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Epistemic uncertainties and natural hazard risk assessment – Part 2: Different natural hazard areas

K. J. Beven^{1,2}, S. Almeida³, W. P. Aspinall⁴, P. D. Bates⁵, S. Blazkova⁶,
E. Borgomeo⁷, K. Goda⁴, J. C. Phillips⁴, M. Simpson⁷, P. J. Smith¹,
D. B. Stephenson⁸, T. Wagener^{3,9}, M. Watson⁴, and K. L. Wilkins⁴

¹Lancaster Environment Centre, Lancaster University, Lancaster, UK

²Department of Earth Sciences, Uppsala University, Uppsala, Sweden

³Department of Engineering, Bristol University, Bristol, UK

⁴School of Earth Sciences, Bristol University, Bristol, UK

⁵School of Geographical Sciences, Bristol University, Bristol, UK

⁶T. G. Masaryk Water Resource Institute, Prague, Czech Republic

⁷Environmental Change Institute, Oxford University, UK

⁸Department of Mathematics and Computer Science, Exeter University, Exeter, UK

⁹Cabot Institute, University of Bristol, Bristol, UK

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Correspondence to: K. J. Beven (k.beven@lancaster.ac.uk)

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Abstract

This paper discusses how epistemic uncertainties are considered in a number of different natural hazard areas including floods, landslides and debris flows, dam safety, droughts, earthquakes, tsunamis, volcanic ash clouds and pyroclastic flows, and wind storms. In each case it is common practice to treat most uncertainties in the form of aleatory probability distributions but this may lead to an underestimation of the resulting uncertainties in assessing the hazard, consequences and risk. It is suggested that such analyses might be usefully extended by looking at different scenarios of assumptions about sources of epistemic uncertainty, with a view to reducing the element of surprise in future hazard occurrences. Since every analysis is necessarily conditional on the assumptions made about the nature of sources of epistemic uncertainty it is also important to follow the guidelines for good practice suggested in the companion Part 1 by setting out those assumptions in a condition tree.

1 Introduction

In Part 1 we have discussed the issues and difficulties of trying to account for epistemic uncertainties in natural hazard risk assessment, including: the difficulties of evaluating model structures, the difficulties of estimating effective parameter values for particular assessments, the difficulties of assigning probabilities to epistemic sources of uncertainties and eliciting expert opinions about the potential probabilities; the possibility that some of the information available might not be informative in calibrating or evaluating models; the possibility of models not being fit-for-purpose, and the problem of communicating the meaning of uncertainty assessments to potential users and decision makers. In this paper we review how these issues have been addressed in different natural hazard areas, including floods, droughts, landslides and debris flows, dam failures, seismic hazards, tsunamis, the dispersion of volcanic ash clouds, pyroclastic density currents, and damaging wind storms.

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The different natural hazards areas have dealt with these issues in different ways, although there are some commonalities, for example in the use of expert elicitation of probabilities in cases where information is lacking. In some areas the treatment of different types of uncertainty is contested, for good epistemic reasons of course, between Bayesian statistical probability approaches, formal imprecise methods (including fuzzy possibilistic reasoning, imprecise probabilities, interval methods, belief functions, rough sets and other variants) and informal qualitative approaches. In fact, there can be no right answer since if we had sufficient knowledge about epistemic uncertainties for practical applications they would no longer be epistemic. That does not mean that we should neglect the issues, however, since a proper assessment of uncertainty, including the potential for future surprise, might affect the way in which decisions are made in assessing the risks, particularly where the probability component of the risk = probability \times consequences equation is subject to arbitrary variation (e.g. Rougier and Beven, 2013).

2 Flooding

There are five aspects of flood risk assessment that involve important epistemic uncertainties. The first is the assessment of how much rainfall or snowmelt input occurs (either in past or future events); the second is the frequency with which such events might occur and how that might be changing; the third is how much of that input becomes flood runoff; the fourth is the footprint of the flood inundation; and the fifth is the assessment of either past or potential damages. These all apply in the assessment of expected damages for events of different magnitude for making decisions in managing the flood risk and in the management of flood incidents in real time (e.g. Sayers et al., 2002).

In the context of flood risk management, risk is generally treated as the product of a probability of exceedance and an estimate of consequences (often evaluated as a cost of the impacts of an event). Uncertainties in inputs and runoff generation are

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distribution but multiple distributions and the correlation structure between them (e.g. Keef et al., 2013).

The choice of a particular distribution essentially controls the form of the upper tail of the distribution and consequently the assessment of risk. This is common to the other natural hazards that are considered below. Good practice suggests that the statistical uncertainty associated with the tail of the fitted distribution should be evaluated (although this is rarely reported even where it is provided by the analysis software) but essentially we have additional epistemic uncertainties as to what distribution to choose and whether to treat that distribution as stationary or whether clusters of events might come from some more complex stochastic structure (e.g. Koutsoyiannis, 2003, 2010; Montanari and Koutsoyiannis, 2012). If this is the case, then it might result in a significant increase in the range of uncertainty relative to classical statistical analysis (e.g. Koutsoyiannis and Montanari, 2007) irrespective of other sources of epistemic uncertainty.

These issues have led some people to step back to considering the inputs and runoff generation over a catchment more directly in flood risk estimation. This approach was pioneered by Eagleson (1970) using a simple derived distribution model of runoff generation, but increased computer power has allowed continuous simulation over long periods of time using rainfall–runoff models which has the advantage that the variation in antecedent wetness of a catchment prior to an event is part of the simulation (e.g. Beven, 1987; Cameron et al., 1999; Lamb and Kay, 2004; Blazkova and Beven, 2004, 2009). In some cases it is possible to use long series of observed rainfall data to simulate discharges; but for the very long series that are needed to estimate more extreme events it is necessary to use a stochastic model of the inputs (similar to the weather generators used to produce future sequences in climate change impact assessments). This then only shifts the epistemic uncertainty issue of the choice of appropriate distributions or more complex stochastic structures for the space–time characteristics of rainfall (e.g. Chandler et al., 2014). The extreme events generated from such a weather generator depend on the tails of the assumed distribution(s) and it might not be clear

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what type of distribution to use, even where rainfall series are longer than discharge records. It has also been shown that whether a model matches the historical floods data might depend on the particular stochastic input realization and the historical period considered (Blazkova and Beven, 2009).

A further advantage of the continuous simulation approach is that the weather generator can be modified to represent future climates (e.g. Cameron et al., 2000; Wilby and Dessai, 2010; Prudhomme and Davies, 2009; Prudhomme et al., 2010), and that input data might be more readily available for sites for which there are no discharge records (the prediction of ungauged basins problem, Blöschl et al., 2013; Hrachowitz et al., 2013). This latter case still requires that the parameters of a rainfall–runoff model be specified. This is also an epistemic uncertainty issue, even if extrapolations from gauged sites are often made using statistical regression or pooling group methods (e.g. Lamb and Kay, 2004) a process that will be influenced by model structural uncertainty and other uncertainty sources (e.g. McIntyre et al., 2005; Wagener and Wheater, 2006). Experience in predicting the flood characteristics in this way has been somewhat mixed; successful in some basins, but with significant over or underestimation in others (Lamb and Kay, 2004). Improvements to such methods might still be possible but epistemic uncertainty will remain a constraint on accuracy.

Further uncertainties arise in the estimation of the footprint of the flood event. There may be different areas at risk of inundation according to whether the risk is from pluvial, fluvial, coastal or groundwater flooding. By making assumptions about various sources of uncertainty in the modelling of inundation, a forward uncertainty analysis can be used to predict uncertainties in inundation areas and depths using Monte Carlo simulation methods (e.g. Berry et al., 2008). In some cases, historical flood mapping is available that can be used to condition hydraulic models of inundation and constrain the uncertainty in model predictions (Bates et al., 2014). Both Generalised Likelihood Uncertainty Estimation (GLUE, Aronica et al., 1998; Romanowicz and Beven, 2003; Pappenberger et al., 2007; Beven et al., 2014; Neal et al., 2013; Beven and Lamb, 2016) and more formal Bayesian methods (Romanowicz et al., 1996; Hall et al., 2011)

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have been used in this type of conditioning process (e.g. Fig. 1; see also other examples in Beven et al., 2014) but the results will depend on how the various model runs are evaluated as well as what type of inundation model is being used. Recent improvements in flood inundation modelling, however, have been less a result of reducing uncertainties in inputs and conveyance parameters, but rather due to the much better definition of flood plain topography as LIDAR surveys have become more widely available. Even LIDAR however cannot identify all the barriers to flow on a flood plain (e.g. Sampson et al., 2012), and therefore we should expect some interaction between effective conveyance parameters and other features of model implementation in matching historical flood data. Even then there is some suggestion that the effective conveyance parameters identified for one magnitude of event, might not hold for a larger magnitude event (e.g. Romanowicz and Beven, 2003) so that the simple assumption that conveyance parameters are constant might introduce epistemic uncertainty. It is also common to assume that the effective conveyance parameters are spatially constant which, when interacting with other sources of uncertainty might mean that it is not possible to get good fits to inundation observations everywhere in the modelled domain (e.g. Pappenberger et al., 2007).

In many situations, flooding is constrained by the existence of natural levees or artificial flood defences. Such defences are always associated with a residual risk of being overtopped and/or failing, a risk that will vary with the construction methods, programme of maintenance, unauthorised modifications and other factors (van Gelder and Vrijling, 2014). These are all subject to epistemic uncertainties, but are often dealt with using fragility curves that give a probability of failure as a function of water level. Although expressed in terms of probabilities, such fragility curves are often treated as deterministically known. The difficulties of including epistemic uncertainties are discussed, for example, by Goulding et al. (2010) who used forward uncertainty estimation to cascade uncertainty assumptions through the RASP framework used in the UK National Flood Risk Assessments (NaFRA).

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The other part of the risk equation is the evaluation of the consequences of an event. For past events there is some epistemic uncertainty about the damages associated with the event, but there is often considerable uncertainty about what is actually at risk (e.g. Chatterton et al., 2014). Damages that are covered by insurance are generally well known (but subject to commercial confidentiality restrictions and not readily available), but, not all damages are insured and not all are easily expressed in monetary terms (such as damage to habitats, cultural heritage, and loss of life). Indirect damages to businesses and individuals (e.g. as a result of infrastructure failures, health and psychological impacts) can also be difficult to assess). All potential sources of damage are even more difficult to estimate for future events, as a result of epistemic uncertainties about policy changes in flood risk management, planning decisions for flood plain developments, changes in availability of insurance cover, etc. Different loss models might result in quite different estimates of the consequences of an event (e.g. Jongman et al., 2012; Chandler et al., 2014). In the UK there has been a recent debate about the evaluation of flood damages, and therefore the justification of government expenditure on flood defence and maintenance, instigated by Penning-Rowsell (2015) who led the team that developed the standard methodology for evaluating flood damages (Penning-Rowsell et al., 2013).

In flood incident management, epistemic uncertainties might lead to deterministic predictions being quite wrong, even where models of flood discharges and extent of inundation have been calibrated for past events. This is usually handled in one of two ways. Traditionally it was handled by the experience and expertise of the flood forecasters who would make adjustments to model outputs available to them as an event progressed and more information became available. In doing so they would qualitatively allow for perceived epistemic uncertainties. This approach is still used in many countries. An extension of this approach is to base estimates of the uncertainty in model predictions based on the performance of the model in past events. A method such as quantile regression can be used for this (Weerts et al., 2013). The problem for

both approaches is that past experience may not be a good guide to the peculiarities of a new event.

An alternative approach is to assume that all uncertainties can be treated statistically and use a data assimilation approach to correct for over or under-prediction as the event proceeds. Techniques such as the Kalman filter, or stochastic autoregressive modelling, can be used with the advantage that an estimate of the variance of the forecast can also be updated at the same time (see for example, Sene et al., 2014; Young et al., 2014; Smith et al., 2012, 2013a). No explicit account of potential epistemic uncertainties is made in this approach; the aim is only to improve the forecast and minimize the forecast variance at the required lead time as new data become available for assimilation. The approach will often work well when the required lead time is less than the response time of the upstream catchment so that the data assimilation can rely on measured inputs. It works less well in flash flood situations in small catchments with short response times so that forecasts of the inputs are needed to produce a forecast with reasonable response time (Alfieri et al., 2011; Smith et al., 2013b). Rainfall forecasts from Numerical Weather Prediction (NWP) models are still not sufficiently accurate for this purpose but are now used routinely (such as in the European Flood Awareness System hosted at ECMWF, Bartholmes et al., 2009; De Roo et al., 2011) for providing flood alerts some days ahead.

3 Landslides and debris flows

Landslides can also have large negative societal and economic impacts, such as loss of life and damage to infrastructure. Globally, landslides are directly responsible for several thousand deaths per year (e.g. Petley, 2012). A widely cited example is that of the Welsh village of Aberfan, where a flowslide from a colliery spoil tip killed 144 people, 116 of which were children, at the Pantglas Junior School in October 1966 (Johnes, 2000). More recently, the Gunsu mudslide that occurred after heavy rain in August 2010 in China, killed an estimated 1765 people. However, despite the large risks posed by

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landslides, the ability of research to guide and inform management decisions is limited by high levels of uncertainty in model assessments of slope stability. In landslide risk assessment epistemic uncertainties arise from a range of sources, including errors in measurement data, gaps in the understanding of landslide processes and their representation in models, and from uncertain projections of future socio-economic and biophysical conditions (Lee and Jones, 2004).

Landslide risk can be assessed qualitatively or quantitatively. The choice depends on the scale of work (national, regional, local or site-specific), and also on the quality and quantity of data available. For site-specific slopes, physically-based deterministic models centred on slope stability analysis are commonly used to assess the probability of landslide occurrence. Stability conditions are generally evaluated by means of limit equilibrium methods, where the available soil strength and the destabilising effect of gravity are compared in order to calculate a measure of the relative stability of the slope known as the factor of safety. The limit equilibrium method relies on significant simplifications, such as that failing soil mass is rigid, the failure surface is known and the material's failure criterion is verified for each point along this surface, limiting its accuracy and applicability. Whilst widely applied, epistemic uncertainties related to the limited understanding of system processes and functioning can lead to large errors in model predictions. For example, in 1984 an embankment dam in Carsington, England, slipped, despite the fact that limit equilibrium analysis had indicated that the slope was not expected to be at risk of failure. This discrepancy has been shown to be caused by epistemic errors, as brittle soils may exhibit strain-softening behaviour when loaded, leading to progressive failure, a phenomenon which cannot be reproduced using conventional limit equilibrium stability analyses. For this type of soils, finite element analysis using appropriate numerical algorithms and constitutive models are required to achieve a more accurate prediction of stability (Potts et al., 1990).

Physically-based slope stability models are, however, subject to epistemic uncertainties in both the constitutive relationships chosen and the parameter values required by those relationships. Parameter variability is often assessed by making small scale lab-

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oratory measurements of parameters such as cohesion and coefficient of friction but the resulting values may not be directly applicable at the large scale because of the effects of spatial heterogeneities, and additional factors such as root strength (Christian et al., 1994; Rubio et al., 2004; Hall et al., 2004; Hencher, 2010). Although spatial variability of soil properties has been recognised as an important source of epistemic uncertainty in the literature (e.g. El-Ramly et al., 2002; Griffiths and Fenton, 2004), it has often been ignored in previous analyses using limit equilibrium methods. The use of constant values for soil properties over soil deposits may lead to unreliable estimates of the probability of failure of a slope (El-Ramly et al., 2002; Griffiths and Fenton, 2004; Cho, 2007; Griffiths et al., 2009). To account for this source of uncertainty in slope stability problems, some investigators combine limit equilibrium methods with random field theory (e.g. Cho, 2007). Random field theory allows soil properties to be described by a randomly-generated distribution, instead of a single value across the entire modelled space. Moreover, random field theory also allows spatial correlation to be preserved, ensuring that the values of a given property in adjacent slices do not differ as much as between slices which are further apart.

However, given that limit equilibrium methods are based on a two-dimensional analysis where the critical failure surface is a line of arbitrary shape, the influence of the random field is only considered along that line and therefore, when this method of analysis is used, it can be seen as a one-dimensional approach (Griffiths et al., 2009). To overcome this limitation inherent to limit equilibrium methods, while accounting for spatial variability of soil properties, Griffiths et al. (2009) suggest combining a finite-element model with random field theory. The finite-element method is particularly attractive as, in addition to satisfying equilibrium and compatibility, it allows any constitutive framework to be used for the simulation of the mechanical behaviour of the geomaterial. The decision then is what constitutive framework to employ to allow more accurate predictions to be obtained.

The finite-element method has the added advantage of being capable of simulating water flow and coupled hydro-mechanical behaviour under saturated and unsatu-

environmental conditions (e.g. geological, topographical and land-cover conditions) are used instead (e.g. Guzzetti et al., 1999, 2005, 2006; Ercanoglu and Gokceoglu, 2002). These models have become standard in landslide susceptibility assessment at a regional scale (Corominas et al., 2014). By estimating where the slope is most likely to fail (but not the recurrence of failure, i.e. the temporal frequency, or magnitude of the expected landslide), these models can be of great help in land-use planning, guiding planners in the delimitation of suitable areas for future development.

Guzzetti et al. (2006), for example, established for the Collazzone area, Italy, a landslide susceptibility model, through discriminant analysis by finding a combination of predictor variables that maximises the difference between the populations of stable and unstable slopes with minimal error. The generalisation of a very complex problem into a relatively simple statistical model, necessarily introduces errors in model predictions, arising from errors in the predictors used to establish the model, uncertainty in the classification of the terrain units, etc. To estimate uncertainty, Guzzetti et al. (2006) suggest a bootstrapping re-sampling technique. Several landslide susceptibility models are determined, by varying the selected terrain units considered. These ensembles of models are run for the study area and descriptive statistics for estimated susceptibility, including the mean and the standard deviation, are determined. A model relating the mean value and 2σ (a proxy for the model error) is fitted using least square method. This model is used subsequently to provide estimates of the model error.

Another large source of uncertainty affecting the assessment of landslide susceptibility is often introduced by the imprecision with which experts approach a problem. To account for the uncertain and inexact character of the available information and for the possibility of limited information concerning a real system, fuzzy-based risk assessment models have been suggested in the literature (e.g. Ercanoglu and Gokceoglu, 2002; Lin et al., 2012). For example, Ercanoglu and Gokceoglu (2002) deal with uncertainty in the assessment of landslide susceptibility at the regional scale using fuzzy sets and if-then rules. Based on a landslide inventory database, factor analysis is applied to determine the important weights of the factors conditioning landslides in the

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uncertainty is convolved into a question of what statistical distribution should be used. Probabilistic models such as binomial model, Poisson model (Croveti, 2000) and the power-law distribution (Hung et al., 1999; Dussauge-Peisser et al., 2002) have been suggested in the literature to estimate the frequency (or return period) of landslides of a given size.

Assessment of the probability of land-sliding is only one part of the risk equation. The other part is the evaluation of the consequences of an event to estimate the damages and losses that can be expected. This involves delineating the extent of endangered areas, which requires predicting the runout behaviour of a landslide, namely how far and how fast landslide travels once mobilised. Runout behaviour is most commonly assessed using historical records but where models are used, the runout footprint may be highly dependent on the choice of model parameters (e.g. Hürliemann et al., 2008).

4 The safety of dams

The safety of dams is one example of a hazard that involves both natural forcing and engineering design, but one in which the consequences of failure can be catastrophic. Failures can be due to poor engineering design, poor geological assessments of the location, poor maintenance of the structure, or an extreme flood event or landslide into the reservoir. Lists of dam failures (Vogel, 2001)¹² show that such events are not common, but the International Commission on Large Dams (ICOLD, 1995) has estimated that some 0.5 % of all dams failed in the period 1951–1986 and there have been cases with hundreds or thousands of fatalities downstream. There have, no doubt, been many other cases of near failure. A recent example is in the Sheffield area of England where the Ully dam came close to failure as a result of erosion of the downstream dam face during a period of extreme rainfalls in 2007. In the same area, the failure of the Dale

¹<http://www.damsafety.org/news/?p=412f29c8-3fd8-4529-b5c9-8d47364c1f3e>

²http://en.wikipedia.org/wiki/Dam_failure

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Dike dam in 1864, while being filled for the first time, caused 244 fatalities and destroyed 600 houses (Smith et al., 2014). The most fatalities estimated are for the failure of several dams in Henan Province in China in 1975 which killed an estimated 171 000 people and destroyed the houses of 11 million people, following prolonged heavy rain.

A well-known European example was the failure of the Malpasset arch dam in France in 1959 that caused the deaths of 423 people (Londe, 1987; Duffaut, 2014).

Multiple causes make dam failures difficult to predict, and most countries take a highly precautionary approach to regulating for dam safety. The design of the dam and spillway channels for large dams are commonly designed to cope with the estimate of the flood with an annual exceedance probability of 0.0001. This is a much smaller probability than for designing normal flood defences, because of the potential consequences of a failure. Thus there is an issue of defining of such an extreme event, and also what characteristics of such an event might impose the greatest forcing on the dam. The greatest forcing might not come from the highest flood peak if it is of short duration, but from the inflow volume associated with an event of longer duration but smaller peak.

One way of assessing such effects is to run a stochastic event model (as in the use of continuous simulation for flood frequency estimation described earlier). Since hydrological records are generally short, it will not be sufficient to sample from the historical records of extreme events. Instead, a stochastic model of rainfalls, consistent with the historical rainfall statistics, can be used to drive a continuous rainfall–runoff model calibrated on historical discharge data, to generate very long time series of events (e.g. Blazkova and Beven, 2004, 2009). Figure 2a shows the outputs from such a stochastic simulation for the Skalka dam site in the Czech Republic after conditioning parameters of the inputs and rainfall–runoff model on historical flow, snowpack and rainfall records within the Generalised Likelihood Uncertainty Estimation methodology (see Blazkova and Beven, 2009). The variability arising from different parameter sets is clearly seen. Running one of the parameter sets for 100 000 years of simulation, to get a good estimate of the AEP 0.0001 event magnitude, also generates significant variability when

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broken down to periods of 100 years (Fig. 2b). All of the most extreme events in such a simulation can then be routed through the reservoir (Fig. 2c) to test for failure modes. The continuous simulation approach means that the antecedent conditions prior to any event are handled naturally, but clearly the outputs from such simulations are dependent on the epistemic uncertainties associated with all the model components, including the tail assumptions for the driving distributions, the choice of rainfall–runoff model, and the estimation of model parameters given the historical data. A particular feature of fitting such a stochastic model is that whether a model appears to give a good fit to the observed statistics might depend on the particular realisation of generated inputs (Blazkova and Beven, 2009).

Predicting the downstream footprint of a dam failure and consequent potential damages can also be difficult. There are hydraulic models available designed to cope with the high discharges and sharp wave fronts expected with a dam failure (Cao et al., 2004; Xia et al., 2010), but the application in any real case study will depend on the epistemic uncertainty associated with the characteristics of a breach in the dam acting as an upstream boundary conditions for the hydraulic model and the momentum losses in the downstream area as a highly sediment-laden fluid interacts with the valley bottom infrastructure and vegetation. It is also difficult to verify the outputs of such a model (except for small scale physical experiments in the laboratory, though see Hevouet and Petitjean (1999), Begnudelli and Sanders (2007), and Gallegos et al. (2009); for examples of field scale validation) while many damage assessment schemes are based on predictions of flood depths. In the dam break case, velocities will also be important in the threat to life and damage to buildings.

5 Droughts

Drought is one of the most significant natural hazards, with the potential to cause widespread fatality and economic damage, particularly when a drought event might last for years or even decades. As with floods, droughts may be characterised either

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in terms of their natural severity or their impacts. The definition of drought depends on the type of water deficit being considered (rainfall, stream flow etc.). Drought follows the hydrological cycle, as precipitation deficits (meteorological droughts) lead to low soil moisture levels (agricultural/soil drought) and decreased river flows (hydrological drought) which in turn may lead to lowering of reservoir levels and water shortages (socioeconomic drought). Drought periods associated with high temperatures may also have other impacts such as the large number of excess deaths in Europe in the summer of 2003 (Robine et al., 2003).

Drought hazard is widely assessed using indices, such as the standardized precipitation index (SPI) or Palmer Drought Severity Index (PDSI). The most straightforward of these consider single environmental variables, such as precipitation (SPI) or groundwater level (Standardized Groundwater Index, Bloomfield et al., 2013). In such cases sources of uncertainty are restricted to commensurability of recorded observation, which may arise for instance from missing data, incomplete or short records (Hong et al., 2014; Hu et al., 2014).

However, the information content of such indices can be low as rainfall or groundwater levels are not the sole drivers of drought impacts. By contrast, more complex indices such as PDSI and the Crop Moisture Index provide a more applicable representation of drought, but with more sources of potential uncertainty due to multiple data sources, parameterizations, and model structures imposed by the indices. For instance, the Palmer Drought Severity Index or the Crop Moisture Index assume that land use and soil properties are uniform over large spatial scales; which makes it difficult to accurately identify the spatial extent affected by a drought (Narasimhan and Srinivasan, 2005). Parameter uncertainty in some drought indices is rarely considered when characterizing drought, yet it has been shown to play a significant role in the identification of major drought events and in the derivation of relevant drought statistics (Samaniego et al., 2013).

Under specific local conditions, shortage of rainfall can have an influence on water availability for human use at a regional scale within 4 months (Marsh et al., 2008).

hydrology of extended low flow series is not valid (Prudhomme et al., 2012, 2013). Hydrological models, which are routinely applied to model low flow occurrence and to characterize hydrological drought duration and deficits in response to particular climatological conditions, also introduce epistemic uncertainty in drought risk assessments, and Duan and Mei (2014) have shown that hydrological model structural uncertainty induces large differences in drought simulation.

In flood risk assessment, extreme value theory is applied to identify a representative flood event for a given return period. In drought risk assessment, this approach does not provide a satisfactory representation of drought characteristics, because drought flows are not well represented as extreme values as they are truncated to zero and because drought characteristics are influenced by the temporal dependence properties of climatological and hydrological time series (Pelletier and Turcotte, 1997; Chung et al., 2000). These properties are not well captured by traditional extreme value theory.

Drought risk can be characterized using metrics of drought duration and intensity (the deficit of water during a drought event), or the joint probability of a sequence of reduced flow events either in isolation or in combination with a water supply system model to assess future drought risk. Drought duration is indicative of drought severity rather than directly responsible for consequence in itself, as a long period of low flow is not necessarily worse than a short, sharp drought. Intensity can be considered a more robust metric of shortage as deviation from a threshold state can develop as a consequence of brief periods of extreme shortfall, longer mild shortfall or some combination of the two. Both these methods are sensitive to the identification of a threshold, which can be non-stationary due to environmental factors. Autocorrelation in drought series can be difficult to identify due to the requirement of capturing both the different temporal scales (daily, annual) and the continuous range of low flows, as correlation in Q_{99} events may be independent from correlation in Q_{95} events).

Epistemic uncertainties related to future climate conditions influence drought risk assessment for water resource planning purposes. A number of studies have looked at forward uncertainty analysis of the potential impacts of climate change on droughts

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not clear which climatic variables are best suited to explain water consumption patterns (Kenney et al., 2008). Demand modelling also plays a key-role in long-term drought risk assessments in water resources. Changes in the spatial and temporal scale of water demand are difficult to project and add a level of epistemic uncertainty to any water resources planning decision. Water managers often rely on extrapolation processes (Jorgensen et al., 2009; House-Peters and Chang, 2011), yet this process has not been entirely successful, with the UK's largest reservoir at Kielder built to meet projections which did not foresee the decline in heavy industry in the North of England (Walker, 2012), a clear case of the impact of epistemic uncertainty about future boundary conditions.

Agricultural drought risk assessments are also faced with epistemic uncertainties. The complexity of drought generating processes and the incomplete knowledge of the effects of drought on soil water characteristics and crop growth mean that epistemic uncertainty impacts any agricultural drought analysis. Crop models are often used to predict drought impacts on yield, yet the unknown duration of drought development, and the possibility of rainfall events that might help crop survival while not being hydrologically effective, is a major source of epistemic uncertainty (Yu et al., 2014) in modelling biomass development and yield.

In many climates severe droughts are rare events and, while not as rare as earthquakes or volcanic events, the extent of the observation record is not sufficient to have captured representative samples of the distribution of the natural processes forcing drought events, even if that distribution can be considered as stationary. Because of their long duration, they are also more prone to mitigation or exacerbation by socio-economic drivers than some other natural hazards. Those responding to or managing water resources during drought will make use of nearby water resources or stored water, taking advantage where possible of independence of drought events in space or time. These factors are difficult to predict and thus make droughts subject to a broad range of epistemic uncertainty sources. In addition, the climate characteristics of drought may alter. Where there are projects of greater propensity to drought

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under climate change, making more robust drought planning essential. A risk-based approach allows multiple sources of drought uncertainty to be evaluated simultaneously and to be presented in terms of the probability of failure (Hall et al., 2012). The usefulness of this approach is determined by the extent to which uncertainties can be identified and quantified as probabilities, individually and in terms of their joint probabilities and effects.

6 Seismic hazards

Probabilistic seismic hazard analysis (PSHA) is a standard approach for characterising potential impacts of future earthquakes (Cornell, 1968; McGuire, 2004). It takes into account numerous earthquake sources and scenarios and integrates their contributions probabilistically as if all the variables considered are aleatory in nature. The primary objective of PSHA is to develop a set of seismic hazard estimates for aiding the revision and implementation of seismic design, for example for provisions in national building codes.

Outputs from PSHA are provided in various forms, such as site-specific hazard curve for safety-critical facilities and regional hazard contour map. The contour map shows expected ground motions (e.g. peak ground acceleration and spectral accelerations) at a selected annual exceedance probability level (typically 1/500 to 1/10000). PSHA involves various types and sources of uncertainties, and thus it is crucial to adopt an adequate mathematical framework to handle uncertainties as probabilities for individual model components and their dependency (Woo, 2011). Physically, these uncertainties can be associated with earthquake source processes in time and space, seismic wave propagation, and seismic effects on structures and socioeconomic systems. PSHA also allows the identification of critical hazard scenarios at different probability levels through seismic disaggregation (McGuire, 2004). This essentially closes the loop between probabilistic and deterministic seismic hazard approaches, which are complementary in nature (McGuire, 2001). The deterministic scenario approaches

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(e.g. Zuccolo et al., 2011) allow the use of more sophisticated models and data, but without attempting to associate a probability with a given scenario. For evaluating seismic risk impact to safety-critical facilities and infrastructure, both approaches should be implemented and should also be accompanied by rigorous sensitivity analysis.

Epistemic uncertainties arise both in the choice of structure for the component models and in the effective values of the parameters necessary. As with the other natural hazards, this means that when model predictions are compared to observational data the prediction errors can have a complex structure that may not be simply aleatory, even if it is common practice to treat them as if they can be described by probability distributions. Representations of alternative hypotheses and assumptions for individual model components are often framed with a logic tree approach (Kulkarni et al., 1984), and the final estimates of seismic hazard parameters are obtained by integrating relevant uncertain model components and by probability weighting of alternative assumptions. Nevertheless, difficulties arise, because not all models, which analysts wish to apply, are based on consistent data/assumptions, and the probabilities of alternatives in the logic tree are often poorly known, unknown, or unknowable (Bommer, 2012; Stein and Stein, 2013). Thus evaluating a full range of alternatives and their associated uncertainties will generally not be feasible.

In practice, given these epistemic sources of uncertainty, it is not a trivial task to assign weights to individual branches of the constructed logic tree and resort is often made to expert elicitation. For major industrial facilities (e.g. dams and nuclear power plants), the development of the logic tree is often carried out according to the Senior Seismic Hazard Analysis Committee (SSHAC) guidelines for expert elicitation (Budnitz et al., 1997). In the face of deep epistemic uncertainties and wide spreads in experts' opinions, special care is essential to avoid the inflation of elicited uncertainties and parameter distributions (Aspinall and Cooke, 2013). Notably, the ways a PSHA is conducted analytically and uncertainties are classified have led to different representations of seismic hazard results with respect to epistemic uncertainties: unconditional fractile (i.e. mean) vs. conditional fractiles (e.g. median or 84th percentile) (Abrahamson and

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Bommer, 2005; McGuire et al., 2005). Typically, because of long-tailed uncertainty distributions, mean hazard estimates are greater than median, and differences between mean and median estimates tend to increase with longer return period or smaller probability of exceedance. The motivation of different approaches is not only rooted in the theoretical aspects but also is related to the practical consequences of the PSHA results, e.g. for safety-critical facilities for which the consideration of very low probability levels is required.

Two of the critical elements in PSHA, which are linked but both subject to considerable epistemic uncertainties, are the estimation of long-term occurrence rates of large extreme or “characteristic” earthquakes (e.g. $M_w = 7.5$ to $M_w = 9$) and the evaluation of the “maximum magnitude” to use in a PSHA, for a given seismotectonic environment. On occasion, the upper bound of the maximum magnitude may not be constrained physically nor statistically (Kagan and Jackson, 2013). The difficulty simply stems from the fact that records of seismicity data are insufficient to derive such long-term occurrence rates reliably, solely from historical catalogues or instrumental databases. The quality, completeness and reliability of an earthquake catalogue evolves over time, affected by the distribution of human settlements and the way in which major events in the historical record have been reported (e.g. newspaper and missionary journals). Since the beginning of the 20th century, seismographic networks have been expanded significantly in terms of instrument numbers and detection sensitivity. But advances in measurement technology and wider geographical coverage of such networks often result in inhomogeneous detection and monitoring capabilities of instrumental catalogues (Tiampo et al., 2007).

Recent PSHA studies for potentially active but less well-instrumented seismically active regions (e.g. the East African Rift) have extended the modelling basis for regional seismicity beyond historical/instrumental earthquake catalogues by using information from mapped geological faults and geodetically-determined rates of strain accumulation (e.g. Hodges et al., 2015). It is noteworthy that such PSHA assessments involve considerable uncertainties but may be better able to capture potential extreme (sur-

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prise) events. Rigorous sensitivity investigations should be accompanied by testing alternative hypotheses and by comparing the impacts of the adopted assumptions on regional seismic hazard assessments. In this regard, a PSHA should be reviewed, from an instrumental perspective, such that a better understanding of seismic hazard assessments and their uncertainties can be achieved (Woo and Aspinall, 2015).

It has become more established in recent years that the recurrence of earthquakes on many mature fault systems and in subduction zones (where multiple plates meet and interact) can be non-Poissonian and quasi-periodic, and thus the hazard and risk potential posed by specific faults or subduction zones may be regarded as time-dependent (Sykes and Menke, 2006). Both physics-driven recurrence models (Shimazaki and Nakata, 1980) and statistics-based renewal models (Cornell and Winterstein, 1988; Matthews et al., 2002) have been adopted in PSHA. A notable example of active seismic regions that are affected by a renewal earthquake process is the Cascadia subduction zone. This involves the geodynamics of the oceanic Juan de Fuca, Gorda, and Explorer plates moving against the continental North American plate. A unique aspect of this subduction zone is that repeated occurrences of M_w 9-class mega-thrust earthquakes – due to subduction plate motions – have been recognised from field evidence only relatively recently and reported in the scientific literature (Satake et al., 2003; Goldfinger et al., 2012). In other words, the recurrence and rupture processes of the Cascadia subduction zone involve major epistemic uncertainties, and yet detailed hazard and risk assessments are necessary from an earthquake disaster preparedness viewpoint. In the last decade, various seismic hazard and risk studies for possible risk mitigation have been carried out by adopting a wide range of time-dependent recurrence models and possible rupture scenarios as a way of trying to account for sources of epistemic uncertainty (Goda and Hong, 2006; AIR Worldwide, 2013). This situation contrasts with the case for the 2011 Tōhoku earthquake, where the consideration of extreme events was not taken up in risk mitigation actions prior to this event, even though there were indications of the impacts of past major tsunami-inducing events in the region. The current knowledge and understanding of

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the Cascadia subduction events are likely to be further updated in the future, and so the scientific assessment framework and tools for quantifying the characteristics and patterns of such earthquakes should also evolve dynamically.

Ground motion models that are used in PSHA constitute another major source of uncertainties. Empirically derived prediction models using observed strong motion records are inherently limited by the availability of strong motion recordings. Even following the dramatic expansions of strong motion networks in active seismic regions (e.g. California, Japan, Taiwan, New Zealand, and Turkey), near-source strong motion data and strong motion data for very large earthquakes (with the notable exception of the 2011 Tōhoku earthquake) are still lacking. This reality forces us to update existing empirical ground motion models from time-to-time by incorporating newly available data or to use computational model simulations of strong motion. Another important issue, related to ground motion modelling using observed ground motion records, is that the majority of the existing ground motion models have been developed based on the ergodic assumption (Anderson and Brune, 1999). The ergodic assumption in the context of ground motion modelling implies that the ground motions required at a specific location can be substituted by recorded ground motions at different locations. There may be limited physical validity for this assumption in reality and, at best, adopting it *faute de mieux* engenders exaggerated epistemic uncertainty in the site-specific case via regression scatter estimates. Practical consequences of adopting this working hypothesis are biased seismic hazard assessments (Atkinson, 2006).

A new generation of ground motion models addresses the problem more rigorously (Stafford, 2014). New strong motion data also offer new insights regarding the earthquake source processes via source inversion (e.g. slip distribution and asperities, i.e. concentrated slip patches; Mai and Beroza, 2002; Lavallee et al., 2006). The improved knowledge of the earthquake source process in turn necessitates updated definitions of the seismological parameters and their use in PSHA. For instance, the asperity-based earthquake source model requires additional parameters to characterise the location and concentration of earthquake slips within a fault plane. Furthermore, measures that

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are used to represent the source-to-site distance (e.g. hypocentral distance and rupture distance) may not be relevant within the extended methodology and may introduce epistemic uncertainties in ground motion predictions for future earthquakes (Goda and Atkinson, 2014). New data and theories facilitate the refinements of existing ground models and PSHA methods in a complex manner that may require the specification of additional uncertain parameters. Further uncertainties may be introduced by the non-linear relationships between ground motion characteristics and structural response and damage in assessing seismic risk.

Improvements in PSHA methods and recent earthquake disasters (e.g. 2004 Sumatra event and 2011 Tōhoku event) have stimulated the development of a new cascading multi-hazard approach for mega-thrust subduction earthquakes. The approach promotes an integrated earthquake impact assessment for a sequence of earthquake-triggered hazards, i.e. mainshock followed by tsunami and multiple aftershocks. The novel multi-hazard methodology takes into account both uncertainty and physical dependency of common earthquake source characteristics for multi-hazard processes (Goda et al., 2015). Coupled simulation of strong motion and tsunami can be performed for the multi-hazard impact assessment.

To account for time-dependent aftershock hazards and risks, occurrence of aftershocks can be simulated by employing the modified Omori's law and then the aftershock hazards can be integrated with the mainshock hazards (e.g. Yeo and Cornell, 2009). Time-dependent aftershock hazards are applicable to both moderate crustal earthquakes and mega-thrust subduction earthquakes. The 2010–2011 Canterbury Plains, New Zealand, sequences (Shcherbakov et al., 2012) highlighted major challenges in seismic risk assessment. This is because the sequences of quakes, which initiated with the 2010 $M_w = 7.1$ Darfield earthquake, migrated towards the east and eventually entailed destructive earthquakes near downtown Christchurch in 2011. Currently, forecasting such evolving spatial aftershock sequences is difficult and including a full accounting for epistemic uncertainties associated with cascading multi-hazards is still at an early stage of development. Nevertheless, it is important, and intellectu-

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ally stimulating, to tackle the challenges of extending current quasi-static, fragmented approaches to dynamic, coherent methods for cascading hazards.

7 Tsunamis

Massive tsunamis triggered by large earthquakes pose major threats to modern society, generating fatalities, disrupting socioeconomic activities, and causing grave economic impact across the world. Forecasting tsunamigenic earthquakes is challenging for the same reasons discussed above for earthquake prediction. Major sources of epistemic uncertainties are related to earthquake rupture processes (e.g. source areas and size, asperity, and kinematic/dynamic rupture process) and inundation/run-up process (e.g. topographical effects, land surface friction, and flow dynamics in urban areas).

Estimating potential earthquake size is one of the most critical factors in predicting the impact of great tsunamis. Inappropriate application of seismological theories could result in gross underestimation of earthquake magnitude of mega-thrust subduction earthquakes (Kagan and Jackson, 2013). Moreover, the earthquake rupture process is complex and highly uncertain, and is governed by pre-rupture stress conditions and frictional properties of the fault that are largely unknown/unobservable and heterogeneous in space. A large earthquake may also trigger a submarine landslide, which acts as secondary sources for tsunami generation (Tappin et al., 2014). To gain further insights into the earthquake rupture process, source inversions can be carried out to characterise the space–time evolution of the rupture by matching key features of simulated data with observations. Although sophisticated mathematical frameworks for source inversion have been developed and implemented, derived earthquake rupture models vary significantly, depending on the methods and data used for inversion (Mai and Beroza, 2002; Lavallee et al., 2006). For instance, location, size, shape, and amplitude of slip asperities differ significantly among inversion models for the 2011 Tohoku earthquake (Goda et al., 2014), reflecting the complexity and uncertainty in imaging the

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rupture process for mega-thrust subduction earthquakes. Additionally, different source modelling approaches, such as surface rupture to ocean bottom, effects of horizontal deformation of steep slopes on vertical deformation, hydrodynamic response of water column, and time-dependent rupture process, slow vs. fast rupture propagation speed, will influence the resulting tsunami waves (Geist, 2002; McCloskey et al., 2008; Løvholt et al., 2012; Satake et al., 2013). All these factors contribute to epistemic uncertainties related to tsunami source modelling.

Topographical features of near- and on-shore areas have major effects on tsunami waves and inundation/run-up. The spatial resolution and accuracy of digital elevation models (DEM) are important for representing local terrain features realistically. Typically, the frictional properties of terrain features are modelled by Manning's roughness coefficients. Different data resolutions will require different effective roughness coefficients, thus affecting tsunami inundation extents. The impacts of uncertainty in the DEM and roughness coefficients will depend on tsunami hazard parameters (Kaiser et al., 2011). For instance, the inundation depths are less sensitive to the data resolutions and characteristics, whereas the flow velocity and momentum, which are also important in evaluating the tsunami-induced forces on buildings (Koshimura et al., 2009), are more sensitive. This issue becomes even more critical when tsunami inundation in dense urban areas is investigated, where buildings are represented as (impermeable) elevation data. The simulated flow velocities in urban streets can be very high.

It is rare that that uncertainties of the DEM data and roughness coefficients are taken into account in conducting tsunami simulations but adopting the same modelling philosophy as probabilistic seismic hazard assessment, probabilistic tsunami hazard analysis (PTHA) has been developed and applied to some major tsunami-prone regions (e.g. Annaka et al., 2007; Thio et al., 2007; Horspool et al., 2014). The main focus and advantage of PTHA are to integrate potential tsunami hazards from various sources (both near-field and far-field) in a probabilistic framework. Epistemic uncertainties are mathematically represented in PTHA through a logic-tree approach by assigning weights to alternatives for different model components. The final output is a tsunami hazard curve

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and probabilistic tsunami inundation maps of inundation depth and other relevant parameters. A major difference between PTHA and PSHA is that differential equations of tsunami wave propagation (typically shallow water equations) in ocean are evaluated directly, whereas in PSHA, seismic wave propagation (as well as earthquake rupture and site response) is approximated using empirical ground motion models. The direct simulation of tsunami waves reduces the uncertainties associated with tsunami hazard assessment, and provides additional information on the tsunami wave time-history and arrival time.

However, PTHA can be computationally demanding. To achieve computational efficiency, PTHA is often formulated based on linear superposition of tsunami waves (i.e. Green's functions) for simplified earthquake sources and is carried out only for near-shore locations (e.g. at 30 m depth). The inundation and run-up processes are often modelled by applying amplification factors (e.g. Løvholt et al., 2014). To improve the tsunami hazard prediction and quantify the effects of epistemic uncertainties, it is desirable to integrate the stochastic source modelling approach (which carries out fully nonlinear inundation simulation of tsunami waves) into the PTHA methodology. Such an extended PTHA could reflect the variability of source characteristics for specific scenarios as well as numerous tsunami sources in developing tsunami hazard curves and maps.

8 Volcanic eruptions and ash clouds

The 2010 eruption of Eyjafjallajökull in Iceland provided a dramatic demonstration of the potential for volcanic ash clouds as a natural hazard. Because of the synoptic weather at the time of the eruption the ash cloud caused enormous disruption to air travel across Europe and the Atlantic with some 10 million air travellers being affected, at a total estimated cost of EUR 1 billion per day (Oxford Economics, 2010). Since then there has been considerable effort expended in the monitoring and prediction of volcanic ash clouds. Ash clouds can also be a problem in many other parts of the world,

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for example as a result of the continuing eruption of Mount Sinabung in Indonesia and the recent 2015 eruption of the Calbuco volcano in Chile. Globally, a network of nine Volcanic Ash Advisory Centres (VAACs) provide a warning service based on monitoring and modelling.

Infrared satellite observations are perhaps the most important tools for monitoring ash but are not without their problems. Ash detection is complicated by a number of factors. The brightness temperature difference (BTD; the difference between brightness temperatures at two infrared channels) used as the basis for infrared ash detection can be affected by false positives and false negatives due to e.g. atmospheric conditions (Simpson et al., 2000; Mackie and Watson, 2015), land surface type and temperature, presence of other aerosols (Prata, 1989; Prata et al., 2001; Pavolonis et al., 2006; Lee et al., 2014) and water/ice (Rose et al., 1995), in addition to particle size (e.g. Millington et al., 2012) and ash cloud opacity (Rose et al., 2001) (see Fig. 3). Sophisticated volcanic ash retrieval schemes such as Francis et al. (2012) and Pavolonis et al. (2013) use a third infrared channel to help with removing these false alarms (Stevenson et al., 2015).

Many assumptions are made about the physical properties of ash in order to make estimates on other physical properties such as ash column loading, ash cloud height and effective radius. For example, in the Met Office 1-D-Variational (1-D-Var) volcanic ash retrieval scheme (Francis et al., 2012) it is assumed that ash particles are spherical to simplify the absorption and scattering calculations, the particle size distribution (PSD) is assumed to be lognormal in shape, and the geometric standard deviation of the distribution is selected from a number of possible values. However, this value can have a significant effect on retrieved ash column loading (e.g. Western et al., 2015). Ash composition, and hence, refractive index data must also be assumed, adding considerable uncertainty (Mackie et al., 2014). There are limited ash refractive index data available, and this choice can also have a significant effect on derived ash properties (e.g. Francis et al., 2012). The PSD geometric standard deviation and refractive index data set are varied within the 1-D-Var algorithm and the solution with the lowest cost is

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generally used; the solution cost of the 1-D-Var scheme can be used as an uncertainty measure, with high costs indicating high uncertainty (Stevenson et al., 2015).

Other sources of uncertainty are introduced in the simulation of satellite imagery using a radiative transfer model, in the meteorological data used within the model, interpolation of that data and so on. Some of these are very generally accounted for the in 1-D-Var algorithm but not all. Other types of observations (e.g. hyperspectral satellite observations, satellite, aircraft or ground-based lidar) are used to add information and/or reduce uncertainty in these types of derived observational data, but are often of much lower temporal or spatial resolution and carry their own assumptions and uncertainties (e.g. Wilkins et al., 2016). Clearly, many of these sources of uncertainty are epistemic in nature and not necessarily aleatory in their characteristics.

Modelling of the hazard is, however, a problem of forecasting. At the UK Met Office the Numerical Atmospheric-dispersion Modelling Environment (NAME) model (Jones et al., 2007) is used in both simulation and forecasting of ash to inform the London VAAC which covers eruptions in Iceland and the impacts on northwest Europe. As with all models, NAME is a simplified representation of the problem, and does not include some of the complex physical processes that control the behaviour of an ash field close to the source of the eruption, notably plume behaviour and particle aggregation. Near-field processes are still the subject of current research (e.g. Taddeucci et al., 2011). Currently, the effects of gravity currents (Bursik et al., 1992a; Sparks, 1986) are also not included in most atmospheric dispersion models. These near-source processes are likely to dominate ash dispersion and transport close to the source, and for large eruptions they could dominate for hundreds of kilometres (Bursik et al., 1992a, b; Sparks et al., 1997), but far from the source are unlikely to affect downwind ash clouds for weak eruptions (Devenish et al., 2012a; Costa et al., 2013).

In NAME an effective source term is used as a boundary condition for the far-field transport and deposition of ash. This includes assumptions about the PSD of the ash. Plume behaviour can vary significantly over time and information derived from deposited ash, often after an event, does not necessarily give a good indication of

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the PSD within the distal ash cloud (Bonadonna and Houghton, 2005). Operationally, a default source term PSD has been used by the London VAAC, based on empirical measurements from Hobbs et al. (1991) which aims to represent the fine ash that survives near-source fall-out (Webster et al., 2012). This component may be of the order of 0.05–10 % of the total erupted mass (Mastin et al., 2009). Mass emission rate (MER) and particle density are also required and are also very difficult to determine experimentally. MER is often represented as a simple empirical power law as a function of plume height with fixed parameters (e.g. Mastin et al., 2009), while in a study of the Eyjafjallajökull eruption, Webster et al. (2012) used a fixed ash density value of 2300 kg m⁻³. It is thought that the empirical function for MER may be biased towards observed data from larger eruptions (Woodhouse et al., 2013). Plume height measurements used to determine MER (e.g. radar) are subject to uncertainties (Arason et al., 2011; Folch et al., 2012), and plumes from weak eruptions such as Eyjafjallajökull can become distorted by local winds, increasing plume height measurement uncertainty and therefore affecting the MER calculation (Webster et al., 2012). All of these factors represent primary epistemic uncertainties in the application of such models. Even a cursory treatment of those uncertainties results in a significant predictive uncertainty (Devenish et al., 2012b).

One way of constraining such uncertainty is to use inversion modelling to learn more about dispersion parameters and model eruption source parameters (ESPs) based on the available observations and prior information (e.g. Stohl et al., 2011; Kristiansen et al., 2012; Moxnes et al., 2014; Pelley et al., 2015). In this way, Kristiansen et al. (2012) estimated optimal volcanic ash source terms for the Eyjafjallajökull eruption using an inversion algorithm with satellite-retrieved ash column loadings, a number of emission scenarios and two atmospheric dispersion models. The inversion-estimated source terms were applied within the models a posteriori to perform long-range forecasts and results were validated using LIDAR and in-situ PSD measurements from research flights. Uncertainties in the a priori emission estimates, model and observations were taken into account within the inversion algorithm, allow-

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ing the result to deviate from the a priori emissions and the observations according to the errors. A genetic algorithm variational method was applied by Schmehl et al. (2011) to elucidate wind direction, wind speed and mass emission rate to be used for forward assimilation in a dispersion model. In this approach a cost function based on the difference between observed and modelled fields was minimised over a series of iterations or until the solution converged. By sampling the source term parameter ranges iteratively, the results could be used to constrain uncertainty in ESPs and/or meteorological fields.

In a different approach to data assimilation, a Bayesian method was adopted by Denlinger et al. (2012) to propagate uncertainty in ESPs within an atmospheric dispersion model and estimate forecast uncertainty. A model was run with ESPs sampled from probability distributions. The model outputs were then assessed by comparison with satellite observations, a likelihood function defined, and a posterior probability distribution determined using Bayes theorem. Wilkins et al. (2014, 2015) used data insertion to initialise NAME using measurement-derived data. Instead of releasing ash with a defined release rate from the volcano vent, it was released several times from “snapshots” of downwind ash clouds defined using retrieved data from infrared satellite imagery, in-situ and other remotely sensed data. While this method does not explicitly deal with uncertainties in the model or observations, it could potentially be used to bypass a lack of knowledge of the ESPs, for instance where the location of the volcano is unknown. The method does, however, require estimations of ash layer thickness, vertical distribution and PSD.

When such models are used for forecasting it is possible to compensate for epistemic uncertainties, at least can be in part, by the assimilation of information about the ash cloud derived from remote sensing and other direct sources such as experimental flights. Data assimilation will then implicitly compensate for some of the epistemic uncertainty associated with the model. However, the propagation of complex epistemic uncertainty in computationally expensive atmospheric-dispersion models is a time con-

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suming and difficult problem to quantify. The characterisation of volcanic ash forecast uncertainties in an operational time scale therefore remains a challenging task.

9 Pyroclastic density currents

Rapidly-moving flows of hot, fragmented gas-rich magmatic products in pyroclastic density currents (PDC; also known as ‘nuées ardentes or pyroclastic flows and surges’) are the biggest killers in explosive volcanic eruptions. However, much is still to be learned about the factors that control their initial formation, their movement across terrain and the ways they injure and kill people, and damage structures. Thus there are multiple sources of epistemic uncertainty about the hazards and risks associated with these dangerous phenomena.

The 79CE eruption of Vesuvius and the remains found at Herculaneum and Pompeii represent a classic historic example of the disastrous impacts of PDCs, and any repeat at this volcano in the future, even on a smaller, less intense scale, could have massive consequences for the heavily-populated surrounding area. Hazard and risk assessments for this situation, undertaken in the last twenty years for the National Emergency Plan (DPC, 1995, 2001), were mostly based on the characterization of a single “Maximum Expected Event” (MEE). Such an event largely corresponds in the expected intensity of effects to the hazardous phenomena that occurred during the last sub-Plinian eruption of Vesuvius, in 1631 CE. However, that definition was not based on a fully quantitative analysis of the whole system and potential ranges of eruptive activity, and no probabilistic estimates were provided of the likelihood of occurrence of the hazard events being considered.

In work for the EXPLORIS project (Neri et al., 2008), probabilistic characterizations of possible future eruptive scenarios at Vesuvius volcano were elaborated and organized within a risk-based framework, and a wide variety of topics relating to this basic problem were pursued: updates of historical data, reinterpretation of previous geological field data and the collection of new fieldwork results, the development of novel

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numerical modelling codes and of risk assessment techniques. To achieve coherence, many diverse strands of evidence had to be unified within a formalised structure, and linked together by expert knowledge. For this purpose, a Vesuvius “Event Tree” (ET) was created to summarise in a numerical-graphical form, at different levels of detail, all the relative likelihoods relating to the genesis and style of eruption, development and nature of volcanic hazards, and the probabilities of occurrence of different volcanic risks in the next eruption crisis. In order to achieve a complete parameterization for this all-inclusive approach, exhaustive hazard and risk models were needed, quantified with comprehensive uncertainty distributions for all factors involved, rather than simple “best-estimate” or nominal values. Thus, a structured expert elicitation procedure was implemented to complement more traditional data analysis and interpretative approaches, and to add a formalized approach to the generic incorporation of epistemic uncertainty in the assessment by way of the Event Tree formulation.

Here, we focus on the issues of epistemic uncertainty in relation to the physical characterization of PDC potential during a Sub-Plinian column collapse eruption, and how the topography of the volcano influences hazard and risk mapping results. Basic effort in this regard, during EXPLORIS, was dedicated to the development and application of a transient 3-D parallel code PDAC, able to simulate the dynamics of the collapse of the volcanic column and the propagation of the associated PDCs (Esposti Ongaro et al., 2007). The model solves the fundamental multiphase flow transport equation of Neri et al. (2003) and provides a means to describe the complexities of the column collapse and the temporal and spatial evolution of flows over the whole 3-D topography of the volcano. However, the full ranges of plausible volcanic and other physical input parameter variations are not amenable to comprehensive exploration in a restricted number of scenario runs, which are limited by computing power and cost. Under these circumstances, the few PDAC runs that were possible were used as indicative references, with expert elicitations used to derive rational, quantitative statements about the most appropriate values to use for variables of interest and, more importantly, to give expression to the scientific uncertainty that attaches to the outcomes of such model runs. For

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instance, distributional expressions for uncertainties on pyroclastic flow run-out distances, peak pressures and temperatures were obtained by elicitation, after detailed consideration of the few simulation model results that were achievable, and of field evidences, old and new.

One significant source of epistemic uncertainty in this context is the role which the actual topography of Somma–Vesuvius will play in the occurrence of a future central eruption from the present Gran Cono of Vesuvius. After analysing several different options, the EXPLORIS group envisaged a subdivision of the Vesuvian Area into two main sectors, Sectors A and B, delimited by the two red lines on Fig. 4a (Sector A includes the area “not protected” by Mt. Somma, and Sector B, the area which is “protected”) representing a first-order source of epistemic uncertainty in respect of the extent to which the presence of the Mt. Somma topography could determine which areas could be invaded by flows, or modify properties of the flows that might affect the two sectors. More detailed analysis of modelled effects within Sector A suggested a sub-division into Sectors A1, A2, A3 and A4, as delineated by the yellow lines on Fig. 4a, with the aim of reducing overall epistemic uncertainty in relation to directional influences on PDC propagation, by allowing more precise analysis of the spatial hazard in the region not protected by Mt. Somma. The bracketed values in each sector show elicited modal probabilities that a PDC will affect that sector, given a Sub-Plinian I scale eruption occurs (probabilities expressed in percentage terms) together with the corresponding credible intervals, in quantile form (5th, 50th, 95th percentiles). From the elicitation outcomes it is evident that the presence of Mt. Somma is expected to reduce, by a factor of about two, the probability of flow invasion into the northern sector. Nevertheless, the associated credible interval results are quite large, reflecting the significant uncertainty associated with judgments about column collapse and PDC phenomena. That said, the elicited probabilities of invasion of the different sub-sectors of Area A are each very similar, and apparently only weakly affected by the preferential propagation directions shown by some of the 3-D simulations (Esposti Ongaro et al., 2008) or by reconstructions of past Sub-Plinian events (Rosi et al., 1993; Cioni et al., 2008).

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Even more critical information, relating to PDC hazards and hence risk mitigation, is represented in the assessed run-outs of PDC, which directly determine the extent of the Emergency Plan Red Zone, i.e. the size of the region that should be evacuated in advance of an eruption, and where about half million people currently live. Figure 4b shows the elicited judgements of maximum run-out distances (in km) for PDCs occurring during a Sub-Plinian I eruption, by sector. Inner arcs (blue) are 95 % confidence levels for a run-out exceeding the distance shown (e.g. 2.5 km for Sector A1), central arcs (green) are the modal (50th percentile) values, and outer arcs (orange) are the run-out distances assessed as having only a 5 % chance of being exceeded (e.g. 13.3 km for A1). A significant difference in anticipated run-outs is again shown for Sectors A and B (a gap of about 2 km between the 50th percentiles), but perhaps the most striking – and important – feature of the results are the large credible intervals associated with these run-out estimates. This outcome was actually expected, given the complexity of the phenomenon being investigated and recognition of the technical limitations of the approaches adopted. In fact, the mechanism and degree of column collapse, i.e. the percentage of mass collapsing back to the ground, can significantly affect the mobility and dispersal of PDCs. On the other hand, reconstructions of the maximum extent of PDCs that occurred during past events are limited by the incomplete preservation of the products, as well as by partial access to the deposits (Cioni et al., 2008). Similarly, the adopted PDAC 3-D code is limited by the vertical resolution of the computational grid, which does not allow accurate modelling of the lower denser portion of the flow (Esposti Ongaro et al., 2007, 2008).

The large epistemic uncertainties regarding the directional controls on PDC probabilities and likely run-outs also influence the expected values of the main physical variables that can be associated with a PDC scenario: e.g. peak dynamic pressure and peak flow temperature. The fact that the EXPLORIS exercise also resulted in large credible intervals associated with these parameter estimates, as well as with the PDC run-outs, clearly reflects expert perceptions of the significant degree to which epistemic uncertainties must affect current attempts to forecast the complex hazard pro-

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cesses being considered. One conclusion is that more field and more numerical work is needed in order to further constrain the areas likely to be affected by future PDCs at Vesuvius.

10 European windstorms

Weather hazards are a major source of societal risk causing death, destruction to infrastructure and disruption to transport and business. Insured losses, currently estimated to cost USD 200 billion annually, are expected to rise dramatically due to climate-change related trends in weather extremes, increasing exposure in developing countries, and increasing world population. Extra-tropical cyclones (also known as windstorms) are major contributors to this impact e.g. insured losses in Europe of USD 9 billion for windstorm Daria (25 January 1990). Furthermore, windstorms often arrive in close succession, which enhances the risk of large aggregate losses e.g. the winter 2013/14 cluster of European windstorms Christian, Xavier, Dirk and Tini caused insured losses of USD 1.38, 0.96, 0.47 and 0.36 billion totalling USD 3.3 billion (source: www.perils.org).

Windstorm loss distributions are inferred from historical weather measurement data (mainly available since 1950) and also increasingly from storm data simulated ab initio from numerical weather and climate prediction models (Schwierz et al., 2010; Pinto et al., 2010; Della-Marta et al., 2010; Renggli et al., 2011; Karremann et al., 2014). The loss distributions are estimated by Monte Carlo simulation using ad hoc combinations of various statistical, dynamical and engineering type models: statistical models for estimating trends and correcting inhomogeneities in the historical data (Barredo, 2010), either low-order parametric stochastic models (the traditional basis of many catastrophe models), or more recently, numerical weather and climate models for simulating large sets of artificial hazard events, statistical models for adjusting biases in numerical model output, and stochastic models for simulating losses from the artificial windstorm events (e.g. compound-Poisson event-loss table models).

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Since many choices are required to develop these models, there are many sources of epistemic uncertainty. To list just a few of the major uncertainties in each type of model:

- Stochastic hazard and loss models often use highly idealised non-physical description of complex storm processes (e.g. polynomial representation of storm tracks). There is the possibility of over-fitting to the data available from relatively short historical periods. There are often overly restrictive assumptions in simulating losses e.g. homogeneity in time, independence of events, independence of frequency and severity.
- Statistical models require distributional assumptions e.g. extreme value models (Brodin and Rootzén 2009; Della-Marta et al., 2009), assumptions about model-dependence of simulated storms (Sansom et al., 2013), and assumptions about dependency in space–time and between events (Bonazzi et al., 2012; Economou et al., 2014).
- Numerical weather and climate models show biases in storm properties that have resisted model improvements over the past 40 years e.g. too zonal storm track over W. Europe (Zappa et al., 2013), poor representation of small horizontal scale processes even at very high resolution e.g. wind gusts (Ólafsson and Ágústsson, 2007), missing processes e.g. sting jets caused by mesoscale features such as stratospheric intrusions (Catto et al., 2010) and non-adiabatic forcing of storms by anomalous oceanic conditions (Ludwig et al., 2014).

Finally, there is also a major overarching source of epistemic uncertainty in how these different model components should be coupled together. At present there is no accepted theory for how one should and should not do this.

Clustering of windstorms provides a good example of an epistemic uncertainty that has recently received much attention and thereby led to model developments. Analysis of historical reanalysis data revealed that windstorm modulation by large-scale climate

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2013). There will remain the possibility, however, that not all possible scenarios are included in such an analysis and there is still the potential for future surprise. This might be mitigated against by carrying out a wider sensitivity analysis (e.g. Pianosi et al., 2014) such as the scenario neutral assessments of the impacts of future change developed by Prudhomme et al. (2009, 2010).

Some differences in practice between different hazard areas are also evident, in part dependent on the availability of data and the potential for doing useful forecasting as well as simulation. It is useful to distinguish three types of uncertainty analysis (e.g. Beven, 2009). The first is a forward analysis where the outputs depend entirely on propagating prior assumptions about the sources of uncertainty, albeit that those prior assumptions might be derived from historical sequences. Risk assessments of droughts, dam safety, landslides, ground motion from earthquakes, and tsunamis tend to be of this type.

The second form of analysis involves conditioning the prior estimates of uncertainty for a simulation model on observational data. Flood inundation maps (using historical flood outlines and discharge estimates), and the inversion methods used for identifying earthquake ruptures, and source terms for ash cloud simulations are of this type. In general such methods will help to constrain model uncertainties, but will dependent on both the range of models considered and the way in which they are evaluated relative to the available observations. A number of conditioning methodologies are available including formal Bayes methods (Bernado and Smith, 2009); Bayes linear methods (Goldstein and Wooff, 2007); Approximate Bayesian Computation (ABC, Vrugt and Sadegh, 2013; Nott et al., 2014) and Generalised Likelihood Uncertainty Estimation (GLUE, Beven and Binley, 1992, 2014; Blazkova and Beven, 2009). The latter can make use of formal and informal likelihood measures and limits of acceptability, as well as alternatives to Bayes equation in combining different model evaluations.

Because epistemic uncertainties are involved, including the potential for non-stationary bias and error characteristics and unknown commensurability errors between observed and predicted variables, it might not always be good practice to use

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formal statistical likelihood measures in such evaluations. Indeed, epistemic uncertainties make it difficult to test such models as hypotheses in rigorous ways, and may mean that multiple model structures might be consistent with the available observations (e.g. Beven, 2006, 2012). There may also be issues of whether the available models are fit-for-purpose when compared with observations, even when the uncertainty associated with those observations is taken into account. It will always be good practice to make explicit the assumptions made in such an analysis. In Paper 1 we have suggested that this might be constructed as a form of Condition Tree.

The third form of uncertainty analysis can be used when the interest is in forecasting a hazard into the near future and when observables are available in real time to allow the use of data assimilation to constrain prediction uncertainties. A variety of data assimilation methods are available from the variational methods commonly used in weather forecasting, to ensemble Kalman filters and Particle filters. Such methods are used in real time forecasting of floods, ash clouds and wind storms. It is perhaps instructive in the context of a discussion of epistemic uncertainties that in generating an ensemble of future weather forecasts, singular vector techniques are used to choose more extreme perturbations in formulating the members of the ensemble, so as to stand a greater chance of bracketing the potential range of future weather over the lead time of a few days. The ensemble members should therefore be considered to be of unknown probability, even if the outputs are sometimes interpreted in probabilistic ways (such as in decisions about alert status in the European Flood Awareness System based on simulated river flows forced by ECMWF ensemble predictions of rainfalls).

12 Co-emergent and cascading hazards

The earlier discussion has mostly been concerned with the characteristics of individual hazards but it is clear that an assessment of risk very often needs to allow for the joint occurrences of multiple hazards, either for hazards of different types affecting a single location, or the joint occurrence of a hazard at multiple locations simultaneously (e.g.

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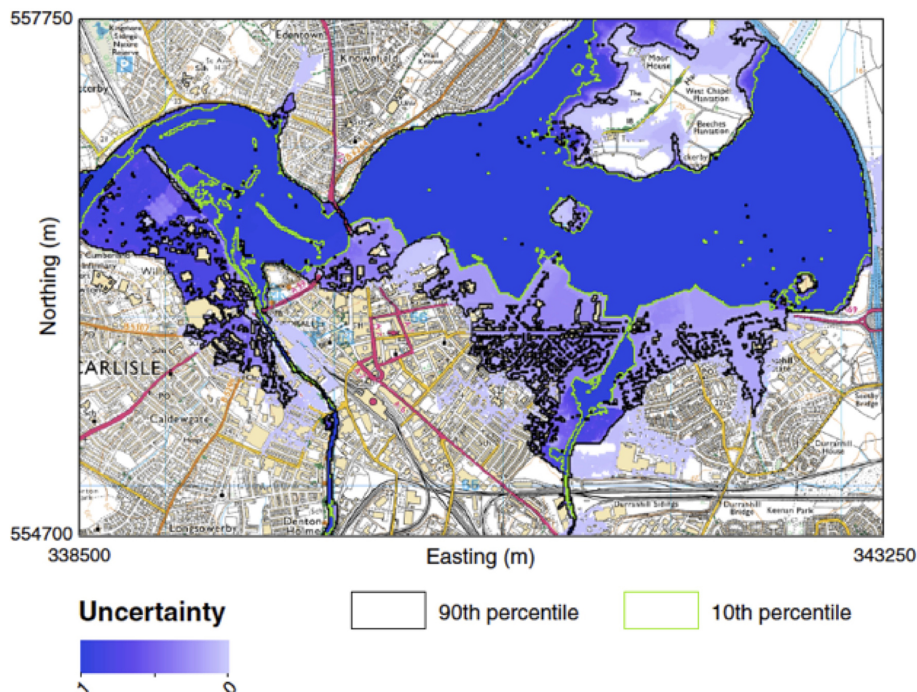
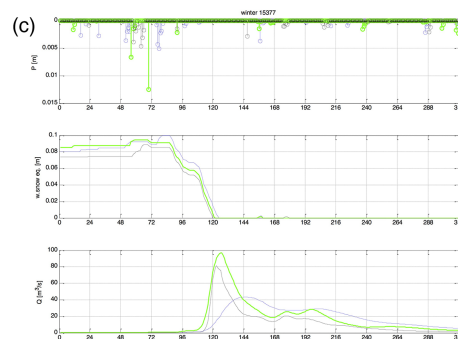
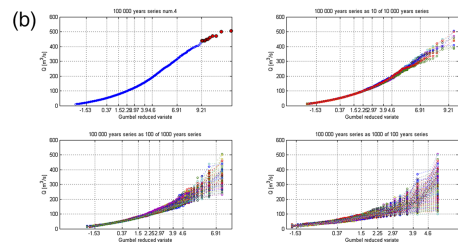
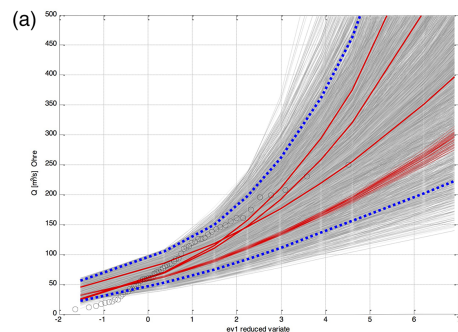


Figure 1. Uncertainty in inundation extent, as colour coded chance of flooding, resulting from the flood with annual exceedance probability 0.01, River Eden valley in the vicinity of Carlisle, Cumbria, UK (after Neal et al., 2013).

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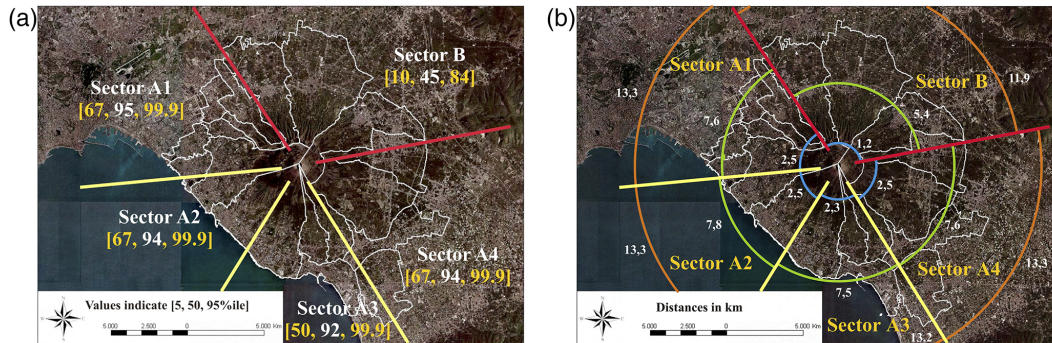


Figure 4. (a) Broad segmentation of area around Vesuvius recognizing the first-order effect of Mt. Somma topography in determining areas that might be invaded by pyroclastic density current flows (PDC) as the result of a Sub-Plinian I eruption. The bracketed values in each sector show elicited modal probabilities that a PDC will affect that sector (expressed in percentage terms) together with the corresponding credible intervals, in quantile form (5th, 50th, 95th percentiles). (b) Elicited estimates of maximum run-out distances (in km) for PDCs occurring during a Sub-Plinian I eruption, by sector. Inner arcs (blue) are 95 % confidence levels for exceeding distance shown (e.g. 2.5 km for Sector A1), central arcs (green) are expected (50th percentile) values, and outer arcs (orange) are the run-out distances assessed has having only a 5 % chance of being exceeded (from Neri et al. (2008), with permission).

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