ivarsson, 1997).

6 **3.4.2 Snowmelt model**

7 One of the most popular methods employed to forecast snowmelt is to correlate air
8 temperature with snowmelt data. Such a relation was first used for an Alpine glacier by
9 Finsterwalder and Schunk (1887) and has since then been extensively applied and further
10 refined (Kustas et al., 1994; Rango and Martinec, 1995; Hock, 1999, 2003). Recently, the
11 most widely accepted temperature-index model is that of Hock (2003). The approach of daily
12 melt assumes the form:

$$13 \quad M' = f_m(T_d - T_0) . \quad (11)$$

14 where T_0 is a threshold temperature beyond which melt is assumed to occur (typically 0°C),
15 and f_m is a degree-day factor. Widely used empirical f_m is suggested here (e.g., Gottlieb,
16 1980; Lang, 1986; Braun et al., 1994; Hock, 2003), which is decided according to canopy
17 cover of one area in percent, beginning time of snowmelt, etc., In this study, the degree-day
18 factor is calculated by

$$19 \quad f_m = 2.92 - 0.0164F . \quad (12)$$

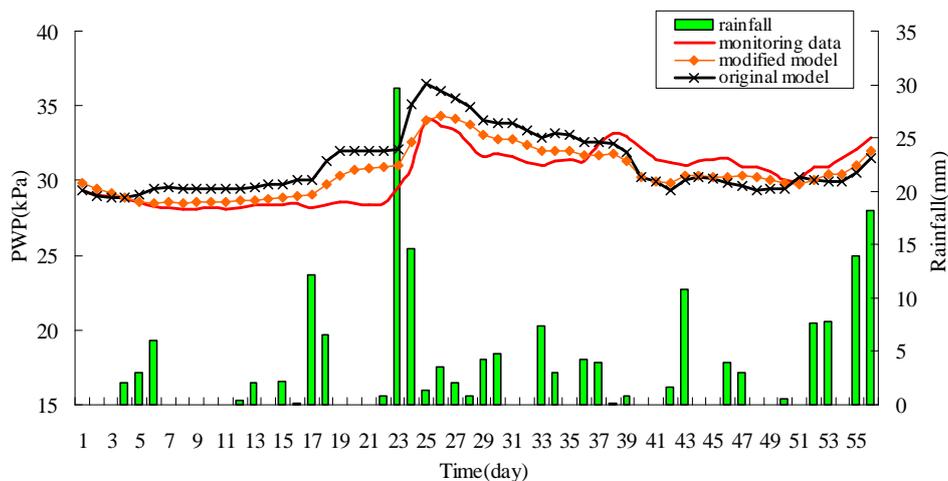
20 where F is canopy covers of Aggenalm Landslide area in percent (Esko, 1980).

21



1 4 Results

2 4.1 Performance of modified tank model in heavy rainfall season



3

4 Figure 8 Estimation of change of *PWP* using our modified tank model (snowmelt + time lag
5 1+2) and the original tank model during summer (snow free) (07.07.2009-31.08.2009).

6 As shown in Fig. 8, our modified tank model and original tank model considering no time lag
7 are used to estimate the change of *PWP* in summer. Both the original and modified tank
8 model do a reasonably good job at estimating changes in *PWP* during summer.. The original
9 model, however, generally overestimates the *PWP* curve. The modified model matches the
10 measurement curve better due to the infiltration *time lag* 2. Error analysis in Fig. 10 quantifies
11 the model's performance.



1 **4.2 Performance of modified tank model in snowmelt season**

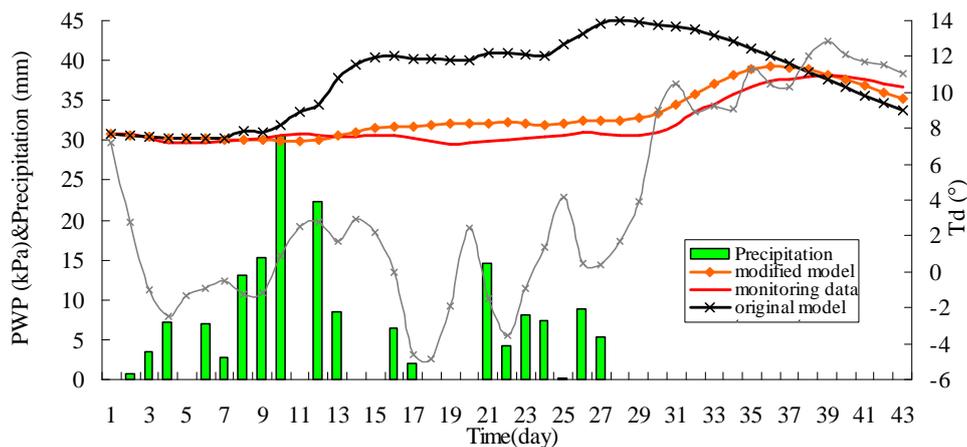
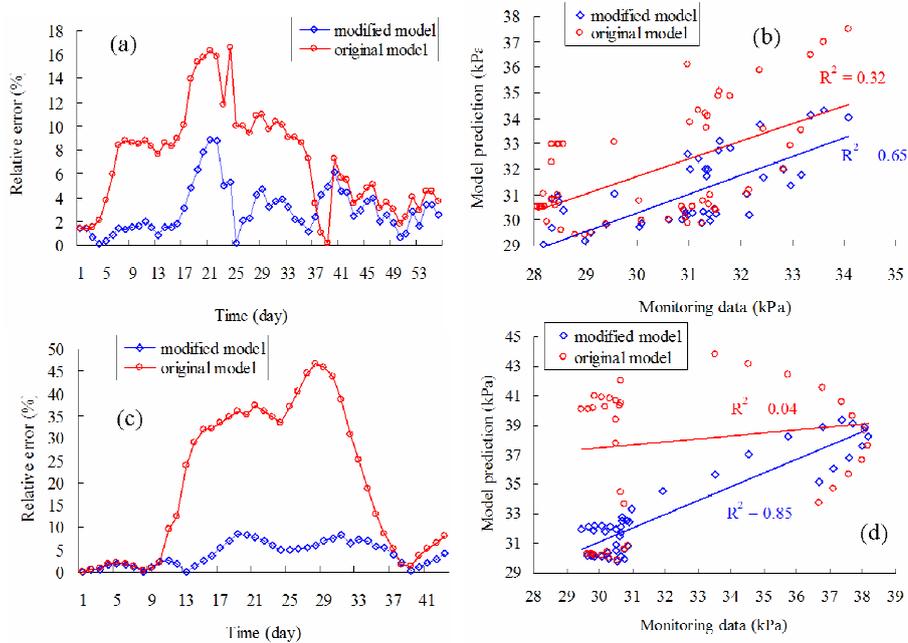


Figure 9 Estimation of change of PWP using our modified tank model (snowmelt + time lag 1+2) and original tank model in snowmelt season (04.03.2009-15.04.2009).

2 The original model without snow accumulation and snowmelt does a poor job at estimating
 3 PWP during spring, as the change of PWP missing the accumulation *time lag 1* caused by the
 4 original model to overestimate PWP from the day 12-33. The modified tank model much
 5 better reflects the peak of snowmelt (33th-37th day) and matches the measurement curve well
 6 in consideration of *time lag 1*. The deviation derives from the naturally limited accuracy of
 7 snow accumulation and snowmelt models. The Fig.10 indicates evaluation index of original
 8 and modified tank model including correlation, root mean square error (RMSE), and relative
 9 error. As shown in Fig. 11, modified tank model simulated the PWP levels in whole
 10 monitoring period.



1
 2 Figure 10 Evaluation of original and modified tank model (a) Correlation between
 3 measurements and original/modified tank model during a 54-day rainfall period (n=54) Root
 4 mean square errors (RMSE) for the original and modified models are 1.9 and 0.97
 5 respectively. (b) Correlation between measurements and original/modified tank model in
 6 snowmelt period (n=47). Root mean square error (RMSE): Original model 5.4/Modified
 7 model 1.3. (c) Relative error of original and modified tank model in summer (n=54). (d)
 8 Relative error of original and modified tank model during spring (n=47).

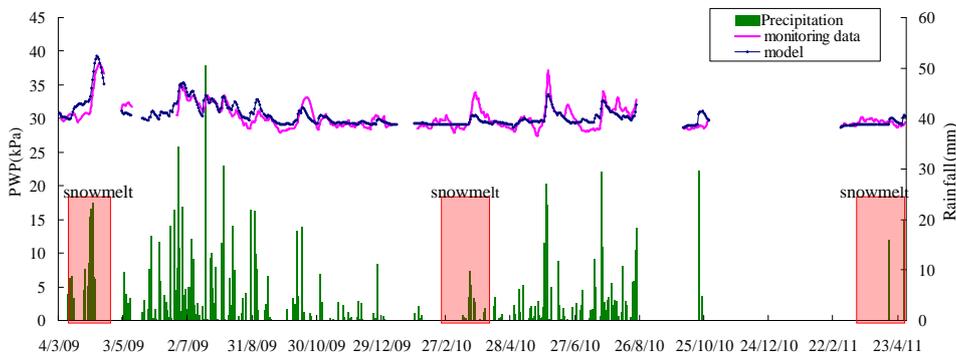


Figure 11 Simulation of *PWP* using the modified tank model throughout the monitoring



period (04.03.2009-23.04.2011).

1 **5 Discussions**

2 In order to evaluate the performance of the modified tank model with respect to heavy rainfall
3 and snowmelt, the two most important forces for accelerating slope movement.

4 **5.1 Performance of modified tank model in heavy rainfall season**

5 The modified tank model describes the fluctuation of *PWP* reasonably well, especially during
6 heavy rainfall days such as 23th to 26th day (43 mm) and 51th to 55th day (45 mm) (Fig. 8). The
7 relative errors in Fig.10a are less than 3% and 4% during these days. Dry periods (such as 2nd
8 to 7th day and 17th to 21st) agree with *PWP* measurement, with a relative error of 2-9% as
9 shown in Fig. 10a. The low water content of the landslide materials during the dry season
10 appears to reduce the infiltration rates (Fredlund and Xing, 1994; Schaap and Van Genuchten,
11 2006). And *PWP* levels increase very slowly or not at all during these periods. As a result, the
12 relative error of our modified model is slightly higher than that during wetter intervals.
13 Compared with the original model, our model better represents *PWP* monitoring data. Fig.10b
14 indicates a higher linear correlation between measurements and modified tank model with
15 0.65 (RMSE -0.97) than the original tank model with 0.29 (RMSE -1.9).

16 **5.2 Performance of modified tank model in snowmelt season**

17 We found a better correlation between measurements and our modified tank model with 0.86
18 (RMSE -0.97) than the original tank model in which all precipitation was assumed to be
19 rainfall and snowmelt was not considered with 0.04 (RMSE -5.4) during snowmelt period. It
20 has to be pointed out that the snowmelt estimation is still not very precise, as the temperature-
21 index model is relatively simple (Garen and Marks, 2005; Herrero et al., 2009; Lakhankar et
22 al., 2013). Also, we do not consider surface runoff due to the high permeability of surface
23 deposits. Our modified tank model, however, provides a useful estimation of increased *PWP*
24 in creeping landslide masses several 10's of meters deep.

25 **5.3 Highlights of our modified model**

26 Compared to the traditional permeability-based on methods (Fredlund and Xing, 1994; Chen
27 and Young, 2006; Schaap and Van Genuchten, 2006; Weill et al., 2009), our modified tank
28 model just needs historical monitoring data and doesn't need to consider uncertainties of



1 material properties. Compared to the recent multi-tank model researches (Ohtsu et al., 2003;
2 Takahashi, 2004; Takahashi et al., 2008; Xiong et al., 2009), our modified tank model does
3 not require complicated algorithms and several observation boreholes to optimize the
4 parameters. It is a straightforward approach. The model integrates the snow accumulation/
5 melt model which is few considered in other tank model researches. We present a flexible
6 approach since the model can simulate groundwater table at least two years continuously
7 without obvious accumulative error unlike permeability-based numerical models or
8 optimization parameter-based models needing refreshment at times (Takahashi et al., 2008;
9 Xiong et al., 2009).

10

11 **6 Conclusions**

12 Pore water pressure is one of the important dynamic factors in deep-seated slope
13 destabilization and our modified tank model could help to anticipate critical states of deep-
14 seated landslide stability a few days in advance by predicting changes in pore water pressure.
15 In this paper, we proposed a modified tank model for estimation of increased pore water
16 pressure induced by rainfall or snowmelt events in a deep-seated landslide. Compared to the
17 original tank model, we simulate the fluctuation of *PWP* more accurately by reducing the time
18 lag effects induced by snowmelt and infiltration into a long path of deep-seated landslide. In
19 this modified model, a statistical method based on temperature and humidity is used for
20 diagnosis of precipitation types and a snowmelt model based on temperature index is
21 integrated into it, also included an equivalent infiltration method which can describe the
22 infiltration relative reliably is in the modified model to reduce their time lag effect.

23

24 **Acknowledgements**

25 The authors thank to the support from the China Scholarship Council, and monitoring data
26 from project “alpEWAS” especially Dr. J. Singer for providing pore pressure data and
27 supervising earlier stages of this project.

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