



*Supplement of*

## **Comparison of debris flow observations, including fine-sediment grain size and composition and runout model results, at Illgraben, Swiss Alps**

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**Figure S1: Video recordings of debris flows. The video camera is placed at the Survey Station (see Figure 1c in main text)**



**Table S1: Measurements from monitoring station at the Illgraben**

| Event start             | Front velocity CD 28-29 (m/s) | Max flow depth laser (m) | Max flow depth radar (m) | Mean bulk density laser (kg/m <sup>3</sup> ) | Peak velocity (quantile 0.99) laser CD 28-29 (m/s) | Peak velocity (quantile 0.99) radar CD 28-29 (m/s) | Peak discharge (quantile 0.99) laser CD 28-29 (m/s) | Volume laser CD 28-29 (m <sup>3</sup> ) | Flow duration (min) |
|-------------------------|-------------------------------|--------------------------|--------------------------|--|--|--|---|---|---------------------|
| <b>21.06.2019 21:44</b> | 6.62                          | 3.13                     | 2.69                     | 1870   | 6.55   | 6.57   | 147.61  | 97394                                   | 43                  |
| <b>02.07.2019 01:26</b> | 3.86                          | 1.75                     | 1.73                     | 1971   | 5.78   | 5.38   | 65.58   | 73188                                   | 52                  |
| <b>26.07.2019 19:46</b> | 8.69                          | 1.39                     | 1.41                     | 2223   | 9.74   | 9.98   | 93.26   | 113310                                  | 65                  |
| <b>11.08.2019 19:07</b> | 6.95                          | 1.81                     | 1.89                     | 2323   | 6.90   | 6.91   | 95.63   | 88064                                   | 88                  |
| <b>20.08.2019 19:03</b> | 0.89                          | 1.13                     | 1.10                     | 2031   | 1.36   | 1.36   | 8.06  | 6137                                    | 37                  |
| <b>24.06.2021 17:11</b> | 8.18                          | 2.40                     | 2.49                     | 1750   | 8.16   | 8.10   | 162.20  | 105032                                  | 38                  |
| <b>06.07.2021 20:43</b> | 8.69                          | 2.50                     | 2.58                     | 1605   | 8.65   | 8.67   | 186.61  | 76906                                   | 28                  |
| <b>16.07.2021 05:43</b> | 2.78                          | 2.38                     | 2.44                     | 1916   | 3.22   | 3.30   | 60.70   | 80879                                   | 77                  |
| <b>07.08.2021 16:22</b> | 2.32                          | 2.49                     | 2.17                     | 1884   | 2.89   | 2.74   | 41.19   | 38737                                   | 46                  |
| <b>19.09.2021 08:57</b> | 1.25                          | 1.13                     | 1.22                     | 1697   | 1.41   | 1.39   | 10.67   | 8538                                    | 43                  |
| <b>05.06.2022 12:33</b> | 3.39                          | 2.08                     | 2.15                     | 1690   | 4.14   | 4.32   | 55.42   | 39498                                   | 55                  |
| <b>04.07.2022 22:54</b> | 8.18                          | 2.49                     | 2.60                     | 1189   | 8.46   | 7.36   | 169.14  | 175929                                  | 39                  |
| <b>08.09.2022 02:06</b> | 1.91                          | 1.93                     | 1.77                     | 1592   | 1.85   | 1.87   | 20.94   | 9283                                    | 20                  |

**Table S2: Exemplary evaluation of the simulations of the debris flow event on 24.06.2021**

Table S2a: Input data composed of raster and shape files, simulation settings and measurements from the monitoring station.

| Event  | 24.06.2021     |
|--|----------------|
| DTM  | DTM_0.5.tif    |
| DTM resolution [m]                                 | 0.5            |
| calculation domain                                 | calcdom.shp    |
| release area                                       | hydrograph.shp |
| stop parameter [%]                                 | 5              |
| sim resolution [m]                                 | 0.5            |
| end time [s]                                       | 600            |
| dump step [s]                                      | 2              |
|  |                |
| erosion layer                                      | erosion.shp    |
| erosion density [kg/m3]                            | 2000           |
| erosion rate [m/s]                                 | 0.025          |
| pot. Erosion depth [per kPa]                       | 0.1            |
| critical shear stress [kPa]                        | 1              |
| max erosion depth [m]                              | 1              |
|  |                |
| density [kg/m3]                                    | 1750           |
| inflow direction [°]                               | 60             |
| vol [m3]   | 105032         |
| Qmax [m3/s]  | 162.2          |
| t1 [s]   | 10             |
| v [m/s]  | 8.18           |
|  |                |
| Front velocity CD 28-29 (m/s)                      | 8.18           |
| Max flow depth laser (m)                           | 2.4            |
| Max flow depth radar (m)                           | 2.49           |
| Peak velocity (quantile 0.99) laser CD 28-29 (m/s) | 8.16           |
| Peak velocity (quantile 0.99) radar CD 28-29 (m/s) | 8.1            |
| Flow duration (min)                                | 38             |
|  |                |
| CD28-CD29  | 134m           |
| CD27-CD29  | 460m           |
|  |                |
| Froude number                                      | 1.69           |

Table S2b: Output data with velocity (v) and flow depth (av\_maxd\_P). These variables were compared with the results of the field survey to determine the best-fit simulation (green) for each  $\mu$ . The z-values are calculated from the laser measurement (Max flow depth laser, see above).

| Simulation | $\text{Mu} []$ | $X_i [\text{m}/\text{s}2]$ | v [ $\text{m}/\text{s}$ ] | maxd_P1 [m] | maxd_P2 [m] | maxd_P3 [m] | maxd_P4 [m] | av_maxd_P [m] | Froude number [] | Qmax [ $\text{m}^3/\text{s}$ ] | z value laser | z value radar |
|------------|----------------|----------------------------|---------------------------|-------------|-------------|-------------|-------------|---------------|------------------|--------------------------------|---------------|---------------|
| 1          | 0.02           | 1400                       | 8.9                       | 1.99        | 2.30        | 2.54        | 2.93        | 2.44          | 1.82             | 140                            | 0.09          | 0.09          |
| 2          | 0.02           | 800                        | 7.9                       | 3.00        | 2.94        | 2.84        | 3.03        | 2.95          | 1.47             | 130                            | 0.23          | 0.19          |
| 3          | 0.02           | 1000                       | 7.9                       | 2.63        | 2.71        | 2.62        | 2.89        | 2.71          | 1.53             | 147                            | 0.13          | 0.10          |
| 4          | 0.02           | 1200                       | 8.4                       | 2.22        | 2.38        | 2.40        | 2.71        | 2.43          | 1.72             | 140                            | 0.03          | 0.04          |
| 5          | 0.04           | 1500                       | 7.9                       | 2.94        | 2.86        | 2.65        | 2.86        | 2.83          | 1.50             | 128                            | 0.18          | 0.14          |
| 6          | 0.04           | 2000                       | 8.4                       | 2.60        | 2.64        | 2.57        | 2.69        | 2.63          | 1.66             | 140                            | 0.10          | 0.06          |
| 7          | 0.04           | 2500                       | 8.4                       | 2.45        | 2.55        | 2.54        | 2.78        | 2.58          | 1.67             | 137                            | 0.08          | 0.05          |
| 8          | 0.04           | 3000                       | 8.4                       | 2.04        | 2.55        | 2.69        | 2.97        | 2.56          | 1.68             | 142                            | 0.07          | 0.04          |
| 9          | 0.06           | 12000                      | 7.9                       | 3.21        | 3.12        | 3.00        | 3.12        | 3.11          | 1.43             | 138                            | 0.30          | 0.25          |
| 10         | 0.06           | 8000                       | 7.9                       | 3.31        | 3.22        | 3.20        | 3.50        | 3.31          | 1.39             | 124                            | 0.38          | 0.33          |
| 11         | 0.06           | 9000                       | 8.4                       | 3.38        | 3.26        | 3.16        | 3.39        | 3.30          | 1.48             | 128                            | 0.37          | 0.33          |
| 12         | 0.06           | 10000                      | 7.9                       | 3.19        | 3.09        | 2.97        | 3.22        | 3.12          | 1.43             | 135                            | 0.30          | 0.25          |
| 13         | 0.06           | 14000                      | 8.4                       | 2.62        | 2.59        | 2.67        | 2.95        | 2.71          | 1.63             | 135                            | 0.13          | 0.09          |
| 14         | 0.01           | 800                        | 8.4                       | 2.62        | 2.69        | 2.56        | 2.87        | 2.69          | 1.64             | 138                            | 0.12          | 0.08          |
| 15         | 0.01           | 1000                       | 8.4                       | 2.18        | 2.33        | 2.49        | 2.84        | 2.46          | 1.71             | 138                            | 0.04          | 0.03          |
| 16         | 0.01           | 1200                       | 8.9                       | 1.90        | 2.35        | 2.68        | 3.26        | 2.55          | 1.78             | 142                            | 0.11          | 0.09          |
| 17         | 0.03           | 1000                       | 7.9                       | 2.94        | 2.87        | 2.70        | 3.04        | 2.89          | 1.48             | 139                            | 0.21          | 0.16          |
| 18         | 0.03           | 1500                       | 8.4                       | 2.46        | 2.59        | 2.49        | 2.78        | 2.58          | 1.67             | 144                            | 0.08          | 0.05          |
| 19         | 0.03           | 2000                       | 8.9                       | 2.07        | 2.53        | 2.71        | 2.97        | 2.57          | 1.77             | 145                            | 0.11          | 0.09          |
| 20         | 0.03           | 2500                       | 9.6                       | 1.95        | 2.31        | 2.65        | 3.05        | 2.49          | 1.94             | 136                            | 0.18          | 0.17          |
| 21         | 0.04           | 3500                       | 8.9                       | 1.71        | 2.12        | 2.66        | 3.04        | 2.38          | 1.84             | 136                            | 0.09          | 0.10          |
| 22         | 0.05           | 8000                       | 8.9                       | 1.70        | 2.13        | 2.51        | 2.91        | 2.31          | 1.87             | 137                            | 0.10          | 0.11          |
| 23         | 0.05           | 10000                      | 8.9                       | 2.04        | 2.48        | 2.77        | 3.10        | 2.60          | 1.76             | 137                            | 0.12          | 0.10          |
| 24         | 0.05           | 12000                      | 8.9                       | 1.77        | 2.45        | 2.94        | 3.35        | 2.63          | 1.75             | 136                            | 0.13          | 0.10          |
| 25         | 0.05           | 14000                      | 8.9                       | 1.82        | 2.06        | 2.55        | 3.27        | 2.43          | 1.82             | 136                            | 0.09          | 0.09          |
| 26         | 0.05           | 6000                       | 8.4                       | 2.16        | 2.54        | 2.59        | 2.80        | 2.52          | 1.69             | 146                            | 0.06          | 0.03          |
| 27         | 0.06           | 16000                      | 8.4                       | 2.87        | 2.73        | 2.70        | 2.94        | 2.81          | 1.60             | 133                            | 0.17          | 0.13          |
| 28         | 0.04           | 4000                       | 8.9                       | 1.99        | 2.48        | 2.70        | 3.12        | 2.57          | 1.77             | 139                            | 0.11          | 0.09          |
| 29         | 0.02           | 1600                       | 7.6                       | 2.09        | 2.47        | 2.65        | 3.13        | 2.59          | 1.51             | 139                            | 0.10          | 0.08          |
| 30         | 0.02           | 4000                       | 11.2                      | 1.99        | 1.93        | 2.19        | 2.42        | 2.13          | 2.45             | 152                            | 0.39          | 0.40          |
| 31         | 0.04           | 3200                       | 8.9                       | 1.80        | 2.29        | 2.65        | 3.00        | 2.44          | 1.82             | 135                            | 0.09          | 0.09          |
| 32         | 0.05           | 7000                       | 8.4                       | 1.77        | 2.42        | 2.67        | 2.93        | 2.45          | 1.71             | 139                            | 0.03          | 0.03          |
| 33         | 0.06           | 15000                      | 7.9                       | 2.62        | 2.58        | 2.71        | 3.05        | 2.74          | 1.52             | 137                            | 0.15          | 0.11          |

**Table S3: Details on the modelling approach**

Information on the number of model runs (Table S3a), the intervals between the  $\mu$ - and  $\xi$ -values upon modelling (Table S3b), and event-specific and general input values that were used upon modelling (Tables S3c and S3d, respectively). Finally, Table S3 also lists the results of the model runs per event where the model results and observations had a best fit (Table S3e).

Table S3a: Number of model runs

| Event    | # of simulations | best z-value |
|----------|------------------|--------------|
| 21.06.19 | 43               | 0.06         |
| 02.07.19 | 34               | 0.32         |
| 11.08.19 | 41               | 0.13         |
| 20.08.19 | 36               | 0.02         |
| 24.06.21 | 37               | 0.03         |
| 06.07.21 | 38               | 0.03         |
| 16.07.21 | 30               | 0.03         |
| 07.08.21 | 23               | 0.23         |
| 19.09.21 | 33               | 0.11         |
| 05.06.22 | 12               | 0.01         |
| 04.07.22 | 13               | 0.02         |
| 08.09.22 | 20               | 0.34         |
| Total    | 360              |              |

Table S3b: Variations of  $\mu$  and  $\xi$  val

|       |             |   |
|-------|-------------|---|
| $\mu$ | 0.01        | For $\mu$ we only used the values 0.01, 0.02, 0.03, 0.04, 0.05 and 0.06 upon modelling.   |
| $\xi$ | 1 to > 1000 | Also upon modeling, the intervals between the $\xi$ -values were 1 for those models where we set $\mu = 1$ . For larger $\mu$ -values, we increased the intervals between the subsequent $\xi$ -values to $>> 1000$ . We iteratively changed the values until we found a best-fit between model results and observations. |

Table S3c: Input for RAMMS, which were not event-specific

|                              |                |
|------------------------------|----------------|
| DTM                          | DTM_0.5.tif    |
| DTM resolution [m]           | 0.5            |
| calculation domain           | calcdom.shp    |
| release area                 | hydrograph.shp |
| stop parameter [%]           | 5              |
| sim resolution [m]           | 0.5            |
| end time [s]                 | 1000           |
| dump step [s]                | 2              |
| erosion layer                | erosion.shp    |
| erosion density [kg/m³]      | 2000           |
| erosion rate [m/s]           | 0.025          |
| pot. Erosion depth [per kPa] | 0.1            |
| critical shear stress [kPa]  | 1              |
| max erosion depth [m]        | 1              |
| inflow direction [°]         | 60             |
| t1 Hydrograph [s]            | 10             |

Table S3d: Input for RAMMS, which were event-specific

| Event                         | 21.06.19 | 02.07.19 | 11.08.19 | 20.08.19 | 24.06.21 | 06.07.21 | 16.07.21 | 07.08.21 | 19.09.21 | 05.06.22 | 04.07.22 | 08.09.22 |
|-------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| density [kg/m³]               | 1870     | 1971     | 2323     | 2031     | 1750     | 1605     | 1916     | 1884     | 1697     | 1690     | 1189     | 1592     |
| vol [m³]                      | 97394    | 73188    | 88064    | 6137     | 105032   | 76906    | 80879    | 38737    | 8538     | 39498    | 175929   | 9283     |
| Qmax [m³/s]                   | 147.61   | 65.58    | 95.63    | 8.06     | 162.2    | 186.61   | 60.7     | 41.19    | 10.67    | 55.42    | 169.14   | 20.94    |
| Front velocity CD 28-29 [m/s] | 6.62     | 3.86     | 6.95     | 0.89     | 8.18     | 8.69     | 2.78     | 2.32     | 1.25     | 3.39     | 8.18     | 1.91     |
| Max flow depth laser [m]      | 3.13     | 1.75     | 1.81     | 1.13     | 2.4      | 2.5      | 2.38     | 2.49     | 1.13     | 2.08     | 2.49     | 1.93     |
| Max flow depth radar [m]      | 2.69     | 1.73     | 1.89     | 1.1      | 2.49     | 2.58     | 2.44     | 2.17     | 1.22     | 2.15     | 2.6      | 1.77     |
| Froude Number                 | 1.19     | 0.93     | 1.65     | 0.27     | 1.69     | 1.75     | 0.58     | 0.47     | 0.38     | 0.75     | 1.66     | 0.44     |

Table S3e: Best-fit outputs of RAMMs models

| Event                         | 21.06.19 | 02.07.19 | 11.08.19 | 20.08.19 | 24.06.21 | 06.07.21 | 16.07.21 | 07.08.21 | 19.09.21 | 05.06.22 | 04.07.22 | 08.09.22 |
|-------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| Front velocity CD 28-29 [m/s] | 6.7      | 3.9      | 7.4      | 0.9      | 8.4      | 8.9      | 2.8      | 2.31     | 1.24     | 3.35     | 8.38     | 1.76     |
| Max flow depth [m]            | 2.96     | 2.32     | 2.02     | 1.15     | 2.43     | 2.47     | 2.32     | 1.91     | 1.01     | 2.09     | 2.5      | 1.29     |
| Froude number                 | 1.24     | 0.83     | 1.66     | 0.27     | 1.72     | 1.81     | 0.59     | 0.53     | 0.39     | 0.74     | 1.69     | 0.49     |
| Qmax [m <sup>3</sup> /s]      | 122      | 54       | 78       | 7        | 140      | 158      | 48       | 35       | 9        | 40       | 143      | 17       |
| $\mu$                         | 0.06     | 0.06     | 0.06     | 0.01     | 0.02     | 0.05     | 0.05     | 0.04     | 0.01     | 0.06     | 0.01     | 0.01     |
| $\xi$                         | 4500     | 1000     | 8500     | 12       | 1200     | 10000    | 170      | 105      | 25       | 700      | 1000     | 50       |
| z-value                       | 0.06     | 0.32     | 0.13     | 0.02     | 0.03     | 0.03     | 0.03     | 0.23     | 0.11     | 0.01     | 0.02     | 0.34     |

**Table S4: Measured and calculated properties for each flow (v, flow depth, Froude number, volume, density), best-fit model results ( $\mu$ ,  $\xi$ , z) and related total (S) and Coulomb and turbulent frictions**

For each debris flow event, distinct  $\mu$ - $\xi$  pairs can be used to successfully model the flow properties such as flow velocity and flow depth. The best-fit solutions between model results and observations, characterized by the lowest z-values, are highlighted by the yellow bar. The values of these best-fit results are displayed in Table S5.

| Event    | v [m/s] | Flow Depth [m] | Froude Number | Volume (m <sup>3</sup> ) | Density (kg/m <sup>3</sup> ) | $\mu$ | $\xi$ | z    | Total Friction S [Pa] | Coulomb Friction [Pa] | Turbulent Friction [Pa] | Coulomb Friction [%] | Turbulent Friction [%] |
|----------|---------|----------------|---------------|--------------------------|------------------------------|-------|-------|------|-----------------------|-----------------------|-------------------------|----------------------|------------------------|
| 21.06.19 | 6.6     | 3.1            | 1.19          | 97394                    | 1870                         | 0.01  | 500   | 0.07 | 2166                  | 568                   | 1598                    | 26                   | 74                     |
| 21.06.19 | 6.6     | 3.1            | 1.19          | 97394                    | 1870                         | 0.02  | 550   | 0.10 | 2588                  | 1135                  | 1453                    | 44                   | 56                     |
| 21.06.19 | 6.6     | 3.1            | 1.19          | 97394                    | 1870                         | 0.03  | 800   | 0.10 | 2702                  | 1703                  | 999                     | 63                   | 37                     |
| 21.06.19 | 6.6     | 3.1            | 1.19          | 97394                    | 1870                         | 0.04  | 1000  | 0.11 | 3069                  | 2270                  | 799                     | 74                   | 26                     |
| 21.06.19 | 6.6     | 3.1            | 1.19          | 97394                    | 1870                         | 0.05  | 1300  | 0.11 | 3452                  | 2838                  | 615                     | 82                   | 18                     |
| 21.06.19 | 6.6     | 3.1            | 1.19          | 97394                    | 1870                         | 0.06  | 4500  | 0.06 | 3583                  | 3405                  | 178                     | 95                   | 5                      |
| 02.07.19 | 3.9     | 1.8            | 0.93          | 73188                    | 1971                         | 0.01  | 200   | 0.37 | 1818                  | 347                   | 1470                    | 19                   | 81                     |
| 02.07.19 | 3.9     | 1.8            | 0.93          | 73188                    | 1971                         | 0.02  | 250   | 0.37 | 1871                  | 695                   | 1176                    | 37                   | 63                     |
| 02.07.19 | 3.9     | 1.8            | 0.93          | 73188                    | 1971                         | 0.03  | 300   | 0.37 | 2022                  | 1042                  | 980                     | 52                   | 48                     |
| 02.07.19 | 3.9     | 1.8            | 0.93          | 73188                    | 1971                         | 0.04  | 350   | 0.36 | 2230                  | 1389                  | 840                     | 62                   | 38                     |
| 02.07.19 | 3.9     | 1.8            | 0.93          | 73188                    | 1971                         | 0.05  | 600   | 0.35 | 2227                  | 1737                  | 490                     | 78                   | 22                     |
| 02.07.19 | 3.9     | 1.8            | 0.93          | 73188                    | 1971                         | 0.06  | 1000  | 0.32 | 2378                  | 2084                  | 294                     | 88                   | 12                     |
| 11.08.19 | 7       | 1.8            | 1.65          | 88064                    | 2323                         | 0.01  | 1000  | 0.16 | 1526                  | 409                   | 1117                    | 27                   | 73                     |
| 11.08.19 | 7       | 1.8            | 1.65          | 88064                    | 2323                         | 0.02  | 1000  | 0.18 | 1935                  | 819                   | 1117                    | 42                   | 58                     |
| 11.08.19 | 7       | 1.8            | 1.65          | 88064                    | 2323                         | 0.03  | 2500  | 0.21 | 1675                  | 1228                  | 447                     | 73                   | 27                     |
| 11.08.19 | 7       | 1.8            | 1.65          | 88064                    | 2323                         | 0.04  | 2000  | 0.18 | 2196                  | 1637                  | 558                     | 75                   | 25                     |
| 11.08.19 | 7       | 1.8            | 1.65          | 88064                    | 2323                         | 0.05  | 8000  | 0.14 | 2186                  | 2047                  | 140                     | 94                   | 6                      |
| 11.08.19 | 7       | 1.8            | 1.65          | 88064                    | 2323                         | 0.06  | 8500  | 0.13 | 2588                  | 2456                  | 131                     | 95                   | 5                      |
| 20.08.19 | 0.9     | 1.1            | 0.27          | 6137                     | 2031                         | 0.01  | 12    | 0.02 | 1564                  | 219                   | 1345                    | 14                   | 86                     |
| 20.08.19 | 0.9     | 1.1            | 0.27          | 6137                     | 2031                         | 0.02  | 13    | 0.03 | 1679                  | 437                   | 1241                    | 26                   | 74                     |
| 20.08.19 | 0.9     | 1.1            | 0.27          | 6137                     | 2031                         | 0.03  | 12    | 0.10 | 2001                  | 656                   | 1345                    | 33                   | 67                     |
| 20.08.19 | 0.9     | 1.1            | 0.27          | 6137                     | 2031                         | 0.04  | 21    | 0.12 | 1643                  | 875                   | 769                     | 53                   | 47                     |
| 20.08.19 | 0.9     | 1.1            | 0.27          | 6137                     | 2031                         | 0.05  | 20    | 0.17 | 1901                  | 1094                  | 807                     | 58                   | 42                     |
| 20.08.19 | 0.9     | 1.1            | 0.27          | 6137                     | 2031                         | 0.06  | 30    | 0.25 | 1850                  | 1312                  | 538                     | 71                   | 29                     |
| 24.06.21 | 8.2     | 2.4            | 1.69          | 105032                   | 1750                         | 0.01  | 1000  | 0.04 | 1566                  | 411                   | 1154                    | 26                   | 74                     |
| 24.06.21 | 8.2     | 2.4            | 1.69          | 105032                   | 1750                         | 0.02  | 1200  | 0.03 | 1784                  | 822                   | 962                     | 46                   | 54                     |
| 24.06.21 | 8.2     | 2.4            | 1.69          | 105032                   | 1750                         | 0.03  | 1500  | 0.08 | 2003                  | 1234                  | 770                     | 62                   | 38                     |
| 24.06.21 | 8.2     | 2.4            | 1.69          | 105032                   | 1750                         | 0.04  | 3000  | 0.07 | 2030                  | 1645                  | 385                     | 81                   | 19                     |
| 24.06.21 | 8.2     | 2.4            | 1.69          | 105032                   | 1750                         | 0.05  | 7000  | 0.03 | 2221                  | 2056                  | 165                     | 93                   | 7                      |
| 24.06.21 | 8.2     | 2.4            | 1.69          | 105032                   | 1750                         | 0.06  | 14000 | 0.13 | 2550                  | 2467                  | 82                      | 97                   | 3                      |
| 06.07.21 | 8.7     | 2.5            | 1.75          | 76906                    | 1605                         | 0.01  | 800   | 0.06 | 1883                  | 393                   | 1490                    | 21                   | 79                     |
| 06.07.21 | 8.7     | 2.5            | 1.75          | 76906                    | 1605                         | 0.02  | 1500  | 0.06 | 1580                  | 786                   | 794                     | 50                   | 50                     |
| 06.07.21 | 8.7     | 2.5            | 1.75          | 76906                    | 1605                         | 0.03  | 1750  | 0.08 | 1860                  | 1179                  | 681                     | 63                   | 37                     |
| 06.07.21 | 8.7     | 2.5            | 1.75          | 76906                    | 1605                         | 0.04  | 3000  | 0.09 | 1969                  | 1571                  | 397                     | 80                   | 20                     |
| 06.07.21 | 8.7     | 2.5            | 1.75          | 76906                    | 1605                         | 0.05  | 10000 | 0.03 | 2083                  | 1964                  | 119                     | 94                   | 6                      |
| 06.07.21 | 8.7     | 2.5            | 1.75          | 76906                    | 1605                         | 0.06  | 25000 | 0.12 | 2405                  | 2357                  | 48                      | 98                   | 2                      |
| 16.07.21 | 2.8     | 2.4            | 0.58          | 80879                    | 1916                         | 0.01  | 65    | 0.04 | 2717                  | 450                   | 2267                    | 17                   | 83                     |
| 16.07.21 | 2.8     | 2.4            | 0.58          | 80879                    | 1916                         | 0.02  | 75    | 0.04 | 2865                  | 900                   | 1965                    | 31                   | 69                     |
| 16.07.21 | 2.8     | 2.4            | 0.58          | 80879                    | 1916                         | 0.03  | 95    | 0.05 | 2902                  | 1351                  | 1551                    | 47                   | 53                     |
| 16.07.21 | 2.8     | 2.4            | 0.58          | 80879                    | 1916                         | 0.04  | 125   | 0.07 | 2980                  | 1801                  | 1179                    | 60                   | 40                     |
| 16.07.21 | 2.8     | 2.4            | 0.58          | 80879                    | 1916                         | 0.05  | 170   | 0.03 | 3118                  | 2251                  | 867                     | 72                   | 28                     |
| 16.07.21 | 2.8     | 2.4            | 0.58          | 80879                    | 1916                         | 0.06  | 280   | 0.04 | 3227                  | 2701                  | 526                     | 84                   | 16                     |

|          |     |     |      |        |      |      |       |      |      |      |      |    |    |
|----------|-----|-----|------|--------|------|------|-------|------|------|------|------|----|----|
| 07.08.21 | 2.3 | 2.5 | 0.47 | 38737  | 1884 | 0.01 | 50    | 0.25 | 2417 | 461  | 1955 | 19 | 81 |
| 07.08.21 | 2.3 | 2.5 | 0.47 | 38737  | 1884 | 0.02 | 65    | 0.26 | 2426 | 922  | 1504 | 38 | 62 |
| 07.08.21 | 2.3 | 2.5 | 0.47 | 38737  | 1884 | 0.03 | 65    | 0.25 | 2888 | 1383 | 1504 | 48 | 52 |
| 07.08.21 | 2.3 | 2.5 | 0.47 | 38737  | 1884 | 0.04 | 105   | 0.23 | 2776 | 1845 | 931  | 66 | 34 |
| 07.08.21 | 2.3 | 2.5 | 0.47 | 38737  | 1884 | 0.05 | 150   | 0.25 | 2957 | 2306 | 652  | 78 | 22 |
| 07.08.21 | 2.3 | 2.5 | 0.47 | 38737  | 1884 | 0.06 | 230   | 0.27 | 3192 | 2767 | 425  | 87 | 13 |
| 19.09.21 | 1.3 | 1.1 | 0.38 | 8538   | 1697 | 0.01 | 25    | 0.11 | 1308 | 183  | 1125 | 14 | 86 |
| 19.09.21 | 1.3 | 1.1 | 0.38 | 8538   | 1697 | 0.02 | 30    | 0.12 | 1303 | 366  | 938  | 28 | 72 |
| 19.09.21 | 1.3 | 1.1 | 0.38 | 8538   | 1697 | 0.03 | 43    | 0.17 | 1203 | 548  | 654  | 46 | 54 |
| 19.09.21 | 1.3 | 1.1 | 0.38 | 8538   | 1697 | 0.04 | 50    | 0.18 | 1294 | 731  | 563  | 57 | 43 |
| 19.09.21 | 1.3 | 1.1 | 0.38 | 8538   | 1697 | 0.05 | 80    | 0.23 | 1265 | 914  | 352  | 72 | 28 |
| 19.09.21 | 1.3 | 1.1 | 0.38 | 8538   | 1697 | 0.06 | 160   | 0.20 | 1272 | 1097 | 176  | 86 | 14 |
| 05.06.22 | 3.4 | 2.1 | 0.75 | 39498  | 1690 | 0.01 | 130   | 0.06 | 1822 | 347  | 1474 | 19 | 81 |
| 05.06.22 | 3.4 | 2.1 | 0.75 | 39498  | 1690 | 0.02 | 160   | 0.05 | 1893 | 695  | 1198 | 37 | 63 |
| 05.06.22 | 3.4 | 2.1 | 0.75 | 39498  | 1690 | 0.03 | 210   | 0.05 | 1955 | 1042 | 913  | 53 | 47 |
| 05.06.22 | 3.4 | 2.1 | 0.75 | 39498  | 1690 | 0.04 | 260   | 0.04 | 2127 | 1390 | 737  | 65 | 35 |
| 05.06.22 | 3.4 | 2.1 | 0.75 | 39498  | 1690 | 0.05 | 400   | 0.03 | 2216 | 1737 | 479  | 78 | 22 |
| 05.06.22 | 3.4 | 2.1 | 0.75 | 39498  | 1690 | 0.06 | 700   | 0.01 | 2359 | 2085 | 274  | 88 | 12 |
| 04.07.22 | 8.2 | 2.5 | 1.66 | 175929 | 1189 | 0.01 | 1000  | 0.02 | 1075 | 291  | 784  | 27 | 73 |
| 04.07.22 | 8.2 | 2.5 | 1.66 | 175929 | 1189 | 0.02 | 1200  | 0.04 | 1236 | 582  | 654  | 47 | 53 |
| 04.07.22 | 8.2 | 2.5 | 1.66 | 175929 | 1189 | 0.03 | 1500  | 0.07 | 1396 | 873  | 523  | 63 | 37 |
| 04.07.22 | 8.2 | 2.5 | 1.66 | 175929 | 1189 | 0.04 | 2000  | 0.09 | 1556 | 1164 | 392  | 75 | 25 |
| 04.07.22 | 8.2 | 2.5 | 1.66 | 175929 | 1189 | 0.05 | 6000  | 0.04 | 1586 | 1455 | 131  | 92 | 8  |
| 04.07.22 | 8.2 | 2.5 | 1.66 | 175929 | 1189 | 0.06 | 20000 | 0.08 | 1785 | 1746 | 39   | 98 | 2  |
| 08.09.22 | 1.9 | 1.9 | 0.44 | 9283   | 1592 | 0.01 | 50    | 0.34 | 1424 | 296  | 1128 | 21 | 79 |
| 08.09.22 | 1.9 | 1.9 | 0.44 | 9283   | 1592 | 0.02 | 60    | 0.36 | 1532 | 592  | 940  | 39 | 61 |
| 08.09.22 | 1.9 | 1.9 | 0.44 | 9283   | 1592 | 0.03 | 80    | 0.37 | 1593 | 888  | 705  | 56 | 44 |
| 08.09.22 | 1.9 | 1.9 | 0.44 | 9283   | 1592 | 0.04 | 125   | 0.39 | 1636 | 1185 | 451  | 72 | 28 |
| 08.09.22 | 1.9 | 1.9 | 0.44 | 9283   | 1592 | 0.05 | 150   | 0.35 | 1857 | 1481 | 376  | 80 | 20 |
| 08.09.22 | 1.9 | 1.9 | 0.44 | 9283   | 1592 | 0.06 | 350   | 0.41 | 1938 | 1777 | 161  | 92 | 8  |

**Table S5: Best-fit model results per event**

Each debris flow event can be characterized by a distinct  $\mu$ - $\xi$  pair with a lowest z-value. See Table S2b for best-fit  $\mu$ - $\xi$  pairs per event.

| Event    | v [m/s] | Flow Depth [m] | Froude Number | Volume ( $m^3$ ) | Density (kg/m <sup>3</sup> ) | $\mu$ | $\xi$ | z    | Total Friction [Pa] | Coulomb Friction [Pa] | Turbulent Friction [Pa] | Coulomb Friction [%] | Turbulent Friction [%] |
|----------|---------|----------------|---------------|------------------|------------------------------|-------|-------|------|---------------------|-----------------------|-------------------------|----------------------|------------------------|
| 21.06.19 | 6.6     | 3.1            | 1.19          | 97394            | 1870                         | 0.06  | 4500  | 0.06 | 3583                | 3405                  | 178                     | 95                   | 5                      |
| 02.07.19 | 3.9     | 1.8            | 0.93          | 73188            | 1971                         | 0.06  | 1000  | 0.32 | 2378                | 2084                  | 294                     | 88                   | 12                     |
| 11.08.19 | 7       | 1.8            | 1.65          | 88064            | 2323                         | 0.06  | 8500  | 0.13 | 2588                | 2456                  | 131                     | 95                   | 5                      |
| 20.08.19 | 0.9     | 1.1            | 0.27          | 6137             | 2031                         | 0.01  | 12    | 0.02 | 1564                | 219                   | 1345                    | 14                   | 86                     |
| 24.06.21 | 8.2     | 2.4            | 1.69          | 105032           | 1750                         | 0.02  | 1200  | 0.03 | 1784                | 822                   | 962                     | 46                   | 54                     |
| 06.07.21 | 8.7     | 2.5            | 1.75          | 76906            | 1605                         | 0.05  | 10000 | 0.03 | 2083                | 1964                  | 119                     | 94                   | 6                      |
| 16.07.21 | 2.8     | 2.4            | 0.58          | 80879            | 1916                         | 0.05  | 170   | 0.03 | 3118                | 2251                  | 867                     | 72                   | 28                     |
| 07.08.21 | 2.3     | 2.5            | 0.47          | 38737            | 1884                         | 0.04  | 105   | 0.23 | 2776                | 1845                  | 931                     | 66                   | 34                     |
| 19.09.21 | 1.3     | 1.1            | 0.38          | 8538             | 1697                         | 0.01  | 25    | 0.11 | 1308                | 183                   | 1125                    | 14                   | 86                     |
| 05.06.22 | 3.4     | 2.1            | 0.75          | 39498            | 1690                         | 0.06  | 700   | 0.01 | 2359                | 2085                  | 274                     | 88                   | 12                     |
| 04.07.22 | 8.2     | 2.5            | 1.66          | 175929           | 1189                         | 0.01  | 1000  | 0.02 | 1075                | 291                   | 784                     | 27                   | 73                     |
| 08.09.22 | 1.9     | 1.9            | 0.44          | 9283             | 1592                         | 0.01  | 50    | 0.34 | 1424                | 296                   | 1128                    | 21                   | 79                     |

**Table S6: Grain size data**

Table S6a: Weight percent passing per mesh size for each sample, and Table S6b complete overview of results from sieving (next pages).

|             | Event           | 21.06.19   |                  |                             | 02.07.19   |                  |                             | 26.07.19   |                  |                             | 11.08.19   |                  |                             | 20.08.19   |                  |                             |
|-------------|-----------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|
|             | Sample mass [g] | 1958.7     |                  |                             | 1772.4     |                  |                             | 2856.1     |                  |                             | 3299.7     |                  |                             | 3001.5     |                  |                             |
| Method      | Mesh size [mm]  | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm |
| dry sieving | 125.0000        | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       |
|             | 63.0000         | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       |
|             | 31.5000         | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 55.7       | 98.1             | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       |
|             | 16.0000         | 365.0      | 81.4             | 100.0                       | 0.0        | 100.0            | 100.0                       | 158.9      | 92.5             | 100.0                       | 472.6      | 85.7             | 100.0                       | 327.9      | 89.1             | 100.0                       |
|             | 8.0000          | 239.7      | 69.1             | 85.0                        | 3.4        | 99.8             | 99.8                        | 308.3      | 81.7             | 88.3                        | 380.6      | 74.1             | 86.5                        | 341.7      | 77.7             | 87.2                        |
|             | 4.0000          | 180.2      | 59.9             | 73.7                        | 40.5       | 97.5             | 97.5                        | 258.1      | 72.7             | 78.6                        | 288.3      | 65.4             | 76.3                        | 287.4      | 68.1             | 76.5                        |
|             | 2.0000          | 122.5      | 53.7             | 66.0                        | 88.3       | 92.5             | 92.5                        | 199.3      | 65.7             | 71.0                        | 220.4      | 58.7             | 68.5                        | 198.8      | 61.5             | 69.0                        |
|             | 1.0000          | 110.5      | 48.0             | 59.0                        | 123.6      | 85.6             | 85.6                        | 189.9      | 59.0             | 63.8                        | 211.7      | 52.3             | 61.1                        | 184.7      | 55.3             | 62.1                        |
|             | 0.5000          | 111.4      | 42.3             | 52.0                        | 142.0      | 77.6             | 77.6                        | 187.3      | 52.5             | 56.7                        | 206.6      | 46.1             | 53.8                        | 182.5      | 49.3             | 55.3                        |
| wet sieving | 0.2500          |            | 36.4             | 44.8                        |            | 68.6             | 68.6                        |            | 45.0             | 48.6                        |            | 42.9             | 50.1                        |            | 42.6             | 47.8                        |
|             | 0.1250          |            | 30.6             | 37.6                        |            | 59.0             | 59.0                        |            | 38.2             | 41.3                        |            | 37.7             | 44.0                        |            | 36.2             | 40.6                        |
|             | 0.0630          |            | 25.8             | 31.7                        |            | 49.1             | 49.1                        |            | 31.8             | 34.4                        |            | 31.1             | 36.3                        |            | 30.4             | 34.1                        |
| slurry test | 0.0462          |            | 23.0             | 28.3                        |            | 44.4             | 44.4                        |            | 28.2             | 30.5                        |            | 27.9             | 32.6                        |            | 27.4             | 30.7                        |
|             | 0.0339          |            | 20.2             | 24.8                        |            | 39.6             | 39.6                        |            | 24.2             | 26.1                        |            | 24.2             | 28.3                        |            | 24.0             | 27.0                        |
|             | 0.0224          |            | 15.8             | 19.4                        |            | 30.8             | 30.8                        |            | 18.6             | 20.1                        |            | 18.4             | 21.5                        |            | 18.3             | 20.6                        |
|             | 0.0135          |            | 10.6             | 13.0                        |            | 21.3             | 21.3                        |            | 12.3             | 13.3                        |            | 12.0             | 14.0                        |            | 12.8             | 14.4                        |
|             | 0.0081          |            | 6.4              | 7.9                         |            | 12.5             | 12.5                        |            | 7.4              | 8.0                         |            | 7.2              | 8.4                         |            | 7.9              | 8.9                         |
|             | 0.0050          |            | 4.1              | 5.1                         |            | 7.8              | 7.8                         |            | 4.9              | 5.3                         |            | 4.6              | 5.4                         |            | 5.1              | 5.7                         |
|             | 0.0032          |            | 2.6              | 3.2                         |            | 4.8              | 4.8                         |            | 3.2              | 3.5                         |            | 3.1              | 3.6                         |            | 3.3              | 3.7                         |
|             | 0.0015          |            | 1.1              | 1.3                         |            | 2.5              | 2.5                         |            | 1.7              | 1.8                         |            | 1.4              | 1.6                         |            | 1.9              | 2.1                         |
|             | 0.0000          |            | 0.0              | 0.0                         |            | 0.0              | 0.0                         |            | 0.0              | 0.0                         |            | 0.0              | 0.0                         |            | 0.0              | 0.0                         |

|             | Event           | 24.06.21   |                  |                             | 06.07.21   |                  |                             | 16.07.21   |                  |                             | 07.08.21   |                  |                             | 19.09.21   |                  |                             |
|-------------|-----------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|------------|------------------|-----------------------------|
|             | Sample mass [g] | 2652.5     |                  |                             | 3341.9     |                  |                             | 2511.2     |                  |                             | 2965.8     |                  |                             | 2553.6     |                  |                             |
| Method      | Mesh size [mm]  | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm | Weight [g] | Weight % passing | Weight % passing max. 16 mm |
| dry sieving | 125.0000        | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       |
|             | 63.0000         | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       | 0.0        | 100.0            | 100.0                       |
|             | 31.5000         | 0.0        | 100.0            | 100.0                       | 296.0      | 83.3             | 100.0                       | 434.0      | 84.8             | 100.0                       | 602.3      | 81.7             | 100.0                       | 212.2      | 92.9             | 100.0                       |
|             | 16.0000         | 102.7      | 94.8             | 100.0                       | 290.2      | 66.9             | 100.0                       | 615.7      | 63.2             | 100.0                       | 795.1      | 57.7             | 100.0                       | 405.6      | 79.4             | 100.0                       |
|             | 8.0000          | 152.8      | 87.0             | 91.8                        | 163.4      | 57.7             | 86.2                        | 349.9      | 51.0             | 80.6                        | 279.6      | 49.2             | 85.3                        | 261.1      | 70.7             | 89.0                        |
|             | 4.0000          | 151.6      | 79.2             | 83.6                        | 131.8      | 50.3             | 75.1                        | 200.7      | 44.0             | 69.5                        | 199.4      | 43.1             | 74.8                        | 217.9      | 63.5             | 79.9                        |
|             | 2.0000          | 127.9      | 72.7             | 76.7                        | 84.7       | 45.5             | 68.0                        | 116.3      | 39.9             | 63.1                        | 119.0      | 39.5             | 68.6                        | 151.8      | 58.4             | 73.5                        |
|             | 1.0000          | 125.9      | 66.3             | 69.9                        | 81.8       | 40.9             | 61.1                        | 80.2       | 37.1             | 58.6                        | 102.7      | 36.4             | 63.2                        | 139.3      | 53.8             | 67.7                        |
|             | 0.5000          | 138.8      | 59.2             | 62.5                        | 87.4       | 35.9             | 53.7                        | 76.7       | 34.4             | 54.4                        | 106.6      | 33.2             | 57.6                        | 162.5      | 48.3             | 60.9                        |
| wet sieving | 0.2500          |            | 50.9             | 53.7                        |            | 31.2             | 46.7                        |            | 31.0             | 49.0                        |            | 29.3             | 50.7                        |            | 41.6             | 52.4                        |
|             | 0.1250          |            | 42.5             | 44.9                        |            | 26.2             | 39.1                        |            | 26.6             | 42.1                        |            | 25.0             | 43.4                        |            | 34.6             | 43.6                        |
|             | 0.0630          |            | 35.1             | 37.0                        |            | 21.4             | 32.0                        |            | 22.4             | 35.4                        |            | 20.7             | 35.9                        |            | 28.3             | 35.7                        |
| slurry test | 0.0462          |            | 31.5             | 33.2                        |            | 19.2             | 28.7                        |            | 20.3             | 32.2                        |            | 18.6             | 32.3                        |            | 25.5             | 32.1                        |
|             | 0.0339          |            | 27.4             | 28.9                        |            | 16.4             | 24.5                        |            | 17.7             | 28.0                        |            | 15.9             | 27.7                        |            | 21.5             | 27.0                        |
|             | 0.0224          |            | 21.7             | 22.9                        |            | 12.7             | 18.9                        |            | 14.0             | 22.1                        |            | 12.5             | 21.7                        |            | 16.2             | 20.4                        |
|             | 0.0135          |            | 14.4             | 15.2                        |            | 8.7              | 13.0                        |            | 9.5              | 15.1                        |            | 8.3              | 14.4                        |            | 10.7             | 13.4</td                    |

**Table S7: Results of powder x-ray diffraction analysis**

Measured weight percent per mineral for all four analyzed samples.

|                   | <b>02.07.2019</b> | <b>26.07.2019</b> | <b>20.08.2019</b> | <b>16.07.2021</b> |
|-------------------|-------------------|-------------------|-------------------|-------------------|
| <b>Albite</b>     | 2.0               | 2.0               | 1.8               | 2.0               |
| <b>Calcite</b>    | 10.6              | 7.4               | 10.2              | 17.9              |
| <b>Dolomite</b>   | 24.4              | 16.7              | 23.7              | 19.4              |
| <b>Muscovite</b>  | 17.7              | 22.2              | 19.6              | 18.2              |
| <b>Orthoclase</b> | 3.4               | 2.9               | 2.8               | 3.0               |
| <b>Quartz</b>     | 29.9              | 36.0              | 29.2              | 30.9              |
| <b>Chlorite</b>   | 0.3               | 0.1               | 0.2               | 0.0               |
| <b>Illite</b>     | 11.3              | 12.1              | 11.7              | 8.4               |
| <b>Kaolinite</b>  | 0.0               | 0.1               | 0.1               | 0.0               |
| <b>Smektite</b>   | 0.2               | 0.6               | 0.7               | 0.3               |