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A data-based comparison of flood frequency analysis methods used in France

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Abstract

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Many flood frequency analysis (FFA) implementations are used in operational practice in France. These implementations range from the estimation of a pre-specified distribution to continuous simulation approaches using a rainfall simulator coupled with a rainfall-runoff model. This diversity of approaches raises questions regarding the optimal ambits of each implementation and calls for a nation-wide comparison of their

predictive performances. This paper presents the results of a national comparison of the main FFA imple-

Inis paper presents the results of a national comparison of the main FFA implementations used in France. More accurately, eight implementations are considered,
 corresponding to the local, regional and local-regional estimation of Gumbel and Generalized Extreme Value (GEV) distributions, as well as the local and regional estimation of a continuous simulation approach eventually resulted in a local and a regional version. A data-based comparison framework is applied to these eight competitors to evaluate their predictive performances in terms of reliability and stability, using daily
 flow data data from more than one thousand gauging stations in France.

Results from this comparative exercise suggest that two implementations dominate their competitors in terms of predictive performances, namely the local version of the continuous simulation approach and the local-regional estimation of a GEV distribution. More specific conclusions include the following: (i) the Gumbel distribution is not evitable for Mediterraneon estebacements since this distribution demonstrable loads to

²⁰ suitable for Mediterranean catchments, since this distribution demonstrably leads to an underestimation of flood quantiles; (ii) the local estimation of a GEV distribution is not recommended, because the difficulty in estimating the shape parameter results in frequent predictive failures; (iii) all the purely regional implementations evaluated in this study displayed a quite poor reliability, suggesting that prediction in completely ²⁵ ungauged catchments remains a challenge.





1 Introduction

1.1 Diversity of Flood Frequency Analysis approaches

The Flood Frequency Analysis (FFA) is a central step in a hydrological risk assessment. It has many operational applications including design of civil engineering structures
 (e.g. dam spillways, protection structures for nuclear power plant) or mapping of flood-prone areas. Many FFA approaches exist in the literature. In France, two distinct families of approach are used in practice. The first family comprises FFA implementations that estimate the parameters of a given flood distribution (a Gumbel or a Generalized Extreme Value (GEV) distribution in most cases). The second family uses a continuous simulation approach (Arnaud and Lavabre, 1999, 2002), where a rainfall generator is coupled with a rainfall-runoff model to generate long hydrological series from which extreme quantiles can be inferred. Within both families, parameter estimation can be performed at the local scale using at-site streamflow data only (e.g. Kuczera, 1999; Martins and Stedinger, 2000), at the regional scale using streamflow data from neighboring stations only (e.g. Stedinger and Tasker, 1985, 1986; Hosking and Wallis, 1997),

boring stations only (e.g. Stedinger and Tasker, 1985, 1986; Hosking and Wallis, 1997), or combining local and regional information (e.g. Ribatet et al., 2006).

Many countries prepared and issued national FFA guidelines to help practitioners in realizing their analyses with best practice methods (e.g. Reed et al., 1999; Institution of Engineers Australia, 1987; Interagency Advisory Committee on Water Data, 1982; Stewart et al., 2008). This is not the case in France, where no specific FFA

1982; Stewart et al., 2008). This is not the case in France, where no specific FFA implementation is officially recommended, let alone prescribed by regulation. While practitioners-oriented documents describing the main approaches to FFA have been published (Lang et al., 2007), an extensive comparison of the main FFA implementations used in operational practice in France remains to be performed.





1.2 Challenges facing the evaluation and comparison of FFA approaches

A large number of comparative studies of FFA implementations have been reported in the research literature (e.g. Hosking et al., 1985; Gunasekara and Cunnane, 1992; Kroll and Stedinger, 1996; GREHYS, 1996; Ouarda et al., 2006; Meshgi and Khalili, 2009;

- Sankarasubramanian and Srinivasan, 1999). The comparison framework varies from one study to another, and can be based on Monte Carlo simulations, statistical tests, graphical methods and so on. Bobee et al. (1993) therefore advocated "a systematic approach to comparing distributions used in flood frequency analysis", which is still not agreed upon to our best knowledge.
- In the context of the present paper, where distinct FFA families are to be compared, the comparison framework can hardly be based on Monte Carlo simulations. Indeed, this would require setting up a synthetic experiment to generate "true" data that can be used by all FFA implementations. Ensuring a "fair" simulation setup that would not advantage a particular FFA implementation is feasible when similar implementations
- are considered (e.g. comparing several local estimation methods for a given distribution). However, it is more difficult when both local and regional estimation approaches are considered: how to realistically simulate spatially dependent extremes on a river network? What is a realistic misspecification of the regression model used in regional approaches? Ensuring the fairness of the simulation setup is even more challenging
- ²⁰ if continuous simulation approaches are considered (How to realistically simulate the non-linearity of the rainfall-runoff relationship? How to simulate realistic structural errors for the rainfall simulator or the hydrologic model?).

An alternative to Monte-Carlo comparisons is to implement data-based predictive comparisons, where the estimations from all competing FFA implementations are sim-

²⁵ ply compared with validation data (Gunasekara and Cunnane, 1992; Interagency Advisory Committee on Water Data, 1982). Recently, Renard et al. (2013) proposed a databased comparison framework that could be applied to any FFA implementation. This framework complements (but not replaces) alternative comparison methods based,



for instance, on Monte Carlo simulations. What is most important, this framework enables the comparison of any FFA implementation belonging to each family presented in Sect. 1.1.

1.3 Objectives of the paper

⁵ In this paper we present and compare the results a nation-wide comparison of the predictive performances of FFA implementations in order to find the optimal ambits of each implementation and, if possible, recommend the best FFA methodology for the French rivers.

The paper is built as follows. Section 2 presents the data and methods used in this paper, including the competing FFA implementations (Sect. 2.2), a summary of the comparison framework (Sect. 2.3) and the comparison dataset (Sect. 2.4). Section 3 describes the main results of the comparison, and Sect. 4 further discusses them. Conclusion are drawn in Sect. 5.

2 Data and methods

15 2.1 Short description of the ExtraFlo project

By their nature and danger, the extreme floods cannot be observed often and thoroughly enough to collect the sample of catastrophes adequate for further statistical analysis. Instead, the probabilistic study of extreme values relies on analysis of a limited (in number and space) series of events in time, to infer a probabilistic behaviour of a particular case which is then extrapolated to the whole population of floods. This

- ²⁰ of a particular case which is then extrapolated to the whole population of floods. This procedure encounter certain difficulties:
 - How to extrapolate excessively short time series, when information is generally available on more or less recent events.





- How to set design values for the whole of the territory, whereas the density of the measurement is inevitably limited owing to the spatial variability of rainfall and discharge data.
- How to update our knowledge of extreme events in a non-stationary context.
- ⁵ The objective of the ExtraFlo project (Extreme Rainfall and Floods) was to carry out an inter-comparison of the methods for estimating extreme rainfall and floods used in France, to obtain a better understanding of their respective fields of application. A particular emphasis was placed on compiling reference data files (long at-site time series and regional sets) to pinpoint the pros and cons of each approach with their sensitivity
- to the increasing information. As a result of this work new methods for estimating of extreme values of floods were developed and improved. Moreover, the project placed a range of practical tools concerning the management of flood risk that can be estimated not only according by the hydrological characteristics of river basins but also on the basis of available information.

15 2.2 Competing teams: FFA implementations

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Eight implementations that are frequently used in France are compared in this paper. Note that other approaches are also used in operational practice, in particular the SCHADEX semi-continuous simulation approach (Paquet et al., 2006) or the SPEED method (Cayla, 1995). However they could not be included in this comparative exercise because they could not be fully automated and were therefore not adapted to an application to thousands of sites (see Sect. 2.4). The eight competing implementa-

tions are split according to their estimation scale: purely local, purely regional or mixed local-regional.

2.2.1 The local league: using at-site runoff data only

 $_{\mbox{\tiny 25}}$ The local league contains the following three implementations:





1. Implementation LOC-GUM, corresponding to the estimation of a two-parameter Gumbel distribution using at-site annual maxima (see the Appendix Sect. A1 for details on the Gumbel distribution). A Bayesian estimation is performed, with flat priors ($\pi(\theta) \propto 1$) for both the location and the scale parameters. Maximumposterior values are used as parameter estimates.

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- 2. Implementation LOC-GEV, corresponding to the estimation of a three-parameter GEV distribution using at-site annual maxima (see the Appendix Sect. A1 for details on the GEV distribution). A Bayesian estimation is also performed, with flat priors ($\pi(\theta) \propto 1$) for the location and the scale parameters, and a Gaussian prior with mean zero and standard deviation 0.25 for the shape parameter.
- 3. Implementation LOC-SHY is the local version of the SHYREG method, a continuous simulation approach, coupling a rainfall generator with a rainfall-runoff model to estimate flood quantiles. A description of the various versions of SHYREG can be found in Arnaud and Lavabre (2002), Aubert (2013) and Organde et al. (2013). Note that LOC-SHY uses a regionalized version of the rainfall generator, but is local with respect to discharge data in the sense that the rainfall-runoff model is estimated with local data.

For the first two implementations, the Gumbel and GEV distributions are chosen because they are the most widely used methods in hydrological projects in France (despite the fact that there is no prescribed distribution officially recommended for FFA in France). Moreover, preliminary analyses (not shown) indicated that they performed at least equally well as other distributions, including Log-Normal, Pearson III or Log-Pearson III distributions. The choice of the Bayesian estimation approach is made to facilitate the use of a unique estimation approach at local, regional and local-regional scales. Preliminary analyses (Kochanek et al., 2012; Renard et al., 2013) show that the impact of the estimation approach (e.g. Bayesian, maximum likelihood, moments, linear moments) is small compared to the choice of the parent distribution or the choice of the estimation scale (local, regional or local-regional).





2.2.2 The regional league: estimation in ungauged catchments

The regional league contains the following three implementations:

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- 1. Implementation REG-GUM, corresponding to the regional estimation of a Gumbel distribution by means of regressions linking its parameters with catchment characteristics.
- 2. Implementation REG-GEV, corresponding to the regional estimation of a GEV distribution.
- 3. Implementation REG-SHY, the fully regionalized version of the continuous simulation implementation SHYREG (Aubert, 2013; Organde et al., 2013).
- ¹⁰ The Appendix Sect. A2 provide additional details on the regionalisation procedures for the first two implementations. Again, the choice of these particular two implementations is based on preliminary analyses (Cipriani et al., 2012) that are not fully described here.

2.2.3 The local-regional league: combining at-site data and regional information

The local-regional league contains the following two implementations:

- 15 **1.** Implementation L+R-GUM, corresponding to the local-regional estimation of a Gumbel distribution, using both local and regional information.
 - 2. Implementation L+R-GEV, corresponding to the local-regional estimation of a GEV distribution.

The combination of local and regional information is straightforward in the Bayesian context adopted here: regional estimates are used to specify a prior distribution, while local data are used to compute the likelihood function (see the Appendix Sect. A3 for additional details).

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2.3 Referees: stability and reliability indices

The evaluation criteria are based on performance indices quantifying the reliability and the stability of the FFA implementations. A complete description of the motivation behind these performance indices is given in Renard et al. (2013). In this paper we there-

⁵ fore restrict ourselves to a short presentation of these indices and their practical use to compare FFA implementations.

2.3.1 Reliability indices

The *reliability* indices aim to evaluate the agreement between the estimated distribution at site *i* (whose CDF is noted $\hat{F}^{(i)}$) and validation observations $\left(d_{k}^{(i)}\right)_{k=1:p^{(i)}}$. Impor-

tantly, this requires splitting available data into calibration and validation subsamples. The decomposition adopted in this paper will be described in Sect. 2.4.2.

The *FF* index, used e.g. by England et al. (2003) and Garavaglia et al. (2011), corresponds to the CDF of the estimated distribution computed on the maximum observed validation data. For a given site i, it is computed as follows:

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$$FF^{(i)} = \hat{F}^{(i)}(d_{\max}^{(i)})$$

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If the estimation is reliable (i.e. $\hat{F}^{(i)} = F^{(i)}$, where $F^{(i)}$ denotes the unknown true CDF), it can be shown (Renard et al., 2013) that $FF^{(i)}$ is a realization from a Kumaraswamy distribution with parameters ($n^{(i)}$; (1): $FF^{(i)} \sim K[n^{(i)}; 1]$, whose CDF F_K can be written as $F_K(t) = t^{n^{(i)}}$, $0 \le t \le 1$. The *FF* index focuses on the right tail of the estimated CDF by using the largest element in the validation sample. The adequacy between $FF^{(i)}$ values observed over all validation sites and their theoretical Kumaraswamy distributions under the reliability hypothesis will be assessed using graphical diagnostics and reliability scores that will be described in Sects. 2.3.3 and 2.3.4.

The second reliability index is based on the number of exceedances (within the validation sample) of an estimated *T*-yr quantile $\hat{q}_{T}^{(i)}$ (e.g. Interagency Advisory Committee 4453



(1)



on Water Data, 1982; Gunasekara and Cunnane, 1992; Garavaglia et al., 2011):

$$N_{\mathcal{T}}^{(i)} = \sum_{k=1}^{n^{(i)}} \mathbf{1}_{\left(\hat{q}_{\mathcal{T}}^{(i)}; +\infty\right)} \left(d_{k}^{(i)}\right), \quad \text{where } \mathbf{1}_{\mathcal{A}}(x) = \begin{cases} 1 \text{ if } x \in \mathcal{A} \\ 0 \text{ otherwise} \end{cases}$$

Under the reliability assumption $(\hat{q}_{T}^{(i)} = q_{T}^{(i)})$, $N_{T}^{(i)}$ is a realization from the binomial distribution: $N_{T}^{(i)} \sim \text{Bin}(n^{(i)}, 1/T)$ (Renard et al., 2013). The N_{T} index focuses on reliability for prescribed *T*-yr quantiles. In this paper, we are going to analyze $N_{T=10}$ and $N_{T=100}$ values for 10-yr and 100-yr floods, respectively.

2.3.2 Stability index

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The *stability* of quantile estimates can be quantified by contrasting the values obtained with two different calibration datasets c_1 and c_2 . The decomposition into two calibration subsamples adopted in this paper will be described in Sect. 2.4.2. We stress that stability is only a secondary consideration compared to reliability: indeed, an FFA implementation can be totally unreliable but perfectly stable. Consequently, stability is seen as an additional quality used to further discriminate FFA implementations that

¹⁵ The index SPAN_T (Garavaglia et al., 2011) used in this paper is a measure of the relative deviation between the two estimated *T*-yr quantiles. For a given site *i*, it is defined as follows:

$$SPAN_{T}^{(i)} = 2 \frac{\left| \hat{q}_{T}^{(i)}(\boldsymbol{c}_{1}) - \hat{q}_{T}^{(i)}(\boldsymbol{c}_{2}) \right|}{\hat{q}_{T}^{(i)}(\boldsymbol{c}_{1}) + \hat{q}_{T}^{(i)}(\boldsymbol{c}_{2})}$$

would have similar reliability.

The FFA implementation whose SPAN_{7} is closest to zero is the most stable.



(2)

(3)



2.3.3 Graphical representations

Reliability

Graphical representation of reliability is based on the comparison between the calculated indices and their theoretical distribution under the reliability assumption. Note that

- ⁵ for both reliability indices, this theoretical distribution depends on the number of validation observations $n^{(i)}$, that may vary from site to site. To circumvent this problem, a probability-probability plot (pp-plot) representation is adopted: raw indices are transformed into probabilities by applying the CDF of their theoretical distribution under the reliability hypothesis. Under the reliability hypothesis, the probability-transformed val-
- ¹⁰ ues are then uniformly distributed between 0 and 1, regardless of the sample size $n^{(i)}$. It is therefore possible to plot the probability-transformed values for all sites against empirical frequencies, yielding reliability pp-plots as illustrated in Fig. 1. Curves closer to the diagonal correspond to more reliable FFA implementations.

Note that for the N_T index, the theoretical binomial distribution is a discrete distribution. It is therefore necessary to randomize its probability-transformed values in order to ensure that they are uniformly distributed. The randomization procedure is described in Renard et al. (2013).

Stability

The comparison of stability between competing FFA implementations is based on com-

²⁰ paring the distribution of SPAN^(*i*)_{*T*} over all sites $i = 1 : N_{\text{sites}}$, as illustrated in Fig. 1. The FFA implementation whose SPAN_{*T*} distribution remains the closest to zero is the most stable.

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2.3.4 Scores

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The graphical representations can be further summarized into numerical scores that will provide a more synthetic view of the performances of FFA implementations over the various performance indices.

⁵ For reliability indices *FF* and N_T , the score is based on the area between the diagonal line and the reliability curve, with a normalization ensuring that the score is varying between 0 (low reliability) and 1 (perfect reliability). For any probability-transformed index *w*, the score can be computed as:

score = $1 - 2 \cdot \text{Area}(\text{curve}, \text{diagonal})$

$$= 1 - \frac{2}{N_{\text{site}} + 1} \sum_{i=1}^{N_{\text{site}}} \left| w^{(i)} - \frac{i - 0.5}{N_{\text{site}}} \right|$$
(4)

Analogically, a stability score can be derived based on the area between the y axis and the SPAN_T curve, normalized to vary between 0 (low stability) and 1 (perfect stability):

score = $1 - 0.5 \cdot \text{Area}(\text{curve}, y \text{ axis})$

$$= 1 - \frac{1}{2N_{\text{site}}} \sum_{i=1}^{N_{\text{site}}} \text{SPAN}_{T}^{(i)}$$

15 2.4 Playground: daily runoff dataset

2.4.1 Dataset description

Daily runoff series from 1076 gauging stations located throughout France are used (see Fig. 2). Catchment sizes range from 10 to 2000 km^2 . All series have at least 20 yr of data (20–39 yr: 535 stations (49.7 %); 40–59 yr: 476 stations (44.2 %); 60 yr and more: 65 stations (6.1 %)). The quality-control procedures have been implemented to remove stations with measurement problems or stations corresponding to heavily regulated catchments (Renard et al., 2008).



(5)



These 1076 gauging stations are representative of the main hydrological and climate regimes found in mainland France. For regime-specific analyses, it is useful to cluster these stations into homogenous regions. This is achieved by using the hydroecoregions defined by Wasson et al. (2004), as illustrated in Fig. 2.

5 2.4.2 Reliability and stability decompositions

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As explained in Sect. 2.3, the computation of reliability indices requires decomposing of all dataset time series into calibration-validation subsamples. For stability the datasets are also divided into two subsamples: calibration dataset no. 1 (c_1) and calibration dataset no. 2 (c_2). These decompositions are performed as follows: for reliability, the 593 series with 20 to 40 yr of data are used to calibrate regional implementations, or the regional part of local-regional implementations. The remaining 483 series (with more than 40 yr of data) are further decomposed:

- 20 yr are randomly chosen (independently on each site) to calibrate local implementations, or the local part of local-regional implementations.
- All remaining years (at least 20 yr) are used as validation data. Importantly, the validation data are therefore exactly the same for all implementations.

For stability, two distinct types of decompositions are implemented:

- The type I decomposition focuses on stability with respect to local data: for each of the 483 series with more than 40 yr, 20 yr are randomly assigned to the c_1 subsample, and 20 other years are randomly assigned to the c_2 subsample. Obviously, purely regional implementations are insensitive to this decomposition, since they do not use local data.
- The type II decomposition focuses on stability with respect to regional data: the 593 series with 20 to 40 yr of data are randomly split into two subsamples c_1 and
- c_2 . Obviously, purely local implementations are insensitive to this decomposition, since they do not use regional data.





3 Results

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3.1 Comparison of quantile estimates

Before describing the comparison in terms of reliability and stability, it is of interest to assess how different the various competing implementations are. To this aim, Fig. 3 compares the 100-yr flood estimated by each implementation with the one estimated by the implementation LOC_GUM, considered as the reference in this figure.

Both local implementations LOC_GEV and LOC-SHY systematically yields larger quantiles in South-Eastern France (sometimes exceeding +40%). Elsewhere in the country, smaller and larger quantiles are found with no clear spatial pattern for implementation LOC_GEV, while LOC-SHY quantiles tend to be systematically larger than LOC_GUM ones.

The local-regional implementation L+R_GUM generally yields small differences with the reference, suggesting that for a Gumbel distribution, local and local-regional estimations yield similar estimates. By contrast, The local-regional implementation L+R_GEV yields markedly higher quantiles in South-Eastern France.

All three regional implementations REG_GUM, REG_GEV and REG-SHY yield marked differences (both positive and negative) with the reference, but no distinctive spatial pattern can be observed. This suggests that the estimation scale (local or regional) has an important impact on quantile estimates.

20 3.2 Results for the local league

Figure 1 shows reliability and stability indices for the regional implementations. Amongst them, LOC-SHY clearly outperforms its two opponents (LOC_GUM and LOC_GEV): it is both more reliable (especially for extreme values, index *FF*) and more stable. The poor performance of the locally-estimated GEV distribution is worth not-

²⁵ ing: it is markedly unreliable and much less stable than other implementations (especially for high quantiles). The behavior of the *FF* curves near the upper-right corner is





noteworthy: it indicates that for about 20 % of the stations, a flood observed during the validation period was deemed impossible by LOC-GEV (yielding *FF* values equal to one). This is due to errors in estimating the shape parameter of the GEV distribution, yielding an upper bound for the estimated GEV pdf that is exceeded during the valida-

tion period. Note that this does not imply that the GEV distribution should be avoided: the problem might rather be due to its local estimation, as will be further discussed in Sect. 3.4.

3.3 Results for the regional league

Figure 4 shows reliability indices for regional implementations and shows that none of them reach an acceptable reliability. The continuous simulation implementation REG-SHY appears more reliable for index *FF*, but still yields unreliable predictions for the 10yr flood, as shown by index N_{10} . More detailed analyses (not shown here) suggest that the main reason for such poor performances is the difficulty in setting up a regression with catchments' characteristics: the explanatory power of such regressions remain quite low and result in unreliable predictions at ungauged sites.

3.4 Results for the local-regional league

Figure 5 shows reliability and stability indices for the two local-regional implementations for Gumbel and GEV distributions. Both implementations yield similar results: the reliability is acceptable and stabilities are similar. The use of a GEV distribution
²⁰ yields slightly more reliable predictions according to index *FF*, at the cost of a slightly lower stability with respect to regional information (type II). The differences between the Gumbel and GEV distributions will be further discussed in Sect. 3.5.

It is important to notice that the local-regional estimation of a GEV distribution yields acceptable reliability and stability, which was not the case for purely local or regional estimation approaches. This is illustrated in Fig. 6, which compares those three estima-

estimation approaches. This is illustrated in Fig. 6, which compares those three estimation approaches. In terms of reliability, implementation L+R_GEV clearly outperforms





its two opponents for both indices *FF* and N_{10} . In terms of stability, implementation L+R_GEV appears much more stable than both its purely local counterpart (type I stability) and its purely regional counterpart (Type II stability). These observations confirm that the GEV distribution is a sensible candidate for FFA, but that reliably estimating this distribution requires using both local and regional information.

3.5 Stratification by region

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The results were presented so far at the scale of the whole country. However, Sect. 3.1 suggested that the differences between some implementations followed specific regional patterns. Figure 7 therefore shows reliability indices for Mediterranean (top, corresponding to regions 6 and 8 in Fig. 2) and Oceanic (bottom, regions 9, 10, 12 and 13 in Fig. 2) catchments. For readability, only implementations LOC-SHY, L+R_GUM and L+R_GEV (which appear to be the most reliable ones) are presented.

For Mediterranean catchments, the use of a Gumbel distribution (L+R_GUM) consistently yields below-diagonal reliability curves, denoting a tendency to underestimate

quantiles. On the other hand, both implementations LOC-SHY and L+R_GEV yield acceptably similar reliability diagnostics. A tendency to slightly over-estimate large quantiles (indices FF and N_{100}) might be suspected for LOC-SHY.

For Oceanic catchments, all three implementations yield similar results, suggesting that the evidence for rejecting the Gumbel distribution is weak in this region. We note

however that using a GEV distribution does not deteriorate reliability (as long as it is estimated with a local-regional approach), and might therefore be preferred to the Gumbel distribution for its larger flexibility.

Lastly, a note of caution is made for this figure regarding the indices N_{10} and N_{100} . It might appear surprising at first sight that curves are closer from the diagonal for N_{10} than for N_{100} . However, this does not suggest that estimates of the 10-yr flood are more reliable that estimates of the 100-yr flood. Indeed, while comparing implementations for a given reliability index makes complete sense, direct comparison of reliability indices for an implementation is not meaningful, because the power to detect non-reliability



strongly varies from index to index. In this particular case, curves appear closer from the diagonal for N_{100} mostly because detecting failures in the estimation of the 100-yr flood is much more challenging than for the 10-yr flood, given the available sample size.

5 3.6 Summary for all implementations

Results for all implementations can be summarized by means of the reliability and stability scores described in Sect. 2.3.4. Figure 8 shows these scores on a radar plot, which allows confirming that the best overall competitors are LOC-SHY and L+R_GEV. LOC-SHY yields the highest stability scores, and the highest reliability scores for indices *FF* and *N*₁₀₀. L+R_GEV has a higher score for index *N*₁₀, and might be slightly more reliable than LOC-SHY for Mediterranean catchments. Note that implementation L+R_GUM is not considered as a finalist because, despite its excellent stability, it is systematically less reliable than LOC-SHY or L+R_GEV, and has been shown to be inadequate in the Mediterranean region (Sect. 3.5).

15 4 Discussion

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4.1 Results for different local sample sizes

The results presented in this paper are conditional on the particular decompositions that were set up for stability and reliability assessments, and more precisely, on the sample size of 20 yr for local data. One may therefore question whether the main findings of this study would still hold with different sample sizes.

Figure 9 indicates that the performances of the local-regional implementation L+R_GEV and of LOC-SHY are not very sensitive to the local sample size. On the other hand, the performances of the local implementation LOC_GEV strongly deteriorate when the local sample size decreases. This indicates that the general conclusions summarized in Sect. 3.6 hold even more markedly with short samples.





Unfortunately, evaluating how performances evolve with larger samples is more challenging within this data-based comparison framework: indeed, the available series are not long enough to implement insightful calibration-validation decompositions with e.g. 40 yr used for calibration. The performance of local implementations is likely to improve with largest calibration samples. However, whether or not this would suffice to bridge the gap with the best implementations (L+R_GEV and LOC-SHY) remains to be seen. Monte-Carlo experiments suggest that estimation errors can remain guite large even

with "long" series of 40–50 yr (not shown). This suggests that the benefit of complementing local data with either regional information (L+R_GEV) or information on the rainfall-runoff relationship (LOC-SHY) may well remain significant with larger samples.

4.2 Comparison with literature results

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Some results described in this paper have already been partly reported in the literature. In particular, the difficulty to locally estimate a GEV distribution with relatively short samples has been demonstrated through Monte-Carlo experiments (e.g. Martins

and Stedinger, 2000). The data-based comparison exercise described in this paper indicates that the resulting estimation errors lead to poor predictive performances that can also be demonstrated on real data.

The main original results brought by this study are related to the comparison between distinct families of FFA implementations, including two distinct paradigms (estimation of

- a pre-specified distribution vs. continuous simulation) and several estimation scales (local, regional, local-regional). Such between-family comparisons are much more scarce in the literature. As far as we know, there have been no study that reported Monte-Carlo investigations to compare such distinct families, which is most probably due to the difficulty in setting up a fair Monte-Carlo experiment, as explained in the introduc-
- tion. Some authors compared the estimates arising from distinct families (e.g. Neppel et al., 2007), but they restricted to describing the differences between families, as opposed to ranking them according to their predictive performances. The evaluation carried out in this paper moves one step further by assessing and comparing predictive





performances, which is necessarily a data-based exercise. For instance, the fact that the continuous simulation implementation LOC-SHY yields reliable predictions could not have been convincingly demonstrated using Monte-Carlo simulations only (see discussion in Sect. 1.2).

5 4.3 Limitations of the comparison framework

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While the comparison framework yielded valuable insights on the relative merits of distinct implementations, it is still affected by several limitations that are discussed here. Firstly, the ability to detect predictive failures for large quantiles is restricted by the length of available data. With the typical sample sizes (40–100 yr), demonstrating a prediction failure for a 1000- or 10 000-yr quantile (which are of interest for risky structures such as dams or nuclear plants, for instance) is affected by huge uncertainty. It is therefore unclear whether the good performances of some implementations (LOC-SHY and L+R_GEV), as evaluated with limited sample sizes, still hold for extreme quantiles. On the other hand, the implementations showing poor performances have no reason to become highly capable when extrapolated to extreme quantiles, and can, therefore, be discarded.

A second limitation is that the comparison framework only produces global performance diagnostics, computed over a large number of sites. As a consequence, one should keep in mind that an implementation with excellent global performance may still fail on one or a few particular sites, without such isolated failures being detected by the global performance diagnostics.

Lastly, we stress that the comparison described in this paper was carried out with daily runoff (whose availability is much better than runoff recorded at a shorter time step). The good performance of some implementations (LOC-SHY and L+R_GEV) re-

²⁵ mains to be confirmed for shorter time steps, which are also of primary interest in engineering practice (e.g. flood peak estimation for flood design).





5 Conclusions

The objective of this paper was to report the results of a national comparison of the main FFA approaches used in France. This comparison was performed within a databased framework, which enabled a direct assessment of the predictive performances of candidate FFA approaches. The main conclusions that can be drawn from the work

- can be summarized in the following points:
 - Two approaches, namely the local version of SHYREG and the local-regional estimation of a GEV distribution, seem to provide generally satisfactory results in terms of reliability and stability. The differences between the quantiles estimated by these two approaches are technically moderate.
 - 2. In general, a local-regional estimation approach yields at least as good performances as its purely local or regional counterpart, and in some cases, it even clearly outperforms both of them.
 - 3. In the oceanic-influenced catchments, the use of a Gumbel distribution seems acceptable. Local estimates yield relatively good performance indices. However the use of both the Gumbel or the GEV distribution within the mixed local-regional estimation approach results in similar or slightly improved reliability and stability indices.
 - 4. In the Mediterranean area, we would not recommend to use the Gumbel distribution, because it demonstrably underestimates quantiles. However, the local estimation of a GEV distribution is not recommended either, because the difficulty in estimating the shape parameter results in a clear lack of reliability. Therefore we recommend using LOC-SHY or local-regional mixed procedure for estimating the GEV-based quantiles in this area.





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5. Estimation of flood quantiles in ungauged catchments remains a genuine challenge: all competing regional approaches evaluated in this work lead to a quite low reliability.

Appendix A

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5 FFA implementations – basic formulae

A1 Local implementations

The PDF and CDF of the Gumbel distribution are:

$$f(x) = \frac{1}{\lambda} \exp\left(-\frac{x-\mu}{\lambda} - \exp\left(-\frac{x-\mu}{\lambda}\right)\right)$$

$$F(x) = \exp\left[-\exp\left(-\frac{x-\mu}{\lambda}\right)\right]$$

$$\lambda > 0,$$
(A1)

where μ and λ are the location and the scale parameters. The PDF and CDF of the GEV distribution are:

$$f(x) = \frac{1}{\lambda} \left(1 - \frac{\xi(x-\mu)}{\lambda} \right)^{\frac{1}{\xi} - 1} \exp\left(- \left(1 - \frac{\xi(x-\mu)}{\lambda} \right)^{\frac{1}{\xi}} \right)$$

$$F(x) = \exp\left(- \left(1 - \frac{\xi(x-\mu)}{\lambda} \right)^{\frac{1}{\xi}} \right)$$

$$\lambda > 0, \xi \neq 0, 1 - \frac{\xi(x-\mu)}{\lambda} > 0,$$

(A2)

where μ , λ and ξ are the location, scale and shape parameters.

Note that three families of distributions can be obtained depending of the value of the shape distribution: the Frechet family ($\xi < 0$, left-bounded distribution), the Weibull family ($\xi > 0$, right-bounded distribution) and the Gumbel family ($\xi \rightarrow 0$, unbounded distribution).





A2 Regional implementations

The regional estimation of Gumbel and GEV distributions uses a regression to link locally-estimated parameters with catchment characteristics. Let θ_i denote the locally-estimated location or scale parameter at site *i*, σ_i denote its estimation standard devi-

ation (i.e. the posterior standard deviation in this Bayesian context), and $x_i^{(1)}, \ldots, x_i^{(N_{cov})}$ denote a set of N_{cov} catchment characteristics used as covariates. The regression model for location and scale parameters can be written as follows:

$$\log(\theta_i) = \beta_0 + \sum_{j=1}^{N_{\text{cov}}} \beta_j x_i^{(j)} + \varepsilon_i, \varepsilon_i \sim N(0, \sqrt{\sigma_{\varepsilon}^2 + \sigma_i^2}).$$
(A3)

For the GEV distribution, and additional regression is required for the shape param-10 eter. Since no significant relationship with catchment characteristics could be found, a 11 constant regression is specified as follows:

$$\xi_i = \beta_0 + \varepsilon_i, \varepsilon_i \sim N(0, \sqrt{\sigma_{\varepsilon}^2 + \sigma_i^2})$$
(A4)

Catchment characteristics are selected following Cipriani et al. (2012): (i) catchment area; (ii) mean elevation; (iii) mean 10-yr rainfall (as given by Benichou and Le Breton, 1987); (iv) mean IDPR index (Index of Development and Persistence of the River networks (Mardhel et al., 2004), used as a proxy for the infiltration capacity). Moreover, regressions are estimated separately for each of the regions shown in Fig. 2. A Bayesian estimation is used (with flat priors on $(\beta_0, ..., \beta_{N_{cov}}, \log(\sigma_{\varepsilon}))$).

A3 Local-regional implementations

In local-regional implementations, a regional estimation is first applied to derive a prior distribution. At a given site i, the prior distribution of the location parameter is given





by: $\log(\mu_i) \sim N(\hat{\mu}_i, \hat{\sigma}_{\varepsilon}^{(\mu)})$. $\hat{\mu}_i$ is computed by applying the regression in Eq. (A3), i.e. $\hat{\mu}_i = \exp\left(\hat{\beta}_0 + \sum_{j=1}^{N_{cov}} \hat{\beta}_j x_i^{(j)}\right)$, and $\hat{\sigma}_{\varepsilon}^{(\mu)}$ is the estimated standard deviation of regression errors. Similarly, priors for the scale and shape parameters are given by:

- Scale: $\log(\lambda_i) \sim N(\hat{\lambda}_i, \hat{\sigma}_{\varepsilon}^{(\lambda)})$
- [GEV only] Shape: $\xi_i \sim N(\hat{\xi}_i, \hat{\sigma}_{\varepsilon}^{(\xi)})$

At-site data are then used to compute the likelihood, and the posterior distribution therefore combines local and regional information.

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Fig. 1. Reliability (*FF*, N_{10}) and stability (SPAN₁₀, SPAN₁₀₀) indices for local implementations.







Fig. 2. Location of the gauging stations used in this study.

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Fig. 3. Relative differences between 0.99-quantiles.





Fig. 4. Reliability indices for regional implementations.







Fig. 5. Reliability (FF, N10) and stability (SPAN100 – type I, SPAN100 – type II) indices for local-regional implementations.







Fig. 6. Reliability (FF, N10) and stability (SPAN100 – type I, SPAN100 – type II) indices for local, regional and local-regional estimation of a GEV distribution.







Fig. 7. Reliability indices for Mediterranean (top) and Oceanic (bottom) catchments.





Fig. 8. Summary of reliability and stability scores for all implementations.







Fig. 9. Reliability (FF, N10) and stability (SPAN100 – type I, SPAN100 – type II) indices for three implementations, using 10 or 20 yr of local data for calibration.



