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Abstract

Two-dimensional avalanche simulation software operating in three-dimensional terrain is widely used for hazard zoning and engineering to predict runout distances and impact pressures of snow avalanche events. Mountain forests are an effective biological protection measure; however, the protective capacity of forests to decelerate or even to stop avalanches that start within forested areas or directly above the treeline is seldom considered in this context. In particular, runout distances of small- to medium-scale avalanches are strongly influenced by the structural conditions of forests in the avalanche path. We present an evaluation and improvement of a novel forest detrainment function implemented in the avalanche simulation software RAMMS for avalanche simulation in forested terrain. The new approach accounts for the effect of forests in the avalanche path by detraining mass, which leads to a deceleration and runout shortening of avalanches. The relationship is parameterized by the detrainment coefficient K (Pa) accounting for differing forest characteristics. We varied K when simulating 40 well-documented small- to medium-scale avalanches which released in and ran through forests of the Swiss Alps. Analyzing and comparing observed and simulated runout distances statistically revealed values for K suitable to simulate the combined influence of four forest characteristics on avalanche runout: forest type, crown closure, vertical structure and surface roughness, e.g. values for K were higher for dense spruce and mixed spruce-beech forests compared to open larch forests at the upper treeline. Considering forest structural conditions within avalanche simulation will improve current applications for avalanche simulation tools in mountain forest and natural hazard management.

1 Introduction

Avalanche dynamics models are widely used for hazard zoning and engineering to predict runout distances and impact pressures of snow avalanche events (Gruber and

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Margreth, 2001; Ancey et al., 2003; Gruber and Bartelt, 2007). The effect of mountain forests as an effective biological protection measure against avalanches has been rarely addressed in this context (Berger and Rey, 2004; Gruber and Bartelt, 2007; Teich and Bebi, 2009). Large destructive avalanches which often destroy the forest without a significant deceleration are of major interest in hazard zoning (e.g. Gruber and Häfner, 1995; Fuchs et al., 2005). Yet, small- to medium-scale¹ frequent avalanches are also often a threat to roads, railways and ski-runs below the forest (Techel et al., 2013). Especially when it comes to decisions about the size and extent of avalanche defense measures (including afforestation) in potential starting zones in forested areas, e.g. in newly created forest openings due to wind disturbance, or directly above the treeline, forest and civil engineers could benefit from reliable avalanche simulation in forested terrain (e.g. Weir, 2002; Schönenberger et al., 2005; Bebi et al., 2009).

The avalanche flow is not only influenced by terrain characteristics, but also by vegetation in the avalanche path (McClung, 2003). A recent study showed that forest structural parameters, e.g. the type of forest and the stem density in avalanche starting zones, have a significant influence on runout distances of small- to medium-scale avalanches starting in forested areas (Teich et al., 2012a). For large avalanches released high above the treeline, this effect is however negligible (de Quervain, 1979; Bartelt and Stöckli, 2001; Margreth, 2004; Schneebeli and Bebi, 2004; Christen et al., 2010b). The decreasing speeds and runout distances of large-scale avalanches depend mainly on the topography and the distance an avalanche travels through open terrain before penetrating into forests (McClung, 2003; Takeuchi et al., 2011; Anderson and McClung, 2012; Teich et al., 2012a). Both cases have only rarely been implemented in avalanche models (Anderson and McClung, 2012).

Flow models used for avalanche simulation often employ Voellmy-type relations splitting the total basal friction into a velocity independent dry-Coulomb term and

¹For avalanche size definitions we refer to typical path lengths where “small” < 100 m (volume < 1000 m³), “medium” < 1000 m (volume < 10 000 m³) and “large” < 2000 m (volume < 100 000 m³) avalanche length (EAWS, 2012).

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a velocity dependent “viscous” or “turbulent” friction (Voellmy, 1955). The friction approach has been applied by several authors to model the effect of forest on avalanche runout by increasing friction in forested areas compared to open unforested terrain (Gubler and Rychetnik, 1991; Bartelt and Stöckli, 2001; Gruber and Bartelt, 2007; Teich and Bebi, 2009), and has been verified for few real large-scale avalanche events (Casteller et al., 2008; Takeuchi et al., 2011). Avalanche-forest interactions may however be only poorly represented within the framework of this model (Teich et al., 2012b). Especially for small-scale avalanches physical processes within the avalanche flow such as snow entrainment (mass uptake) and detrainment (mass extraction) along the avalanche path are important and are not included in the calibrated Voellmy friction coefficients (Maggioni et al., 2012; Bovet et al., 2013). The local braking effect of forests on avalanche flow seems to be difficult to model with a frictional relationship at the grid scale (Feistl et al., 2013).

Instead of using higher friction values, Feistl et al. (2012, 2013) propose an additional detrainment function to account for avalanche-forest interactions. Based on field observations, they assume that trees stop fractions of the granular snow flow by a combination of impact, rubbing dissipation, deflection, cohesion and jamming. The stopped snow deposits behind trees, groups of trees or remnant stumps and, therefore, mass is directly extracted from the avalanche flow and the corresponding momentum is removed from the total momentum of the moving snow. This detrainment function accounts for the braking effect of forests on avalanche flow, and can be implemented in numerical avalanche dynamics models. The relationship is parameterized by the detrainment coefficient K , representing forest characteristics such as forest stand density or mean stem diameters. Currently, values of K for forested areas have only roughly been estimated and tested for few real avalanche events (Feistl et al., 2013).

Detailed analyses of two-dimensional avalanche simulation software working in three-dimensional terrain objectively require a suitable data selection and a comprehensive and standardized way of processing multiple simulation results (Fischer, 2013). Processing and analyzing large quantities of one-dimensional

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avalanche model outputs automatically have been conducted in several studies (e.g. Ancey, 2005; Gauer et al., 2009; Eckert et al., 2009). In contrast, multidimensional simulation data has mainly been evaluated manually along predefined cross sections within the avalanche path (e.g. Christen et al., 2010b; Bühler et al., 2011). Comparing two-dimensional simulation results with field observations for a high number of avalanche events manually is however time consuming and rather subjective. To overcome this weakness, a standardized evaluation and comparison method for models operating in three-dimensional terrain has been suggested by Fischer (2013). This approach is employed here to analyze avalanche simulation results automatically and objectively.

In this study, we apply a novel detrainment modeling approach in order to investigate the effect of different forest characteristics on small- to medium-scale avalanches. We compare simulation results of the avalanche simulation software RAMMS (Christen et al., 2010a) with runout observations of avalanches released in forests of the Swiss Alps in order to improve the forest detrainment function. The avalanche dataset consists of 40 avalanches which started in forests and either stopped in forested terrain within 50–400 m or ran through forests and stopped in unforested areas with a maximum runout distance of 700 m. We evaluate our model by systematically analyzing parameters characterizing forest structural conditions and their effects on simulated compared to observed runout distances. The overall aim is to define combinations of forest characteristics corresponding to a specific value of the detrainment coefficient K to be applicable in practice.

2 Theory

2.1 Avalanche flow model

In this contribution, avalanche flow is modeled using depth-averaged mass and momentum equations; for a detailed mathematical description see Christen

et al. (2010a). To briefly summarize: avalanche flow is characterized by unsteady and uniform motion with varying flow depth and velocity. Therefore, avalanche flow depth $H(x, y, t)$ and mean avalanche velocity $U(x, y, t)$ are the unknown field variables. The depth-averaged field variables are a function of time (t) and space (x, y) and, thus, the equations to model avalanche flow, i.e. mass balance and momentum equations, are solved from avalanche release ($t = 0$) to avalanche deposition.

The mass balance in terms of the avalanche flow depth (H) is given by

$$\partial_t H + \partial_x(HU_x) + \partial_y(HU_y) = \dot{Q}(x, y, t) \quad (1)$$

where $\dot{Q}(x, y, t)$ denotes the mass production source term with $\dot{Q} = \dot{Q}_e + \dot{Q}_d$, the sum of the volumetric entrainment \dot{Q}_e and detrainment \dot{Q}_d rates. The mass production source term specifies the mass uptake (entrainment) with $\dot{Q} > 0$ (i.e. $\dot{Q}_e > 0$ and $\dot{Q}_d = 0$) or mass extraction (detrainment) $\dot{Q} \leq 0$ (i.e. $\dot{Q}_e = 0$ and $\dot{Q}_d < 0$) from the snow cover per unit area as a function of time t ; U is the velocity in x and y direction.

The component wise depth-averaged momentum balance is given by

$$\partial_t(HU_x) + \partial_x \left(c_x HU_x^2 + g_z k_{a/p} \frac{H^2}{2} \right) + \partial_y(HU_x U_y) = S_{gx} - S_{fx} \quad (2)$$

and

$$\partial_t(HU_y) + \partial_y \left(c_y HU_y^2 + g_z k_{a/p} \frac{H^2}{2} \right) + \partial_x(HU_x U_y) = S_{gy} - S_{fy} \quad (3)$$

where c_x and c_y are the velocity profile shape factors, $k_{a/p}$ is the earth pressure coefficient and $S_f = (S_{fx}, S_{fy})^T$ is the total friction (for details on c and $k_{a/p}$ we refer to Christen et al., 2010a). The right-hand side terms of Eqs. (2) and (3) add up to the driving, gravitational acceleration g in x and y direction. That is, avalanche flow

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resistance is implemented by a “Voellmy-fluid” friction relation assuming small shear strains in the flow body (Salm et al., 1990; Bartelt et al., 1999):

$$S_{g_x} = g_x H \quad \text{and} \quad S_{g_y} = g_y H. \quad (4)$$

The model splits the total basal friction S_f into a velocity independent dry-Coulomb term which is proportional to the normal stress at the flow bottom (friction coefficient μ) and a velocity dependent “viscous” or “turbulent” friction (friction coefficient ξ) (Salm, 1993):

$$S_{f_x} = \frac{U_x}{\|\mathbf{U}\|} \left[\mu g_n H + \frac{g \|\mathbf{U}\|^2}{\xi} \right] \quad \text{and} \quad S_{f_y} = \frac{U_y}{\|\mathbf{U}\|} \left[\mu g_n H + \frac{g \|\mathbf{U}\|^2}{\xi} \right] \quad (5)$$

where g_n is the surface normal component of the vector of gravitational acceleration $g = (g_x, g_y)$ (see Fig. 1). $\|\mathbf{U}\|$ is the magnitude and direction of the mean flow velocity given by $\|\mathbf{U}\| = \sqrt{U_x^2 + U_y^2}$. Therefore, snow characteristics and topographical conditions such as slope angle are represented via the inverse velocity.

2.2 Improved avalanche modeling in forested terrain

The approach proposed by Feistl et al. (2012, 2013) to model the braking effect of forests on avalanches is based on extracting the mass of snow which is caught behind trees leading to a deceleration and significant runout shortening of avalanches (Eq. 6). When modeling avalanche flow in forested terrain, we assume that potential snow entrainment (mass uptake) is negligible for small- to medium-scale avalanches that started in forests. In fact, we hypothesize that snow detrainment, i.e. mass removal by trees, remnant stumps or dead wood, is predominant in forests and, thus, the mass production source term (see Eq. 1) corresponds to $\dot{Q} \leq 0$ (as the sum of the volumetric entrainment rate $\dot{Q}_e = 0$ and the volumetric detrainment rate $\dot{Q}_d < 0$). This assumption is based on observations where trees in the path of small- to medium-scale

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5 avalanches did not break and, therefore, act like obstacles and “detrain” respectively extract avalanche mass (Faug et al., 2004). The extracted mass stops promptly and, thus, is instantly subtracted from the flow (Eq. 1) and the momentum of the stopped mass is removed from the total momentum of the avalanche flow (Eqs. 2 and 3). The

$$\dot{M}_d = -\frac{K}{\|\mathbf{U}\|} \quad \text{where} \quad \dot{M}_d = \rho \cdot \dot{Q}_d \quad (6)$$

10 with \dot{M}_d as the mass lost by the avalanche in front of tree-stands. The density of the avalanche snow is denoted with ρ .

This relationship indicates that the higher the velocity the less snow is removed from the flow. Parameter K accounts for the braking power of different forest types per square meter and, therefore, depends on forest characteristics such as stand density or mean stem diameter (Fig. 1).

15 3 Materials and methods

3.1 Avalanche data

20 Our evaluation and operationalization of the forest detrainment function were based on 40 small- to medium-scale avalanches released in forests with runout distances ranging between 50 and 700 m. Within this dataset, 38 wet and dry snow avalanches were observed during the winters 1986–1990 in the Swiss Alps (avalanches #1 to #38; Table A1). For these avalanches, the starting points were specified as x , y coordinates and runout distances were recorded from the starting point in 5 m steps as the horizontal projection. Detailed data on avalanche characteristics and forest parameters in the avalanche starting zone were collected in the field close to the events

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(Schneebeli and Meyer-Grass, 1993). Since adequately detailed maps of release areas existed only for 26 of these avalanches, we reconstructed the release areas of the remaining 12 avalanches based on given avalanche starting points, maximum release widths, field notes and photos taken shortly after the avalanche events combined with digital elevation model (DEM) and orthophotograph analyses (Vassella, 2012). In addition, two avalanches (#39 and #40; Table A1) which released in forests near Davos, Switzerland in the winter 2011/12 were mapped using a hand-held differential GPS device (for details see Feistl et al., 2013). Forest structural parameters (Table 1), terrain variables and avalanche characteristics such as the type of snow (dry or wet snow avalanche) or the distance an avalanche ran through forest were assigned to all 40 avalanche events based on collected field data, orthophotographs and DEM analyses (Table A1). Avalanche release volumes (V_r) were calculated corresponding to mapped and reconstructed release areas and given release heights mainly measured in the field or estimated based on measurements of nearby snow and weather stations.

We chose forest and terrain variables due to pretests of potentially relevant variables and their compatibility with existing assessment methods. Forests were classified in three types dependent on the main tree species: “beech forests” containing beech as well as mixed beech-spruce forests with the main tree species European beech (*Fagus sylvatica* L.), “spruce forests”, i.e. evergreen coniferous forests dominated by Norway spruce (*Picea abies* (L.) H. Karst.), and “larch forests” as deciduous coniferous forests formed by European larch (*Larix decidua* Mill.) at the upper treeline. Forest density was characterized by the variable crown closure describing the intensity of the crown coverage in three aggregated classes (see Table 1). The crown coverage was delineated and digitized in GIS by orthophotograph analyses based on the classification system of Bebi et al. (2001). The stage of development indicates the mean stem diameter distribution as well as the age of the forest which are also represented somewhat by the vertical structure (Tables 1 and A2). The terrain variables overall mean slope angle, the cross-slope curvature and terrain roughness were determined from a high-resolution DEM, which was gained from airborne lidar (light

detection and ranging) data with a spatial resolution of 2 m and a vertical accuracy of approximately 0.5 m. Cross-slope curvature was defined by the relative position of a cell to its surrounding pixels in a 3 pixel \times 3 pixel moving-window. The mean value of the curvature raster was taken for the avalanche track to assign the corresponding category “gully” or concave slope, and “flat” terrain, i.e. almost no curvature. Terrain roughness was expressed as the standard deviation of the terrain height undulations (differences in elevation) within a 3 pixel \times 3 pixel pixel moving-window with corresponding categories “low” and “high”. For a detailed methodological description we refer to Teich et al. (2012a). In addition to the terrain roughness gained from the DEM, the small-scale surface roughness was also assigned to each avalanche. This variable was mapped in the field and describes the nature of the surface cover. Categories are “smooth”, “knobby”, “scree” and “stumps/shrubs/saplings” (Table 1).

3.2 Simulation software and set-up

The forest detrainment function (Eq. 6) was implemented in the current version of the avalanche simulation software RAMMS (RAPid Mass Movement System). Based on a two-dimensional depth-averaged flow model (Eqs. 1–4), RAMMS calculates the development of avalanche flow depth $H(x, y, t)$ and depth-averaged avalanche velocities $U(x, y, t)$ as a function of time t (see Sect. 2.1); the system of partial differential equations is solved numerically using first and second order finite volume techniques (Christen et al., 2010a). The depth-averaged field variables H and U are used to predict avalanche runout distances or impact pressures in complex three-dimensional terrain. Three spatially explicit quantities are required to perform the numerical calculation: (1) a DEM, (2) release areas (A_r), and (3) model friction parameters (μ and ξ , Eq. 5). In addition, to run RAMMS including the forest detrainment function, forested areas (A_f) have to be defined in the model domain and assigned a K value theoretically corresponding to specific forest characteristics such as forest density, age or undergrowth.

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We determined forested areas based on existing forest maps and orthophotograph analyses. In order to focus the evaluation and operationalization on the detrainment function only, snow density was set to $\rho = 300 \text{ kg m}^{-3}$ and we kept the friction parameters constant at $\mu = 0.29 \text{ ms}^{-2}$ and $\xi = 1500 \text{ ms}^{-2}$ throughout this study. We chose this combination since the estimated release volumes of our avalanche dataset range between 19 and 3398 m^3 which corresponds to the avalanche size class “tiny” ($< 5000 \text{ m}^3$), and is applied in practice to simulate frequent avalanches (10 yr return period), in unchanneled terrain above 1500 m a.s.l. (Buser and Frutiger, 1980; Salm et al., 1990). The simulations are based on a DEM with a spatial resolution of 2 m and a vertical accuracy of approximately 0.5 m. The mapped release areas and measured release heights were used to specify the initial conditions for each simulation run. All simulations were accomplished without any pre-defined stopping criteria.

For each observed avalanche a reference simulation was computed by running RAMMS without accounting for any forest influence in the avalanche path ($K = 0$). In order to find optimal values for K dependent on different forest characteristics, we then simulated each observed avalanche with varying values for K of 5, 10, 20, 30, 40, 60, 80, 100, 130, 160, 190 and 220 Pa. These K values were chosen based on results of a computational experiment performed by Feistl et al. (2013).

The main simulation results are maximums over time t of the flow depth $H(x, y, t)$ and the two dimensional slope parallel velocities $U(x, y, t)$ at a constant density ρ . As usually applied in hazard assessment (Eckert et al., 2010), the according peak pressure field can then be derived as

$$P(x, y) = \rho U_{\text{peak}}^2(x, y) \quad (7)$$

where x, y denote the two dimensional Cartesian coordinates. Here U_{peak} corresponds to its maximum U value over the entire simulation time t :

$$U_{\text{peak}}(x, y) = \max_t U(x, y, t) \quad (8)$$

For our analyses, we exported the spatially explicit maximum pressure output.

3.3 Analyzing simulation results

To compare the two-dimensional model outputs with the one-dimensionally recorded avalanche runout distances, we applied the analysis method AIMEC (Automated Indicator based Model Evaluation and Comparison) presented by Fischer (2013).

The AIMEC-approach allows for a standardized and objective evaluation of two-dimensional simulation results. The simulation results are transformed from Cartesian coordinates (x, y) to a coordinate system dependent on the specific avalanche path (s, l) (Fig. 2), here applied for the peak pressure:

$$P(x, y) \rightarrow \tilde{P}(s, l) \quad (9)$$

As a scalar metric, the runout indicator is defined based on the peak pressure (Eq. 7), and evaluated for each simulation run. This runout indicator corresponds to the horizontal projection of length measured along the avalanche path coordinate s where the cross sectional maximum peak pressure value:

$$\tilde{P}_{\text{cross}}^{\max}(s) = \max_t \tilde{P}(s, l) \quad (10)$$

falls below a certain pressure limit $\tilde{P}_{\text{cross}}^{\max}(s) < P_{\text{limit}}$ (Fig. 2).

The choice of the pressure threshold (P_{limit}) is of great importance for reliable runout indicators and further analyses. Since we ran the simulations without any pre-defined stopping criteria such as for the flow momentum or flow depth, no realistic stopping may be modeled in flat natural terrain. Defining runout distance based on thresholds for the maximum flow momentum or the minimum flow depth on the contrary could also lead to a misinterpretation of simulation results, especially for small-scale avalanches, which would influence further analyses considerably. These problems were avoided by applying a pressure based runout indicator to determine simulated runout distances (Fischer, 2013).

We ran AIMEC with pressure thresholds P_{limit} of 1, 3, 5 and 10 kPa as well as 0.5 kPa for very small avalanches with release volumes $V_r < 100 \text{ m}^3$; however,

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differences between corresponding runout indicators were low. In particular, for very small avalanches ($V_r < 100 \text{ m}^3$) the differences between runout indicators determined with $P_{\text{limit}} = 3 \text{ kPa}$ and $P_{\text{limit}} = 1 \text{ kPa}$ for the reference simulations with $K = 0$ ranged between 1 and 66 % (mean = 22 %). When calculating the difference between both runout indicators for all avalanches of our data set, the mean difference was rather low with only 14 % (ranges between 0 and 67 %). For simulations performed with the forest detrainment ($K > 0$), mean differences between the two runout indicators ($P_{\text{limit}} = 3 \text{ kPa}$ and $P_{\text{limit}} = 1 \text{ kPa}$) decreased for very small avalanches ($V_r < 100 \text{ m}^3$) to 2 % and for all avalanches to 7 %. Due to such small differences, we applied a pressure threshold of $P_{\text{limit}} = 3 \text{ kPa}$ throughout this study which corresponds to a pressure threshold used for hazard zone mapping in Switzerland (BFF/SLF, 1984). That is, for avalanches with return periods $\leq 30 \text{ yr}$ an impact pressure $> 3 \text{ kPa}$ is assigned to have consequences regarding land-use planning (Jóhannesson et al., 2009).

In order to measure the differences of simulated runout indicators ($\text{runout}_{\text{sim}}$) to observed runout distances ($\text{runout}_{\text{obs}}$), the relative runout difference (Δrunout in [%]) is introduced

$$\Delta\text{runout} = \left(\frac{\text{runout}_{\text{sim}} - \text{runout}_{\text{obs}}}{\text{runout}_{\text{obs}}} \right) \cdot 100 \quad (11)$$

where positive values indicate overestimated runout distances respectively negative values for Δrunout reveal that runout distances were underestimated by the avalanche simulation software compared to the recorded ones.

3.4 Statistical analysis

For an evaluation of general dependencies between variables describing forest structure, topography and avalanche characteristics, and the response variable Δrunout , we calculated Spearman's rank correlation coefficient (r_S) for categorical and continuous predictor variables since it is known as non-parametric and does not assume a linear relationship. In addition, Pearson's correlation coefficient (r)

was calculated for all continuous variables and Δrunout to reveal potential linear dependencies and to measure their strengths. A correlation was assumed to be statistically significant if the respective p value was $0.01 < p \leq 0.05$ and highly significant for $p \leq 0.01$.

The evaluation and operationalization of the avalanche model included four steps:

1. We tested all variables against Δrunout (further referred to as $\Delta\text{runout}_{\text{ref}}$) for the reference simulations without any influence of forest ($K = 0$).
2. Based on the simulations including the mass extracting effect of forests parameterized with the detrainment coefficient K , we determined an optimal K value for each avalanche event (K_{opt}). That is, one value for K was defined for each of the 40 avalanche events which resembled the observed runout distances “best”, i.e. where K approaches zero of Δrunout , on condition that $\Delta\text{runout} \geq 0$. A conservative evaluation of simulation results leading to overestimated rather than to underestimated runout distances is preferred to reveal optimal K values which are applicable in practice.
3. We again calculated r_S and r respectively, and tested the forest parameters forest type, crown closure, vertical structure, stage of development and surface roughness as well as the release volume and the distance an avalanche ran through forest against the response variable K_{opt} .
4. We defined K values based on specific forest characteristics and their combined effects to be applicable in practice for reliable avalanche simulation in forested terrain.

We evaluated our derived K values by simulating two avalanche events additionally observed in 2012 in forested terrain in the Swiss and Bavarian Alps. These avalanches differed in forest conditions and the distance they ran through forest as well as in the snow type. To further test the practical applicability of the derived K values we ran RAMMS using a default simulation set-up and compared simulation results manually.

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4 Results

4.1 Avalanche simulation with $K = 0$

Runout distances were overestimated by RAMMS for 38 of 40 investigated avalanches in forested terrain when forests' influence was not considered. The relative runout difference $\Delta\text{runout}_{\text{ref}}$ (Eq. 11) revealed overestimations by RAMMS up to 700%. The two avalanches with negative values for $\Delta\text{runout}_{\text{ref}}$ (-34 and -48 %) are of very small release volumes ($V_r < 50 \text{ m}^3$).

Variables which affected $\Delta\text{runout}_{\text{ref}}$ of our dataset significantly are the release height, the snow type, the absolute as well as the relative distance an avalanche ran through forest, and the small-scale surface roughness (Table 2). Dependencies between the continuous variables release height, and absolute and relative distance through forest are not linear since no significant correlations were found when calculating Pearson's correlation coefficient (r). However, it could be assumed that increasing release heights, accompanied with increasing release volumes (see Table A2), are related to an increase in $\Delta\text{runout}_{\text{ref}}$. That is, the bigger an avalanche, the larger the difference between observed and simulated runout distances. Both correlations imply, that a loss of avalanche volume modeled for forested areas may lead to a significant runout shortening and a more realistic avalanche simulation which would match the observations.

Differences between observations and simulations were significantly higher for dry snow avalanches compared to wet snow avalanches (Fig. 3). Thus, one can assume that the accompanying snow densities and thermal snow temperatures also determine the detraining effect of forests. Here, snow density was kept constant at $\rho = 300 \text{ kg m}^{-3}$ which is often applied for dry snow avalanches. The snow type was also correlated with release volume and release height (Table A2) where the latter one also influenced $\Delta\text{runout}_{\text{ref}}$ significantly (Table 2). The nature of the surface cover, i.e. surface roughness, was correlated significantly with $\Delta\text{runout}_{\text{ref}}$. That is, a scree slope

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and higher small obstacles such as stumps and shrubs in the avalanche path were related to larger differences between observed and simulated runout distances and, therefore, also determine the amount of snow deposited in the avalanche track.

Besides surface roughness, distributions of $\Delta\text{runout}_{\text{ref}}$ suggest influences of other forest parameters on avalanche simulations (Fig. 3). In particular, runout indicators for avalanches that started in spruce forests were highly overestimated (median = 88 %; mean = 154 %), but less overestimated for avalanches which ran through beech forests (median = 52 %; mean = 79 %) or larch forests (median = 44 %, mean = 49 %). For simulations without any forest influence, $\Delta\text{runout}_{\text{ref}}$ was largest for avalanches which ran through evergreen, dense forests with a more than two-layered vertical structure, containing different age classes and varying stem diameters.

Mean slope angle, cross-slope curvature and terrain roughness in terms of local differences in elevation (in contrast to surface roughness describing the nature of the surface cover) did not influence $\Delta\text{runout}_{\text{ref}}$ significantly. This strengthens the theory that avalanche-forest interactions need to be implemented by a function dependent on forest characteristics in combination with snow conditions only.

4.2 Avalanche simulation with varying K values

For the next step of our evaluation and further operationalization, we calculated Δrunout for each simulation run with varying values for K and analyzed relationships between forest characteristics and Δrunout . In general, increasing K values corresponded to decreasing runout indicators where the strength of this effect seemed to decrease around K values of 150 Pa and higher (Figs. 4 and 5). Very small avalanches with release volume $V_r < 100 \text{ m}^3$ showed diverging simulation results. For such avalanches, values of Δrunout were often negative when applying the forest detrainment function; one avalanche simulation did not even start with the smallest chosen K value of 5 Pa. However, differences between avalanche simulations in terrain covered with different forest types are visible, especially between larch forests and the two other forest types, spruce and beech forests, when calculating mean values of

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Δ runout corresponding to each chosen K value for the three categories separately (Fig. 4). In addition, differences in the vertical structure of a forest stand as well as in crown closure had a higher influence on the amount of snow extracted from the avalanche flow compared to a differing stage of development (Fig. 5). The latter forest variable is however relatively well represented by the vertical structure (Table A2). The nature of the surface cover also influenced the amount of snow removed from the avalanche flow. The effect of differences in small-scale surface roughness could have been even underestimated since our simulation set-up allowed not to account for changes in surface roughness in unforested areas.

In terms of the operationalization, optimal values for K (K_{opt}) were assigned to each observed avalanche based on the election rule that Δ runout approaches zero on condition Δ runout ≥ 0 . A significant correlation was found between K_{opt} and the forest type (Fig. 6) as well as for the release volume and the absolute distance an avalanche ran through forest (Table 2); the latter two were even linear with $r = 0.35$ and $p = 0.028^{\text{a}}$ for release volume respectively $r = -0.44$ and $p = 0.005^{\text{b}}$ for the distance through forest. Thus, the larger the release volume the higher is K_{opt} , respectively the longer the distance an avalanche runs through forest the lower the corresponding K_{opt} . According to theory K however should only account for forest characteristics.

Thus, we propose to choose a “best” value of K to simulate avalanche runout in forested terrain dependent on the four forest characteristics forest type, crown closure, vertical structure and surface roughness. Based on Figs. 5 and 6, possible values for K can be obtained to predict avalanche runout distances in forested terrain. According to this, K values of 5 Pa may be assigned to areas covered with larch forests, 80 Pa to forests dominated by spruce and 100 Pa to beech and mixed beech-spruce forests. These values should be adapted with K values corresponding to classes of the forest characteristics crown closure, vertical structure and surface roughness (see Fig. 5), e.g. the mean value of the respective K values for these four forest characteristics were calculated for our case studies (see Sect. 4.3). The influence of K values higher than

approximately 150 Pa on Δ runout decreases (Fig. 5). Therefore, K values > 150 Pa seem to be not meaningful for modeling avalanche-forest interactions.

4.3 Case studies

In order to test the practical application of our results, we simulated two additionally observed avalanches with RAMMS including the forest detrainment function (Table 3). Therefore, we assigned a “best” K value to forested areas based on the four forest parameters forest type, crown closure, vertical structure and surface roughness, and the corresponding categories (see Table 1).

Values of K were estimated based on Figs. 4–6. For forest type, crown closure, vertical structure and surface roughness K values close to Δ runout = 0 were chosen and, then, the mean value of K was calculated (Table 3). We ran RAMMS with a default simulation set-up, i.e. values for friction parameters μ and ξ were not kept constant but defined by an automatic procedure of RAMMS depending on terrain features such as gullies or flat slopes, elevation, the return period (set to 10 yr) and the avalanche size class (“tiny”). The simulations were based on a 2 m grid for the avalanche observed in Switzerland respectively a 1 m grid for the one from Germany. Forested areas and forest characteristics were delineated based on pixel maps, orthophotographs, and photographs taken during field visits. Again, we ran the simulations until the final pressure patterns were reached. In practice a stopping criteria of 5% of the total momentum is often applied indicating that if the sum of all momenta of all grid cells is lower than 5% of the maximum momentum sum, the simulation is stopped (Christen et al., 2010). However, test-simulation runs applying this threshold have shown that runout distances of our case studies and, therefore, such small-scale avalanches, were highly underestimated. In contrast, we ran our simulations without any stopping criteria and analyzed the simulation results by only displaying the grid-cells of the runout area which exceeded a pressure threshold of 3 kPa. This corresponds to our limit for the maximum peak pressure (P_{limit}) when defining runout distances by applying AIMEC

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(see Sect. 3.3) as well as to the impact pressure threshold with consequences for hazard zone mapping in Switzerland (BFF/SLF, 1984; Jóhannesson et al., 2009).

The simulation results showed a good agreement with the observed runout when applying the novel forest detrainment function with values for the detrainment coefficient K dependent on four forest characteristics (Fig. 7). Even if the runout areas did not match the observed ones exactly, runout distances were predicted relatively well by the model for both avalanche events; simulated runout distances stopped within -6 to 3 m compared to the observed ones.

5 Discussion

In this study, we applied a novel detrainment modeling approach (Feistl et al., 2012, 2013) to account for avalanche-forest interactions within computational avalanche simulation. The aim was to evaluate and improve the forest detrainment function (Eq. 6) and, therefore, to quantify the detrainment coefficient K which controls the amount of snow caught behind trees in the avalanche path.

In general, immediate stopping and removal of a certain amount of mass by trees has a greater influence on small- to medium-scale avalanches than on larger avalanches (Feistl et al., 2013). Large-scale avalanches are able to break and uproot trees linked to a low energy consumption which increases avalanche mass and, therefore, flow energy (Bartelt and Stöckli, 2001). When applying a Voellmy-type relation which is often employed by avalanche flow models, the effect of forests on such avalanches can be modeled by increasing friction compared to unforested terrain (Bartelt and Stöckli, 2001). This is not valid for modeling small-scale avalanches in forested terrain: previous simulations of our dataset with RAMMS with alternating ξ values for forested areas ($100\text{--}1000\text{ m s}^{-2}$) showed that runout distances of 31 out of the 40 avalanches were still overestimated when applying the smallest chosen ξ value of 100 m s^{-2} (Teich et al., 2012b). Moreover, simulating small-scale avalanches with a model based on frictional relationships only is generally questionable (Sailer et al., 2008) and, therefore, including

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physical processes within the avalanche flow such as snow entrainment (mass uptake) and detrainment (mass extraction) is important (Bovet et al., 2013). For example, mass extraction by forests as realized in this study leads to a significant deceleration and runout shortening of small- to medium-scale avalanches (see also Feistl et al., 2013).

The results gained from analyzing reference simulations accomplished without any forests' influence ($K = 0$) highlight the importance of modeling local braking effects of forests on avalanche flow. Significant correlations between the predictor variables release height and the distance an avalanche ran through forest with the response variable $\Delta\text{runout}_{\text{ref}}$ suggest that a loss of avalanche volume modeled for forested areas will lead to shorter runout distances. In addition, local surface roughness due to stumps and shrubs or scree slopes also affected $\Delta\text{runout}_{\text{ref}}$ significantly. This effect should also be considered for small- to medium-scale avalanches' simulation in unforested areas such as large forest openings caused by natural disturbances which are often interspersed with shrubs, fallen logs, remnant stumps and root plates of upturned trees (Fig. 8). Remained dead wood is able to increase the surface roughness at least over the first 10–20 yr after the die-back (Brown et al., 1998; Rammig et al., 2007). Indeed, the effective heights and interacting avalanche flow depths also determine the mass deposited behind obstacles (Faug et al., 2004; Naaim et al., 2004). Based on sporadic field samples we can assume effective heights of approximately 0–30 cm for “smooth” slopes, 30–50 cm for “knobby” terrain, and 30–150 cm for “scree” slopes as well as for terrain interspersed with stumps, shrubs and/or saplings. The significant correlation between the snow type and $\Delta\text{runout}_{\text{ref}}$ indicates that the effectiveness of the mass removal by forests is also determined by snow densities as well as thermal snow temperatures, e.g. as more wet and viscous the snow as slower the avalanche (Vera et al., 2012).

In the next step, we simulated each avalanche with varying K values (between 5 and 220 Pa) and assigned an optimal value for K (K_{opt}) to each avalanche event. In general, runout distances decreased with increasing K values while this effect decreased around $K=150$ Pa. However, some of the 40 observed avalanches were still

overestimated by RAMMS when simulating with the highest chosen K value of 220 Pa. On the one hand, partially misinterpreting the orthophotographs and DEMs when reconstructing 12 release areas could have affected the simulation results (Vassella, 2012). On the other hand, other processes such as the influence of thermal snow temperature on the avalanche flow (see above) and the effect of different topographic features, usually modeled by varying friction parameters μ and ξ , could have also influenced the simulations. In order to reduce uncertainties related to the avalanche modeling process and to account for effects of varying K values on the simulations only, we used constant values for μ and ξ throughout this study (see Sect. 3.2). Although not all avalanches of our dataset ran through unchanneled terrain, constant values for μ and ξ were valid in our study since friction parameters are mainly relevant for larger avalanches (Gruber and Bartelt, 2007; Christen et al., 2010b). Alternatively, a physically based implementation of curvature effects may lead to an improved representation of topographical conditions (Fischer et al., 2012).

The statistical analyses between predictor variables and the response variable K_{opt} revealed that the forest type in which an avalanche released and ran through had an influence on Δrunout . Thus, the forest type mainly determines the K value to be chosen for avalanche simulation in forested terrain in combination with crown closure, vertical structure, and surface roughness since:

- clear differences of mean Δrunout between the categories of these forest parameters are visible (Fig. 5),
- these variables can be largely derived from remote sensing-based data (orthophotographs, lidar-data) possibly combined with sporadic field samples, but no extensive measurements are required,
- other studies on the effect of forest structural parameters on observed runout distances emphasize the relevance of these forest characteristics (e.g. McClung, 2003; Teich et al., 2012a).

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The case studies performed by simulating two additional avalanches verified this argumentation (Table 3 and Fig. 7): the good agreement of the simulated and observed runout distances when applying K values based on the four suggested forest characteristics encourages the applicability of the forest detrainment function for hazard analyses and, therefore, for a practical natural hazard and protection forest management.

For these two avalanches we applied a default simulation set-up and analyzed the simulation results manually, but based on an avalanche pressure threshold of > 3 kPa used for hazard mapping in Switzerland (BFF/SLF, 1984). Impact or peak pressure results are in general of high interest in snow avalanche modeling to estimate the avalanches' destructive potential, and are utilized for hazard zoning and engineering affecting land-use planning in many countries (Jóhannesson et al., 2009).

We also chose the threshold of $P_{\text{limit}} = 3$ kPa when analyzing our simulation results automatically by applying AIMEC (Fischer, 2013). That is, a pressure based runout indicator was used to determine simulated runout distances. In the case of very small avalanches, the pressure threshold P_{limit} has to be defined carefully since predefined pressure limits could be too high, i.e. never be exceeded. Defining too low pressure limits could however lead to a misinterpretation of the simulation results, e.g. when accounting for runout which is attributed to non-realistic stopping in flat natural terrain due to a diffusive runout behavior arising from the flow model (Fischer, 2013). The $P_{\text{limit}} = 3$ kPa yielded reliable runout indicators and differed not considerably from runout indicators determined with lower values. In contrast, a $P_{\text{limit}} > 3$ kPa is not appropriate to determine runout indicators of small-scale avalanches since tested values of 5 and 10 kPa were not exceeded for many simulated avalanches of our dataset. However, a verification of the results received with AIMEC is still necessary since numerical solutions can include singularities, especially when simulating small-scale avalanches.

In this study, we could only compare observed and simulated avalanche runout distances. Reliable observations as well as measurements and experiments on

the effect of forests on the avalanche flow which also contain more avalanche characteristics such as avalanche velocity and avalanche mass balance are rare. In addition, more well-documented avalanches in forested terrain have to be analyzed in the way we did to establish better grounded results on the role of forest type, crown closure, vertical structure and surface roughness in avalanche simulation to further improve the new forest detrainment function, in particular in forested areas with varying decelerating effects. The presented findings are however a valuable first step to simulate small- to medium-scale avalanches in forested terrain to be applicable in hazard analyses.

6 Conclusions and outlook

The applied forest detrainment function, which can be implemented in numerical avalanche dynamics models, will improve the simulation of small- to medium-scale avalanches in forested terrain considerably. A value for the detrainment coefficient K can now be defined dependent on the four forest parameters forest type, crown closure, vertical structure and surface roughness. As the suggested forest characteristics can be largely derived from remote sensing-based data (orthophotographs, lidar-data), there is a high potential for practical implementations. In addition, we demonstrated that applying a standardized method to analyze a high number of two-dimensional avalanche simulation results automatically increases the reliability of an objective software evaluation; the employed method AIMEC provided accurate runout indicators as the basis for further analyses.

Implementing avalanche-forest interactions in avalanche simulation will facilitate current applications for such software, e.g. by better accounting for the protective effects of forests in natural hazard mapping (Berger and Rey, 2004; Gruber and Bartelt, 2007), for managing mountain forests efficiently (Weir, 2002; Brang et al., 2006; Teich and Bebi, 2009) or to value “avalanche protection by forests” as a key ecosystem service in mountainous regions (Grêt-Regamey et al., 2013). The forest detrainment

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function will be implemented in the next version of RAMMS and tested by practitioners based on the findings gained in this study.

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Table 1. Forest parameters and corresponding categories assigned to each avalanche.

Variable	Description and categories
Forest type	(1) “Beech forests” contain deciduous and coniferous forests, but mostly dominated by European beech (<i>Fagus sylvatica</i> L.) (2) Norway spruce (<i>Picea abies</i> (L.) H.KARST.) dominated “spruce forests” (3) “Larch forests” formed by European larch (<i>Larix decidua</i> MILL.) at the upper tree line
Crown closure	(1) Dense to loose (Crown coverage > 70 %) (2) Scattered (Crown coverage 40–70 %) (3) Open (Crown coverage < 40 %)
Vertical structure	(1) One layer (2) Two layer (3) > Two layers (4) Clumped or grouped
Stage of development	(1) Pole stage forest and young timber trees ($8 < \text{DBH}^* \leq 40$ cm) (2) Middle-aged timber trees and old timber trees $\text{DBH} > 40$ cm (3) Mixed
Surface roughness	(1) Smooth (2) Knobby (3) Scree (4) Stumps/shrubs/saplings

* Mean diameter at breast height: outside bark diameter measured 1.37 m above the forest floor on the uphill side of the tree.

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Table 2. Significant^a ($0.01 < p \leq 0.05$) and highly significant^b ($p \leq 0.01$) Spearman rank correlation coefficients (r_S) between predictor variables and $\Delta\text{runout}_{\text{ref}}$ calculated for the reference simulation runs with $K = 0$, and between predictor variables and the assigned optimal value for K (K_{opt}).

Predictor variable	r_S			
	$\Delta\text{runout}_{\text{ref}} (K = 0)$		K_{opt}	
Forest type	–	–	0.39	($p = 0.014^{\text{a}}$)
Surface roughness	0.41	($p = 0.011^{\text{a}}$)	–	–
Snow type	–0.37	($p = 0.019^{\text{a}}$)	–	–
Release volume	–	–	0.58	($p < 0.001^{\text{b}}$)
Release height	0.36	($p = 0.025^{\text{a}}$)	–	–
Absolute distance through forest	–0.53	($p = 0.001^{\text{b}}$)	–0.51	($p = 0.001^{\text{b}}$)
Relative distance through forest	0.34	($p = 0.039^{\text{a}}$)	–	–

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Table 3. Characteristics and K values corresponding to selected forest parameters of two avalanches which were not included in previous analyses to verify the results of the operationalization.

Location (Country)	Dischma valley (CH)	K (Pa)	Brecherspitz (GER)	K (Pa)
Snow type	wet		dry	
Release volume (m ³)	5043		1324	
Forest parameters				
Forest type	mainly larch	5	beech	100
Crown closure	mainly open	50	scattered to dense	125
Vertical structure	one layer	75	one to two layers	75
Surface roughness	knobby	75	smooth	25
Assigned K value		50		80

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Table A1. Avalanche data.

#	Snow type	Release height	Release volume V_r	Observed runout distance	Distance through forest	Mean slope angle	Cross-slope curvature	Terrain roughness	Forest type	Crown closure	Vertical structure	Stage of development	Surface roughness
#	[-]	[cm]	[m ³]	[m]	[m]	[°]	[-]	[-]	[-]	[-]	[-]	[-]	[-]
1	dry	110	692	100	100	34	flat	low	spruce	open	> two	old	smooth
2	wet	50	1635	100	100	38	flat	high	spruce	open	> two	mixed	stumps
3	dry	140	1308	500	30	35	gully	high	spruce	open	> two	young	knobby
4	dry	140	2296	400	200	37	flat	high	spruce	open	two	young	knobby
5	dry	140	1254	400	65	37	gully	high	spruce	open	one	old	scree
6	dry	140	3398	500	75	38	gully	high	larch	open	> two	old	knobby
7	dry	100	995	90	90	31	flat	high	spruce	open	one	young	stumps
8	dry	100	670	90	90	30	flat	high	spruce	open	> two	old	knobby
9	wet	30	251	120	120	38	gully	low	beech	dense	one	young	smooth
10	dry	40	353	600	100	32	gully	high	spruce	open	grouped	mixed	stumps
11	dry	40	122	600	80	31	gully	high	spruce	open	one	old	smooth
12	wet	20	116	360	350	37	gully	high	spruce	open	> two	mixed	stumps
13	wet	30	35	200	200	39	gully	high	larch	open	one	young	knobby
14	wet	30	20	200	200	40	flat	high	larch	open	two	old	knobby
15	wet	30	32	200	200	40	gully	high	spruce	open	one	old	knobby
16	wet	100	516	700	100	36	gully	high	larch	open	> two	young	knobby
17	wet	40	40	100	100	38	flat	low	larch	dense	one	young	scree
18	wet	50	418	160	125	38	gully	high	beech	dense	one	young	smooth
19	wet	15	125	120	120	38	gully	low	beech	dense	one	young	smooth
20	wet	70	19	180	180	35	flat	low	spruce	open	grouped	mixed	knobby
21	wet	60	167	180	180	35	flat	low	spruce	dense	grouped	mixed	stumps
22	dry	45	256	60	60	29	gully	low	spruce	dense	one	mixed	stumps
23	dry	110	948	120	120	30	flat	high	spruce	open	> two	mixed	stumps
24	wet	40	111	100	100	39	gully	low	spruce	open	> two	mixed	scree
25	wet	40	335	130	125	38	gully	low	beech	dense	one	young	smooth
26	wet	40	97	50	50	43	gully	low	beech	dense	two	mixed	knobby
27	wet	40	203	100	100	41	flat	low	beech	dense	two	mixed	scree
28	wet	40	285	150	130	41	gully	low	beech	open	two	mixed	smooth
29	wet	40	269	120	120	41	gully	high	beech	scattered	two	young	smooth
30	wet	30	202	120	120	38	gully	high	beech	dense	one	young	smooth
31	wet	20	47	120	120	41	gully	low	beech	scattered	two	young	smooth
32	dry	50	49	120	120	29	flat	low	spruce	open	one	young	stumps
33	dry	60	796	400	400	30	flat	low	larch	open	one	young	stumps
34	dry	50	298	400	160	30	flat	low	larch	open	two	young	knobby
35	dry	45	220	400	65	32	gully	low	spruce	scattered	grouped	mixed	shrubs
36	wet	125	39	50	50	40	flat	high	spruce	open	grouped	young	knobby
37	wet	20	142	100	100	41	gully	low	beech	open	two	mixed	smooth
38	wet	20	167	130	125	38	gully	low	beech	dense	one	young	smooth
39	wet	50	567	276	NA	31	flat	NA	spruce	scattered	two	old	NA
40	wet	50	669	345	NA	31	flat	NA	spruce	dense	two	old	NA

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Table A2. Cross-correlations between observed parameters. Significant^a ($0.01 < p \leq 0.05$) and highly significant^b ($p \leq 0.01$) Spearman rank correlation coefficients (r_s) in bold.

	Snow type	Release height	Release volume	Observed runout distance	Distance through forest	Mean slope angle	Cross-slope curvature	Terrain roughness	Forest type	Crown closure	Vertical structure	Stage of development
Release height	-0.58 ($p < 0.001^b$)	-	-	-	-	-	-	-	-	-	-	-
Release volume	-0.53 ($p < 0.001^b$)	0.64 ($p < 0.001^b$)	-	-	-	-	-	-	-	-	-	-
Observed runout distance	-0.26 ($p = 0.104$)	0.17 ($p = 0.304$)	0.24 ($p = 0.138$)	-	-	-	-	-	-	-	-	-
Distance through forest	0.33 ($p = 0.04^a$)	-0.35 ($p = 0.033^a$)	-0.24 ($p = 0.142$)	0.30 ($p = 0.070$)	-	-	-	-	-	-	-	-
Mean slope angle	0.70 ($p < 0.001^b$)	-0.50 ($p = 0.001^b$)	-0.42 ($p = 0.007^b$)	-0.28 ($p = 0.079$)	0.08 ($p = 0.629$)	-	-	-	-	-	-	-
Cross-slope curvature	0.17 ($p = 0.295$)	-0.47 ($p = 0.002^b$)	-0.14 ($p = 0.388$)	0.20 ($p = 0.220$)	-0.15 ($p = 0.357$)	0.39 ($p = 0.013^a$)	-	-	-	-	-	-
Terrain roughness	-0.16 ($p = 0.333$)	0.29 ($p = 0.079$)	0.29 ($p = 0.077$)	0.31 ($p = 0.061$)	-0.08 ($p = 0.644$)	-0.05 ($p = 0.784$)	0.05 ($p = 0.748$)	-	-	-	-	-
Forest type	-0.39 ($p = 0.012^a$)	0.44 ($p = 0.004^b$)	0.10 ($p = 0.530$)	0.42 ($p = 0.008^b$)	0.05 ($p = 0.770$)	-0.46 ($p = 0.003^b$)	-0.40 ($p = 0.011^a$)	0.28 ($p = 0.091$)	-	-	-	-
Crown closure	-0.432 ($p = 0.005^b$)	0.38 ($p = 0.016^a$)	0.15 ($p = 0.347$)	0.29 ($p = 0.072$)	0.03 ($p = 0.839$)	-0.19 ($p = 0.253$)	-0.17 ($p = 0.291$)	0.44 ($p = 0.005^b$)	0.53 ($p < 0.001^b$)	-	-	-
Vertical structure	-0.06 ($p = 0.699$)	0.38 ($p = 0.017^a$)	0.11 ($p = 0.493$)	0.10 ($p = 0.533$)	-0.20 ($p = 0.231$)	-0.05 ($p = 0.753$)	-0.22 ($p = 0.177$)	0.10 ($p = 0.538$)	0.21 ($p = 0.193$)	0.34 ($p = 0.031^a$)	-	-
Stage of development	-0.03 ($p = 0.873$)	-0.02 ($p = 0.890$)	-0.03 ($p = 0.839$)	-0.09 ($p = 0.574$)	-0.17 ($p = 0.319$)	-0.03 ($p = 0.874$)	0.02 ($p = 0.886$)	-0.13 ($p = 0.436$)	-0.03 ($p = 0.850$)	0.12 ($p = 0.445$)	0.51 ($p < 0.001^b$)	-
Surface roughness	-0.38 ($p = 0.019^a$)	0.35 ($p = 0.031^a$)	0.13 ($p = 0.424$)	0.03 ($p = 0.864$)	-0.10 ($p = 0.531$)	-0.48 ($p = 0.002^b$)	-0.40 ($p = 0.012^a$)	0.08 ($p = 0.633$)	0.53 ($p = 0.001^b$)	0.24 ($p = 0.154$)	0.30 ($p = 0.064$)	0.40 ($p = 0.012^a$)

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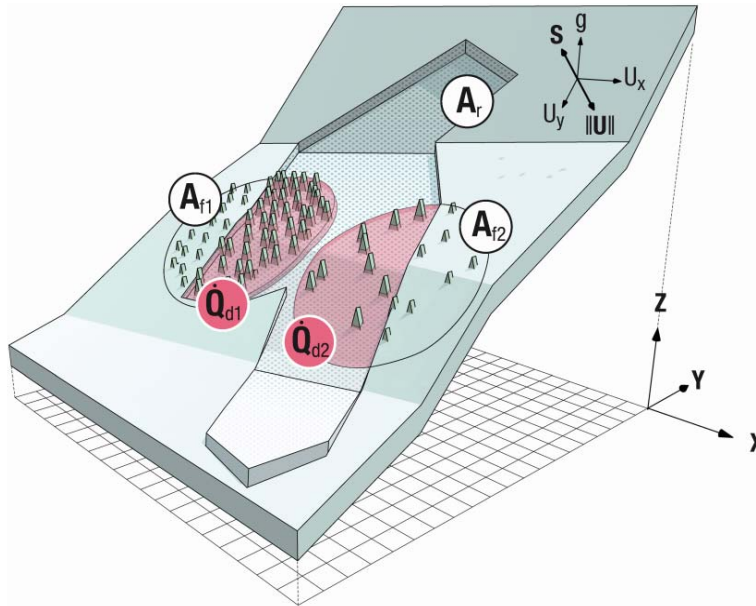


Fig. 1. Schematic illustration of avalanche modeling in forested terrain. The release area (A_r) as well as forested areas (A_f) have to be defined by the avalanche expert and assigned an appropriate K value dependent on specific forest characteristics which determine the detrainment rate (\dot{Q}_d). Avalanche flow in general is modeled by the velocities in x and y direction (U_x and U_y) and by the friction S acting in the opposite direction than $\| \mathbf{U} \|$, and the gravitational acceleration g .

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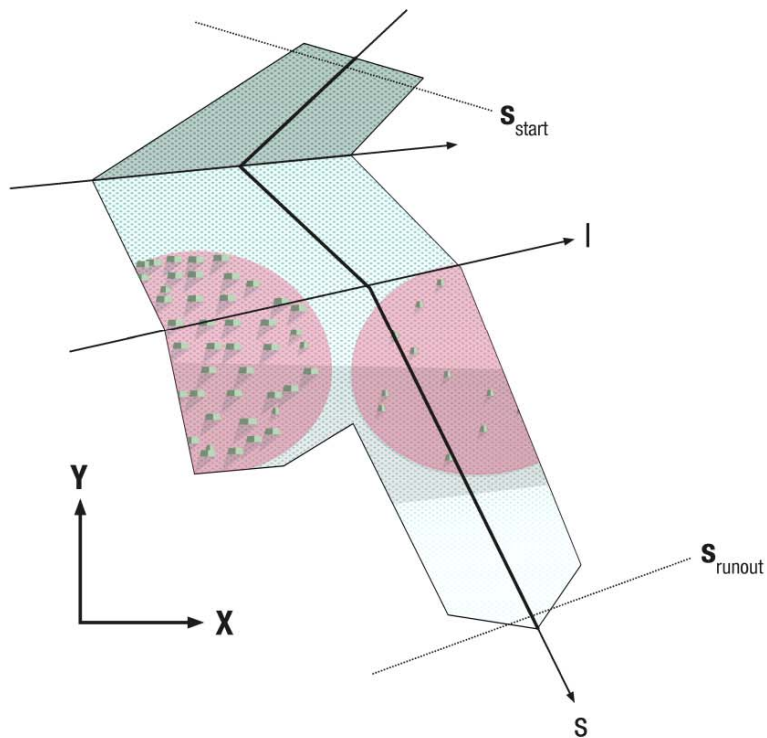


Fig. 2. Schematic avalanche simulation result (see Fig. 1; red areas correspond to forests with specific forest characteristics, e.g. tree density illustrated by green dots), e.g. the outline of the peak pressure field with a new coordinate system along the central flow line $z(x, y)$ in bold.

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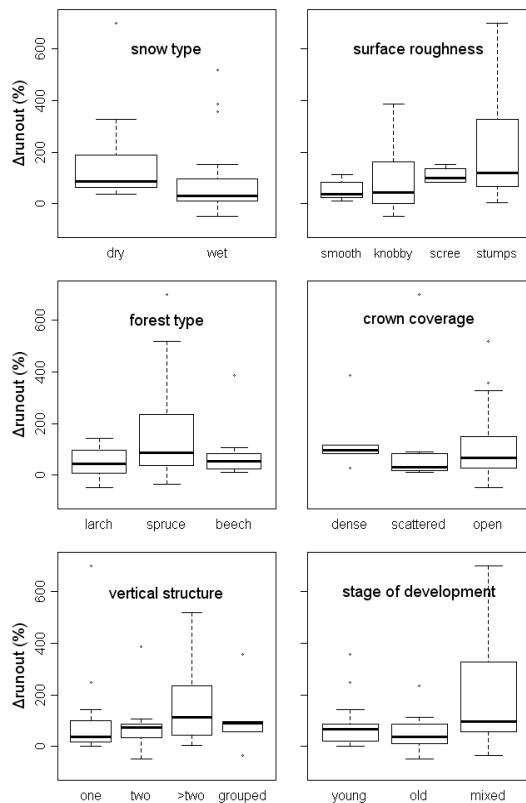


Fig. 3. Difference between simulated and observed runout distances ($\Delta\text{runout}_{\text{ref}}$) calculated for the reference simulation runs without any forests influence ($K = 0$) shown for the subsets of variables snow type and small-scale surface roughness which are statistically significant (first row) and for the subsets of four other forest structural parameters (no statistically significant relationships). Boxplots show minimum values, the lower quantile (Q 0.25), the median (Q 0.5), the upper quantile (Q 0.75) and maximum values of $\Delta\text{runout}_{\text{ref}}$. Points are relative positions of extreme values.

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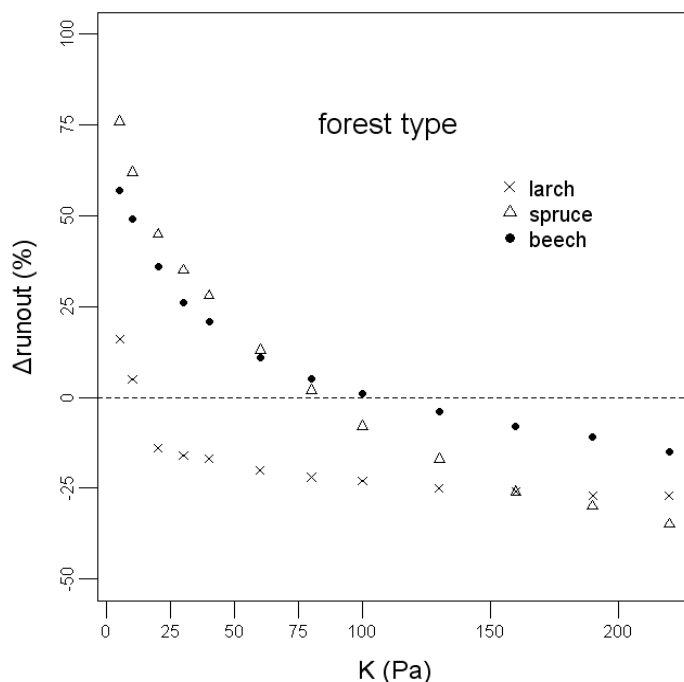


Fig. 4. Mean values of Δrunout for each applied K value calculated separately for the three forest type categories. The dashed line corresponds to $\Delta\text{runout} = 0$ indicating the potential mean optimal K value for each category.

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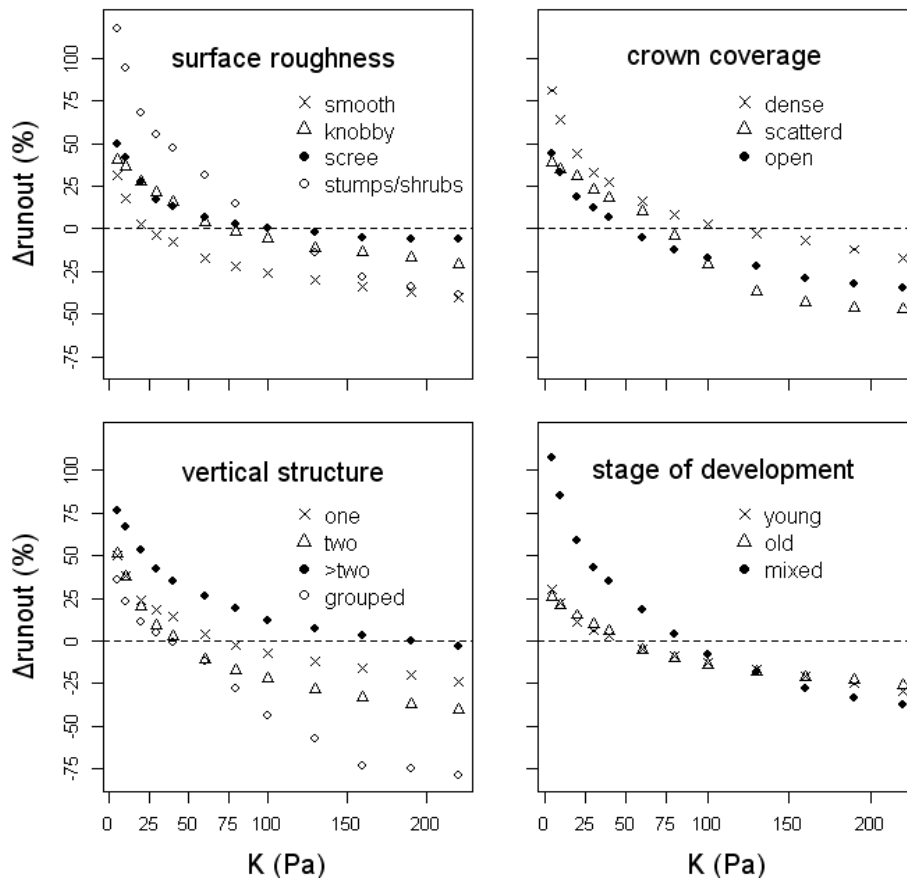


Fig. 5. Mean values of Δ runout for each applied K value calculated separately for the corresponding categories of four forest variables. The dashed line corresponds to Δ runout = 0 indicating the potential mean optimal K value for each category of the respective forest variable.

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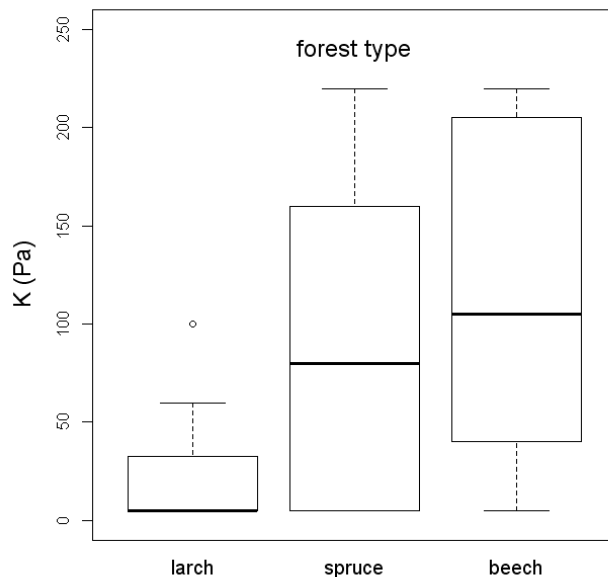


Fig. 6. Optimal K values (K_{opt}) assigned to each observed avalanche based on simulations with varying values of K shown for subsets of different forest types. Boxplots show minimum values, the lower quantile (Q 0.25), the median (Q 0.5), the upper quantile (Q 0.75) and maximum values of K_{opt} . Point is relative position of extreme value.

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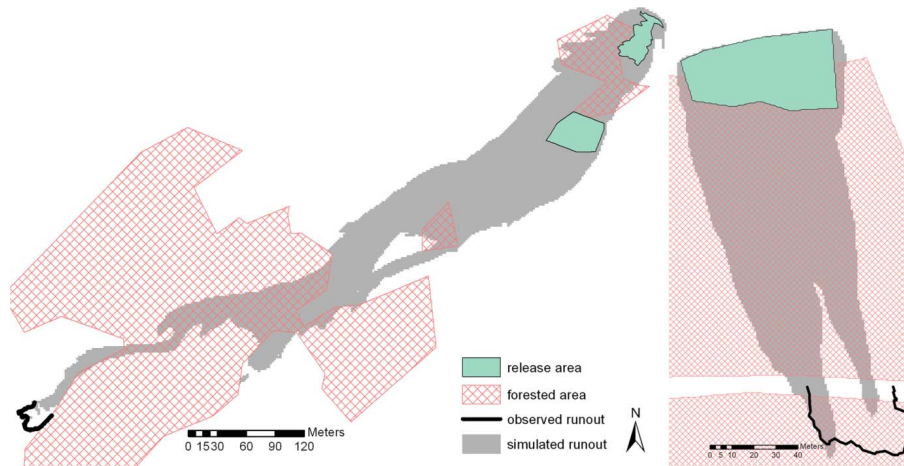


Fig. 7. Simulation results gained with RAMMS including the forest detrainment function by applying the “best” value for the detrainment coefficient K for forested areas in comparison to the observed runout distances of the two case studies “Dischma valley” (left) and “Brecherspitz” (right).

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Fig. 8. Snow detoured by a stump highlighting the significant effect of surface roughness on small-scale avalanches which should be considered in avalanche simulations.

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